Supporting Information for the manuscript

## Structure calculation from unambiguous long-range amide and methyl ${ }^{1} \mathrm{H}-\mathbf{- 1}^{\mathbf{H}} \mathrm{H}$ distance restraints for a micro-crystalline protein with MAS solid-state NMR spectroscopy

by

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Supplementary Figure 1. Sequential walk from a $3 \mathrm{D} N \cdot \mathrm{~N}, \mathrm{H}$ RFDR correlation experiment. The correlations are solely based on ${ }^{1} \mathrm{H}$ and ${ }^{15} \mathrm{~N}$ chemical shifts and can assist sequential assignments when ${ }^{13} \mathrm{C}$ based backbone experiments do not yield unambiguous assignments. In addition to sequential correlation (blue), non-sequential contacts (e.g. across the beta-strand) are observed (red). The 3D experiment was recorded within 4 h employing a RFDR mixing time of 8 ms , setting $t_{1}{ }^{\text {max }}\left({ }^{15} \mathrm{~N}\right)=20 \mathrm{~ms}$.


Supplementary Figure 2. Sequential walk for dynamic residues in the N-terminus (using the pulse scheme represented in Figure 1C of the main manuscript). The experiment confirms TROSY based assignments in the N-terminus of $\alpha$-spectrin SH3. ${ }^{1}$ The experiment was recorded in 4 h employing a RFDR mixing time of 8 ms .


Supplementary Figure 3. First increment of a time-shared 3D H••N/C,H correlation experiment (pulse scheme represented in Figure 1F of the main manuscript). The spectrum was recorded using 8 scans. The experimental time for each increment amounts to ca. 2 s . The CP transfer time was restricted to $1000 \mu$ s to suppress longrange ${ }^{1} \mathrm{H}^{\mathrm{N}} /{ }^{13} \mathrm{C}^{\alpha}$ transfers.


Supplementary Figure 4. Complementary time-shared 3D experiments with synchronous ${ }^{13} \mathrm{C}$ and ${ }^{15} \mathrm{~N}$ evolution periods (as in Figure 4 of the main manuscript, but displaying the full ${ }^{1} \mathrm{H}$ spectral window). Artifacts in B ) at ${ }^{1} \mathrm{H}$ chemical shifts of $4.6,3.5$, and 3.0 ppm are due to insufficient water suppression and $[\mathrm{Cu}(\mathrm{edta})]^{2-}$. Cross peaks at the water resonance frequency can be attributed to correlations between amide and exchanging hydroxyl protons which exchange rapidly with water. ${ }^{2}$


Supplementary Figure 5. Buildup of cross peak intensity for G28 as a function of the RFDR mixing time $\tau_{\text {mix }}$. Data was extracted from the $3 \mathrm{D} N \cdot \mathrm{~N}, \mathrm{H}$ spectra. Intensities found for different $\tau_{\text {mix }}$ are scaled with respect to the intensity of the diagonal peak of G28 in each case in order to correct for pulse imperfections during RFDR mixing. Neither $T_{1}$ decay in general nor differential $T_{1}$ decay during $\tau_{\text {mix }}$ is expected to be significant for these
short mixing times. ${ }^{3}$ Cross peak intensities reach a plateau at long mixing times due to spin diffusion. Data have been fit using a mono-exponential function in order to guide the eye and aid identification of suitable experimental mixing times. A quantitative analysis of the data is beyond the focus of the manuscript. In contrast, for our structure calculation we employed two independent spectra (with 3 and 8 ms mixing) with different upper distance values (see main manuscript for a description of the transformation from intensities to distances). This approach is in agreement with Zhou et al. ${ }^{4}$ and allows fast data acquisition.


Supplementary Figure 6. A) Correlation between the upper bound of the manually assigned distance restraints and the corresponding distances in the X-ray structure. The restraint upper bounds derived from the manual assignments and TALOS+ match the "real" (i. e. X-ray) distances reasonably well. Restraint upper bounds are obtained following the protocol described in "Structure calculation from unambiguous manual assignments" in the Experimental Section of the main manuscript. B) Correlation for the automated calculation. Restraints were obtained from ambiguous data, using only the proton chemical shift encoded $\mathrm{H} \cdot \mathrm{C} / \mathrm{N}, \mathrm{H}$ correlations. The data points represent the restraints obtained by ARIA in the final assignment iteration. Despite the poor correlation obtained in the iterative automated assignment, a very high correlation between X-ray and NMR structure is achieved in the later stage of the structure calculation procedure (backbone RMSD of $1.6 \AA$ ). "Restraint upper bounds" refers to the distance extracted from the cross peak intensities according to Eq. (1) and (2) in the main manuscript. Restraints containing a single assignment possibility at the end of the automated procedure (unambiguous) are shown in black, whereas restraints that remain ambiguous are in red. "X-ray distance" denotes the ${ }^{1} \mathrm{H},{ }^{1} \mathrm{H}$ distance in accordance with the cross peak assignment and can therefore differ in A ) and B ).


Supplementary Figure 7. Precision (A) and accuracy, i.e. deviation from the X-ray structure 2 NUZ , (B) as a function of residue. The red and black curves refer to the backbone and all atoms RMSD, respectively. Circles denote the residues for which methyl-amide distance restraints were available

## Simulated annealing protocols for structure calculation

All structure calculations were performed in $\mathrm{CNS}^{5}$ with the standard molecular dynamics simulated annealing (SA) protocols implemented in ARIA. ${ }^{6,7}$ Except for the number of molecular dynamics steps, all parameters were set to their default values. The lengths of the different SA stages used in the 3 calculations performed are listed in Supplementary Table 1. In each case, a randomized structure served as a starting conformation for the SA. For the calculation with dihedral angle restraints alone, only the SA stages in torsion angle space were accomplished. The calculation applying manually assigned unambiguous distance restraints corresponded to a single ARIA iteration. The automated calculation from ambiguous unassigned cross peaks was performed in ARIA 2.3, using 9 iterations (100 structures calculated per iteration).

The total computational times (using 20 processors) were: (i) 21 min for the calculation with TALOS+ derived restraints, (ii) 139 min for the unambiguous restraints and (iii) 175 min for the complete ARIA procedure from unassigned cross peaks.

Supplementary Table 1: Number of molecular dynamics steps in the simulated annealing protocol employed for the different calculations. As a result of the longer time-step employed in TAD (Torsion Angle Dynamics) $(27 \mathrm{fs})$, the effective length of the TAD phases is actually 9 x shorter. For the sake of consistency, the lengths of the different phases are here expressed in number of Cartesian MD steps.

| Type of MD | SA phase | TALOS+ <br> restraints only | manual | automated |
| :--- | :--- | ---: | ---: | ---: |
| Torsion | high Temp. | 20000 | 50000 | 20000 |
|  | cooling 1 | 100000 | 120000 | 50000 |
| Cartesian | cooling 1 | - | 120000 | 50000 |
|  | cooling 2 | - | 96000 | 40000 |

Supplementary Table 2: Distance values from distance restraints among amide protons and between amide and methyl protons in the structure calculation from unambiguous manual assignments.

| Residue 1 | Atom 1 | Residue 2 | Atom 2 | Upper distance <br> $(\AA)$ | X-ray <br> distance $(\AA)$ | Mixing <br> time (ms) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | HN | 33 | HN | 8.0 | 4.8 | 3 |
| 8 | HN | 61 | HN | 8.0 | 4.1 | 3 |
| 9 | HN | 8 | HN | 4.6 | 4.5 | 3 |
| 9 | HN | 9 | HG1\# | 3.3 | 3.0 | 3 |
| 9 | HN | 11 | HN | 7.0 | 6.2 | 3 |
| 9 | HN | 31 | HN | 8.0 | 3.0 | 3 |
| 9 | HN | 32 | HN | 8.0 | 5.0 | 3 |
| 10 | HN | 9 | HG2\# | 3.5 | 3.6 | 3 |
| 10 | HN | 10 | HD1\# | 3.8 | 4.3 | 3 |
| 10 | HN | 10 | HD2\# | 4.0 | 4.2 | 3 |
| 10 | HN | 29 | HN | 8.0 | 8.1 | 3 |
| 10 | HN | 30 | HD1\# | 8.0 | 4.5 | 3 |
| 10 | HN | 31 | HN | 8.0 | 4.9 | 3 |
| 10 | HN | 58 | HN | 8.0 | 6.9 | 3 |
| 10 | HN | 59 | HN | 8.0 | 2.6 | 3 |
| 10 | HN | 61 | HN | 8.0 | 4.4 | 3 |
| 11 | HN | 10 | HN | 4.5 | 4.5 | 3 |
| 11 | HN | 13 | HN | 6.7 | 5.7 | 3 |
| 11 | HN | 28 | HN | 8.0 | 3.8 | 3 |


| 11 | HN | 29 | HN | 8.0 | 3.7 | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11 | HN | 30 | HN | 8.0 | 5.0 | 3 |
| 11 | HN | 31 | HN | 8.0 | 4.2 | 3 |
| 11 | HN | 59 | HN | 8.0 | 5.0 | 3 |
| 12 | HN | 12 | HD2\# | 3.9 | 3.5 | 3 |
| 12 | HN | 13 | HN | 2.6 | 2.4 | 3 |
| 12 | HN | 28 | HN | 8.0 | 4.9 | 3 |
| 12 | HN | 57 | HN | 8.0 | 6.0 | 3 |
| 12 | HN | 58 | HG1\# | 8.0 | 3.4 | 3 |
| 12 | HN | 58 | HN | 8.0 | 4.6 | 3 |
| 12 | HN | 59 | HN | 8.0 | 4.3 | 3 |
| 13 | HN | 14 | HN | 4.6 | 4.4 | 3 |
| 13 | HN | 15 | HN | 7.9 | 6.2 | 3 |
| 13 | HN | 27 | HN | 8.0 | 5.4 | 3 |
| 13 | HN | 28 | HN | 8.0 | 4.9 | 3 |
| 13 | HN | 29 | HN | 8.0 | 6.4 | 3 |
| 13 | HN | 58 | HN | 8.0 | 6.0 | 3 |
| 14 | HN | 15 | HN | 4.6 | 4.6 | 3 |
| 14 | HN | 27 | HN | 8.0 | 3.3 | 3 |
| 15 | HN | 16 | HN | 4.7 | 4.0 | 3 |
| 15 | HN | 25 | HN | 8.0 | 2.9 | 3 |
| 15 | HN | 26 | HN | 8.0 | 5.0 | 3 |
| 15 | HN | 27 | HN | 8.0 | 4.7 | 3 |
| 16 | HN | 16 | HE21 | 6.7 | 6.6 | 3 |
| 16 | HN | 25 | HN | 8.0 | 5.0 | 3 |
| 17 | HN | 15 | HN | 7.4 | 6.1 | 3 |
| 17 | HN | 24 | HN | 8.0 | 4.1 | 3 |
| 17 | HN | 25 | HN | 8.0 | 4.7 | 3 |
| 18 | HN | 16 | HN | 7.7 | 6.5 | 3 |
| 18 | HN | 19 | HN | 4.6 | 2.0 | 3 |
| 18 | HN | 22 | HN | 8.0 | 4.8 | 3 |
| 19 | HN | 17 | HN | 7.9 | 5.9 | 3 |
| 19 | HN | 22 | HN | 8.0 | 3.5 | 3 |
| 19 | HN | 23 | HN | 8.0 | 6.0 | 3 |
| 19 | HN | 24 | HN | 8.0 | 7.8 | 3 |
| 22 | HN | 51 | HN | 8.0 | 7.9 | 3 |
| 22 | HN | 52 | HN | 8.0 | 4.3 | 3 |
| 23 | HN | 23 | HG1\# | 3.3 | 2.3 | 3 |
| 23 | HN | 24 | HN | 4.5 | 4.4 | 3 |
| 23 | HN | 25 | HN | 7.4 | 6.4 | 3 |
| 23 | HN | 44 | HN | 8.0 | 6.1 | 3 |
| 23 | HN | 51 | HN | 8.0 | 5.4 | 3 |
| 23 | HN | 52 | HN | 8.0 | 3.3 | 3 |
| 23 | HN | 53 | HN | 8.0 | 4.9 | 3 |
| 24 | HN | 25 | HN | 4.6 | 4.5 | 3 |
| 25 | HN | 14 | HN | 8.0 | 7.4 | 3 |
| 25 | HN | 24 | HG2\# | 3.6 | 2.5 | 3 |
| 25 | HN | 26 | HN | 4.6 | 4.4 | 3 |


| 25 | HN | 27 | HN | 7.8 | 6.6 | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | HN | 13 | HN | 8.0 | 7.5 | 3 |
| 26 | HN | 24 | HG2\# | 5.7 | 4.5 | 3 |
| 26 | HN | 29 | HN | 8.0 | 4.3 | 3 |
| 27 | HN | 29 | HN | 8.0 | 4.7 | 3 |
| 28 | HN | 14 | HN | 8.0 | 6.3 | 3 |
| 30 | HN | 31 | HN | 4.6 | 4.3 | 3 |
| 31 | HN | 9 | HG1\# | 8.0 | 5.0 | 3 |
| 31 | HN | 29 | HN | 7.6 | 6.6 | 3 |
| 31 | HN | 30 | HD1\# | 4.7 | 3.9 | 3 |
| 31 | HN | 30 | HG2\# | 3.5 | 3.0 | 3 |
| 31 | HN | 32 | HN | 4.6 | 4.5 | 3 |
| 31 | HN | 33 | HN | 7.5 | 6.2 | 3 |
| 32 | HN | 11 | HN | 8.0 | 8.4 | 3 |
| 32 | HN | 44 | HN | 8.0 | 7.4 | 3 |
| 32 | HN | 45 | HN | 8.0 | 3.1 | 3 |
| 32 | HN | 46 | HN | 8.0 | 5.2 | 3 |
| 33 | HN | 32 | HG2\# | 3.6 | 2.7 | 3 |
| 33 | HN | 32 | HN | 4.6 | 4.5 | 3 |
| 33 | HN | 34 | HD1\# | 6.2 | 6.3 | 3 |
| 34 | HN | 7 | HN | 8.0 | 7.8 | 3 |
| 34 | HN | 8 | HN | 8.0 | 8.9 | 3 |
| 34 | HN | 34 | HD1\# | 3.7 | 3.8 | 3 |
| 34 | HN | 34 | HD2\# | 3.9 | 3.6 | 3 |
| 34 | HN | 42 | HN | 8.0 | 7.9 | 3 |
| 34 | HN | 44 | HN | 8.0 | 4.6 | 3 |
| 35 | HN | 42 | HN | 8.0 | 7.2 | 3 |
| 35 | HN | 43 | HN | 8.0 | 3.1 | 3 |
| 35 | HN | 44 | HN | 8.0 | 5.2 | 3 |
| 38 | HD21 | 39 | HN | 6.2 | 4.1 | 3 |
| 38 | HD21 | 40 | HN | 7.2 | 4.7 | 3 |
| 38 | HD21 | 41 | HN | 7.6 | 5.0 | 3 |
| 38 | HD21 | 42 | HE1 | 8.0 | 7.7 | 3 |
| 38 | HD21 | 42 | HN | 8.0 | 8.4 | 3 |
| 39 | HN | 40 | HN | 2.6 | 2.5 | 3 |
| 39 | HN | 42 | HE1 | 8.0 | 5.1 | 3 |
| 40 | HN | 41 | HN | 2.7 | 2.3 | 3 |
| 40 | HN | 42 | HE1 | 8.0 | 5.0 | 3 |
| 40 | HN | 42 | HN | 7.0 | 6.3 | 3 |
| 41 | HE1 | 42 | HN | 7.7 | 7.5 | 3 |
| 41 | HN | 42 | HE1 | 8.0 | 4.9 | 3 |
| 41 | HN | 42 | HN | 4.5 | 4.2 | 3 |
| 41 | HN | 55 | HN | 8.0 | 4.2 | 3 |
| 41 | HN | 56 | HN | 8.0 | 6.5 | 3 |
| 42 | HE1 | 35 | HN | 8.0 | 7.8 | 3 |
| 42 | HN | 53 | HN | 8.0 | 3.1 | 3 |
| 42 | HN | 55 | HN | 8.0 | 3.4 | 3 |
| 43 | HN | 42 | HN | 4.5 | 4.5 | 3 |


| 43 | HN | 44 | HN | 4.6 | 4.5 | 3 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 44 | HN | 34 | HD1\# | 8.0 | 3.6 | 3 |
| 44 | HN | 50 | HN | 8.0 | 7.1 | 3 |
| 44 | HN | 51 | HN | 8.0 | 2.7 | 3 |
| 44 | HN | 52 | HN | 8.0 | 4.9 | 3 |
| 44 | HN | 53 | HN | 8.0 | 4.3 | 3 |
| 45 | HN | 44 | HG1\# | 3.3 | 3.6 | 3 |
| 45 | HN | 44 | HN | 4.5 | 4.4 | 3 |
| 46 | HN | 44 | HN | 7.3 | 6.1 | 3 |
| 46 | HN | 49 | HN | 8.0 | 3.4 | 3 |
| 46 | HN | 50 | HE22 | 8.0 | 7.6 | 3 |
| 46 | HN | 50 | HN | 8.0 | 4.9 | 3 |
| 46 | HN | 52 | HN | 8.0 | 8.7 | 3 |
| 49 | HN | 47 | HD22 | 8.0 | 7.2 | 3 |
| 49 | HN | 50 | HE22 | 8.0 | 7.8 | 3 |
| 49 | HN | 50 | HN | 4.7 | 4.4 | 3 |
| 49 | HN | 51 | HN | 7.9 | 7.0 | 3 |
| 50 | HE21 | 50 | HE22 | 1.7 | 1.7 | 3 |
| 50 | HN | 50 | HE22 | 7.4 | 6.5 | 3 |
| 50 | HN | 51 | HN | 4.6 | 4.4 | 3 |
| 51 | HN | 23 | HG1\# | 8.0 | 3.0 | 3 |
| 51 | HN | 34 | HD1\# | 8.0 | 3.6 | 3 |
| 51 | HN | 46 | HN | 8.0 | 4.9 | 3 |
| 51 | HN | 52 | HN | 4.6 | 4.3 | 3 |
| 51 | HN | 53 | HN | 7.9 | 6.0 | 3 |
| 52 | HN | 53 | HN | 4.6 | 4.5 | 3 |
| 53 | HN | 53 | HG1\# | 3.3 | 2.9 | 3 |
| 55 | HN | 40 | HN | 8.0 | 5.5 | 3 |
| 55 | HN | 42 | HE1 | 8.0 | 5.8 | 3 |
| 55 | HN | 43 | HN | 8.0 | 7.7 | 3 |
| 55 | HN | 56 | HN | 2.9 | 2.8 | 3 |
| 56 | HN | 57 | HN | 2.8 | 2.7 | 3 |
| 57 | HN | 42 | HN | 8.0 | 6.5 | 3 |
| 58 | HN | 56 | HN | 7.2 | 4.4 | 3 |
| 58 | HN | 58 | HG\# | 2.1 | 2.3 | 3 |
| 58 | HN | 59 | HN | 4.6 | 4.4 | 3 |
| 59 | HN | 12 | HD2\# | 8.0 | 3.9 | 3 |
| 59 | HN | 13 | HN | 8.0 | 6.6 | 3 |
| 59 | HN | 31 | HN | 8.0 | 6.6 | 3 |
| 59 | HN | 60 | HN | 4.6 | 4.2 | 3 |
| 59 | HN | 61 | HN | 7.8 | 6.2 | 3 |
| 60 | HN | 10 | HN | 8.0 | 4.8 | 3 |
| 60 | HN | 61 | HN | 4.6 | 4.6 | 3 |
| 61 | HN | 9 | HG2\# | 8.0 | 5.3 | 3 |
| 61 | HN | 9 | HN | 8.0 | 4.9 | 3 |
| 61 | HN | 10 | HD1\# | 8.0 | 7.3 | 3 |
| 61 | HN | 10 | HD2\# | 8.0 | 6.8 | 3 |
| 61 | HN | 61 | HD1\# | 4.0 | 3.9 | 3 |


| 7 | HN | 33 | HN | 12.0 | 4.9 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 | HN | 60 | HN | 12.0 | 8.2 | 8 |
| 9 | HN | 9 | HG2\# | 3.4 | 2.3 | 8 |
| 9 | HN | 12 | HN | 10.3 | 9.1 | 8 |
| 9 | HN | 30 | HN | 12.0 | 7.0 | 8 |
| 9 | HG1\# | 59 | HN | 12.0 | 4.2 | 8 |
| 9 | HG2\# | 60 | HN | 12.0 | 5.5 | 8 |
| 11 | HN | 10 | HD2\# | 4.5 | 4.7 | 8 |
| 11 | HB\# | 12 | HN | 3.0 | 3.2 | 8 |
| 11 | HN | 30 | HD1\# | 12.0 | 3.8 | 8 |
| 11 | HN | 58 | HN | 12.0 | 7.7 | 8 |
| 11 | HN | 61 | HN | 12.0 | 8.7 | 8 |
| 12 | HN | 10 | HD2\# | 6.3 | 5.1 | 8 |
| 12 | HN | 12 | HD1\# | 3.7 | 3.6 | 8 |
| 12 | HN | 58 | HG2\# | 12.0 | 5.2 | 8 |
| 12 | HD1\# | 59 | HN | 12.0 | 4.0 | 8 |
| 13 | HN | 11 | HB\# | 3.9 | 3.2 | 8 |
| 13 | HN | 12 | HD2\# | 4.2 | 4.7 | 8 |
| 13 | HN | 25 | HN | 12.0 | 8.0 | 8 |
| 13 | HN | 57 | HN | 12.0 | 6.5 | 8 |
| 14 | HN | 16 | HN | 7.6 | 7.2 | 8 |
| 14 | HN | 24 | HG2\# | 12.0 | 7.3 | 8 |
| 15 | HN | 16 | HE21 | 9.5 | 9.2 | 8 |
| 15 | HN | 24 | HG2\# | 12.0 | 3.7 | 8 |
| 15 | HN | 53 | HG2\# | 12.0 | 6.9 | 8 |
| 16 | HE21 | 16 | HE22 | 1.7 | 1.7 | 8 |
| 17 | HN | 16 | HE22 | 8.0 | 6.3 | 8 |
| 17 | HN | 52 | HN | 12.0 | 8.7 | 8 |
| 18 | HN | 24 | HG2\# | 12.0 | 7.1 | 8 |
| 22 | HN | 25 | HN | 11.1 | 10.3 | 8 |
| 23 | HN | 23 | HG2\# | 3.4 | 3.9 | 8 |
| 23 | HG1\# | 46 | HN | 12.0 | 4.1 | 8 |
| 23 | HG2\# | 46 | HN | 12.0 | 3.5 | 8 |
| 24 | HG2\# | 16 | HN | 12.0 | 4.3 | 8 |
| 24 | HN | 23 | HG2\# | 3.6 | 2.1 | 8 |
| 24 | HN | 24 | HG2\# | 3.4 | 3.7 | 8 |
| 25 | HE\# | 13 | HN | 12.0 | 3.1 | 8 |
| 25 | HE\# | 25 | HN | 5.1 | 4.4 | 8 |
| 25 | HE\# | 26 | HN | 5.3 | 5.5 | 8 |
| 25 | HE\# | 58 | HN | 12.0 | 4.3 | 8 |
| 26 | HN | 11 | HB\# | 12.0 | 3.9 | 8 |
| 26 | HN | 14 | HN | 12.0 | 7.1 | 8 |
| 26 | HN | 16 | HN | 12.0 | 8.6 | 8 |
| 26 | HN | 30 | HD1\# | 11.6 | 8.2 | 8 |
| 26 | HN | 31 | HN | 12.0 | 8.3 | 8 |
| 26 | HN | 49 | HN | 12.0 | 10.5 | 8 |
| 26 | HN | 53 | HG1\# | 12.0 | 6.4 | 8 |
| 27 | HN | 11 | HB\# | 12.0 | 4.1 | 8 |


| 28 | HN | 10 | HD2\# | 12.0 | 4.8 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 28 | HN | 26 | HN | 7.1 | 6.2 | 8 |
| 28 | HN | 30 | HN | 7.8 | 6.6 | 8 |
| 29 | HN | 11 | HB\# | 12.0 | 2.3 | 8 |
| 29 | HN | 25 | HN | 12.0 | 8.1 | 8 |
| 29 | HN | 30 | HD1\# | 6.0 | 5.1 | 8 |
| 31 | HN | 8 | HN | 12.0 | 7.2 | 8 |
| 32 | HN | 8 | HN | 12.0 | 7.8 | 8 |
| 32 | HG2\# | 32 | HN | 3.2 | 3.7 | 8 |
| 32 | HN | 47 | HD21 | 12.0 | 8.1 | 8 |
| 33 | HD1\# | 8 | HN | 12.0 | 6.9 | 8 |
| 33 | HN | 9 | HG1\# | 12.0 | 4.0 | 8 |
| 33 | HD2\# | 34 | HN | 4.6 | 4.6 | 8 |
| 33 | HN | 35 | HN | 6.6 | 6.3 | 8 |
| 33 | HN | 44 | HN | 12.0 | 7.9 | 8 |
| 34 | HN | 35 | HN | 2.9 | 2.2 | 8 |
| 34 | HD2\# | 43 | HN | 12.0 | 6.8 | 8 |
| 34 | HN | 44 | HG2\# | 12.0 | 5.1 | 8 |
| 34 | HN | 49 | HN | 12.0 | 11.1 | 8 |
| 35 | HN | 32 | HN | 9.7 | 8.7 | 8 |
| 35 | HN | 33 | HD2\# | 5.9 | 4.6 | 8 |
| 38 | HD21 | 41 | HE1 | 11.8 | 7.9 | 8 |
| 40 | HN | 41 | HE1 | 9.7 | 6.3 | 8 |
| 41 | HN | 41 | HE1 | 7.5 | 5.6 | 8 |
| 41 | HN | 43 | HN | 7.5 | 6.7 | 8 |
| 41 | HN | 53 | HN | 12.0 | 6.9 | 8 |
| 41 | HE1 | 55 | HN | 12.0 | 6.5 | 8 |
| 42 | HE1 | 33 | HD1\# | 12.0 | 5.2 | 8 |
| 42 | HE1 | 35 | HD21 | 12.0 | 10.1 | 8 |
| 42 | HE1 | 43 | HN | 7.8 | 6.5 | 8 |
| 42 | HN | 44 | HG2\# | 7.6 | 5.4 | 8 |
| 42 | HN | 53 | HG1\# | 12.0 | 5.3 | 8 |
| 42 | HE1 | 56 | HN | 12.0 | 7.0 | 8 |
| 42 | HN | 56 | HN | 12.0 | 6.0 | 8 |
| 43 | HN | 33 | HD2\# | 12.0 | 5.9 | 8 |
| 44 | HG2\# | 43 | HN | 5.5 | 5.3 | 8 |
| 44 | HN | 44 | HG2\# | 3.3 | 2.3 | 8 |
| 44 | HN | 53 | HG1\# | 12.0 | 4.4 | 8 |
| 45 | HN | 35 | HN | 12.0 | 6.4 | 8 |
| 45 | HN | 50 | HE22 | 12.0 | 7.1 | 8 |
| 45 | HN | 52 | HN | 12.0 | 8.9 | 8 |
| 46 | HN | 23 | HN | 12.0 | 8.0 | 8 |
| 47 | HD21 | 47 | HD22 | 1.7 | 1.7 | 8 |
| 49 | HN | 47 | HD21 | 9.4 | 6.1 | 8 |
| 50 | HN | 50 | HE21 | 7.0 | 5.6 | 8 |
| 51 | HN | 23 | HG2\# | 12.0 | 4.0 | 8 |
| 51 | HN | 24 | HN | 12.0 | 7.3 | 8 |
| 51 | HN | 50 | HE22 | 7.9 | 7.3 | 8 |


| 51 | HN | 53 | HG2\# | 7.3 | 6.0 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 52 | HN | 19 | HN | 12.0 | 7.2 | 8 |
| 52 | HN | 23 | HG1\# | 12.0 | 3.6 | 8 |
| 52 | HN | 24 | HN | 12.0 | 7.3 | 8 |
| 52 | HN | 50 | HN | 7.8 | 7.4 | 8 |
| 53 | HN | 22 | HN | 12.0 | 8.0 | 8 |
| 53 | HG2\# | 23 | HN | 12.0 | 5.2 | 8 |
| 53 | HG2\# | 42 | HE1 | 12.0 | 7.3 | 8 |
| 53 | HN | 42 | HE1 | 12.0 | 8.6 | 8 |
| 53 | HG2\# | 43 | HN | 12.0 | 5.4 | 8 |
| 53 | HG1\# | 52 | HN | 5.8 | 4.6 | 8 |
| 53 | HN | 53 | HG2\# | 3.3 | 2.3 | 8 |
| 55 | HN | 25 | HE\# | 12.0 | 6.5 | 8 |
| 55 | HB\# | 42 | HE1 | 12.0 | 3.0 | 8 |
| 55 | HB\# | 56 | HN | 2.6 | 2.6 | 8 |
| 56 | HN | 53 | HN | 9.1 | 8.0 | 8 |
| 56 | HN | 56 | HB\# | 2.0 | 2.2 | 8 |
| 56 | HB\# | 57 | HN | 2.8 | 3.0 | 8 |
| 56 | HN | 58 | HG2\# | 7.1 | 4.9 | 8 |
| 56 | HN | 59 | HN | 10.2 | 8.7 | 8 |
| 57 | HN | 53 | HN | 9.1 | 7.6 | 8 |
| 57 | HN | 58 | HG2\# | 5.7 | 3.9 | 8 |
| 57 | HN | 59 | HN | 7.9 | 6.9 | 8 |
| 58 | HN | 9 | HN | 12.0 | 9.4 | 8 |
| 58 | HG1\# | 11 | HN | 12.0 | 4.3 | 8 |
| 58 | HN | 12 | HD1\# | 12.0 | 3.7 | 8 |
| 58 | HN | 42 | HE1 | 12.0 | 8.5 | 8 |
| 58 | HG1\# | 58 | HN | 3.3 | 3.0 | 8 |
| 58 | HN | 58 | HG2\# | 3.3 | 2.4 | 8 |
| 58 | HG2\# | 59 | HN | 3.6 | 3.3 | 8 |
| 58 | HN | 60 | HN | 7.5 | 6.3 | 8 |
| 59 | HN | 9 | HG2\# | 12.0 | 4.0 | 8 |
| 59 | HN | 11 | HB\# | 12.0 | 5.4 | 8 |
| 61 | HN | 9 | HG1\# | 12.0 | 3.5 | 8 |
| 61 | HN | 31 | HN | 12.0 | 7.3 | 8 |

Supplementary Table 3: Torsion angle restraints obtained from TALOS $+^{8}$.

| Residue | Phi | Phi error | Psi | Psi error |
| :---: | :---: | :---: | :---: | :---: |
| 6 | -124 | 35 | 157 | 25 |
| 7 | -140 | 52 | 154 | 43 |
| 8 | -119 | 47 | 147 | 26 |
| 9 | -138 | 21 | 160 | 15 |
| 10 | -118 | 27 | 123 | 18 |
| 11 | -81 | 12 | 123 | 23 |
| 12 | -95 | 14 | -44 | 10 |


| 13 | -144 | 59 | 162 | 17 |
| :---: | :---: | :---: | :---: | :---: |
| 16 | -121 | 34 | 124 | 21 |
| 17 | -94 | 40 | 134 | 46 |
| 23 | -146 | 36 | 158 | 26 |
| 24 | -119 | 33 | 141 | 32 |
| 25 | -128 | 39 | 132 | 23 |
| 26 | -121 | 55 | 139 | 51 |
| 27 | -62 | 29 | 130 | 16 |
| 30 | -97 | 37 | 116 | 42 |
| 31 | -93 | 27 | 129 | 20 |
| 32 | -98 | 21 | 125 | 24 |
| 34 | -96 | 33 | -36 | 25 |
| 38 | -99 | 69 | 150 | 44 |
| 39 | -65 | 31 | -30 | 17 |
| 40 | -99 | 32 | -16 | 30 |
| 41 | -133 | 29 | 135 | 37 |
| 42 | -123 | 27 | 137 | 41 |
| 43 | -110 | 33 | 131 | 24 |
| 44 | -131 | 16 | 158 | 18 |
| 45 | -130 | 29 | 135 | 23 |
| 46 | -102 | 54 | 133 | 30 |
| 50 | -128 | 47 | 154 | 26 |
| 52 | -112 | 50 | 152 | 32 |
| 55 | -57 | 13 | -35 | 12 |
| 56 | -68 | 15 | -14 | 14 |
| 58 | -130 | 33 | 158 | 24 |
| 59 | -124 | 42 | 132 | 26 |
| 61 | -106 | 63 | 109 | 37 |

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