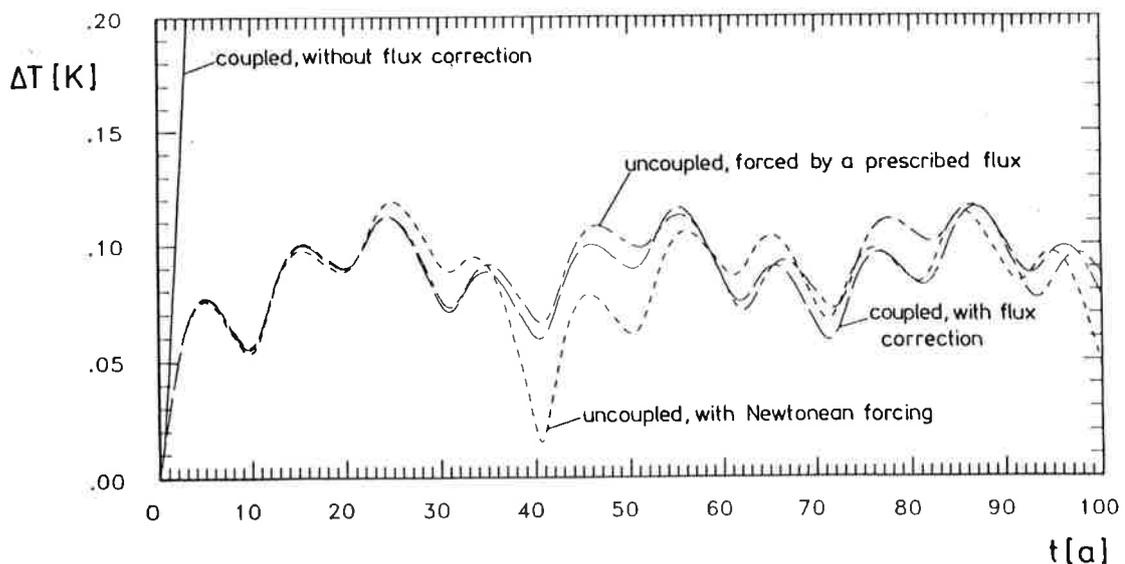


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A FLUX CORRECTION METHOD FOR REMOVING THE CLIMATE DRIFT OF COUPLED ATMOSPHERE-OCEAN MODELS

by
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A Flux Correction Method for Removing the Climate Drift of Coupled Atmosphere-Ocean Models

by

Robert Sausen, Knut Barthel and Klaus Hasselmann

Summary

A method is proposed for removing the drift of coupled atmosphere-ocean models, which in the past has often hindered the application of coupled models in climate response and sensitivity experiments. A constant ocean-atmosphere flux correction field is introduced in the boundary conditions coupling the two sub-systems together in order to balance the inconsistencies of the ocean-atmosphere flux fields evaluated separately for the individual sub-systems in independent, uncoupled mode equilibrium climate computations. The method ensures that the coupled model operates at the reference climate state for which the individual model sub-systems were designed without affecting the dynamical response of the coupled system in climate variability experiments. The method is illustrated for a simple two component box model and an ocean general circulation model coupled to a two layer diagnostic atmospheric model.

1. Introduction

A characteristic feature of the climate system is its multi-time-scale structure, arising from the widely differing time scales of the basic climate sub-systems atmosphere, ocean, cryosphere and biosphere. This has an important influence both on the natural climate variability and on the time dependent response of the climate to anthropogenic or other external factors. To simulate these effects quantitatively, coupled models are needed.

Unfortunately, the coupling of different climate sub-systems poses a number of technical problems. An obvious problem arising from the different time scales is the synchronization or matching of the numerical integration of sub-systems characterized by widely differing time steps. Here we consider another, more subtle problem, which has consistently plagued numerical experiments with coupled models: model drift (cf. Gates et al., 1985; Washington et al., 1980; Manabe et al., 1979). For illustration, we limit the discussion to the case of coupled ocean-atmosphere models, but the analysis applies generally to any coupled system.

When two general circulation models of the atmosphere and ocean are coupled to give a single model, it is found that the coupled system gradually drifts into a new climate equilibrium state, which is far removed from the present climate. The coupled model climate equilibrium may be so unrealistic (for example, with respect to sea ice extent, or the oceanic equatorial current system) that climate response or sensitivity experiments relative to this state become meaningless. This occurs regularly even when the individual models have been carefully tested in detailed numerical experiments in the decoupled mode and have been shown to yield satisfactory simulations of the climate of the separate ocean or atmosphere sub-systems.

The drift of the coupled model is clearly a sign that something is amiss with the models. However, we suggest that it is not necessary to wait with climate response and sensitivity experiments with coupled models until all causes of model drift have been properly identified and removed. Model drift is, in fact, an extremely sensitive indicator of model imperfections. The finding that the equilibrium climate into which a coupled model drifts is unacceptably far removed from the real climate does not necessarily imply that the model dynamics are too unrealistic for the model to be useful for climate response and sensitivity experiments. One should therefore devise methods for

separating the drift problem from the basically independent problem of determining the change of simulated climate induced by a change in boundary conditions and external forcing (climate response), or by changes in the physical and numerical formulation of the model (model sensitivity).

The separation of the response and sensitivity analysis from the problem of simulating the mean climate has, of course, long been standard practice in climate experiments with atmospheric models. The change $\Delta\Phi$ in the climate state resulting from changes in the external forcing-boundary conditions or model formulation is determined as the difference $\Delta\Phi = \Phi_r - \Phi_c$ between the climate Φ_r computed in a response experiment and the climate Φ_c of a control run simulating the mean climate. In this manner systematic deviations between the simulated and observed mean climate cancel, and the quality of the response computation depends only on the ability of the model to simulate the climate derivative $\partial\Phi/\partial e$ with respect to the relevant parameter e describing the externally (or internally) induced climate change.

The same approach can be applied also to the case in which the control experiment is drifting in a coupled model (cf. Schlesinger et al., 1985). However, in this case the validity of the method is restricted to the finite time interval during which the model control climate has not drifted too far away from the initial (observed) climate state. This normally excludes precisely those time scales that one would like to study with a coupled model, namely the adjustment time scales of the slow system (in our case, the ocean), since these are identical to the time scales for the adjustment of the model to its incorrect equilibrium state.

However, the separation of the mean climate and climate response problems can be achieved for coupled models rather simply by an alternative technique, the flux correction method, which we describe in this paper. The errors that result in a drift of the coupled model are compensated in this method by constant correction terms in the flux expressions by which the separate subsystem models are coupled together. The correction terms have no influence on the dynamics of the system in climate response or sensitivity experiments, but ensure that the "working point" of the model lies close to the climate state for which the individual models were originally tuned.

A simple physical interpretation and the (rather straightforward) mathematical derivation of the flux correction technique are given in section 2. The

method is illustrated for a simple example in section 3. A more realistic application to a global ocean circulation model coupled to a simplified diagnostic atmospheric model is presented in section 4. Section 5 describes an application of the technique using the coupled model of section 4 for a climate response experiment. The conclusions are summarized in the final section 6.

2. Drift removed by flux correction

The basic principle of the flux correction method is to couple the atmosphere and the ocean in such a manner that in the unperturbed case each sub-system simulates its own mean climate in the same manner as in the uncoupled mode, but responds fully interactively to the other sub-system in climate response or sensitivity experiments. The method of coupling is indicated in electrical systems terminology in Fig. 1. The atmospheric and oceanic state vectors are denoted by Φ and Ψ , respectively. In the uncoupled mode (panel a), the boundary data Φ^b , Ψ^b required by each sub-system model is provided by observations. In the fully coupled mode (panel b), the boundary data are computed from the other model, and the system adjusts to an equilibrium state which is determined only by the incoming solar radiation S_0 and by internal parameters of the model, such as surface albedo, atmospheric CO₂ concentration, etc. In the flux correction method, the coupling is carried out only for variations (Φ' , Ψ') of the climate state about its mean state ($\bar{\Phi}$, $\bar{\Psi}$). The mean state ($\bar{\Phi}$, $\bar{\Psi}$) in each system is established as in the uncoupled mode by the observed external boundary conditions. The basic principle of the flux correction method is that we distinguish between 'AC' and 'DC' components. In climate response and sensitivity experiments we are interested only in the 'AC' components. The flux correction method ensures that the 'working points' of the individual models are maintained at the values for which the models were designed, i.e. at the uncoupled model values, by maintaining the original mean 'bus voltages' $\bar{\Phi}$, $\bar{\Psi}$. ('AC' should be interpreted in this analogy not as a 'high frequency component', but as any variation on any time scale about the reference state $\bar{\Phi}$, $\bar{\Psi}$. The coupling condenser is infinitely large.)

If the mean climate state computed by the fully coupled model (panel b) lies close to the climate state predicted by the separate models (panel a), it is clear that within the framework of linear perturbation theory the flux corrected computation (panel c) should give results identical to the fully coupled computation for a small perturbation (Φ' , Ψ'). The difficulty with the fully coupled approach is that the differences between the equilibrium climates computed in the decoupled and coupled modes are generally too large to apply linearized theory. As pointed out above, this does not necessarily imply unacceptable inadequacies of the models, but is simply a consequence of the strong nonlinearity of the climate system. A 10 K change in the global mean temperature represents less than a 3 % change of the global mean tempe-

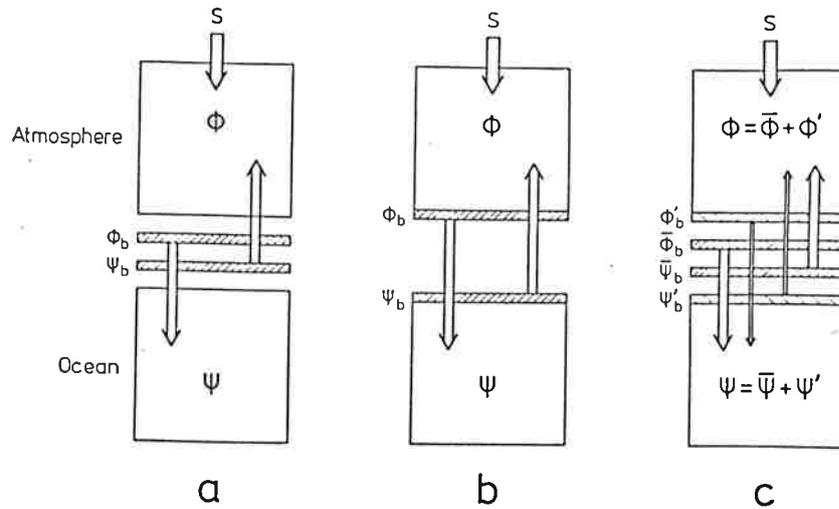


Figure 1: Boundary or coupling conditions of atmosphere and ocean models in different modes: (a) uncoupled, (b) fully coupled and (c) flux corrected.

perature of 288 K. In terms of radiative fluxes, which are proportional to the fourth power of the temperature, this translates into a 12% flux error (keeping other factors constant). If all fluxes in the model can be computed to accuracies of this order, one would normally regard the model as sufficiently accurate for first order climate response studies. Nevertheless, a 10 K global temperature change implies a major distortion of the mean climate, and it would generally not be meaningful to use this state as reference state for climate response or sensitivity experiments. A 10 K temperature increase could, for example, remove all sea ice and strongly diminish the high latitude response to an increase of CO₂ concentration, cf. Manabe and Stouffer (1980). In the decoupled mode, flux errors in the 10% range do not seriously distort the mean climate of the subsystem, since the prescribed boundary values of the complementary sub-system prevent the modeled sub-system from drifting too far away from the observed state. The disparity between the very high model fidelity needed to simulate the mean climate with a coupled model and the less stringent requirements for response and sensitivity studies is overcome in the flux correction method by separating the mean climate and climate variation problems: the mean climate is simulated with the same accuracy as in the decoupled mode, while retaining the full dynamics of the coupled system in climate variation simulations.

To translate this concept into a specific correction procedure, consider a coupled atmosphere (ϕ)-ocean (ψ) model whose evolution is described by the equations

$$\frac{\partial \phi}{\partial t} = G_A(\phi, t) + F(\phi^b, \psi^b, t) + E_A(\phi, \psi, t) , \quad (2.1)$$

$$\frac{\partial \psi}{\partial t} = G_O(\psi, t) - F(\phi^b, \psi^b, t) + E_O(\phi, \psi, t) , \quad (2.2)$$

where G_A and G_O are source functions representing all physical processes occurring within the atmospheric and oceanic sub-system, resp., and F is the flux between the sub-systems (positive from ocean to atmosphere). We assume that the model evolution differs from the evolution of the true system (ϕ_{true}, ψ_{true}) by (unknown) model errors E_A, E_O :

$$\frac{\partial \phi}{\partial t} = \frac{\partial \phi_{true}}{\partial t} + E_A(\phi, \psi, t) , \quad (2.3)$$

$$\frac{\partial \psi}{\partial t} = \frac{\partial \psi_{true}}{\partial t} + E_O(\phi, \psi, t) . \quad (2.4)$$

A long term strategy of model development must be clearly directed towards identifying and correcting the model errors E_A and E_O . For complex, nonlinear systems, this is generally very time consuming. We consider here the situation in which the errors are already small and we simply wish to remove the drift they cause without otherwise influencing the dynamics of the model.

A possible method to prevent the model equilibrium state from departing too strongly from the observed equilibrium is to introduce a Newtonian correction term (as used, e.g by Sarmiento and Bryan, 1982, in their "robust diagnostic" ocean model). The model equation then takes the form

$$\frac{\partial \phi}{\partial t} = G_A(\phi, t) + F(\phi^b, \psi^b, t) - M_A(\phi - \phi_m) , \quad (2.5)$$

$$\frac{\partial \Psi}{\partial t} = G_O(\Psi, t) - F(\phi^b, \Psi^b, t) - M_O(\Psi - \Psi_m) , \quad (2.6)$$

where ϕ_m and Ψ_m are the observed (measured) atmospheric and oceanic variables, respectively, and M_A and M_O are (normally diagonal) matrices of the Newtonian correction coefficients. In general, relatively large Newtonian coefficients are needed in order to reduce the drift of the coupled mean deviation to same level as the errors of the uncoupled models, so that the system response is significantly dampened. Thus the dynamics of the system is changed, and the method cannot be used for our applications.

In the flux correction method, the errors E_A , E_O in equation (2.1), (2.2) are balanced in the equilibrium state by constant additive flux terms ΔF_A and ΔF_O :

$$\frac{\partial \Phi}{\partial t} = G_A(\Phi, t) + F(\Phi^b, \Psi^b, t) + \Delta F_A , \quad (2.7)$$

$$\frac{\partial \Psi}{\partial t} = G_O(\Psi, t) - F(\Phi^b, \Psi^b, t) - \Delta F_O . \quad (2.8)$$

We choose the flux corrections such that the equilibrium climate (ϕ_c, Ψ_c) of the coupled system is identical to the equilibrium climate (ϕ_u, Ψ_u) attained by each of the sub-systems separately when run in the uncoupled mode. (It is the basic premise of our method that this lies close to the true climate). Substituting the desired equilibrium climate (ϕ_u, Ψ_u) into eq. (2.7) and (2.8) and subtracting from these the equations for the equilibrium climates of the sub-system when computed in the uncoupled mode,

$$\frac{\partial \phi_u}{\partial t} = G_A(\phi_u, t) + F(\phi_u^b, \Psi_m^b, t) , \quad (2.9)$$

$$\frac{\partial \Psi_u}{\partial t} = G_O(\Psi_u, t) - F(\phi_m^b, \Psi_u^b, t) , \quad (2.10)$$

we obtain

$$\Delta F_A = F(\phi_u^b, \Psi_m^b, t) - F(\phi_u^b, \Psi_u^b, t) , \quad (2.11)$$

$$\Delta F_O = F(\phi_m^b, \psi_u^b, t) - F(\phi_u^b, \psi_u^b, t). \quad (2.12)$$

It is seen that by supplying to each sub-system a flux correction representing the difference between the flux computed in the uncoupled experiment, using observed data for the boundary value of the complementary system, and the flux computed, using the boundary values determined in each of the uncoupled experiments, each subsystem receives the flux required to establish the same equilibrium as was found in the uncoupled mode. The constant additive fluxes cancel when considering the deviations of the climate state relative to some reference state, and thus have no effect in climate response or sensitivity experiments.

In the above analysis we have retained the time dependence throughout, since we define the climate equilibrium solutions generally as climate states which are averaged to exclude the statistical variability but include the annual cycle. According to equations (2.11), (2.12), the computation of the flux correction terms requires only diagnostic computations of the fluxes for boundary values taken from the uncoupled mode solutions. For simple systems with a few degrees of freedom, the flux correction term can also be determined from the rate of drift of the coupled system. However, for more complex systems it is generally not straightforward to relate the rate of drift of the full climate state vectors to the individual flux corrections which need to be applied to the separate sub-system interface to balance the drift.

3. An example

To illustrate the flux correction method, we consider a simple nonlinear ocean-atmosphere model with two degrees of freedom. The atmosphere and the ocean are described by their temperatures T_A and T_O , resp., which are governed by the energy balance equations,

$$C_A \frac{dT_A}{dt} = R_A - \lambda_A T_A + k(T_O - T_A), \quad (3.1)$$

$$C_O \frac{dT_O}{dt} = R_O - \lambda_O T_O - k(T_O - T_A). \quad (3.2)$$

Here C_A and C_O denote the atmospheric and oceanic heat capacities, R_A and R_O the solar energy input to each system, $\lambda_A T_A$ and $\lambda_O T_O$ represent the radiative losses (linearized about reference temperatures), and $k(T_O - T_A)$ the flux of energy from the ocean to the atmosphere. R_A is taken as constant, but R_O is represented as the nonlinear function

$$R_O(T_O) = \begin{cases} R_O^{(1)} & \text{for } T_O \leq T_O^{(1)} \\ R_O^{(1)} + \frac{T_O - T_O^{(1)}}{T_O^{(2)} - T_O^{(1)}} (R_O^{(2)} - R_O^{(1)}) & \text{for } T_O^{(1)} < T_O < T_O^{(2)} \\ R_O^{(2)} & \text{for } T_O^{(2)} \leq T_O \end{cases} \quad (3.3)$$

where $R_O^{(2)} > R_O^{(1)}$. The form (3.3) corresponds to the traditional representation of the nonlinear sea-ice albedo feedback in energy balance models. For $T_O \leq T_O^{(1)}$, the sea surface is completely ice covered, while for $T_O \geq T_O^{(2)}$ the sea surface is free of ice.

We take as the observed atmospheric and oceanic temperatures $T_A^{(m)} = 286$ K and $T_O^{(m)} = 288$ K. A "perfect" model (PM), which reproduces these values, is given by one set of parameters in Table 1. We assume that the perfect model is not known and that we have constructed an approximate model AM, whose parameters are also listed in Table 1. The model AM is assumed to have been

tested for each sub-system in the uncoupled mode and we now wish to apply the model in the coupled mode for a response experiment.

Table 1

Numerical values of the coefficients of the "perfect" model PM and the approximate model AM.

	atmosphere	ocean
heat capacity	$C_A = 10^7 \text{ J}/(\text{m}^2\text{K})$	$C_O = 10^8 \text{ J}/(\text{m}^2\text{K})$
solar input	$R_A = 130 \text{ W}/\text{m}^2$	$R_{O(1)} = 120 \text{ W}/\text{m}^2$ $R_{O(2)} = 125 \text{ W}/\text{m}^2$
reference temperatures		$T_{O(1)} = 290 \text{ K}$ $T_{O(2)} = 295 \text{ K}$
coupling constant	$k = 10 \text{ W}/(\text{m}^2\text{K})$	$k = 10 \text{ W}/(\text{m}^2\text{K})$
Newton coefficients	$m_A = 10 \text{ W}/(\text{m}^2\text{K})$	$m_O = 15 \text{ W}/(\text{m}^2\text{K})$
control PM emissivity	$\lambda_A = 0.5245 \text{ W}/(\text{m}^2\text{K})$	$\lambda_O = 0.3472 \text{ W}/(\text{m}^2\text{K})$
reduced	$\lambda_A = 0.5144 \text{ W}/(\text{m}^2\text{K})$	
control AM emissivity	$\lambda_A = 0.5200 \text{ W}/(\text{m}^2\text{K})$	$\lambda_O = 0.3400 \text{ W}/(\text{m}^2\text{K})$
reduced	$\lambda_A = 0.5100 \text{ W}/(\text{m}^2\text{K})$	

In the uncoupled mode, the atmospheric model is driven by the observed oceanic temperature $T_O^{(m)}$ while the ocean model is forced by the observed atmospheric temperature $T_A^{(m)}$,

$$C_A \frac{dT_A}{dt} = R_A - \lambda_A T_A + k(T_O^{(m)} - T_A), \quad (3.4)$$

$$C_O \frac{dT_O}{dt} = R_O - \lambda_O T_O - k(T_O - T_A^{(m)}). \quad (3.5)$$

The atmospheric model has a unique steady state solution

$$T_A^{(u)} = \frac{R_A + kT_O^{(m)}}{\lambda_A + k} \quad (3.6)$$

The ocean model can have either one stable steady state solution or two stable solutions and one unstable solution, depending on the values of the parameters. The stable solutions lie in the first or third regions of (3.3) on either side of the unstable middle region, and are given by

$$T_O^{(u)} = \frac{R_O^{(i)} + kT_A^{(m)}}{\lambda_O + k} \quad (3.7)$$

The index i may take on both values 1 and 2 or only one of the two, depending on whether the values of $T_O^{(u)}$ determined by (3.7) are consistent with the inequalities defining the temperature range for a given $R^{(i)}$ in eq. (3.3). For PM, $(T_A^{(m)}, T_O^{(m)})$ is the only solution. The model AM also yields only one stable solution: $T_A^{(u)} = 286.12$ K, $T_O^{(u)} = 288.20$ K, which differs slightly from the solution of PM which reproduces the observations.

The equilibrium heat flux into the atmosphere for the uncoupled atmospheric model AM is determined as

$$F_A = F(T_A^{(u)}, T_O^{(m)}) = k(T_O^{(m)} - T_A^{(u)}) = 18.78 \text{ W/m}^2, \quad (3.8)$$

while the corresponding flux for the uncoupled ocean model AM is

$$F_O = F(T_A^{(m)}, T_O^{(u)}) = k(T_O^{(u)} - T_A^{(m)}) = 22.01 \text{ W/m}^2 \quad (3.9)$$

An atmospheric "climate response" experiment, in which the parameter λ_A (representing for example a change in the green-house effect) is slightly reduced (2%, see Table 1), while the sea surface temperature is kept fixed, results in a small increase of the atmospheric temperature ($\Delta T_A^{(m)} = 0.27$ K for PM and AM). As the atmosphere is strongly coupled to the ocean, only a weak response is possible. (For a summary of the numerical results see Table 2.)

Table 2

Results of the simple coupled ocean atmosphere model. Temperatures in K.

		control	reduced emissivity	difference
observed	$T_A(m)$	286.00	---	---
	$T_O(m)$	288.00	---	---
uncoupled AM	$T_A(u)$	286.12	286.39	0.27
	$T_O(u)$	288.20	288.20	0.00
	$T_A(u) - T_A(m)$	0.12	0.39	---
	$T_O(u) - T_O(m)$	0.20	0.20	---
uncoupled PM	$T_A(u)$	286.00	286.27	0.27
	$T_O(u)$	288.00	288.00	0.00
	$T_A(u) - T_A(m)$	0.00	0.27	---
	$T_O(u) - T_O(m)$	0.00	0.00	---
coupled without flux correction	$T_A(c)$	295.57	299.10	3.53
	$T_O(c)$	297.94	301.35	3.41
	$T_A(c) - T_A(m)$	9.57	13.10	---
	$T_O(c) - T_O(m)$	9.94	13.35	---
coupled with Newtonian forcing	$T_A(n)$	286.13	286.30	0.17
	$T_O(n)$	288.13	288.20	0.07
	$T_A(n) - T_A(m)$	0.13	0.30	---
	$T_O(n) - T_O(m)$	0.13	0.20	---
coupled with flux correction	$T_A(c)$	286.12	295.30	9.18
	$T_O(c)$	288.20	297.56	9.36
	$T_A(c) - T_A(m)$	0.12	9.30	---
	$T_O(c) - T_O(m)$	0.20	9.56	---
coupled PM	$T_A(c)$	286.00	295.08	9.08
	$T_O(c)$	288.00	297.28	9.28
	$T_A(c) - T_A(m)$	0.00	9.08	---
	$T_O(c) - T_O(m)$	0.00	9.28	---

The coupled model also has either one or two stable equilibrium solutions:

$$T_O^{(c)} = \frac{(k + \lambda_A)R_O^{(i)} + kR_A}{\lambda_A \lambda_O + (\lambda_A + \lambda_O)k}, \quad i = 1, 2; \quad (3.10)$$

$$T_A^{(c)} = \frac{R_A + kT_O^{(c)}}{\lambda_A + k}. \quad (3.11)$$

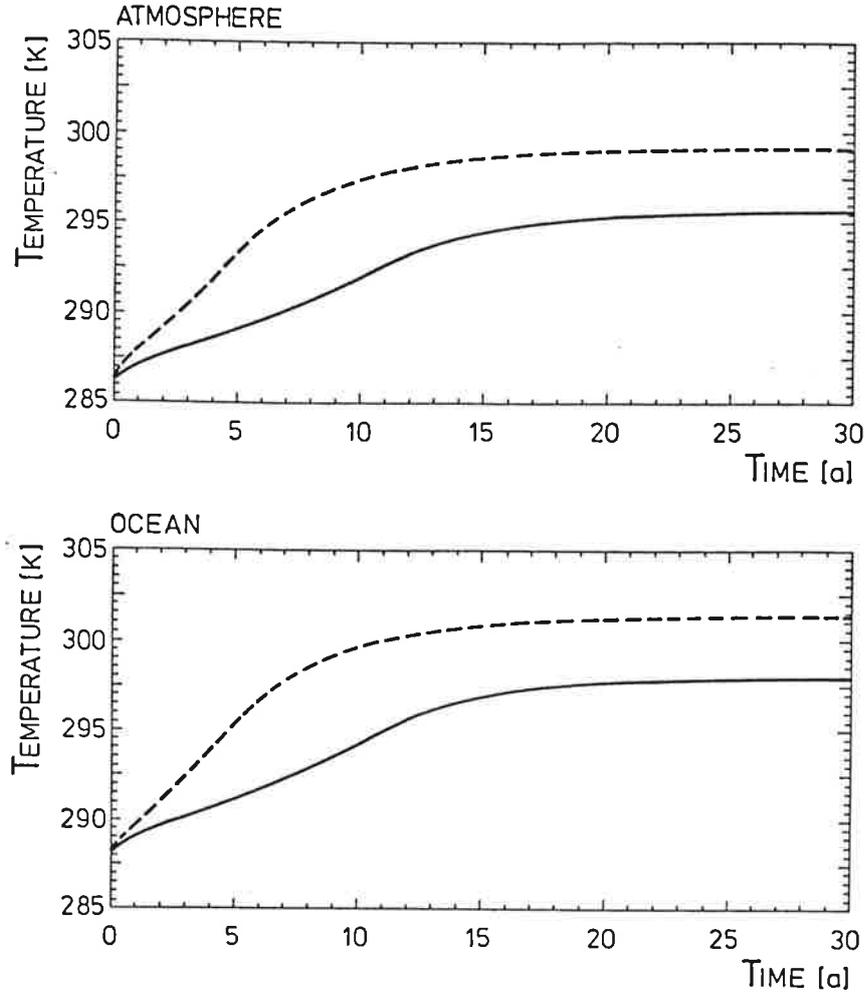


Figure 2: A coupled nonlinear ocean-atmosphere model with two degrees of freedom. Time evolution of the control run (solid line) and the reduced emissivity run (dashed line) without flux correction.

For PM again only one stable solution exists, $T_A^{(c)} = T_A^{(m)}$, $T_O^{(c)} = T_O^{(m)}$. For AM the coupled model drifts into a new equilibrium climate state, $T_A^{(c)} = 295.57$ K, $T_O^{(c)} = 297.94$ K (see Fig. 2, solid curves). The flux from the ocean into the atmosphere for this equilibrium is given by

$$F_C = F(T_A^{(c)}, T_O^{(c)}) = k(T_O^{(c)} - T_A^{(c)}) = 23.7 \text{ W/m}^2. \quad (3.12)$$

A "climate response" experiment with the modified value λ_A (dashed lines in Fig. 2) results in a change of the coupled model of $\Delta T_A^{(c)} = 3.53$ K and $\Delta T_O^{(c)} = 3.41$ K. This is significantly smaller than both the climate drift and the true coupled response of PM ($\Delta T_A = 9.08$ K, $\Delta T_O = 9.28$ K).

If Newtonian feedback terms are introduced as in eq. (2.5), (2.6), the model takes the form

$$C_A \frac{dT_A}{dt} = R_A - \lambda_A T_A + k(T_O - T_A) - m_A(T_A - T_A^{(m)}) , \quad (3.13)$$

$$C_O \frac{dT_O}{dt} = R_O - \lambda_O T_O - k(T_O - T_A) - m_O(T_O - T_O^{(m)}) . \quad (3.14)$$

Setting $m_A = 10 \text{ W}/(\text{m}^2\text{K})$ and $m_O = 15 \text{ W}/(\text{m}^2\text{K})$, for example, the drift of the coupled model AM is reduced to 0.13 K for both the atmospheric and the oceanic temperature. However, the response to the changed λ_A is now also drastically dampened : $\Delta T_A^{(n)} = 0.17 \text{ K}$, $\Delta T_O^{(n)} = 0.07 \text{ K}$.

If we solve the drift problem by the flux correction method, the corresponding flux corrections according to (2.11), (2.12) are given by

$$\Delta F_A = F(T_A^{(u)}, T_O^{(m)}) - F(T_A^{(u)}, T_O^{(u)}) = -k(T_O^{(u)} - T_O^{(m)}) = -2.01 \text{ W}/\text{m}^2 , \quad (3.15)$$

$$\Delta F_O = F(T_A^{(m)}, T_O^{(u)}) - F(T_A^{(u)}, T_O^{(u)}) = +k(T_A^{(u)} - T_A^{(m)}) = 1.22 \text{ W}/\text{m}^2 , \quad (3.16)$$

and the model equations take the form

$$C_A \frac{dT_A}{dt} = R_A - \lambda_A T_A + k(T_O - T_A) - k(T_O^{(u)} - T_O^{(m)}) , \quad (3.17)$$

$$C_O \frac{dT_O}{dt} = R_O - \lambda_O T_O - k(T_O - T_A) - k(T_A^{(u)} - T_A^{(m)}) . \quad (3.18)$$

The equilibrium model climate is now preserved as in the uncoupled case (see Fig. 3, solid lines). The climate response to a variation of λ_A is determined as $\Delta T_A^{(c)} = 9.18 \text{ K}$ and $\Delta T_O^{(c)} = 9.36 \text{ K}$, which agrees with the true response within 1% (cf. Table 2).

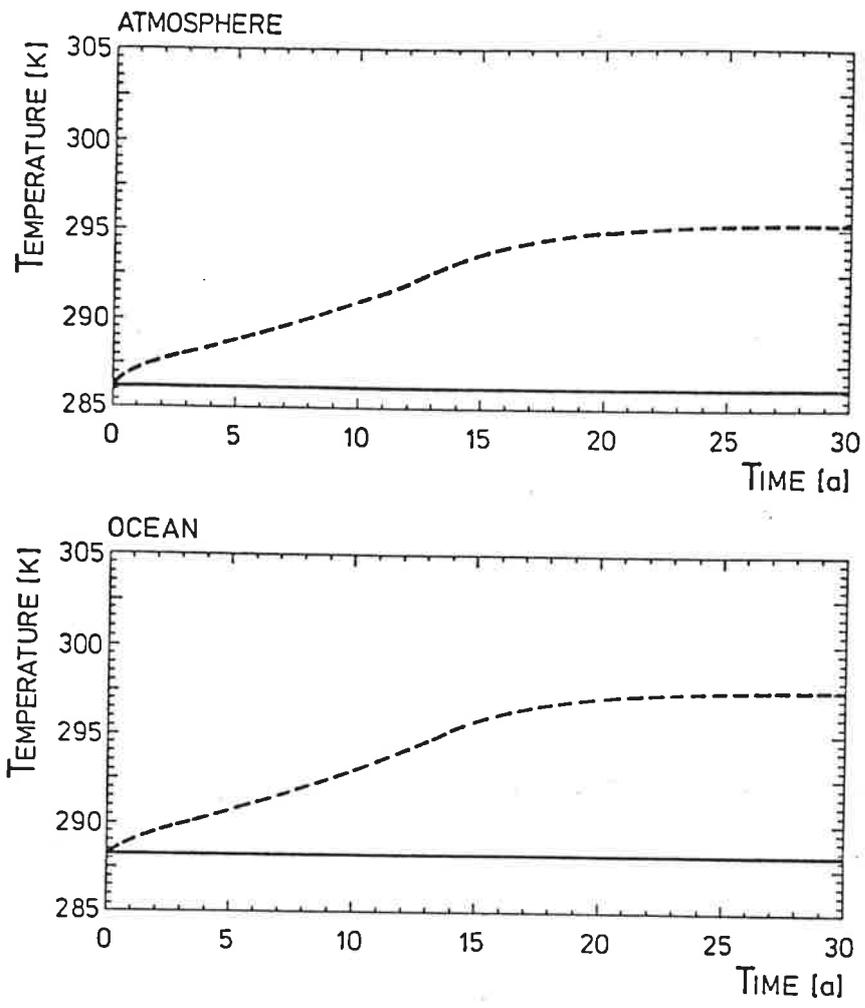


Figure 3: Same as Fig. 2, but with flux correction.

4. Coupling of an oceanic general circulation model to a diagnostic atmospheric model.

The global ocean circulation model used for this coupling experiment is based on the model described in Maier-Reimer et al (1983, 1987). Salinity and temperature are transported in the model by advection only, except for local convection in high latitude regions to maintain static stability and numerical diffusion. The model includes a realistic bottom topography and is run in the present experiment using a $3.54^\circ \times 3.54^\circ$ horizontal grid mesh with 5 vertical levels (at 75, 150, 300, 1000 and 3000 m depth for the horizontal velocity, temperature and salinity, and 112, 225, 650, 2000 and 6000 m for the vertical velocity). In the uncoupled model the circulation is driven by Hellerman's (1967) wind stress using the observed surface values of the salinity and temperature from Levitus and Oort (1977) as surface boundary condition. The model was run without a seasonal cycle. Sea ice was not included.

The atmospheric model is a two layer radiative convective model with horizontal coupling by temperature advection by the observed wind and a (weak) diffusive transport. The evolution equation for the temperature field T is given by

$$\frac{\partial T}{\partial t} = -\nabla \cdot \mathbf{V}T - r \frac{\partial(\omega\theta)}{\partial p} + D\nabla^2 T + \frac{Q}{c_p} \quad (4.1)$$

where \mathbf{V} represents the horizontal wind, ω the vertical component of the wind, and p the pressure, D a diffusion constant, Q the diabatic heating, c_p the heat capacity at constant pressure, and θ the potential temperature. This is given by

$$r\theta = T \quad (4.2)$$

with

$$r = \left(\frac{p}{p_{00}} \right)^{R/c_p} \quad (4.3)$$

R is the gas constant and p_{00} a reference pressure. The observed wind \mathbf{V} is the zonal and annual mean calculated from Oort's (1983) data. The vertical wind ω is determined from the prescribed horizontal wind by the continuity equation

$$\nabla \cdot \mathbf{V} + \frac{\partial \omega}{\partial p} = 0 \quad (4.4)$$

The atmosphere is driven by the annual solar radiation (Coakley, 1979) and by the annual mean of sea surface temperature (SST). In the uncoupled case, this was taken from Levitus and Oort (1977), while in the coupled case, it is calculated by the oceanic model. The surface temperature over land is calculated as the radiative convective equilibrium temperature. A snow-ice albedo parameterization with a step function temperature dependence at 0°C was used. The model was integrated on a $2.5^\circ \times 5^\circ$ latitude-longitude C-grid with the two (temperature) levels at 400 hPa and 800 hPa. For more details see Sausen (1987).

In the coupled experiments, the total heat flux coupling the two systems was computed from the sea surface temperature T_s , taken as the temperature of the uppermost ocean layer (75 m depth), and the temperature T_3 of the lowest atmospheric level according to

$$F = -\varepsilon_s S - \alpha_3 \sigma_B T_3^4 + \alpha_s \sigma_B T_s^4 + H_s \quad (4.5)$$

F consists of the sum of the incoming solar radiation $\varepsilon_s S$ (into the ocean), the infrared radiation $\alpha_3 \sigma_B T_3^4$, $\alpha_s \sigma_B T_s^4$ absorbed and emitted by the ocean, respectively, and the sensible and latent heat flux H_s emitted by the ocean parameterized by the bulk formula

$$H_s = \begin{cases} h_s (\Theta_s - \Theta_3) & , \text{if } \Theta_s > \Theta_3 \\ 0 & , \text{if } \Theta_s \leq \Theta_3 \end{cases} \quad (4.6)$$

with a constant h_s .

The oceanic model uses an implicit time integration scheme with a time step of one month. With respect to this time step the atmospheric model is run in a diagnostic mode. However, the equilibrium atmospheric state was actually computed by integrating the atmospheric model, using the prognostic equation (4.1) with a 1 hour time step, for 120 time steps (five days). (The atmospheric model requires only little computer time).

The equilibrium temperature fields of the atmospheric model in the uncoupled mode are shown in Fig. 4. As only a small diffusion coefficient was used

($D = 1.75 \cdot 10^{-6} \text{ m}^2/\text{s}$), the temperature fields exhibit a structure which is rather too zonal. Figure 5 shows the corresponding equilibrium temperature fields of the oceanic model in the uncoupled mode, while the currents are shown in Figure 6. As the boundary conditions for salinity and wind were not changed in the coupled case, we shall only consider the temperature fields in the following (although the salinity and velocity fields were, of course, also modified in the coupled case).

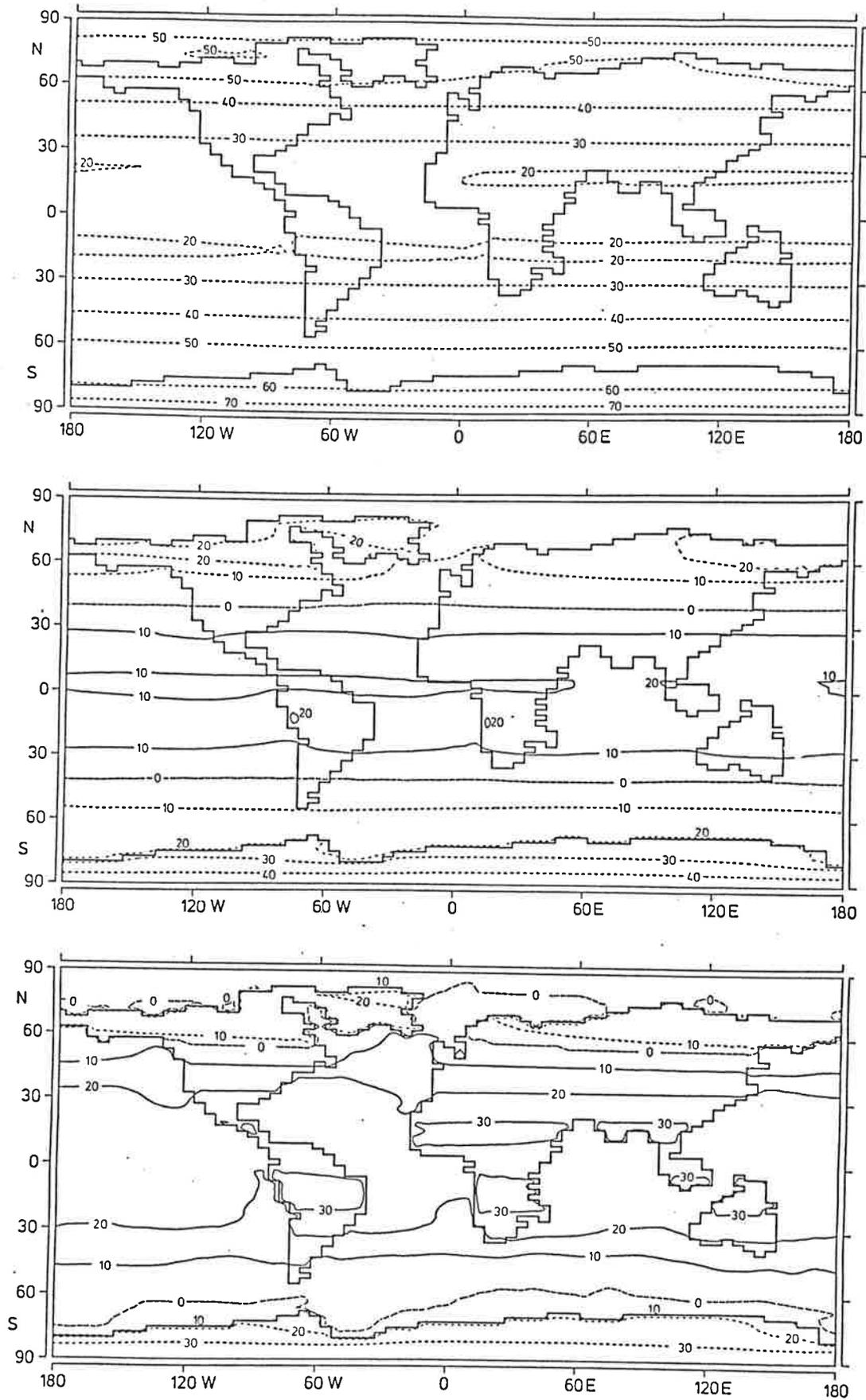


Figure 4: Equilibrium temperature fields in °C of the two level atmospheric energy balance model; (a): 400 hPa, (b): 800 hPa, (c): surface. Isoline intervals are 10°C, Negative isolines are dashed.

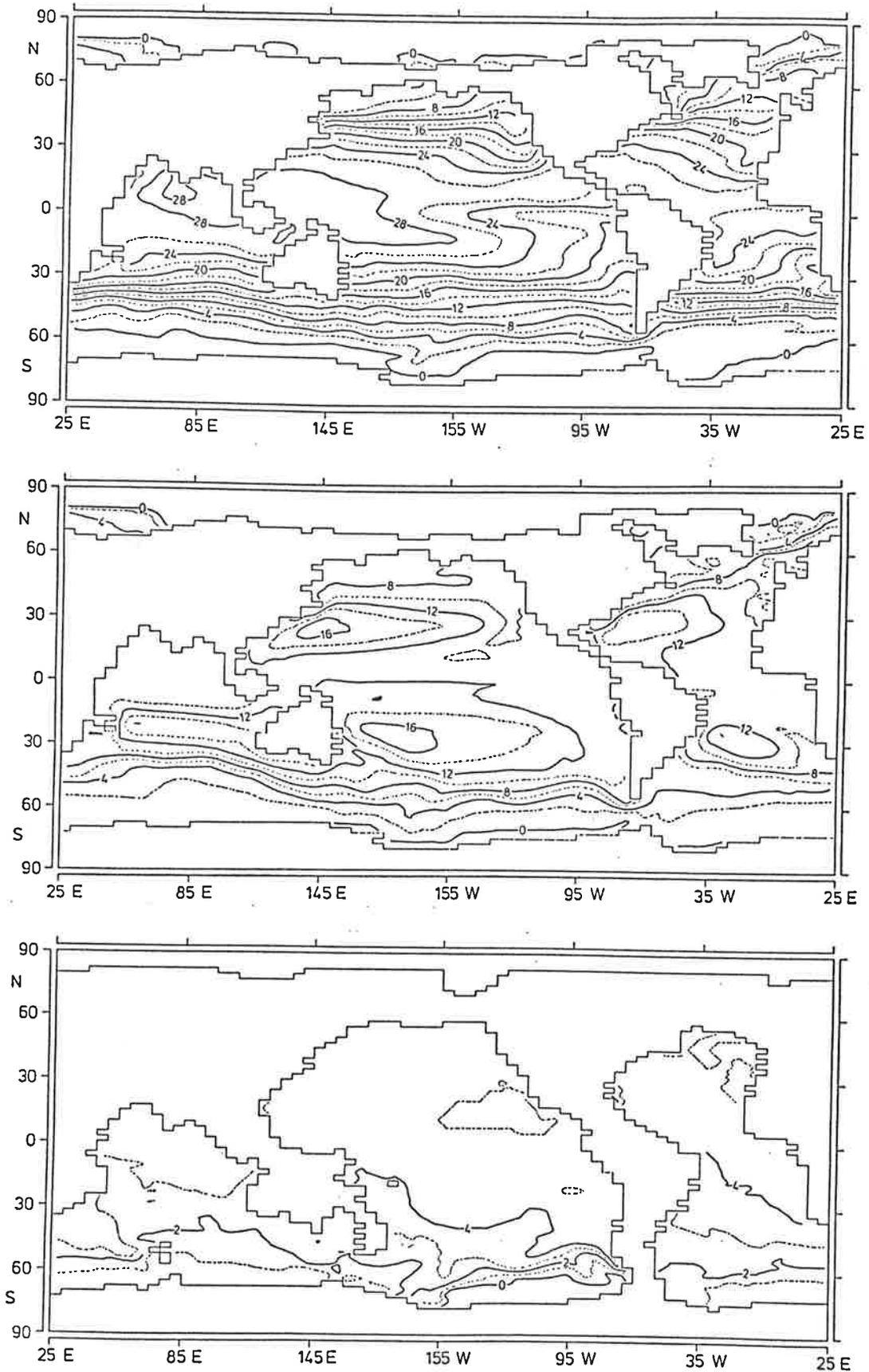


Figure 5: Equilibrium temperature fields of the global ocean general circulation model. (a): 75 m, (b): 300 m, (c): 3000 m. Isoline intervals are 2 °C for panels (a) and (b), 1 °C for panel (c).

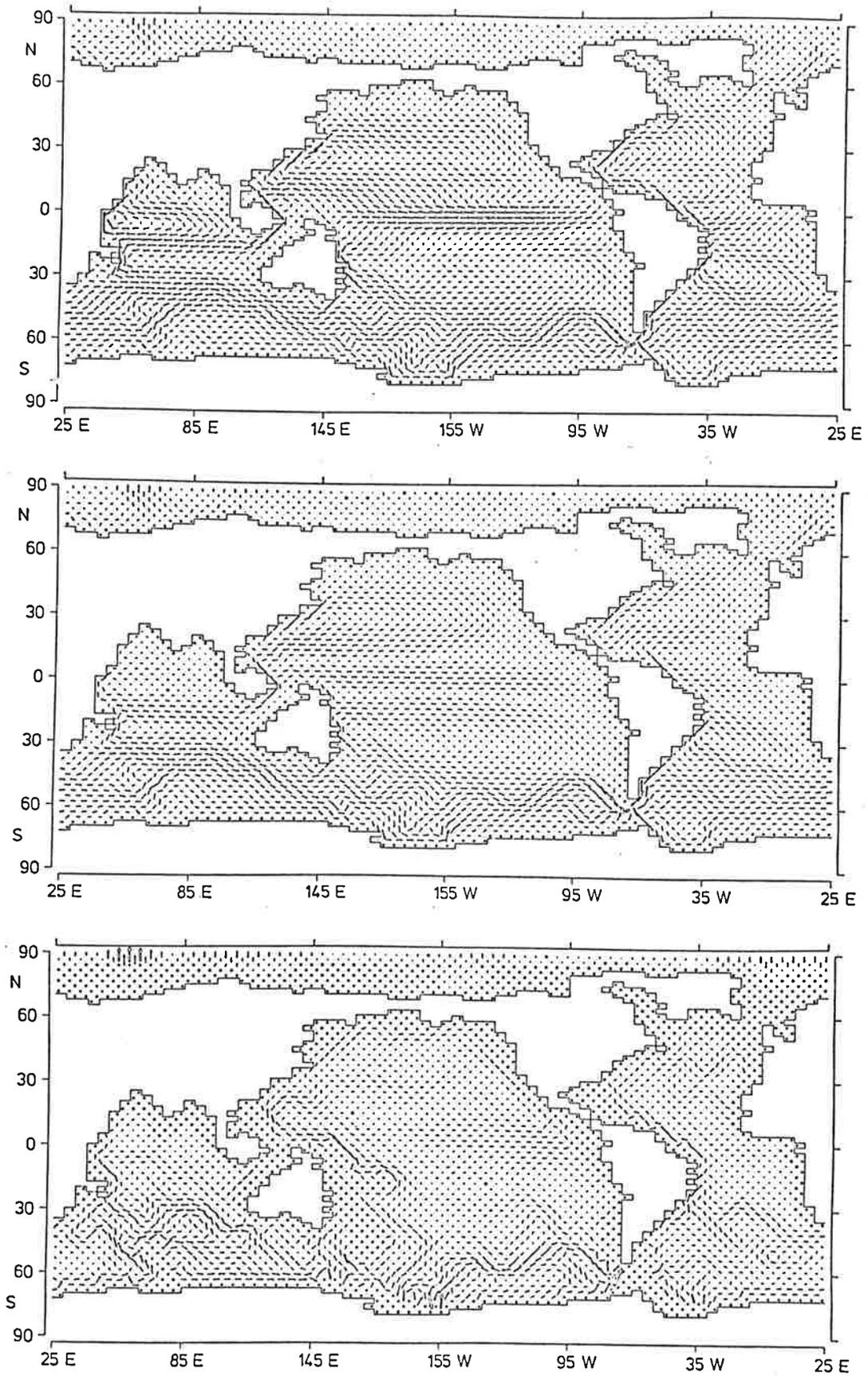


Figure 6: Equilibrium current fields of global ocean general circulation model, (a): 75 m, (b): 300 m, (c): 3000 m.

The total heat flux from the ocean into the atmosphere computed from the atmospheric model in the uncoupled mode is shown in Figure 7. One obtains the expected global structure, with a flux into the ocean in the tropics and out of the ocean at high latitudes. The upwelling areas in the eastern Pacific and eastern Atlantic stand out clearly as maxima of positive flux into the ocean. The Gulfstream region and the Norwegian Sea appear as areas with a large flux into the atmosphere. The high values of the flux from the ocean into the atmosphere in the Arctic Sea is strongly exaggerated due to the lack of sea ice in the present oceanic model.

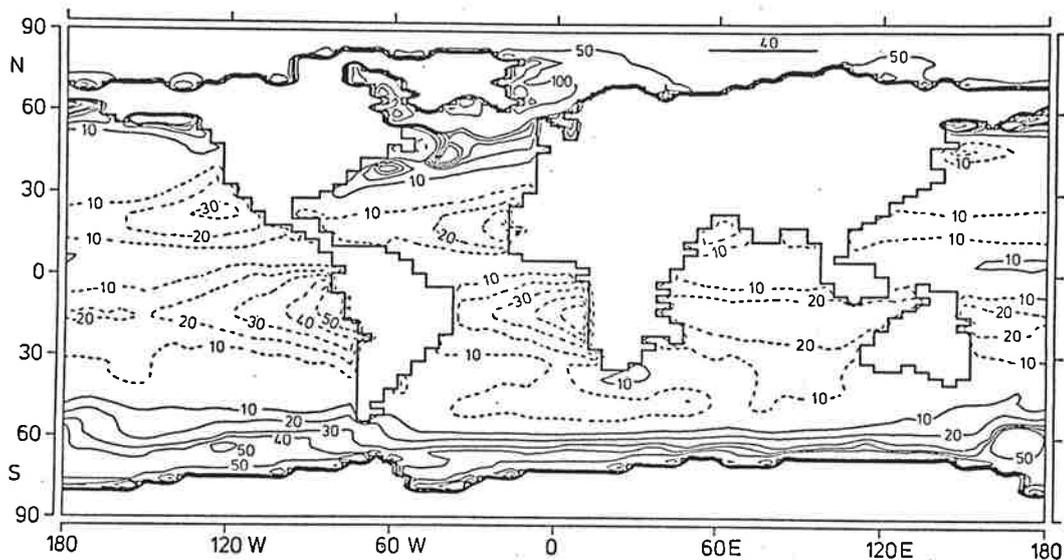


Figure 7: Sea-air heat flux of the atmospheric model in the uncoupled mode. Isolines intervals are 10 Wm^{-2} below 50 Wm^{-2} , 50 Wm^{-2} above 50 Wm^{-2} . Negative isolines are dashed.

The sea-air heat flux of the uncoupled ocean, shown in Fig. 8, differs significantly from the flux computed for the uncoupled atmosphere, Fig. 7. In the North Atlantic and the Norwegian Sea, for example, the atmospheric model yields a heat flux into, rather than out of the ocean. The differences represent an incompatibility of the models which must be corrected for, if both models are to be coupled together. (It could be well argued in the present case that the atmospheric model is considerably less realistic than the oceanic model, and that the "state of the art" of this model does not really justify its use with an ocean model in a coupled mode. Nevertheless, to illustrate the method we assume that we are satisfied with the performance of the atmospheric model in the uncoupled mode).

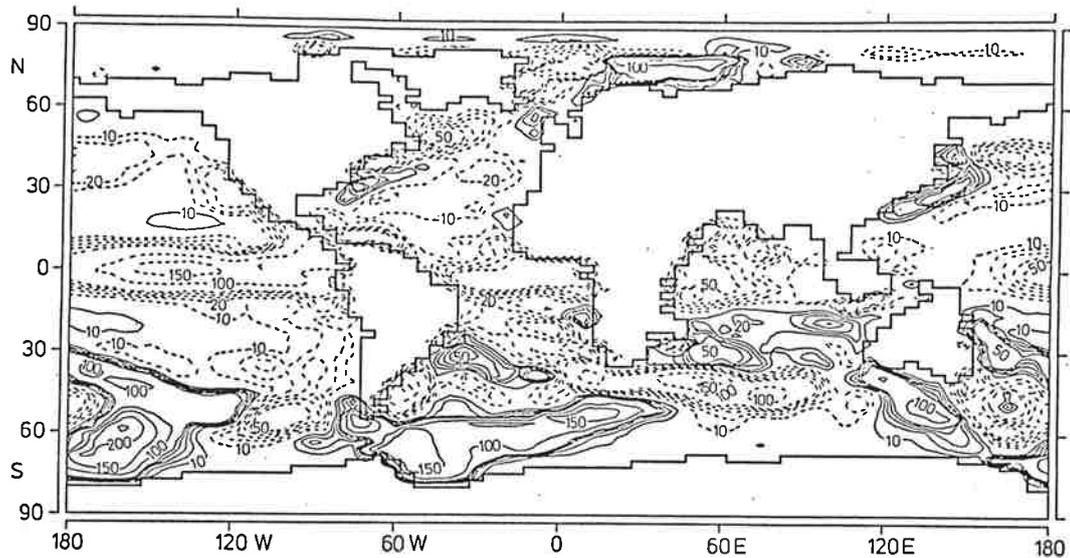


Figure 8: Sea-air heat flux of the oceanic model in the uncoupled model.
(Isoline intervals as in Fig. 7.)

One of the terms occurring in the flux correction expressions is the sea-air flux computed from the boundary values of the atmosphere and ocean corresponding to the equilibrium states of the separate uncoupled model experiments (cf. eq. (2.11) and (2.12)). This is shown in Figure 9. The field exhibits a structure similar to that of Figure 7. The flux correction for the atmosphere is the difference of the flux fields of Figures 7 and 9, and is plotted in Fig. 10. The flux correction is generally small over tropical and midlatitude oceans. However, in the northern Atlantic, the Norwegian Sea, the Arctic Sea, the Weddell Sea and the Ross Sea, it is of the same order as the flux itself. This may be attributed in part to the lack of sea ice. The flux correction for the ocean (Fig. 11) shows rather large values in many regions. This reflects primarily insufficiencies of the atmospheric model.

Starting from the equilibrium solutions of the uncoupled models, the coupled model was integrated for a hundred years both without and with flux correction. The temporal evolution of the global mean temperatures of the atmosphere for both cases is plotted in Figure 12. Without flux correction, the coupled-run climate drifts rapidly away from the uncoupled-run climate. The original surface temperature of 16.4°C decreases by 2.0 K in the first 10 years and by 3.2 K in 100 years. The drift for levels 1 and 2 is similar, but slightly smaller. With flux correction, the temperatures remain close to the initial values. Within one hundred years the surface temperature decreases by only 0.6 K, while the temperatures in level 1 and 2 are lowered by only 0.2 K.

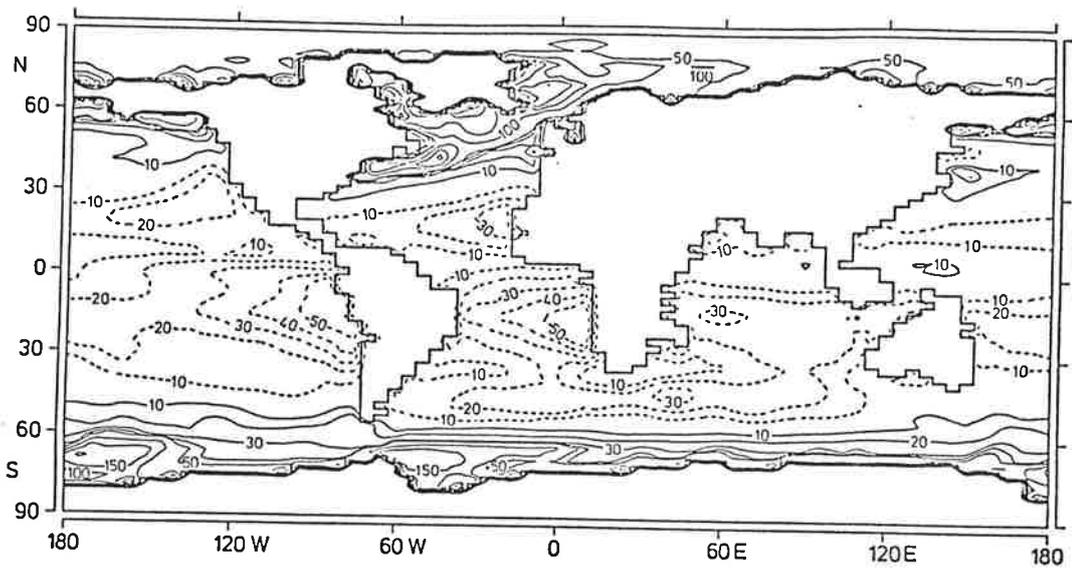


Figure 9: Sea-air heat flux computed for the boundary values corresponding to the equilibrium states of the uncoupled models. (Isoline intervals as in Fig. 7.)

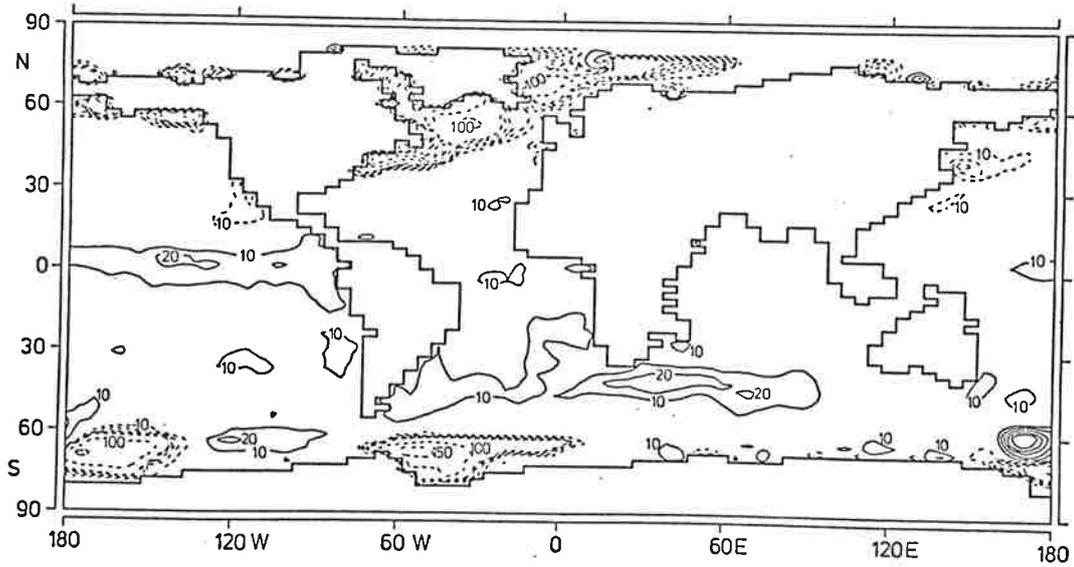


Figure 10: Flux correction for the atmosphere. (Isoline intervals as in Fig. 7.)

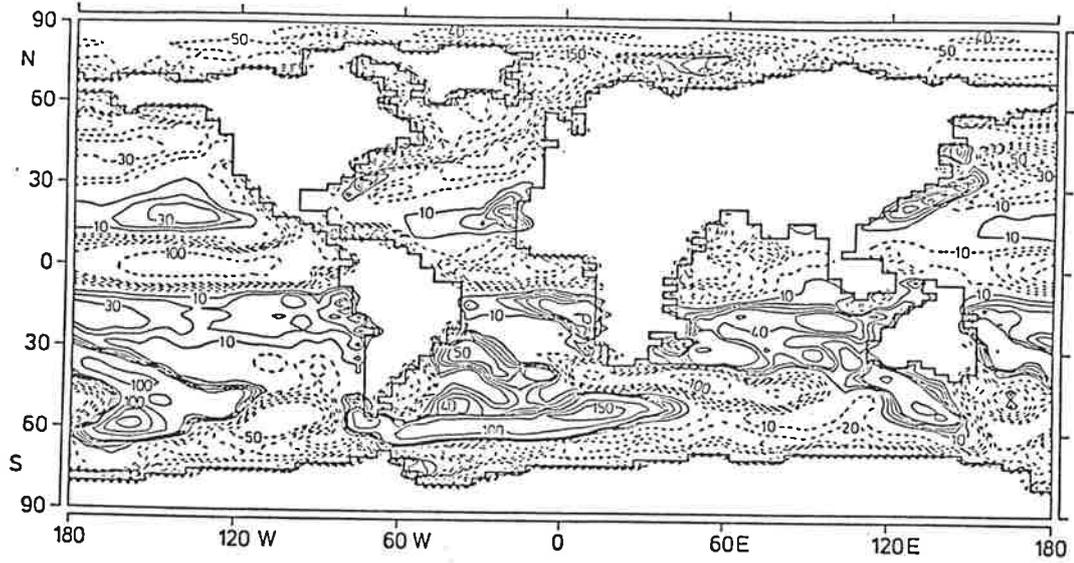


Figure 11: Flux correction for the ocean (Isoline intervals as in Fig. 7.).

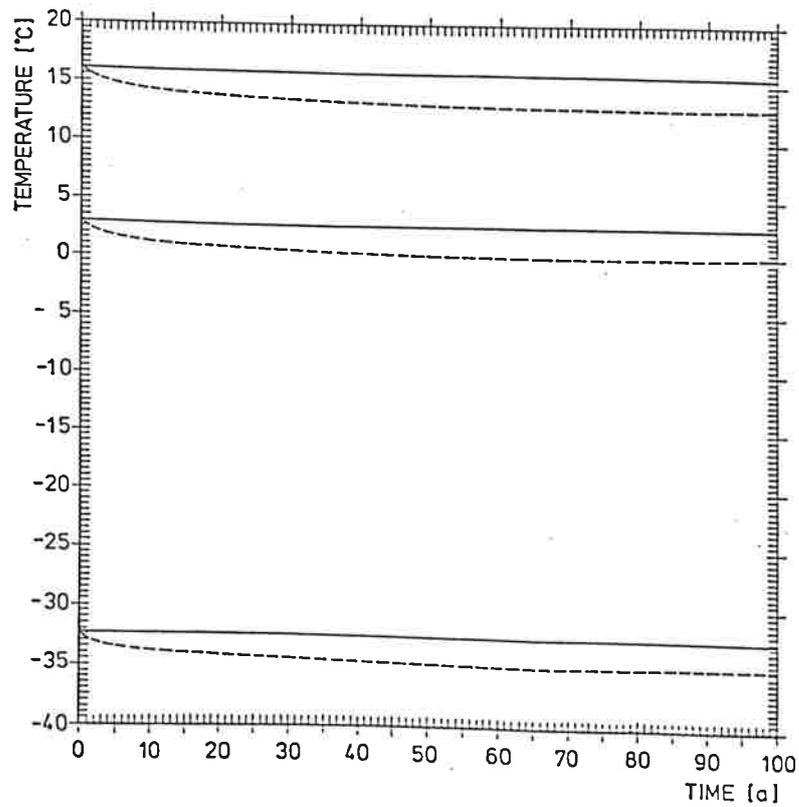


Figure 12: Temporal evolution of the global mean temperatures of the atmosphere, in the coupled model, without flux correction (dashed line) and with flux correction (solid line).

The global mean temperatures of the ocean (Fig. 13) also drift away in the coupled run without flux correction. In contrast to the atmosphere, where the drift time constant is approximately the same for all levels (it is effectively determined by the SST drift rate), the drift rate in the ocean is seen to be strongly dependent on depth. The deeper layers drift away more slowly and take longer to reach an equilibrium than the surface layers.

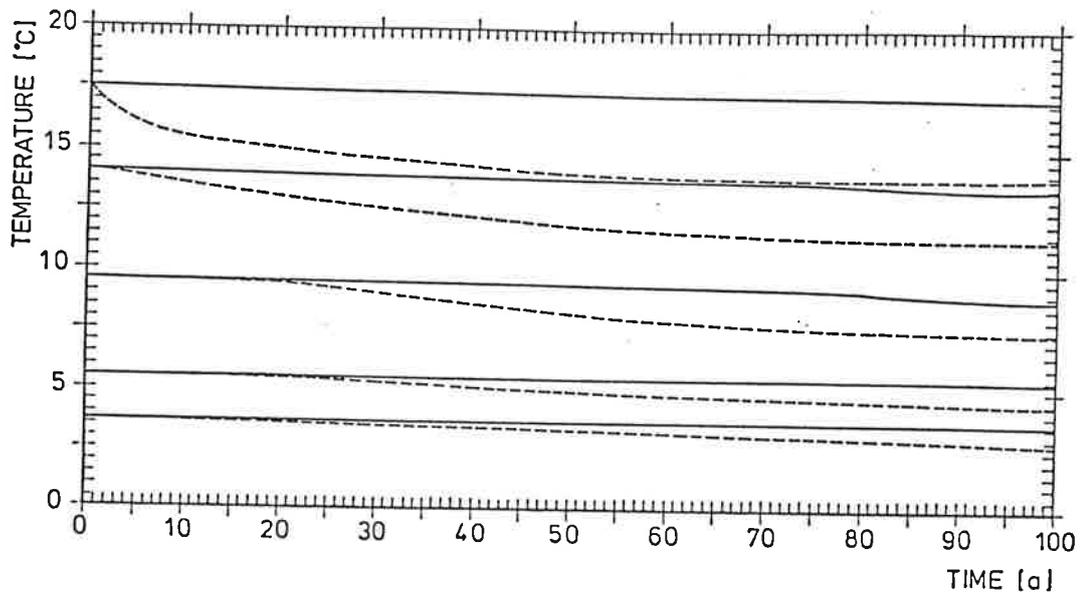


Figure 13: Temporal evolution of the global mean temperatures of the ocean, without flux correction (dashed line) and with flux correction (solid line).

The drift is largely removed after the flux correction is introduced, as seen in the plots of the temperature change over 100 years (Fig. 14 - 18). It should be noted, however, that although the changes are reduced by an order of magnitude, they are not identically zero, as expected theoretically. The drift is largest in the Arctic and Antarctic oceans. The residual drift is due in part to the fact that the uncoupled oceanic model had not completely achieved an equilibrium state after 5000 years integration, so that there the computed flux correction contained a small error. A further contributing factor was in the parameterization of the oceanic convection as an intermittent convective adjustment process. This introduced stochastic noise into the model, which also results in low frequency model drift (K. Hasselmann, 1976).

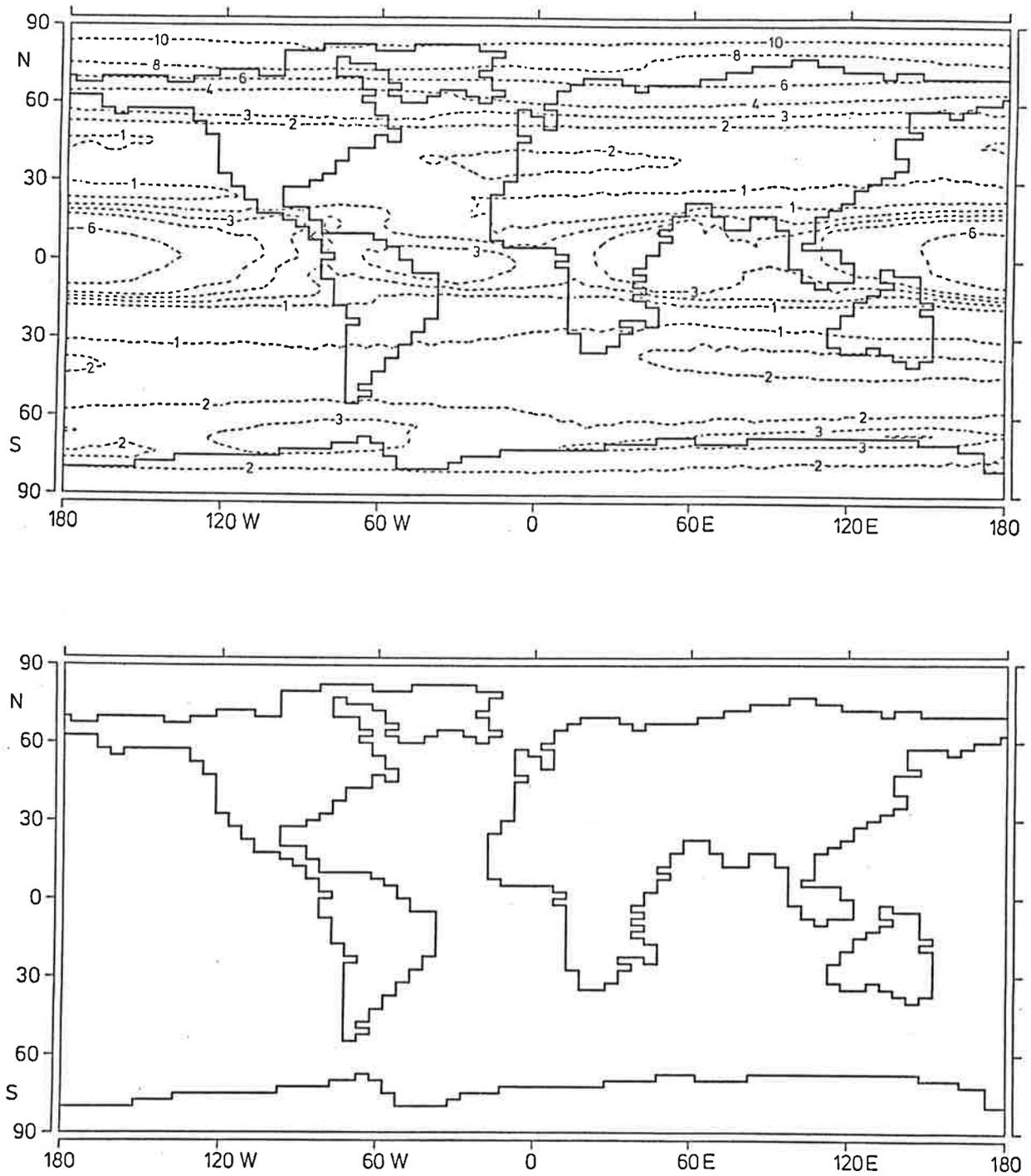


Figure 14: The temperature change in 100 years at 400 hPa, without flux correction (panel a) and with flux correction (panel b). (Isoline intervals are 1 K below 4 K, 2 K above 4 K. (The zero line is not plotted, negative isolines are dashed.)

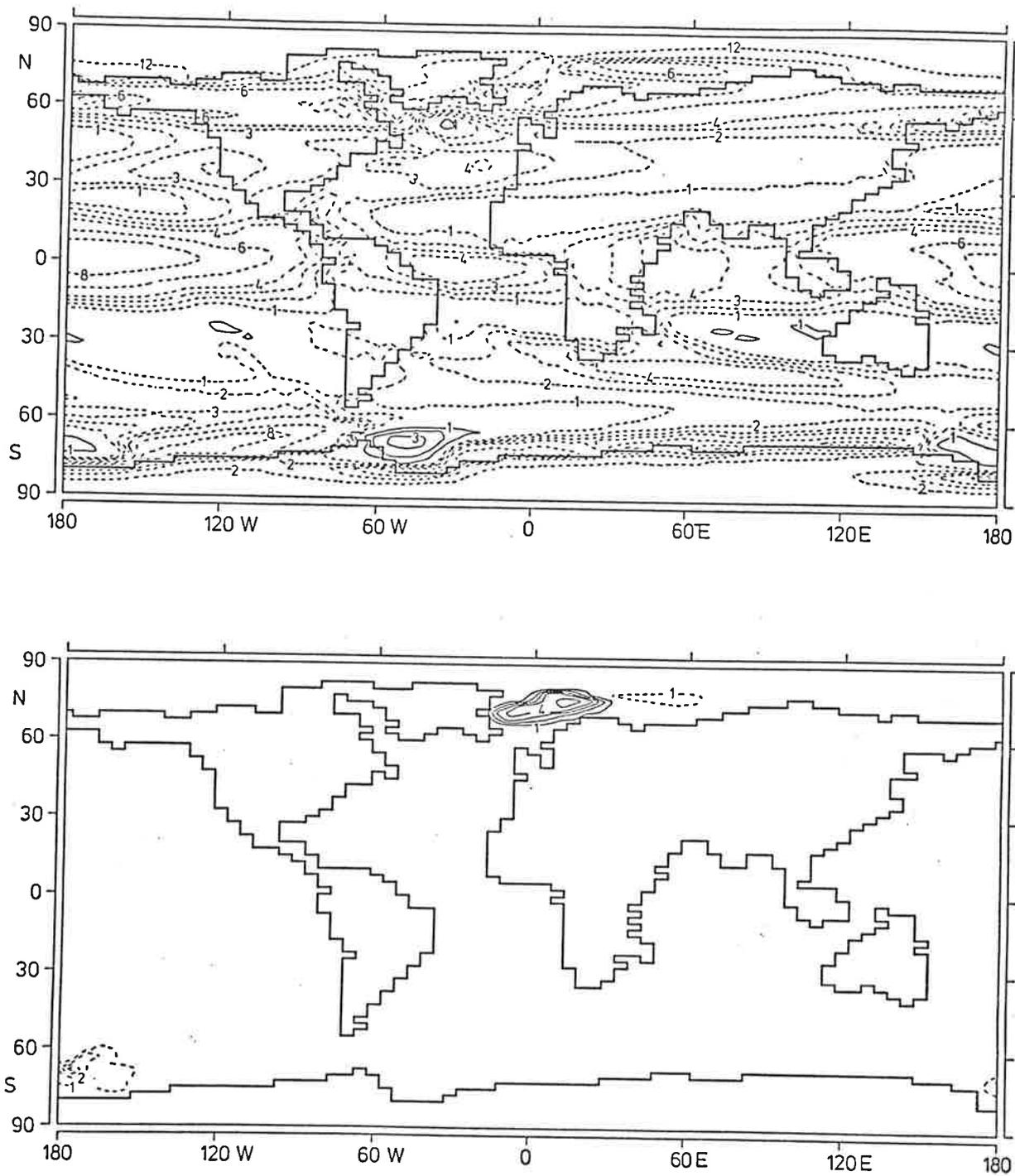


Figure 15: Same as Figure 14 for 800 hPa.

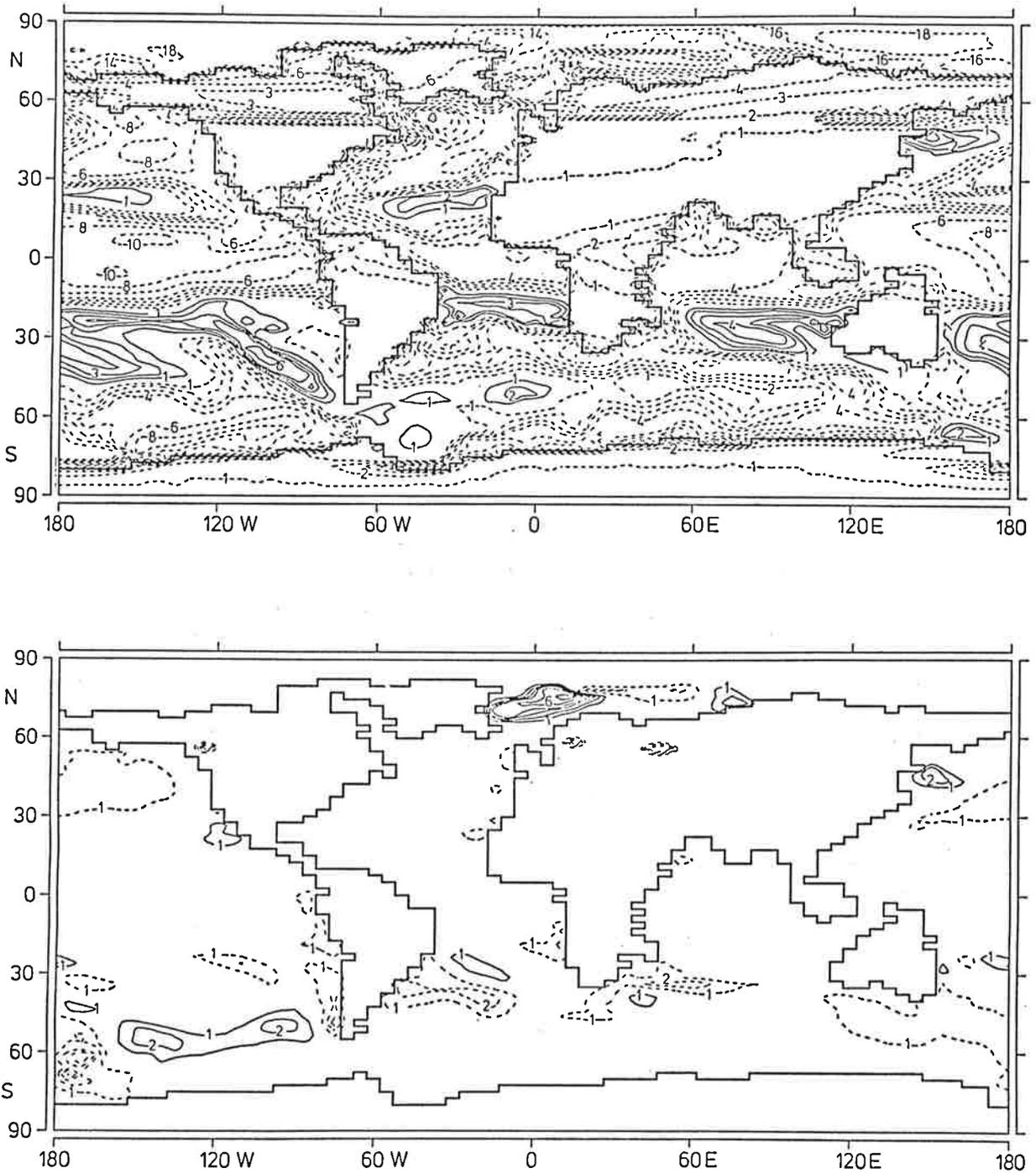


Figure 16: Same as Figure 14 for the surface

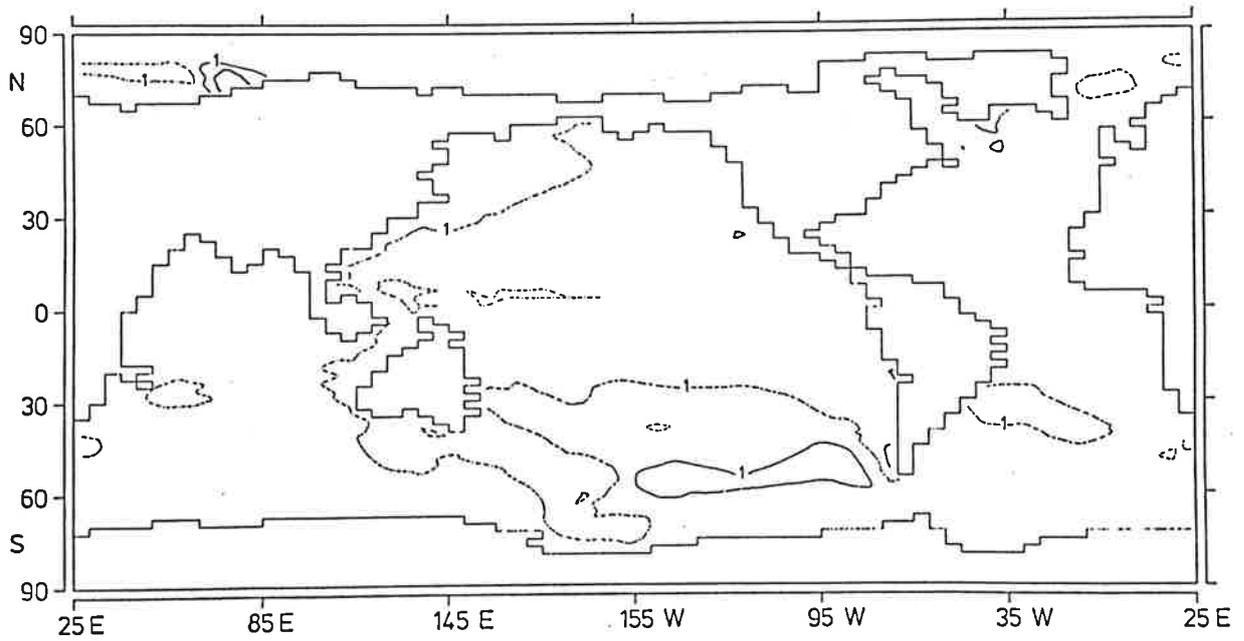
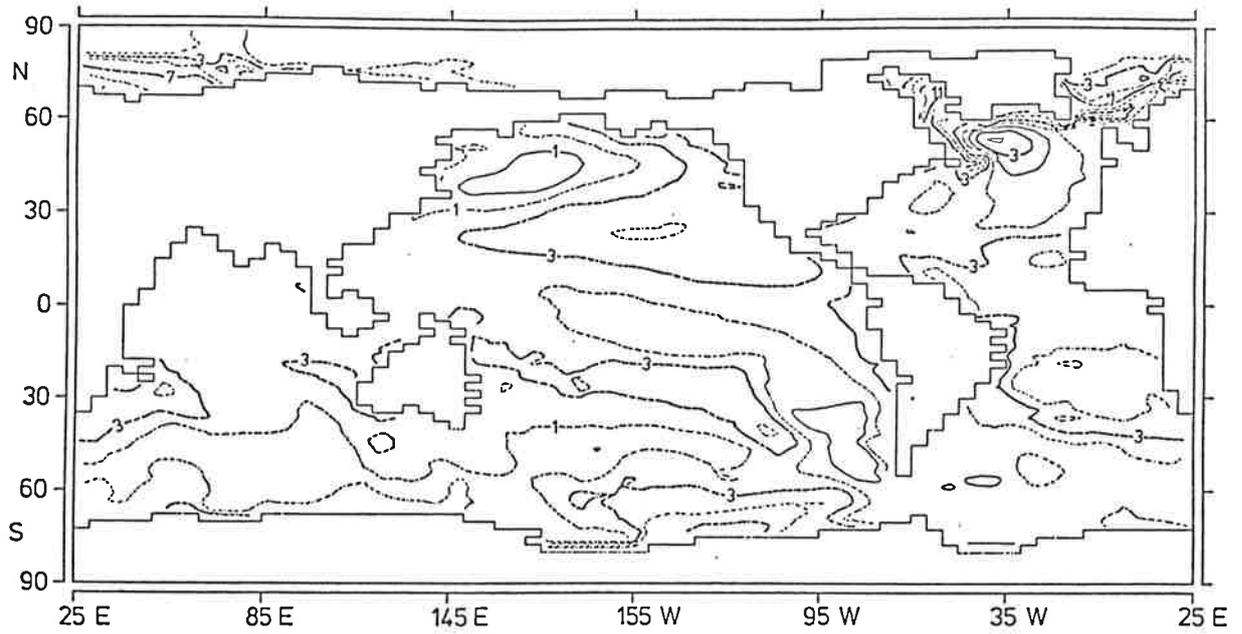


Figure 17: Temperature drift over 100 years at 300 m depth, without flux correction (panel a) and with flux correction (panel b). (Isoline intervals are 2 K, negative isolines are dashed.)

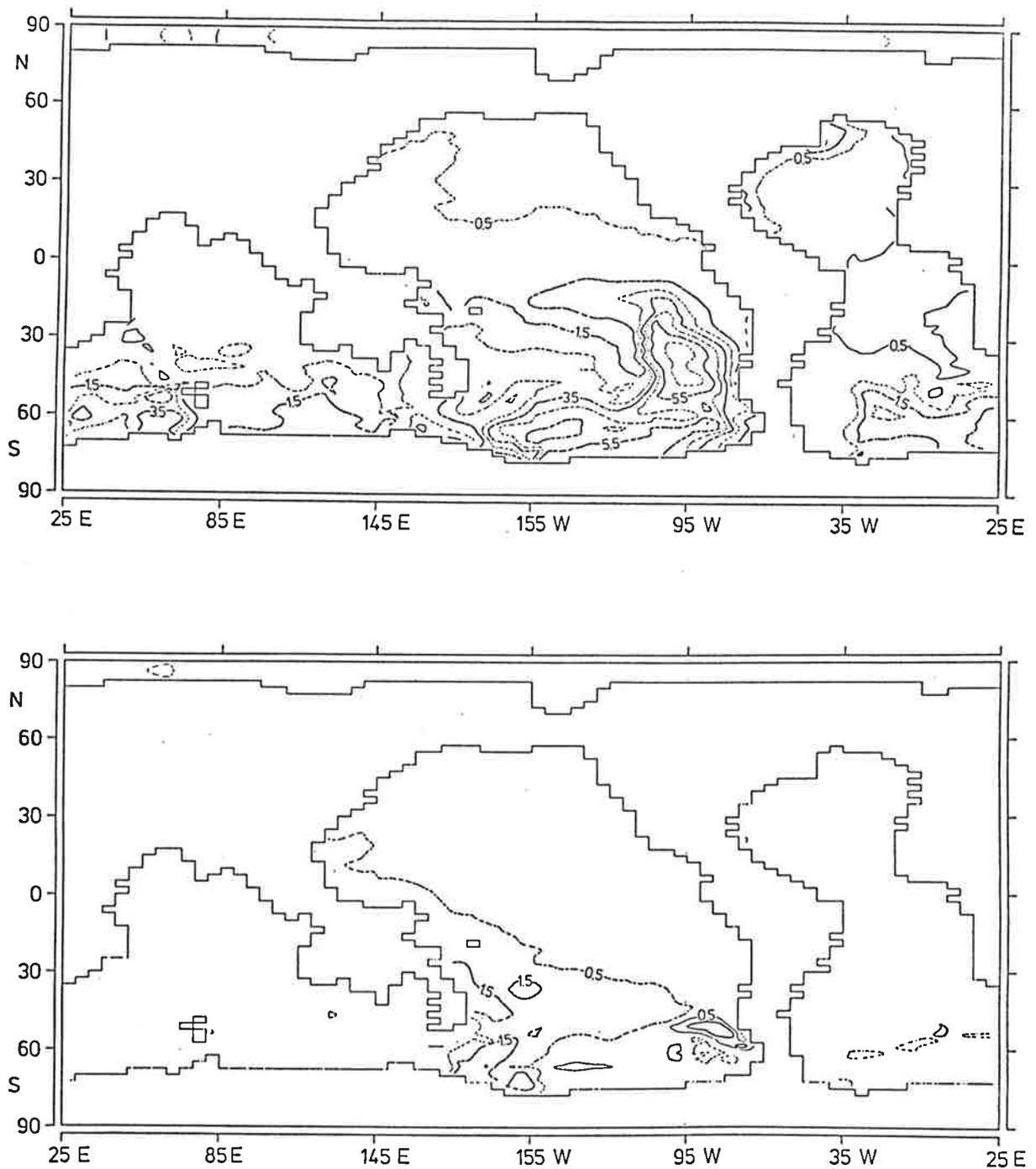


Figure 18: Same as Fig. 17 for 3000 m depth. (Isoline intervals 1 K).

Using a slightly modified oceanic model in which the intermittency in the parameterization of the convection was removed and the oceanic model was integrated in the uncoupled mode for 20000 years to an almost complete equilibrium, Sausen et al. (1987) were able to reduce the residual drift drastically. With the original model, the root mean square error of the atmospheric temperature of the level 2 (800 mb) after one hundred years is reduced from 5.09 K without flux correction to 0.47 K with flux correction. With the modified oceanic model, the residual flux corrected drift of the same level is reduced to 0.07 K. This residual drift of the order of 1% of the uncorrected drift may be attributed to the still remaining drift of the uncoupled oceanic model. For the modified ocean model, Fig. 19 shows the rms error of the oceanic temperature of the 3000 m level. While the drift of the uncorrected coupled run increases very rapidly (solid line) and achieves a value of 3.31 K after 100 years, the drift of the flux corrected coupled model stays rather close to the drift of the uncoupled model, independently from the temperature forcing of the uncoupled ocean. (Both a Newtonian forcing and a forcing by a prescribed heat flux have been used.)

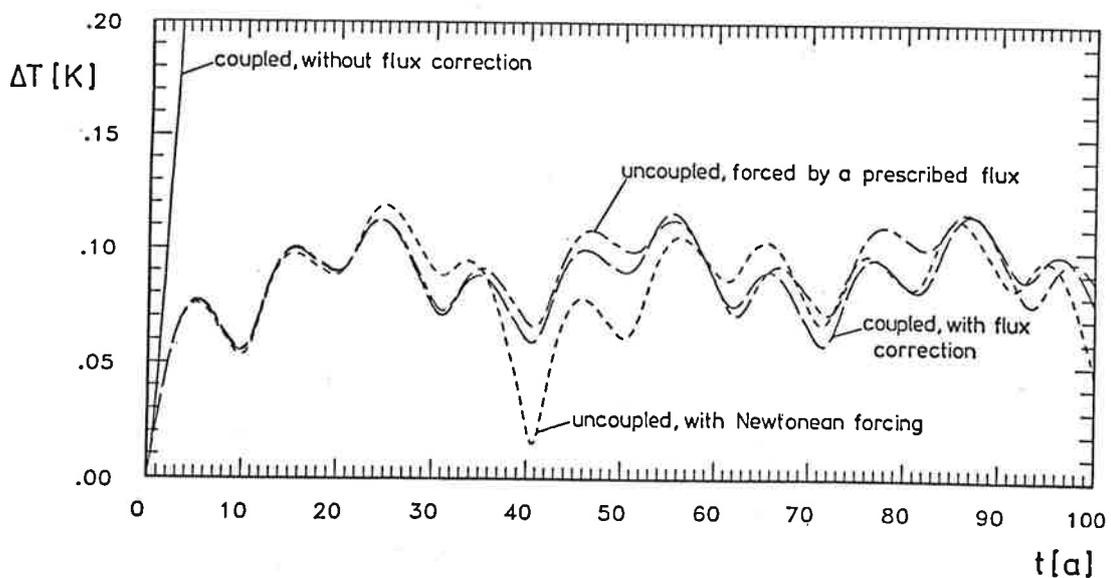


Figure 19: Temporal evolution of the drift (rms-error) of the oceanic temperature at 3000 m.

5. A climate response experiment.

To test the impact of the flux correction method in a climate response application, a "CO₂ experiment" was carried out in which the absorption coefficients for long wave radiation were slightly increased. The coupled model described in the last section was used (with the non-modified ocean model).

The differences in the response for the experiments with and without flux correction are plotted in Fig. 20. The differences in the response are evident, although the present coupled model does not include strongly nonlinear effects such as variable sea-ice, and is therefore less suitable than the simpler model discussed in section 3 for illustrating the distortions created in climate response experiments by an uncorrected climate drift .

Without flux correction the response patterns are generally more noisy and can be regarded as significant only for very large length scales. (The anomalous band structure evident over land between 50°N and 60°N in the non-flux corrected run is not significant. It results from the spatial discretization and the fact that a step function was used to describe the snow-albedo on land. The southern boundary of the snow happens to retreat just one grid point in the run without flux correction, while in the case with flux correction this occurred for only a few points.)

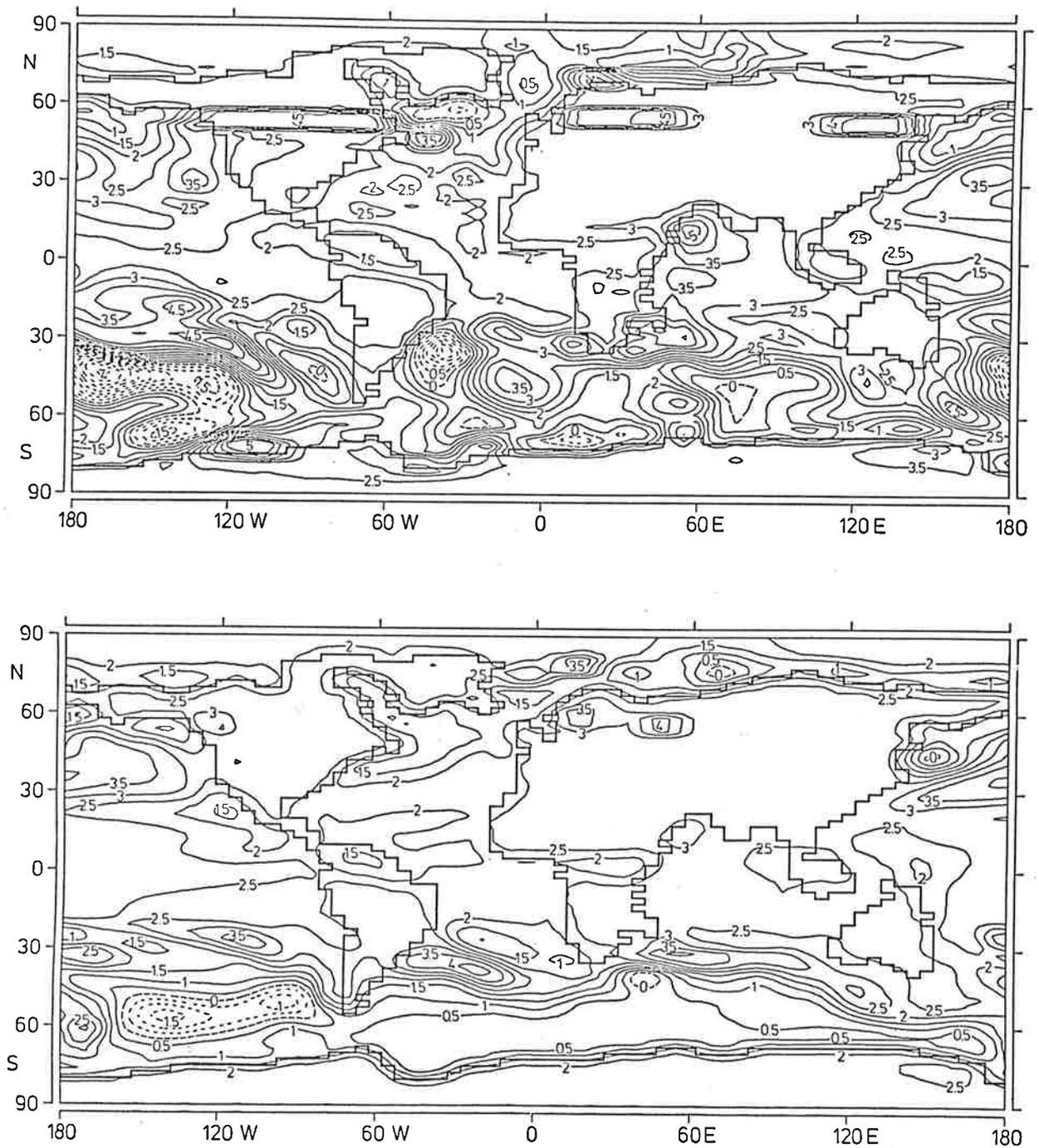


Figure 20: Changes of the surface temperatures after 100 years due to the increased long wave absorption, without flux correction (panel a) and with flux correction (panel b). Isoline intervals are 0.5 K below and 1 K above 5 K, negative isolines are dashed.

6. Conclusions

The flux correction method presented here has been shown to remove the drift in coupled atmosphere-ocean models successfully. The method has been demonstrated both for a simple nonlinear atmosphere-ocean model with two degrees of freedom and an OGCM coupled to a simple two level diagnostic model of the atmosphere.

The application of the method is basically straight forward and requires only diagnostic computations of the fluxes coupling the two sub-systems, using boundary values taken from observations or computed in uncoupled mode experiments.

The flux correction removes only the drift arising from the mean flux inconsistencies of the separate sub-systems. Stochastic flux variations associated with the internal variability of the sub-systems, which can also give rise to model drift, are not removed. However, these represent real physical processes rather than model deficiencies and should therefore in general be retained. Corresponding low frequency variations are observed also in the real climate system and must be similarly taken into account when interpreting the climate response to prescribed external variations.

Finally, we note that the flux correction method is useful not only as a technique for maintaining the coupled model at the "working point" for which the model sub-systems were designed, but also as a diagnostic tool. The flux correction fields show the structure of the mutual inconsistencies of the separate sub-systems, indicating where modifications in the separate sub-system are most needed.

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