

The crystalline structure of metals: why does it matter for crystal plasticity?

Professor Dierk Raabe

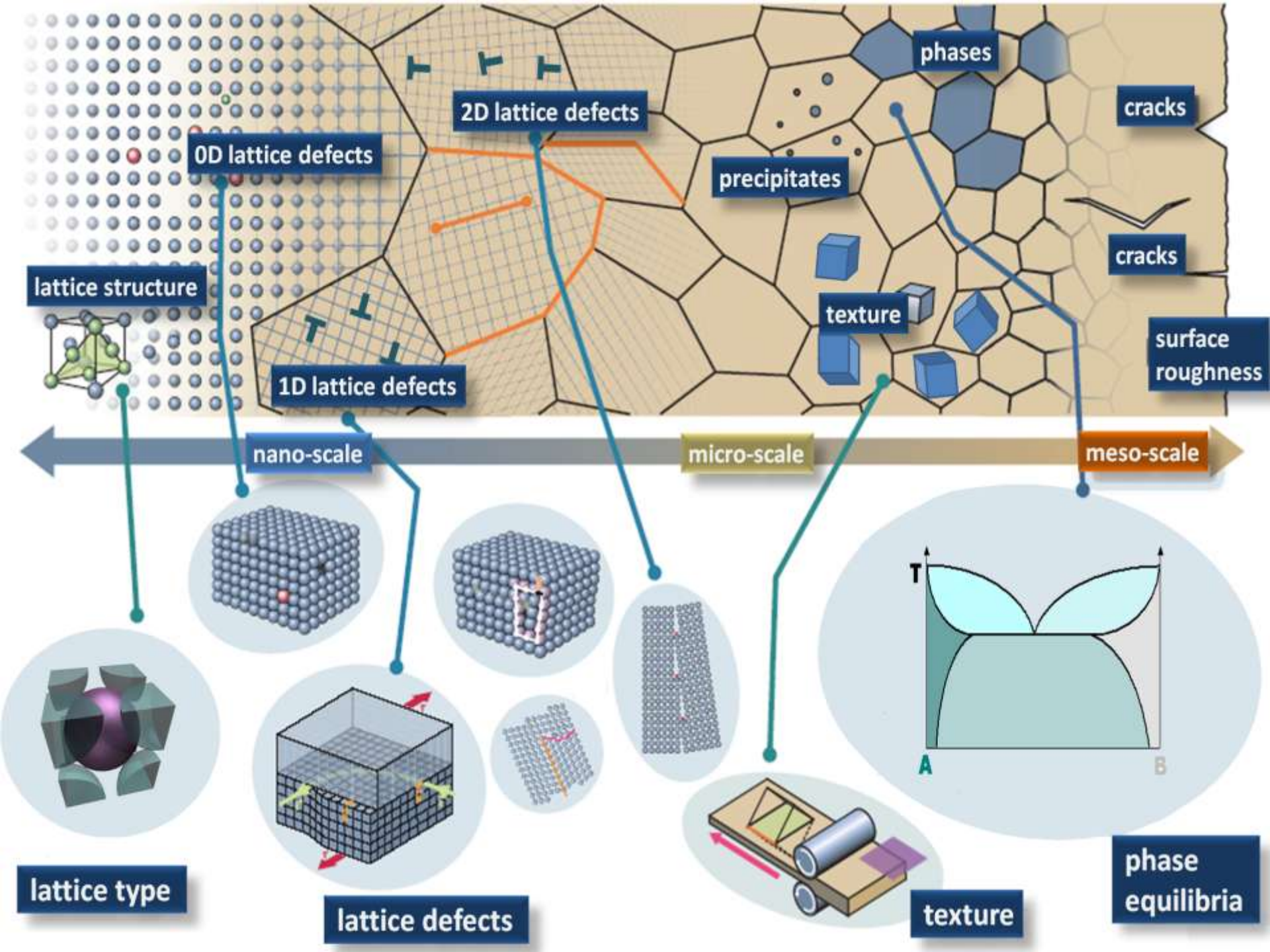


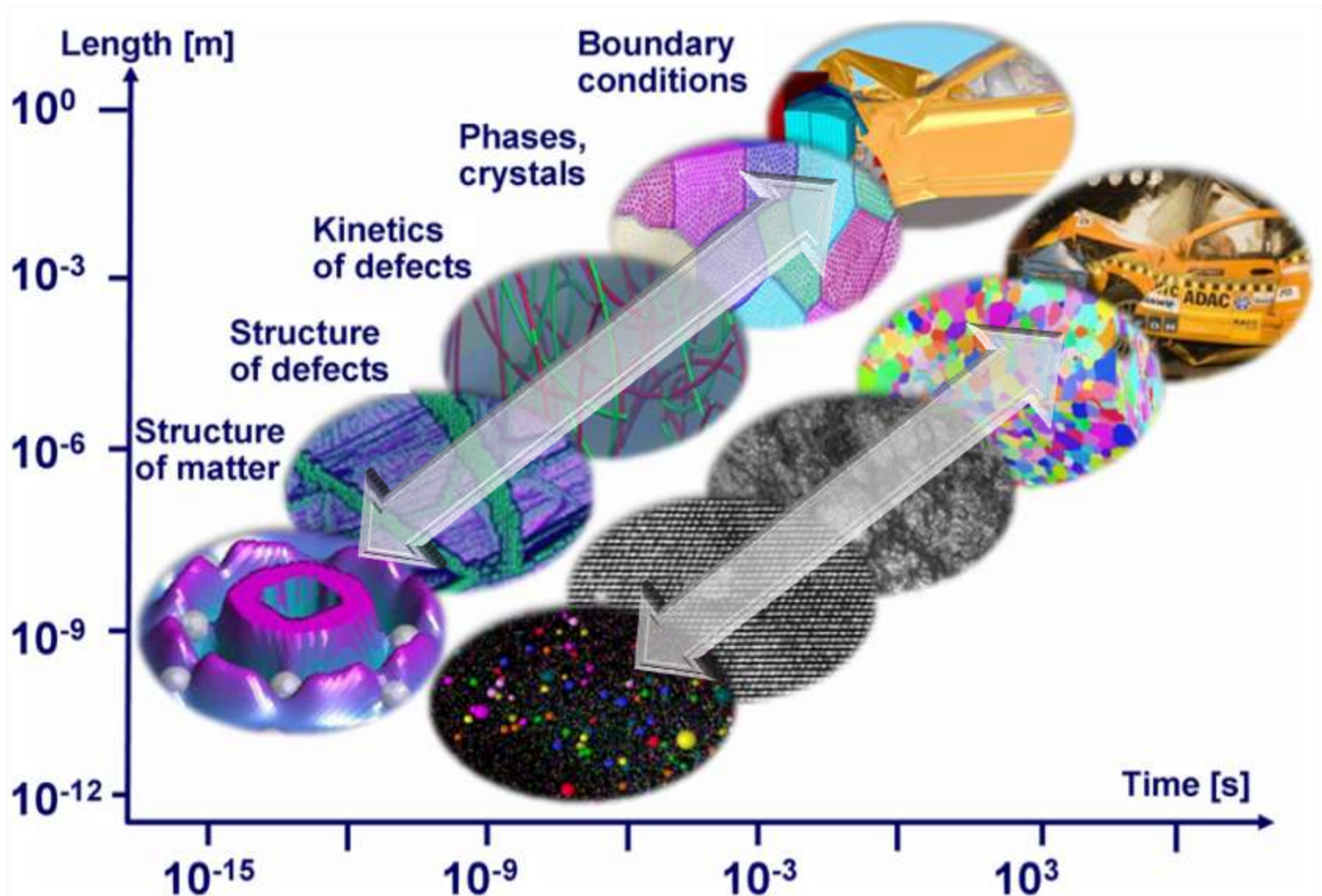
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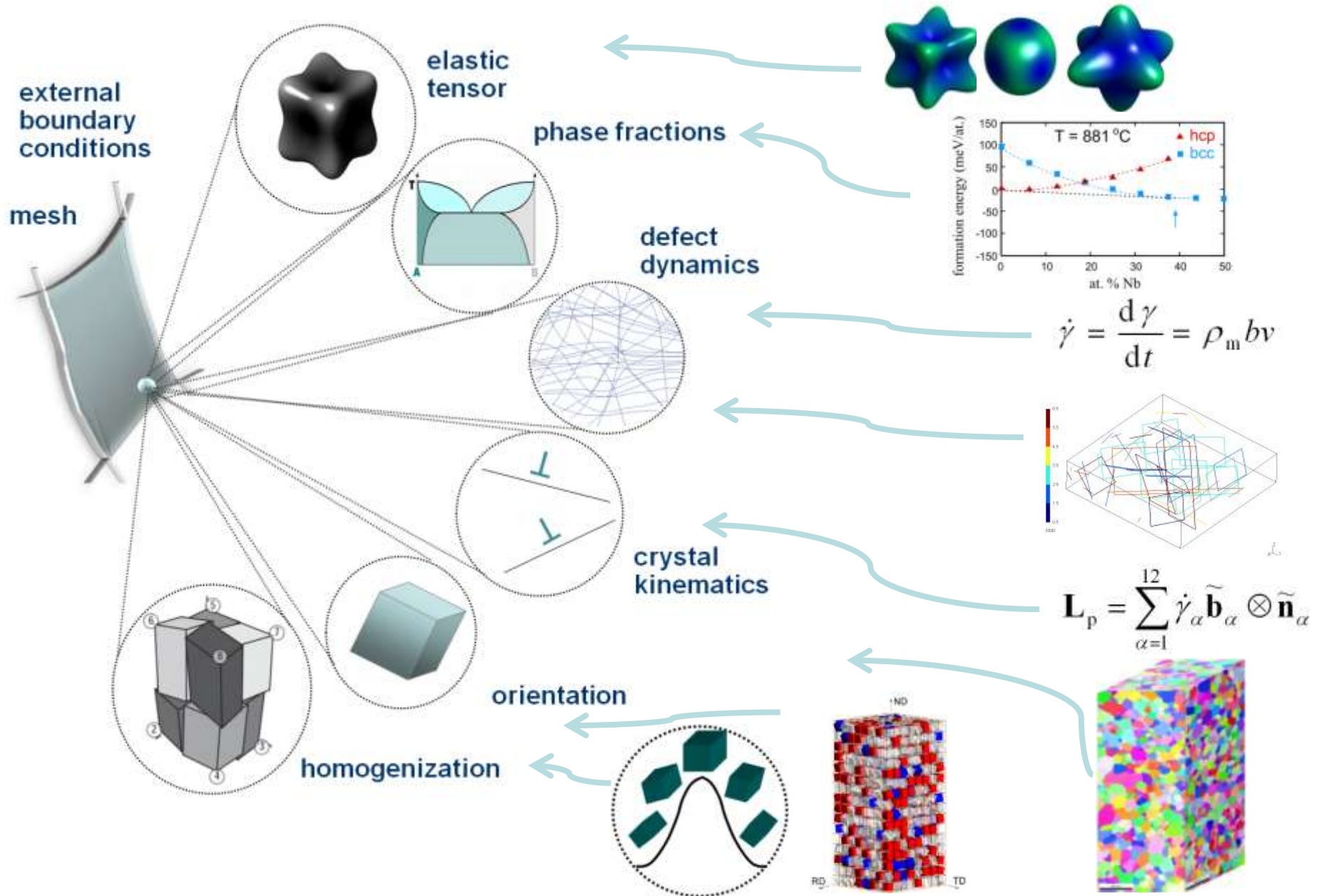
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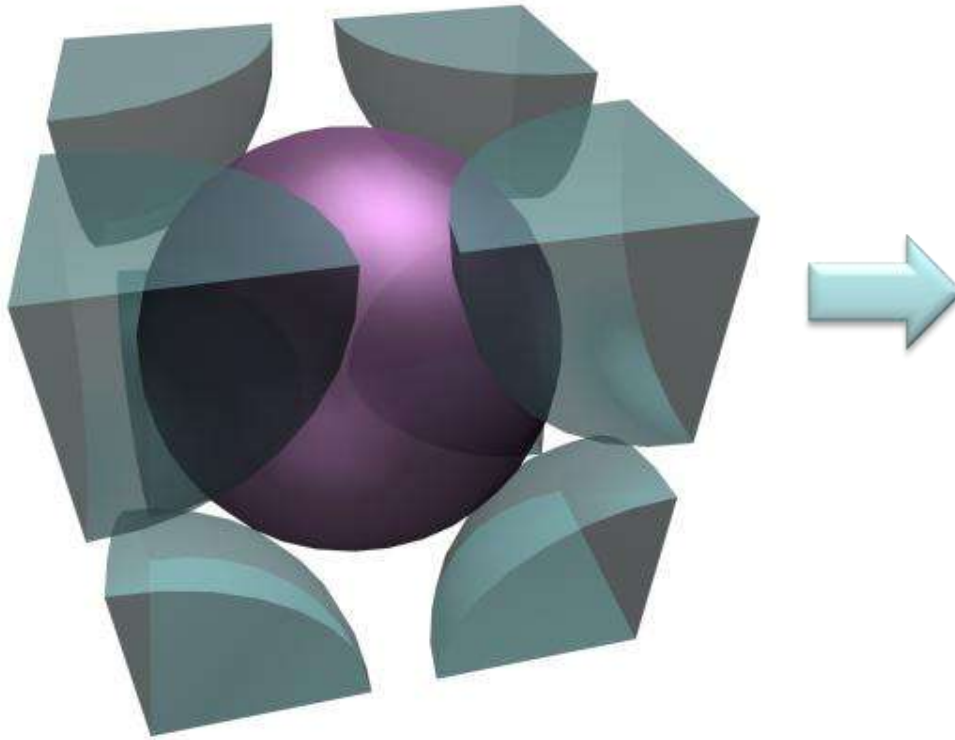
d.raabe@mpie.de



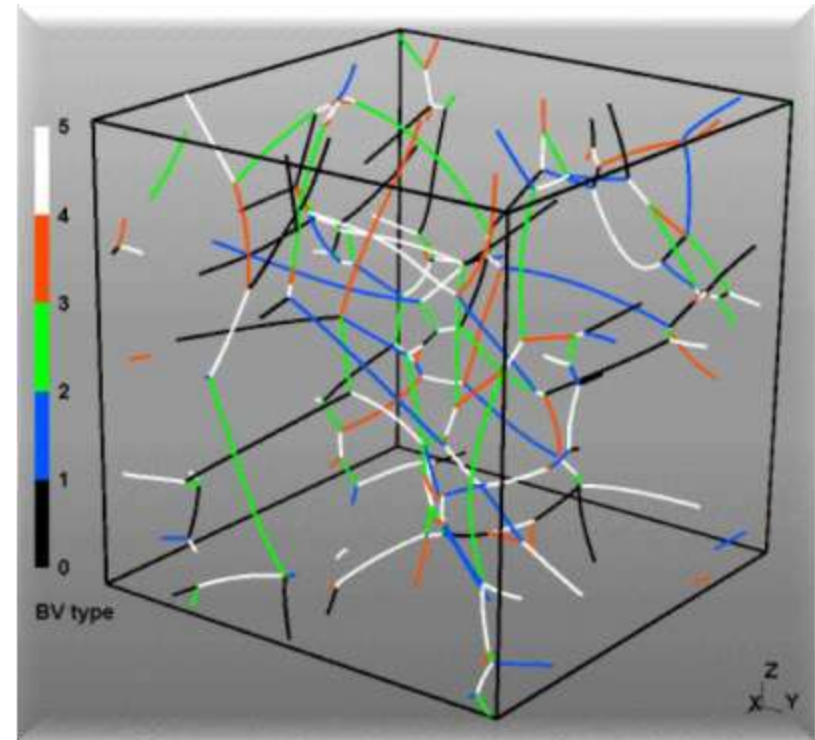




Why is the crystal lattice relevant for understanding complex dislocation structures?



Body centered cubic (bcc) lattice structure





Why is the crystal lattice relevant for understanding complex dislocation structures?

Densely packed planes: glide planes; densely packed translation shear vectors: Burgers vectors

Twinning systems

Stacking fault energy: cross slip, recovery, annihilation, Suzuki effect, twinning, strain hardening, stair rod dislocations, reactions

Shockley partial dislocations ($b = a/6\langle 112 \rangle$)



Special properties of the 3 main lattice types regarding plasticity defects

FCC: stacking fault energy can vary from very low values (α -Brass- 0 wt% Zn in Cu; TWIP steels: $\approx 20 \text{ m J / m}^2$) to very high values (Al : $\approx 180 \text{ m J / m}^2$): Regarding lattice defects in plasticity FCC is not a 'homogeneous' structure

Hex: hcp or hex?; c/a ratio determines slip systems and twinning: some hex metals are very brittle (Mg) and some are very ductile (Ti)

BCC: non-close packed planes: pencil glide behavior; multiple slip systems: $\{110\}$; $\{112\}$; $\{123\}$; complex core of dislocation; twinning vs. anti-twinning glide sense

How frequently do certain crystal structures occur in the PSE?



Li	Be											B	C	N	O	F	Ne
Na	Mg											Al	Si	P	S	Cl	Ar
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
Cs	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
Rb	Ba	La	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
Fr	Ra	Ac															
			Ce	Pr	Nd	Pm	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb	Lu	
			Th	Pa	U	Np	Pu	Am	Cm	Bk	Cf	Es	Fm	Md		Lw	

bcc

fcc

hcp
dhcp

Diamant

FCC: Face centered cubic close packed, (a)	Hexagonal close packed (a, c)	BCC: Body centered cubic (a)
Cu (3.6147)	Be (2.2856, 3.5832)	Fe (2.8664)
Ag (4.0857)	Mg (3.2094, 5.2105)	Cr (2.8846)
Au (4.0783)	Zn (2.6649, 4.9468)	Mo (3.1469)
Al (4.0495)	Cd (2.9788, 5.6167)	W (3.1650)
Ni (3.5240)	Ti (2.506, 4.6788)	Ta (3.3026)
Pd (3.8907)	Zr (3.312, 5.1477)	Ba (5.019)
Pt (3.9239)	Ru (2.7058, 4.2816)	
Pb (4.9502)	Os (2.7353, 4.3191)	
	Re (2.760, 4.458)	

$$= (8 \times 1/8) + 1 = 2$$

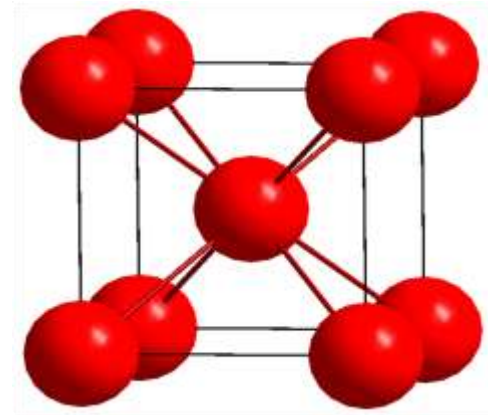
atoms per cell

$$= 4 + 4 = 8$$

coordination number

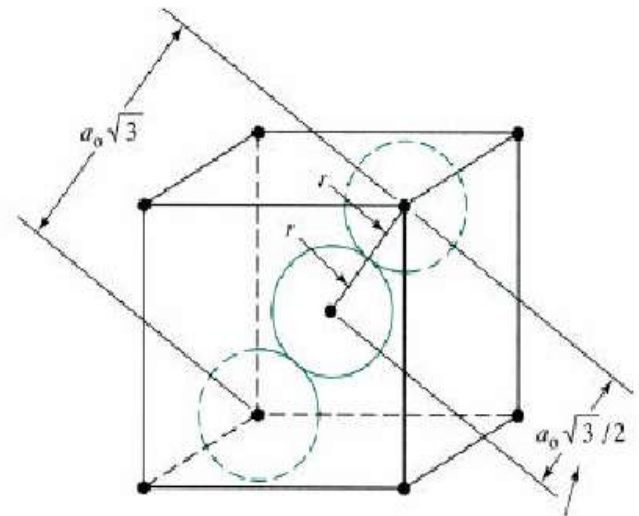
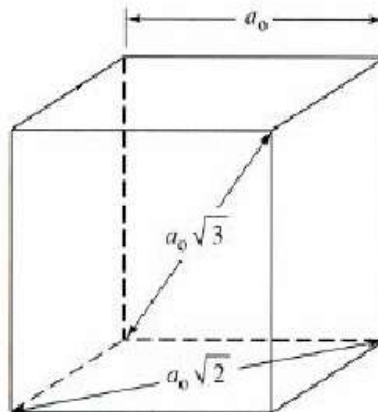
$$= 0.68$$

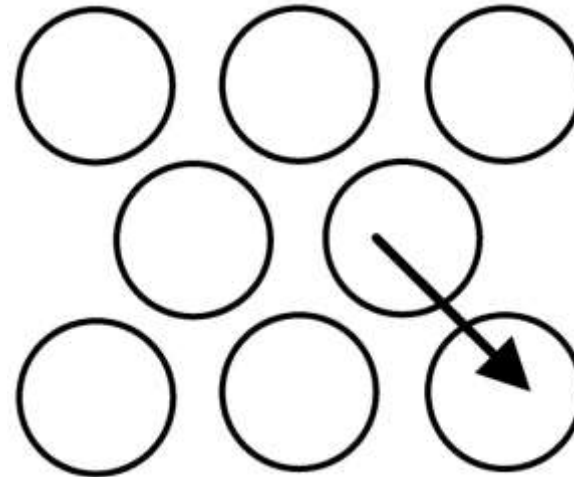
atomic packaging

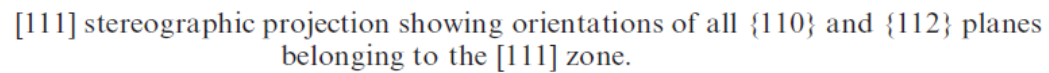


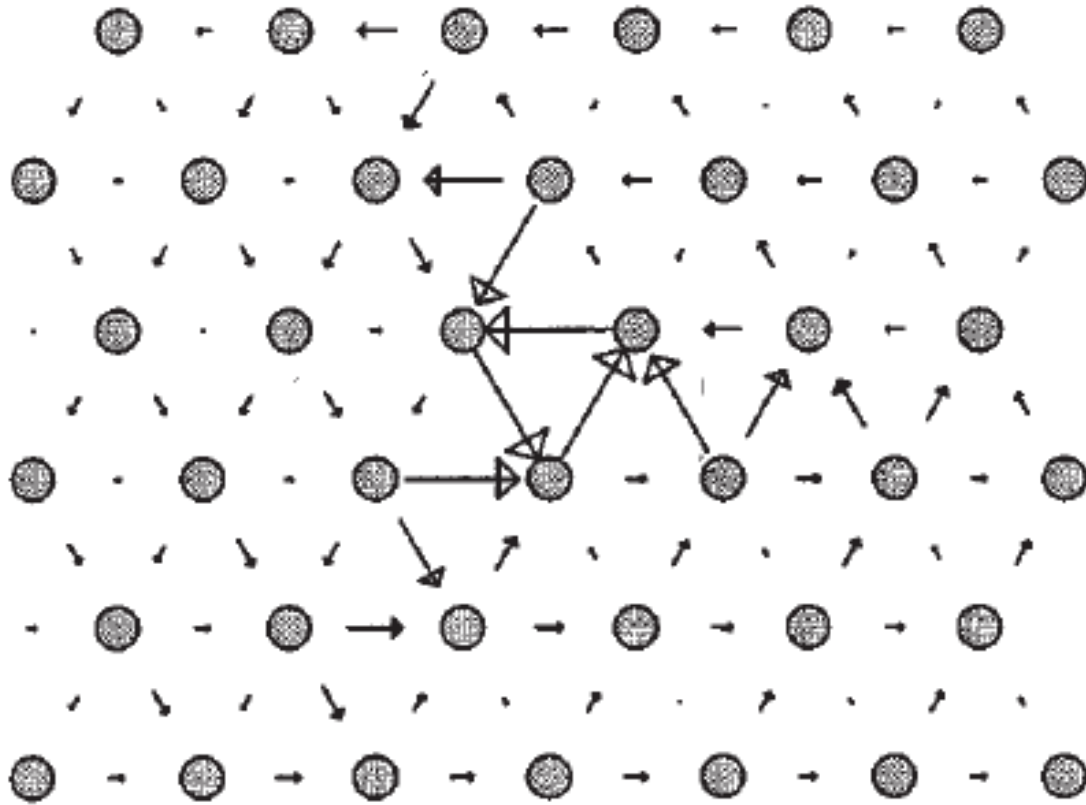
$$4r = \sqrt{3}a$$

$$a = \frac{4}{\sqrt{3}}r$$



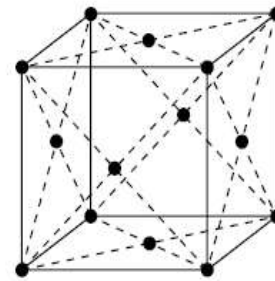
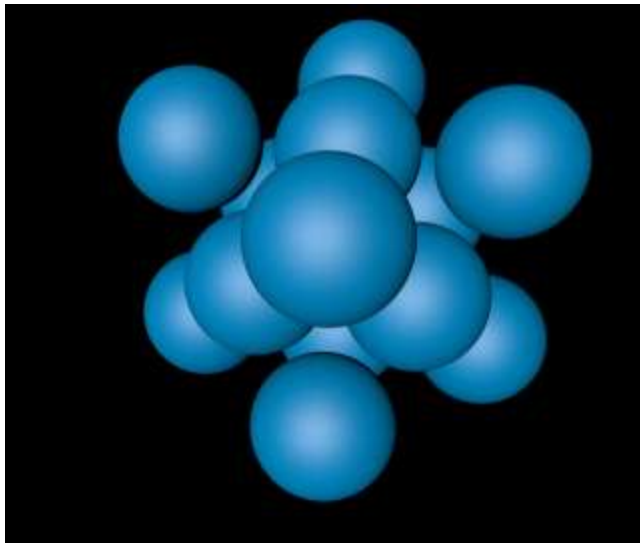




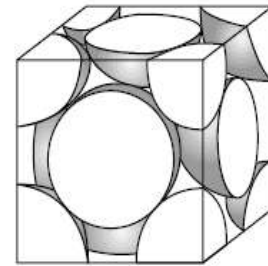


courtesy of V. Vitek

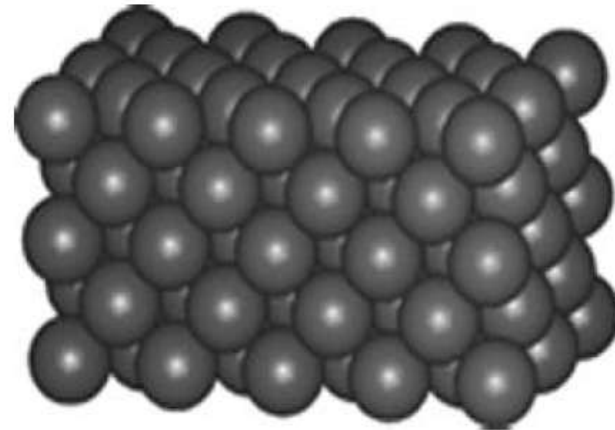
Fe (γ), Al, Cu, Au



(a)



(b)



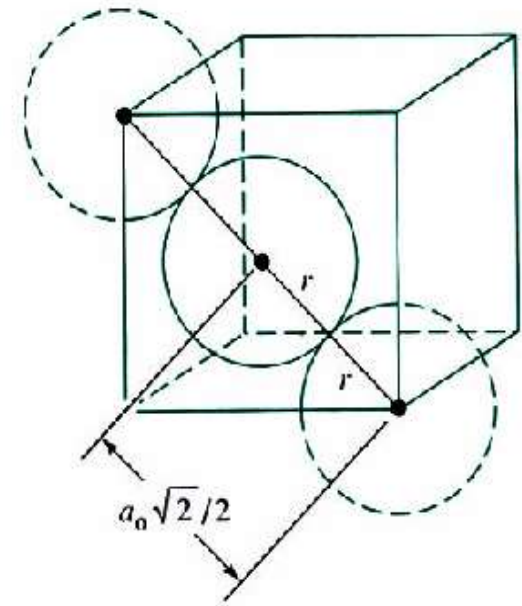
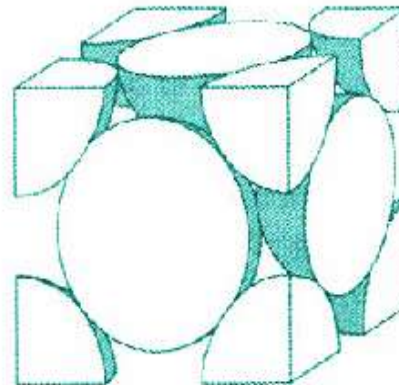
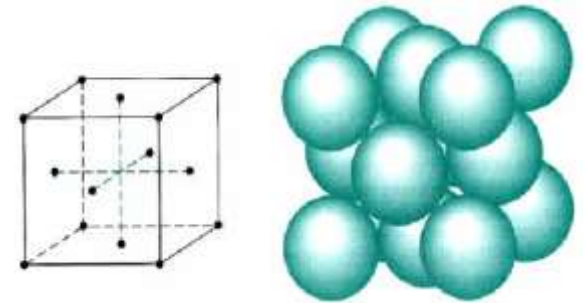
$$\text{atoms per cell} = (8 \times 1/8) + (6 \times 1/2) = 4$$

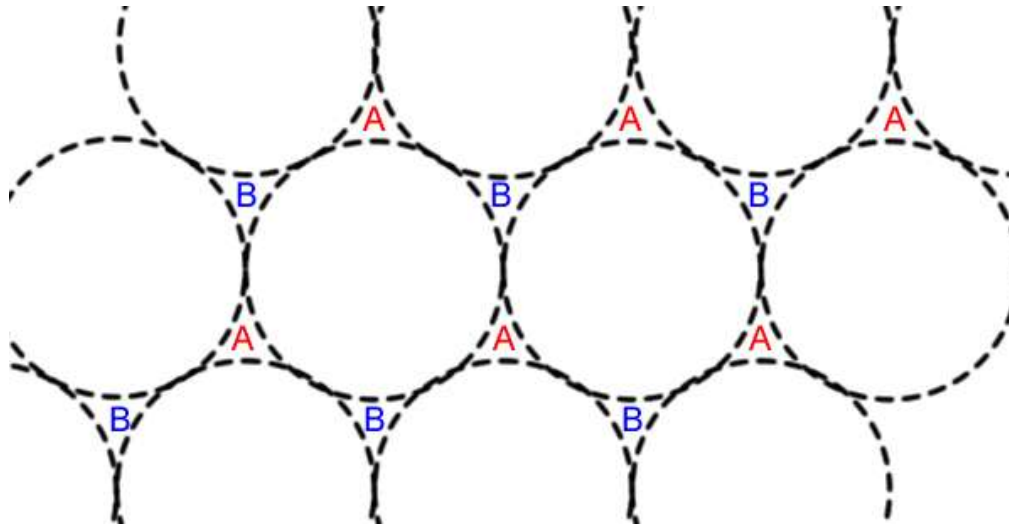
$$\text{coordination number} = 4 + 4 + 4 = 12$$

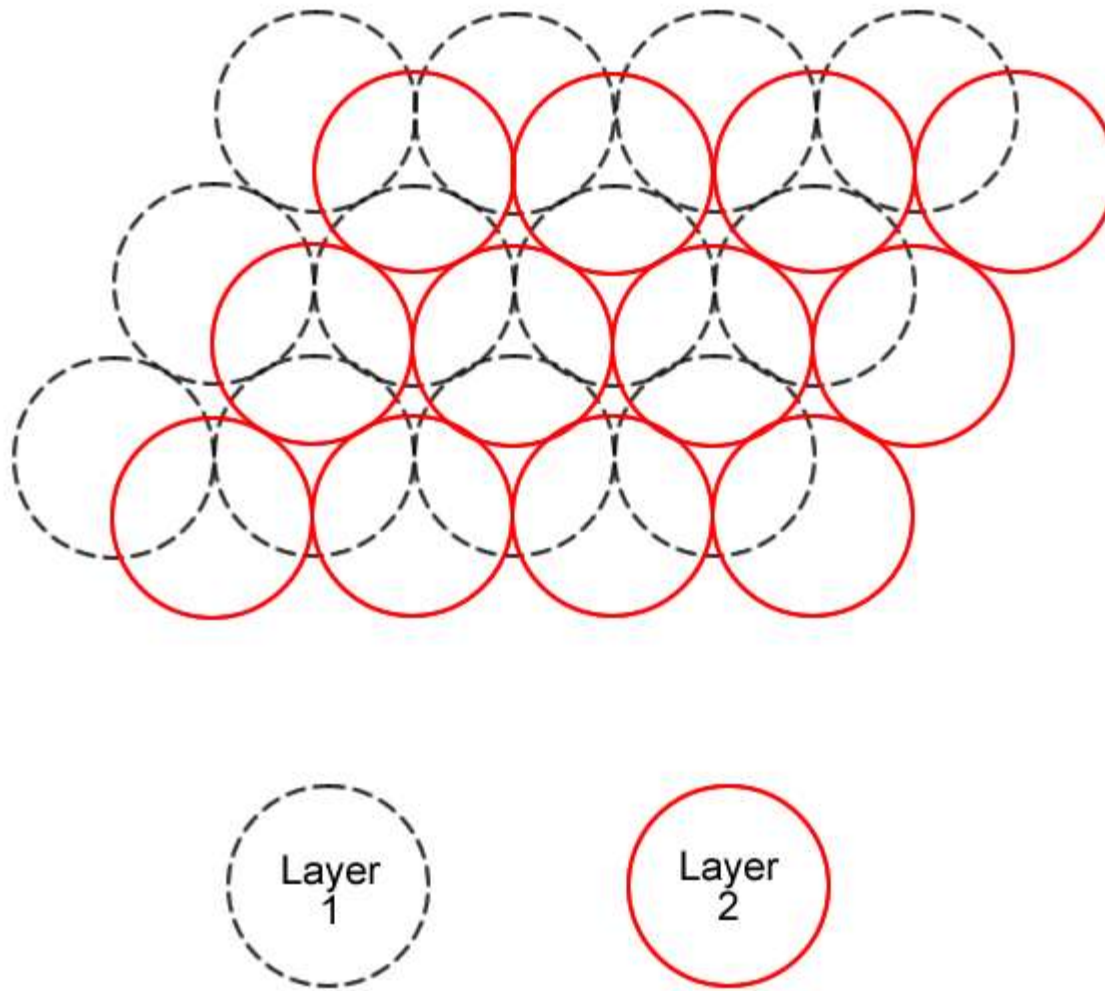
$$\text{atomic packaging} = 0.74$$

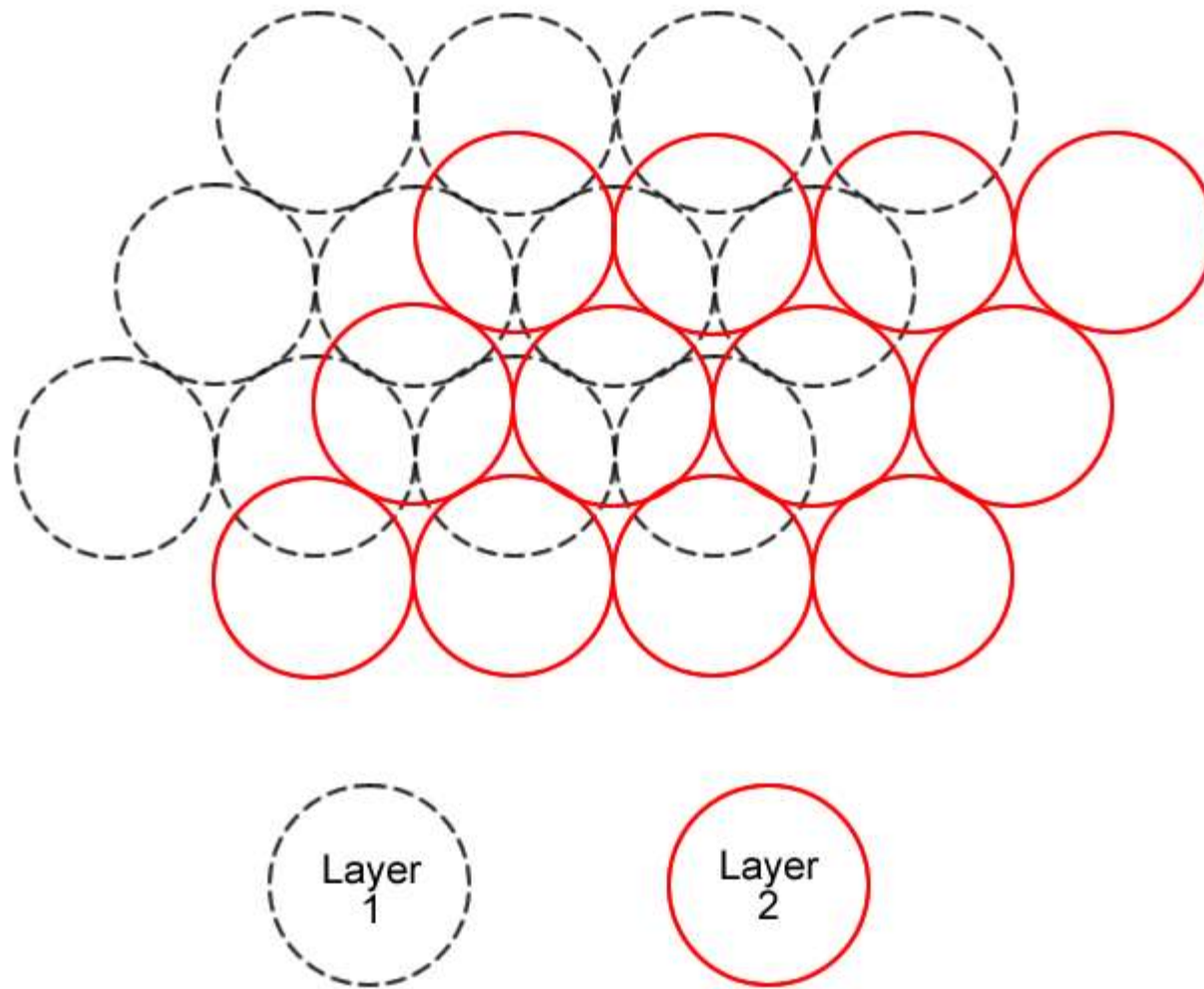
$$4r = \sqrt{2}a$$

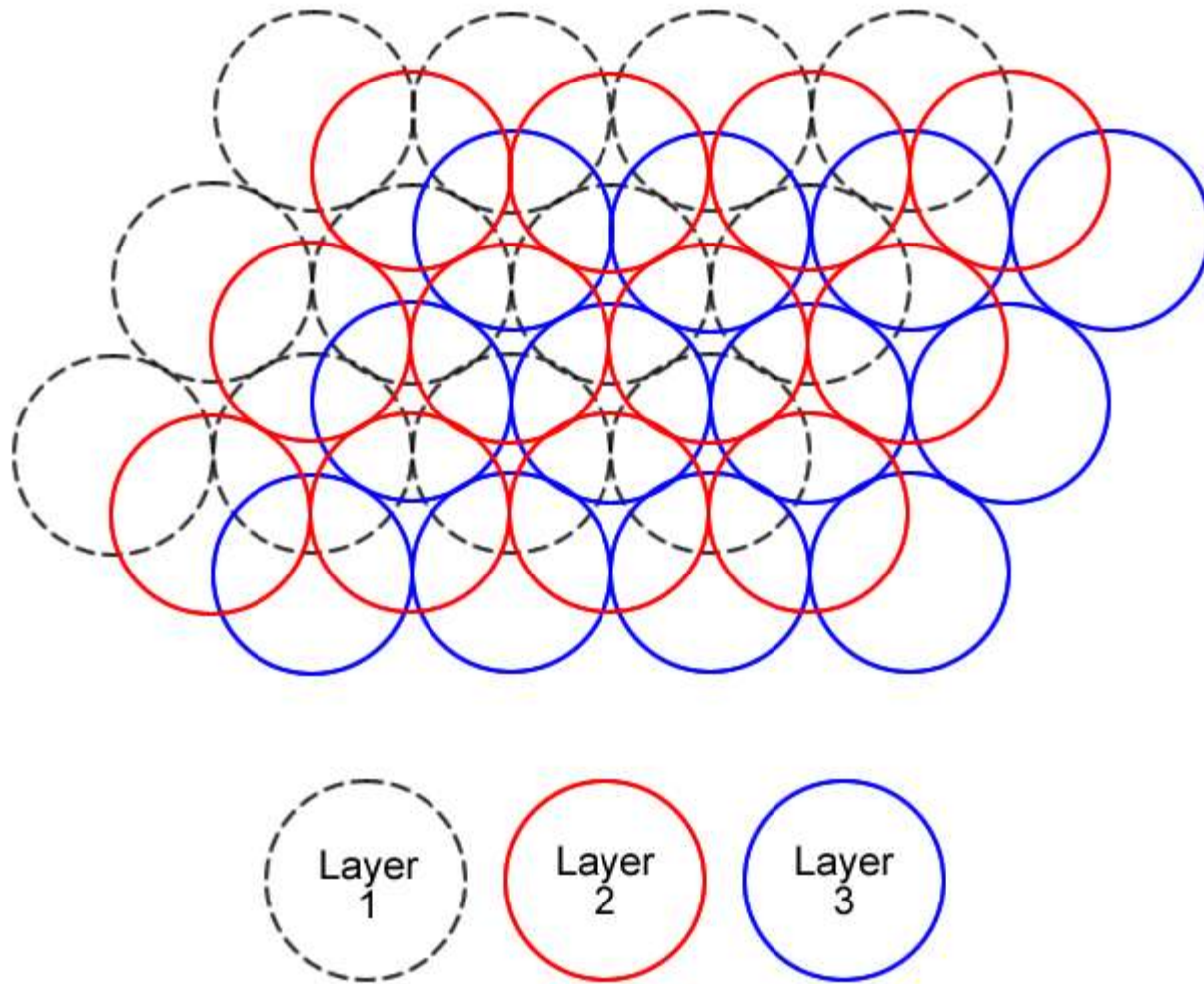
$$a = 2\sqrt{2}r$$

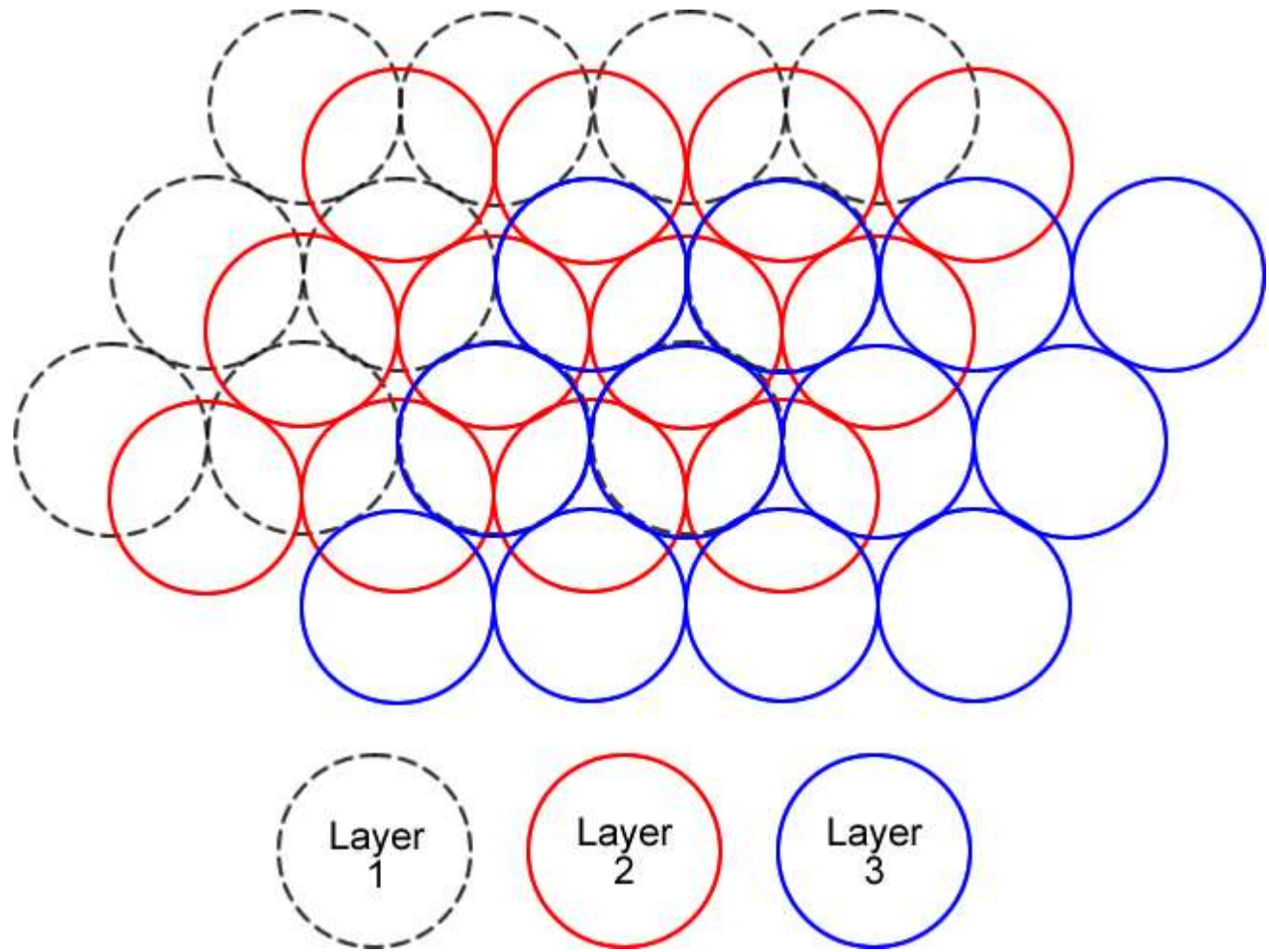


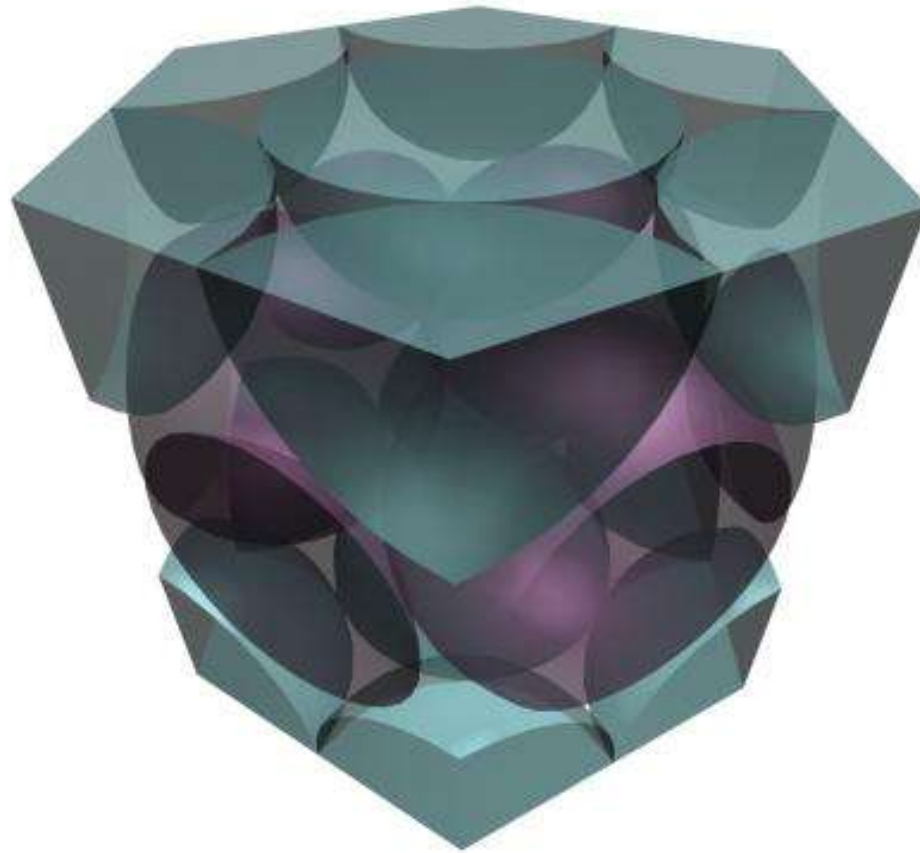






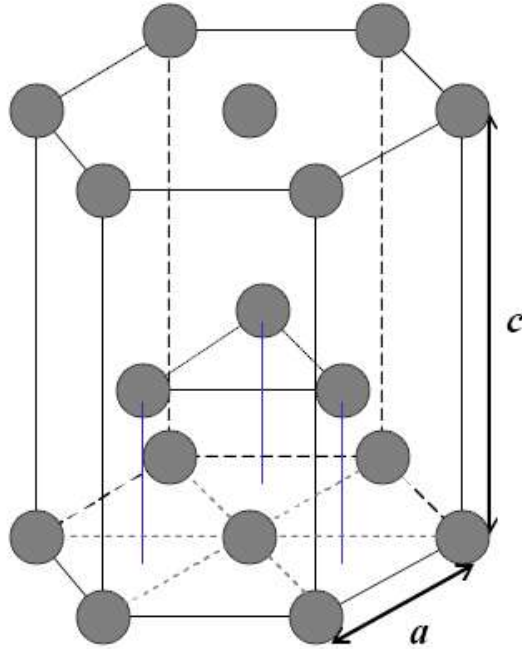




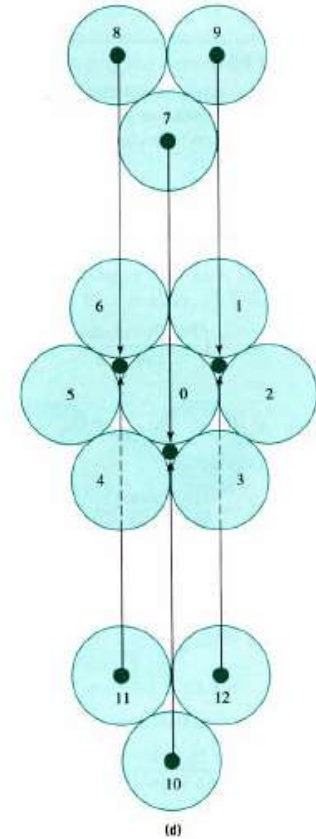
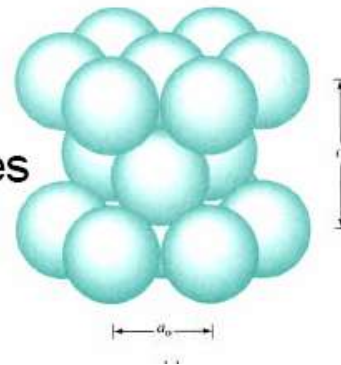
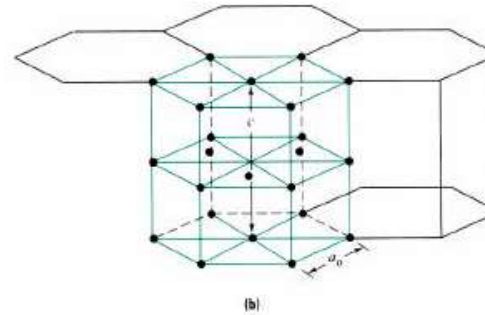
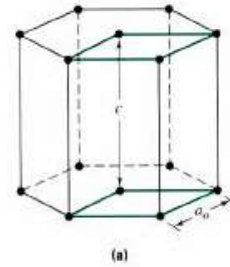


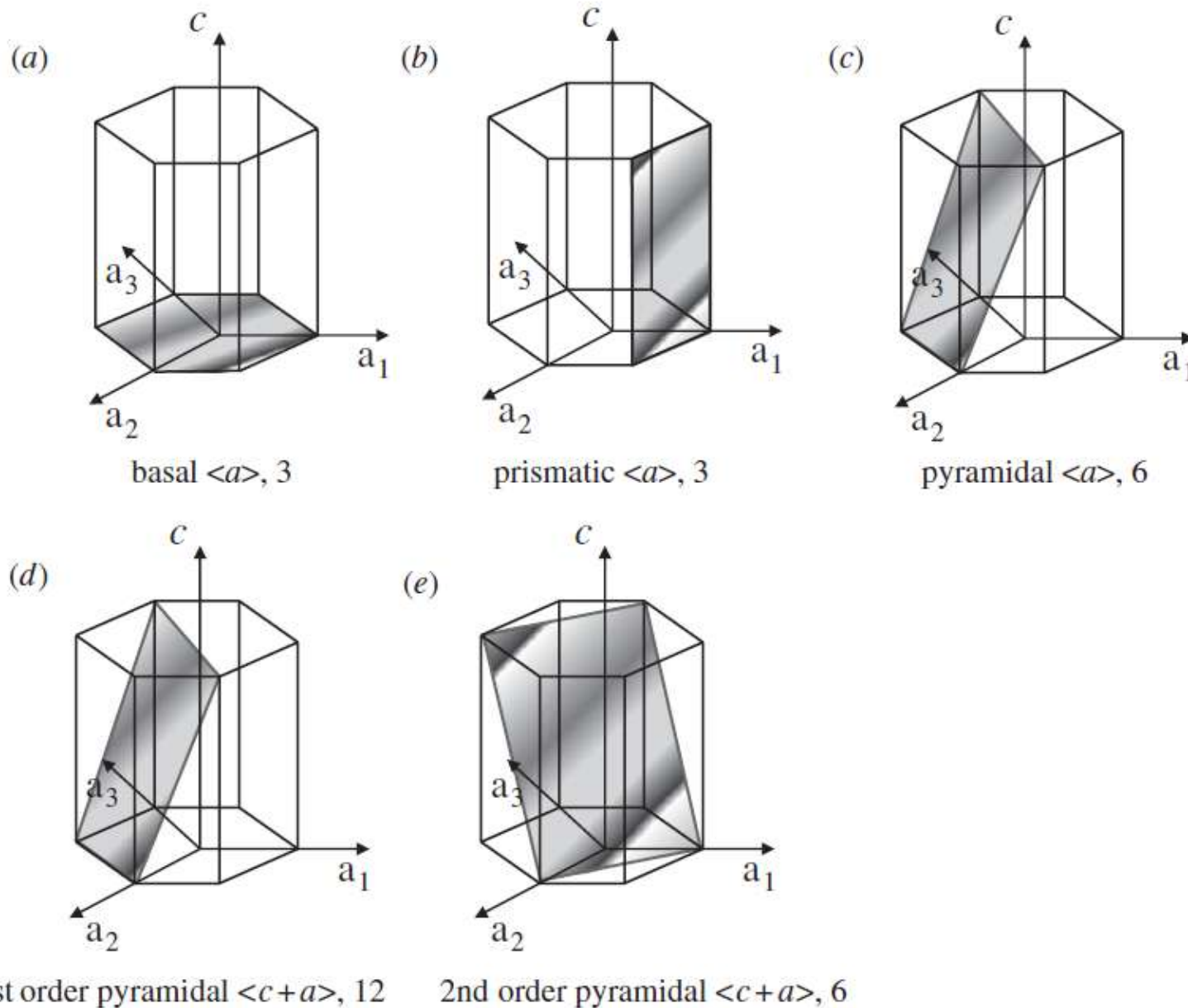
3. HCP: hexagonal close-packed

(Mg, Be, Co, Ti, Zn)

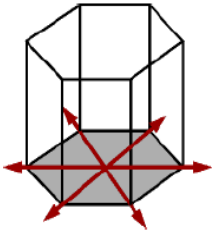
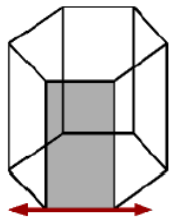
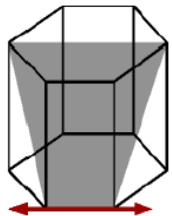


noncubic symmetry: **a** and **c** axes
 $c/a \sim 1.633$

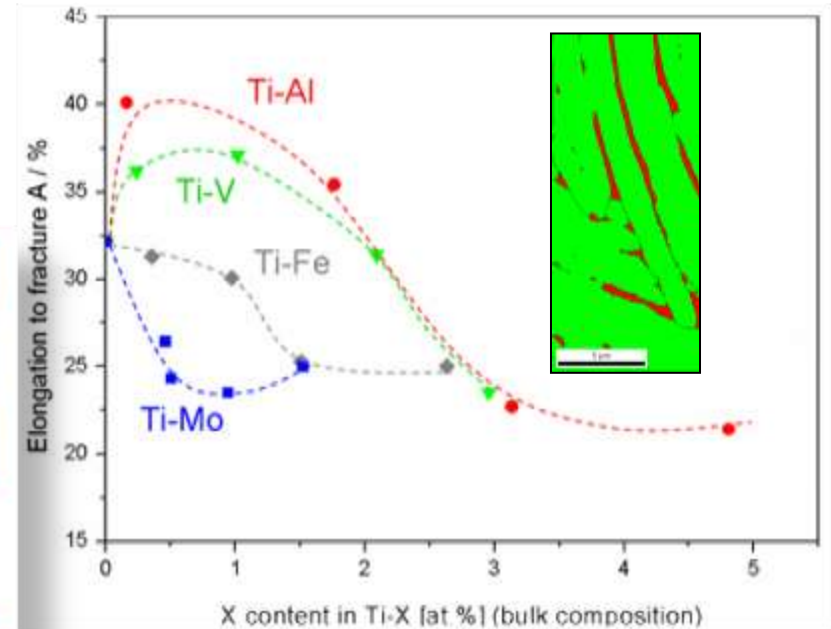
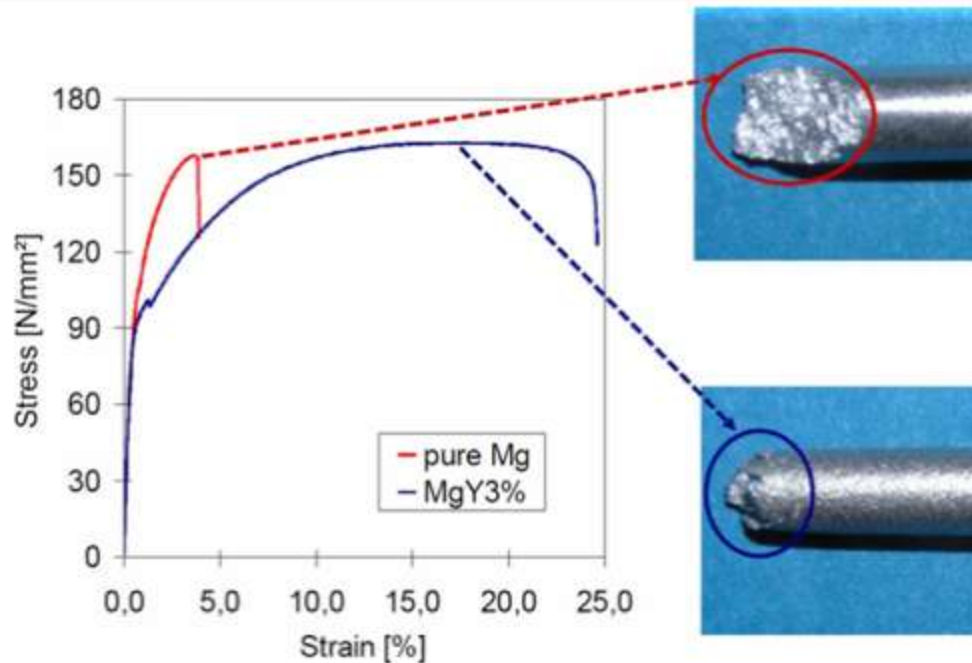




vectors and planes for hexagonal materials

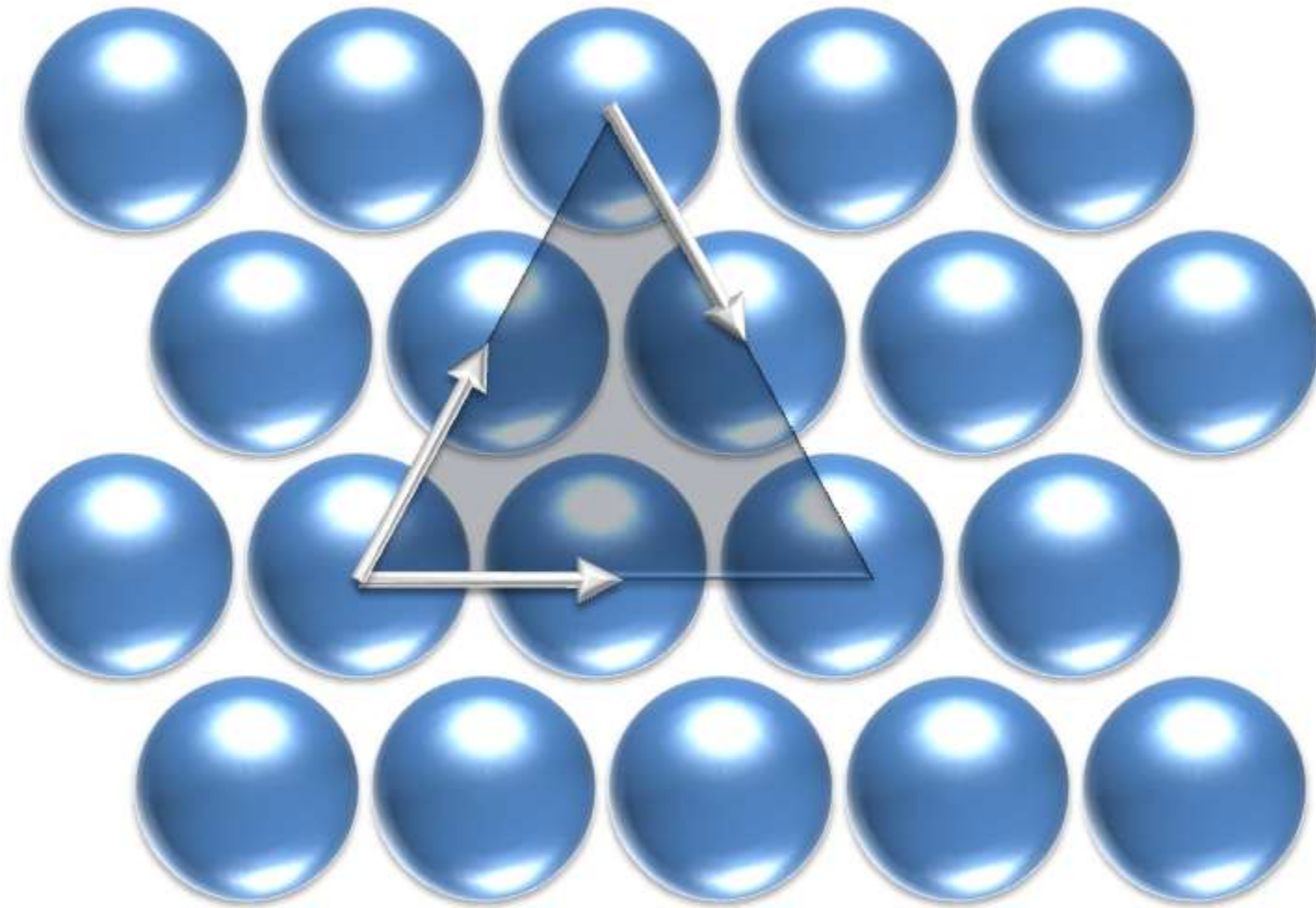
G i t t e r	B e i s p i e l		Gleitebe- nen G		Gleitrich- tung g		Gesamt- zahl der Gleitsy- steme
			Typ	Z a h l	Typ	Z a h l	
h e x	Cd Zn Mg Ti_{α} Be		(0001)	1	[1120]	3	3
	Cd Zn Mg Ti_{α} Be Zr_{α}		(1010)	3	[1120]	1	3
	Mg Ti_{α}		(1011)	6	[1120]	1	6

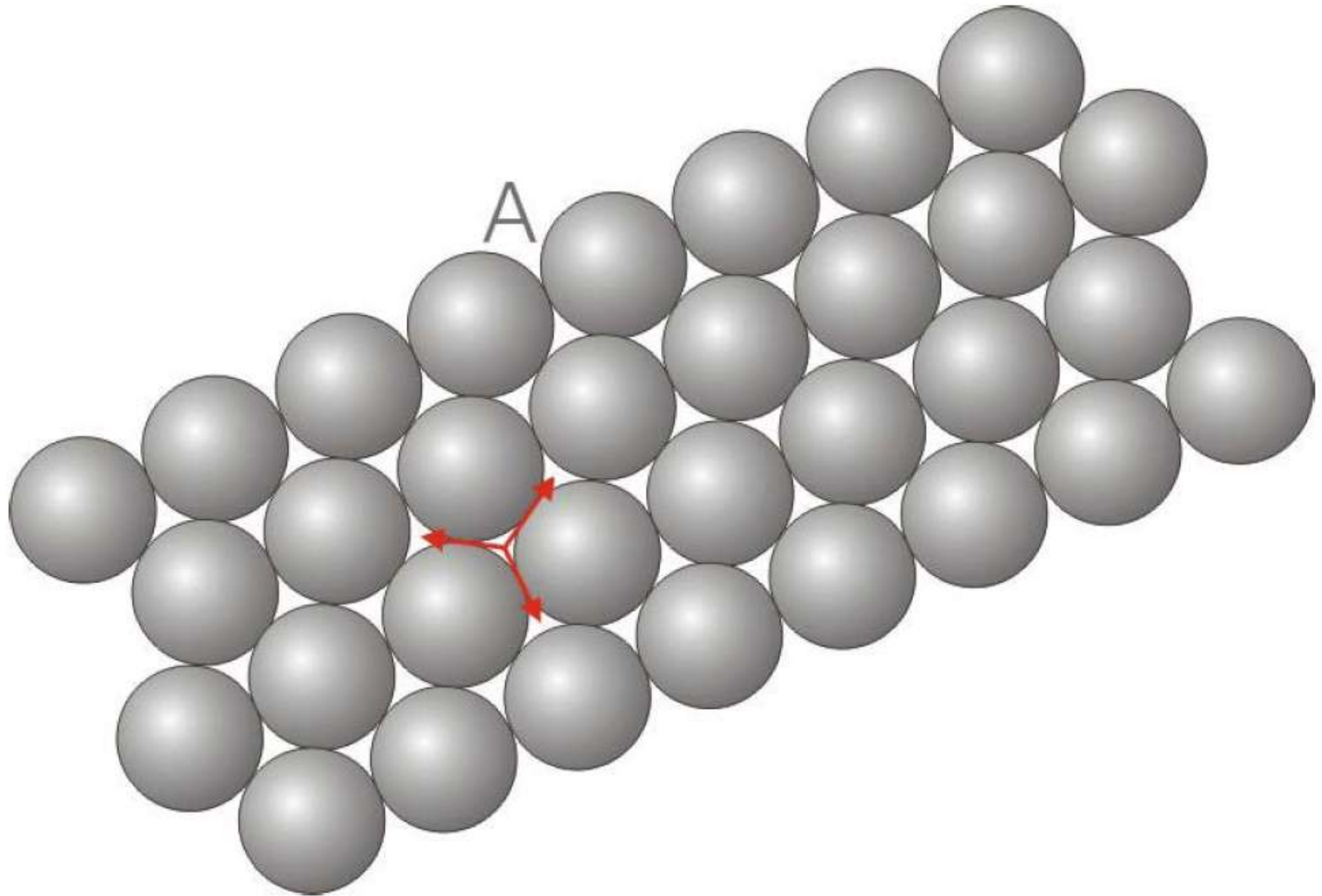
Mg - RE

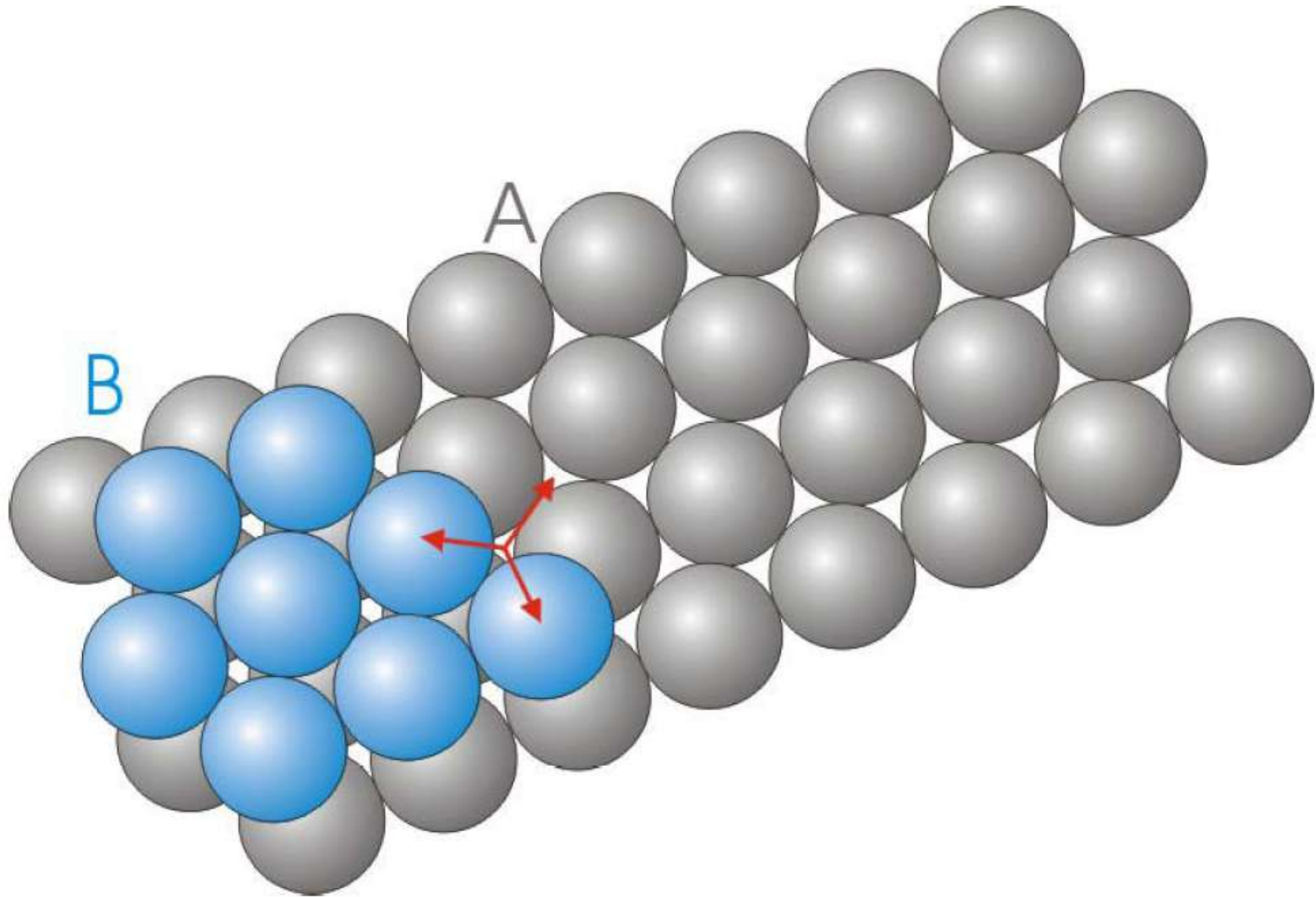


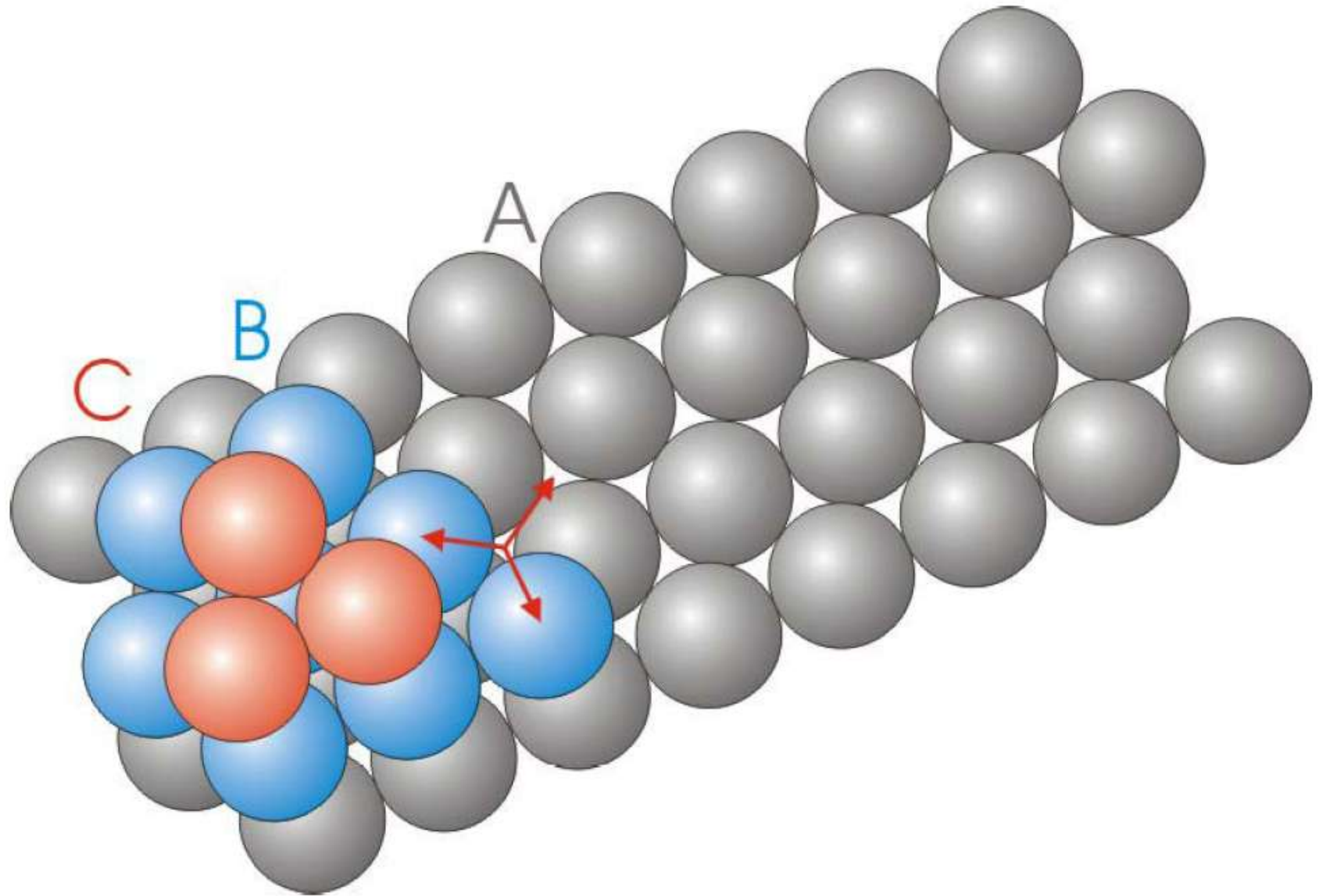
Mg - Li

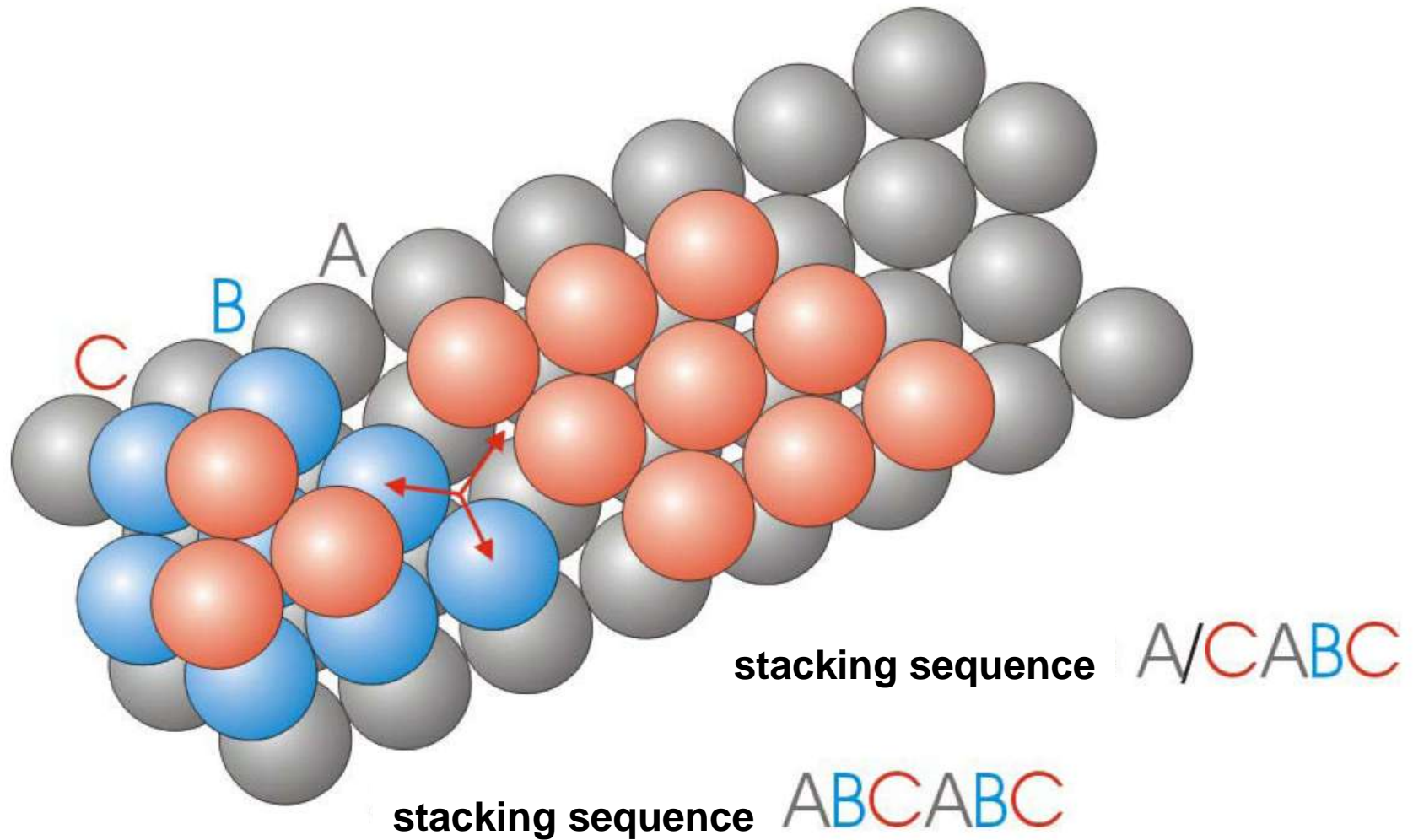


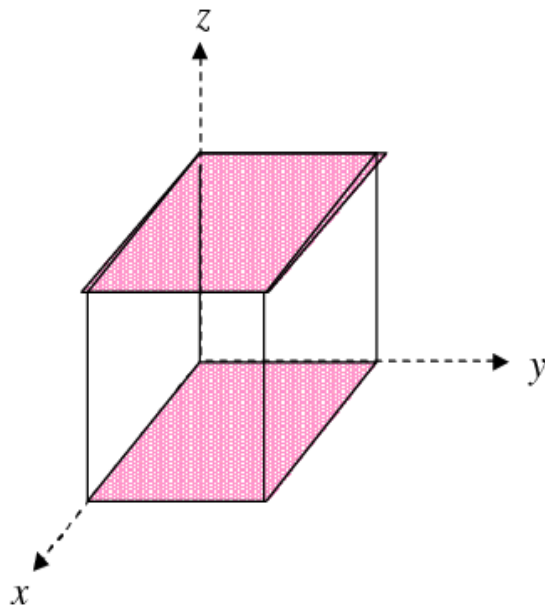
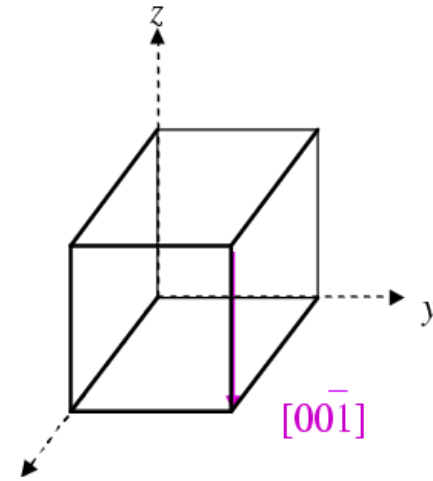
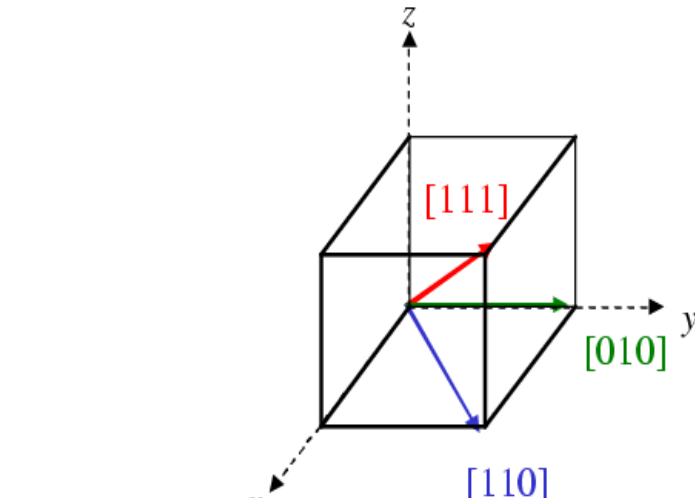






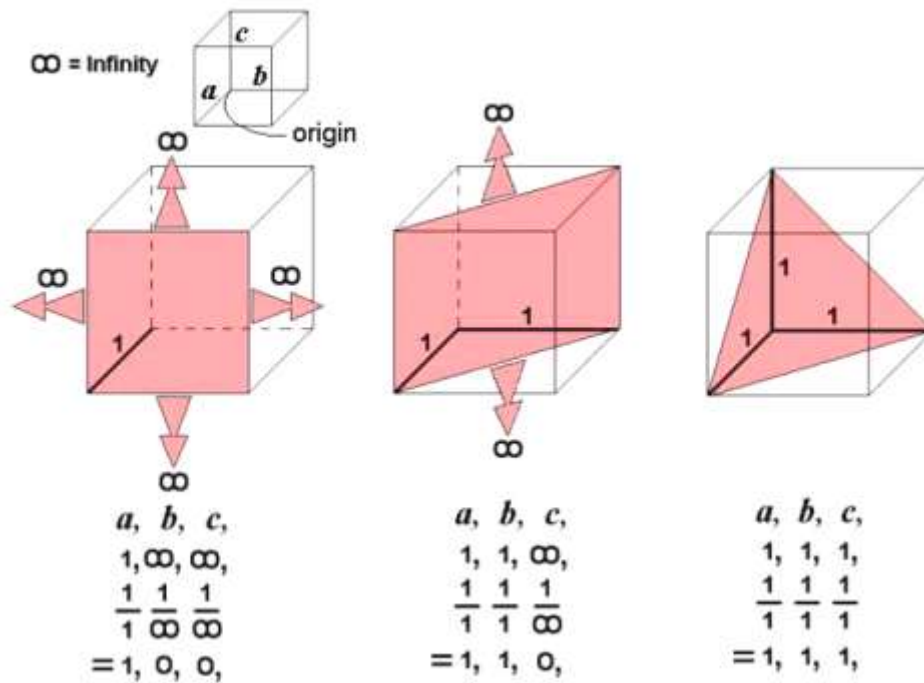
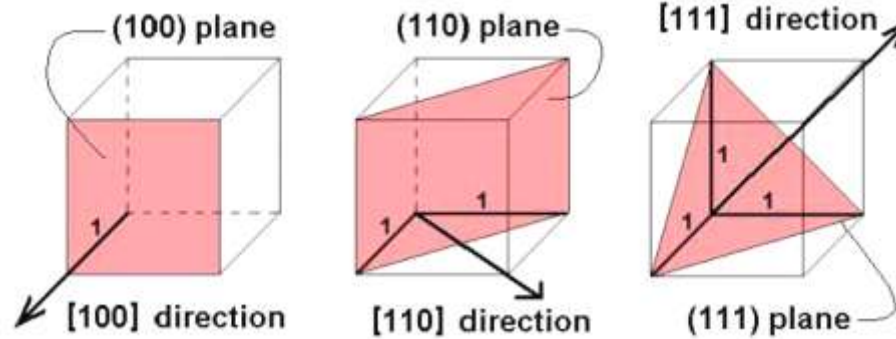






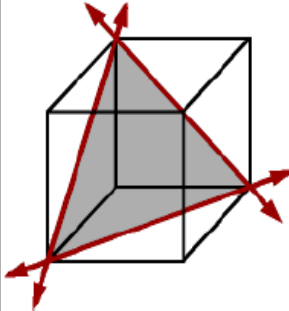
	x	y	z
Intercepts	∞	∞	1
reciprocals	0	0	1
Indices			(001)

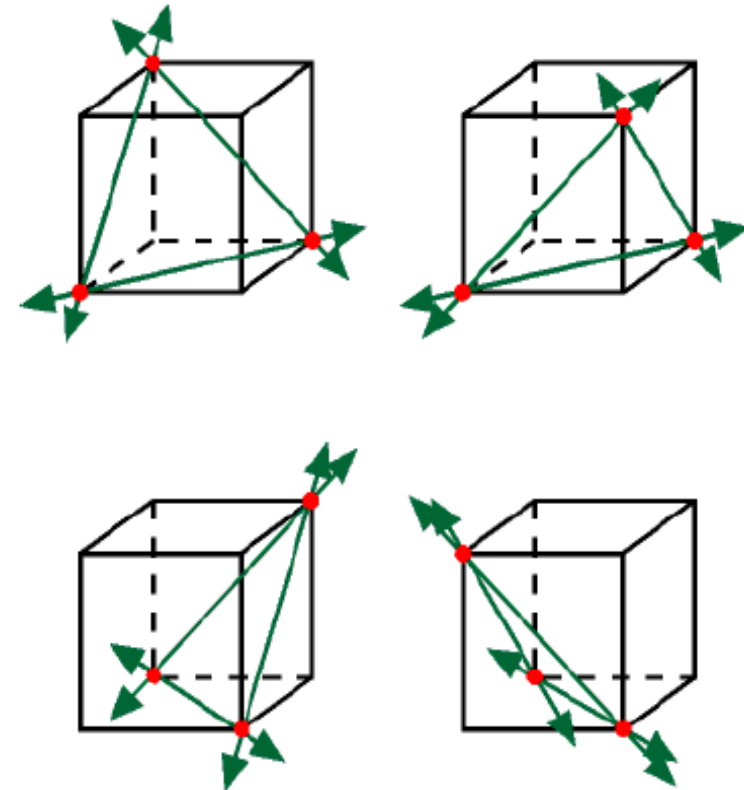
Deriving Miller indices: the description of lattice vectors



Miller Indices of typical planes and directions in FCC metals



Gitter	Beispiel		Gleitebenen G		Gleitrichtung g		Gesamtzahl der Gleitsysteme
			Typ	Zahl	Typ	Zahl	
kfz	Al Cu Ni Ag Au		(111)	4	[110]	3	12

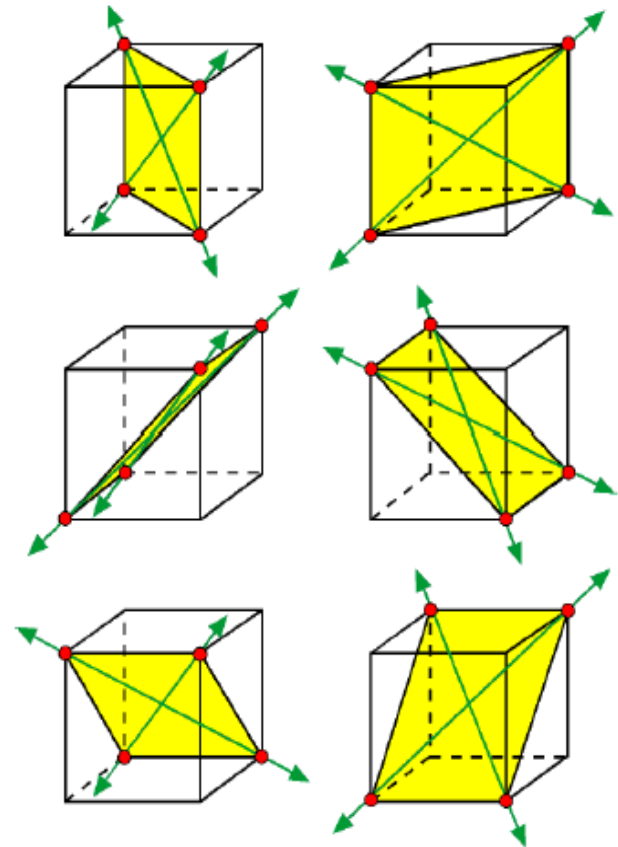


kfz		
4E	x	3R
(111)		[110]
= 12		

Miller Indices of typical planes and directions in BCC metals

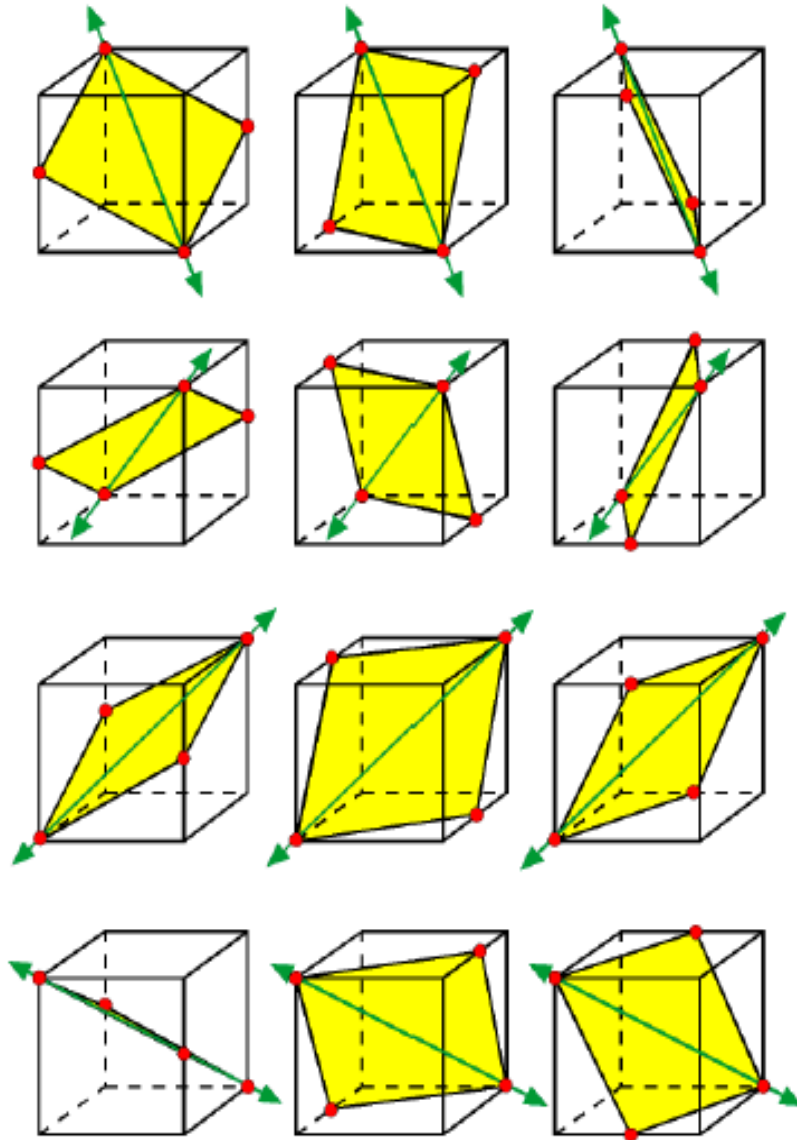


G i t t e r	B e i s p i e l		Gleitebe- nen G		Gleitrich- tung g		Gesamt- zahl der Gleitsys- teme
			Typ	Z a h l	Typ	Z a h l	
k r z	$Fe_{\alpha\delta}$ W Mo Nb Ta		(110)	6	[111]	2	12
	$Fe_{\alpha\delta}$ W Mo Nb		(112)	12	[111]	1	12
	$Fe_{\alpha\delta}$ W_a Mo		(123)	24	[111]	1	24



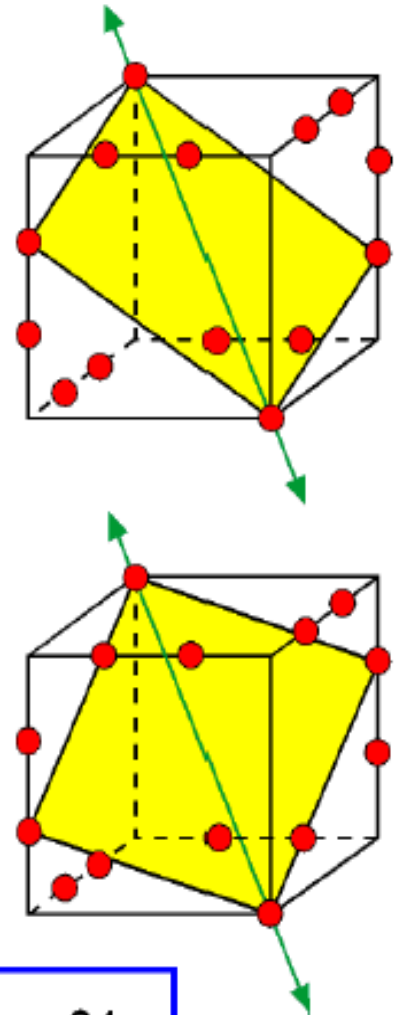
$$\frac{6E}{(110)} \times \frac{2R}{[111]} = 12$$

krz



$$12E \times 1R = 12$$

$$(112) \quad [111]$$



$$24E \times 1R = 24$$

$$(123) \quad [111]$$

$$\langle 100 \rangle = [1, 0, 0], [\bar{1}, 0, 0], [0, 1, 0], [0, \bar{1}, 0], [0, 0, 1], [0, 0, \bar{1}]$$

$$\langle 110 \rangle = [1, 1, 0], [\bar{1}, 1, 0], [1, \bar{1}, 0], [\bar{1}, \bar{1}, 0], [1, 0, 1], [\bar{1}, 0, \bar{1}], \dots$$

	specific	general
direction	$[\quad]$	$\langle \quad \rangle$
plane	(\quad)	$\{ \quad \}$

vectors and planes

