

Alloy design of nanoprecipitate-hardened high-Mn maraging-TRIP and -TWIP steels

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➤ **Introduction**

- Compositions and processing
- Mechanical properties and microstructures
- Characterization of precipitations
- Formation of new austenite during aging
- Conclusions

Steel for automotive applications:

Good combination of **strength**, **ductility**, **price**

Lean Maraging TRIP Steels

- **Ductile low carbon martensite matrix**
- **Small amount of austenite (TRIP, TWIP)**
- **Controlled precipitation hardening**



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Steel	C	Ni	Co	Mo	Ti	Al	Mn	Fe
Maraging	0.01	18	12	4	1.6	0.15	0.05	Balance

Low carbon: ductile martensite

Precipitation hardening

Expensive for automotive applications !

Optimised for very high strength + toughness

We want high strength + ductility

Compositions in mass%: new lean maraging steels



Steel	C	Ni	Co	Mo	Ti	Al	Mn	Fe
Maraging	0.01	18	12	4	1.6	0.15	0.05	Balance
09MnPH	0.01	2	-	1	1.0	0.15	9	Balance
12MnPH	0.01	2	-	1	1.0	0.15	12	Balance
15MnPH	0.01	2	-	1	1.0	0.15	15	Balance



Low carbon: ductile martensite

Precipitation Hardenable

Mn (+Ni): austenite (TRIP)

Vacuum induction melting

Annealing

Hot deformation

Solution heat treatment

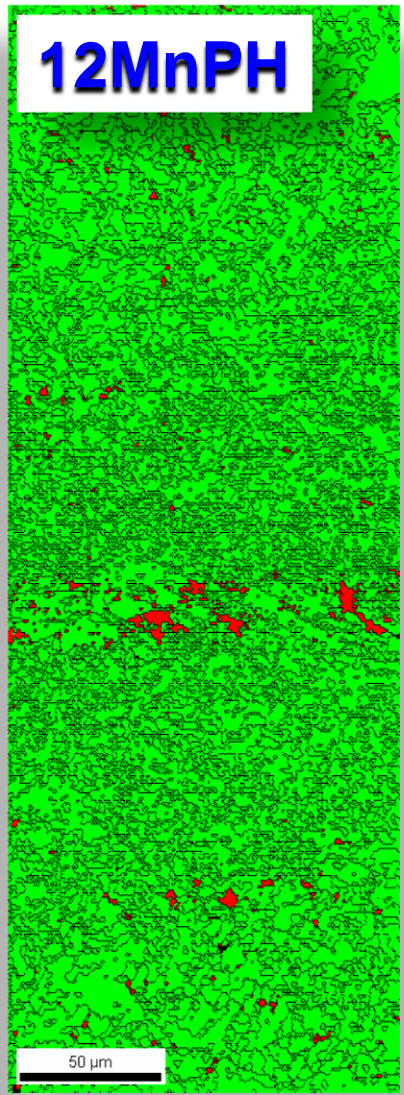
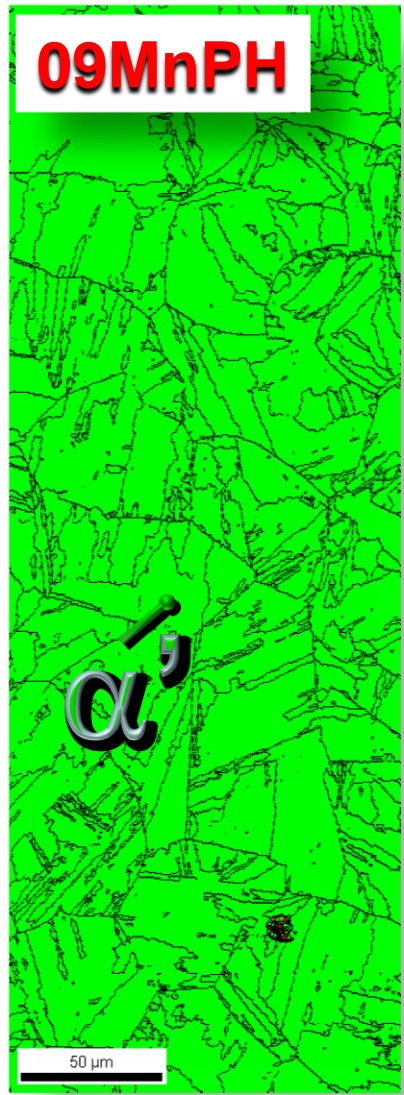
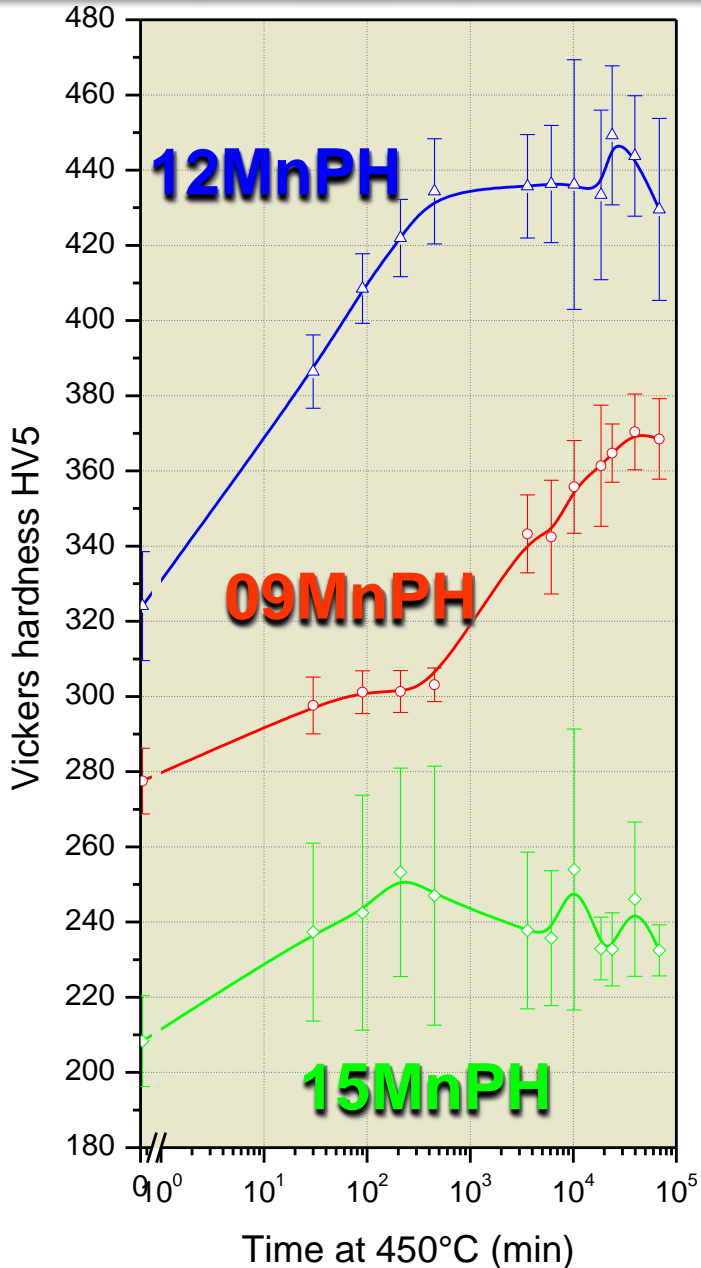
Quenching \Rightarrow **Martensite** + retained austenite

Aging (450°C) “**Maraging**” retained + new austenite



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Hardness during aging at 450°C



Phase	Fraction
Iron - Alpha	0.999
Iron - Gamma	0.000

Phase	Fraction
Iron - Alpha	0.982
Iron - Gamma	0.017

Phase	Fraction
Iron - Alpha	0.386
Iron - Gamma	0.614

12MnPH after aging (48h 450°C)

precipitates in α'

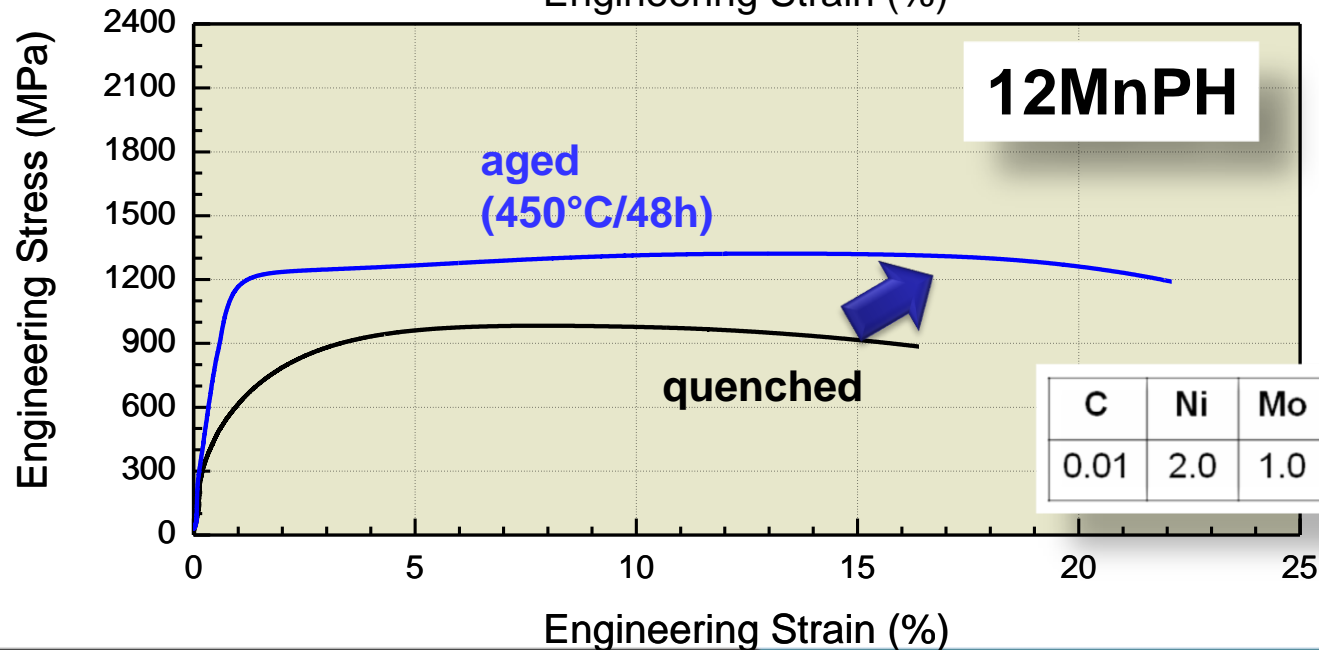
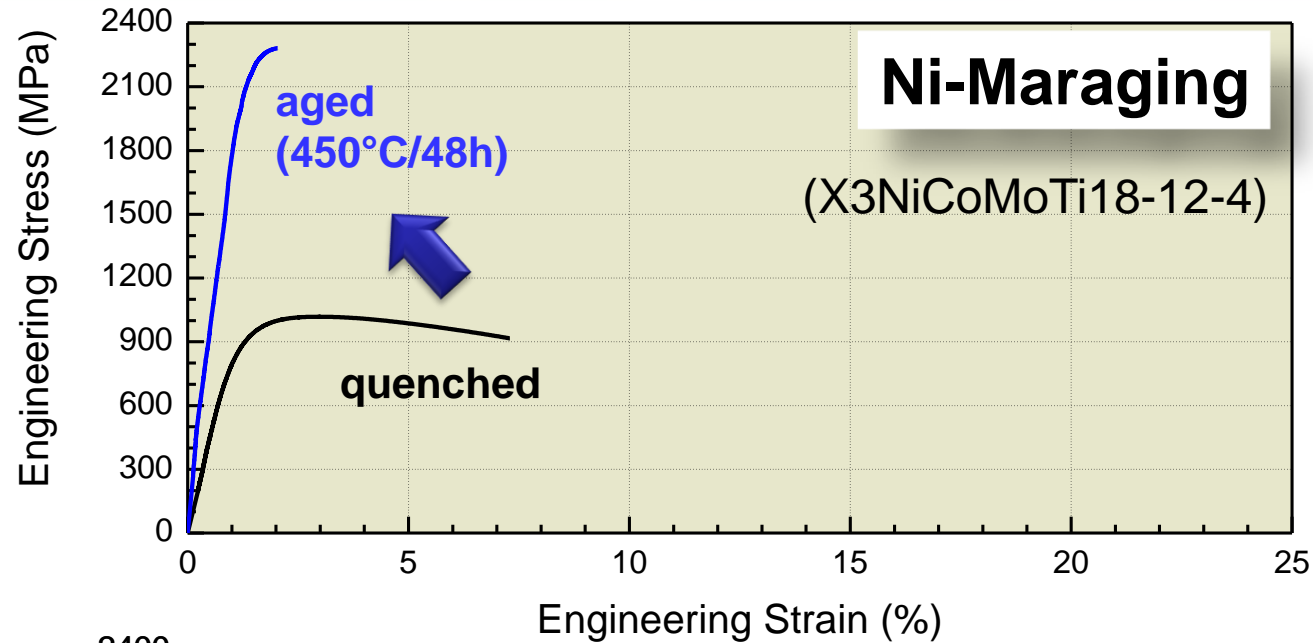
$$x_{Diff} \cong 2\sqrt{Dt} \cong 30nm$$

no precipitates
in austenite

$$x_{Diff} \cong 2nm$$

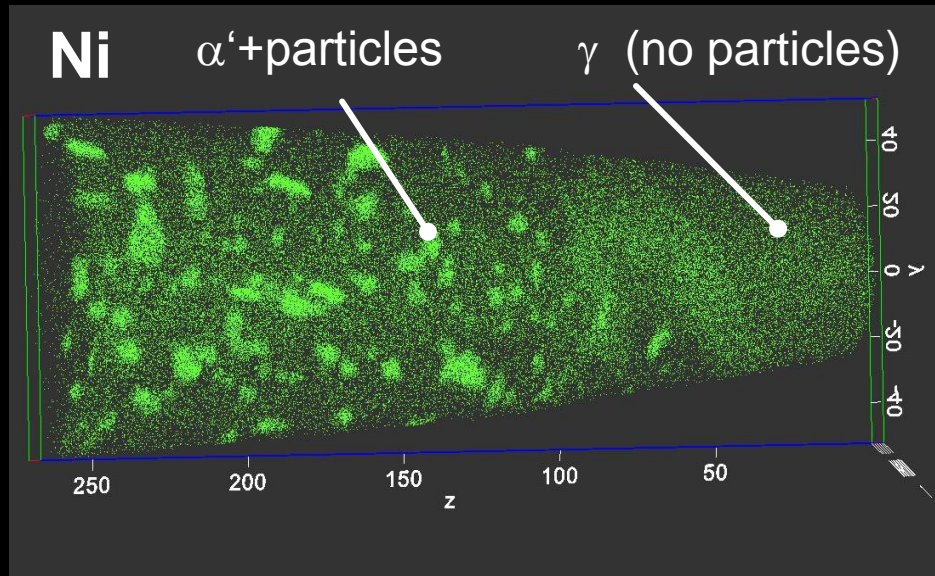
Specimen [STEM BF]
JEOL-TEM 200kV x400k 50%

200.0nm

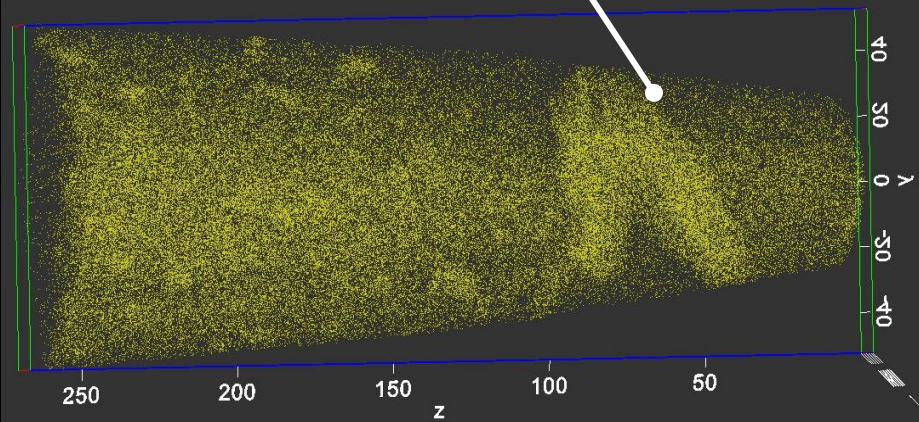


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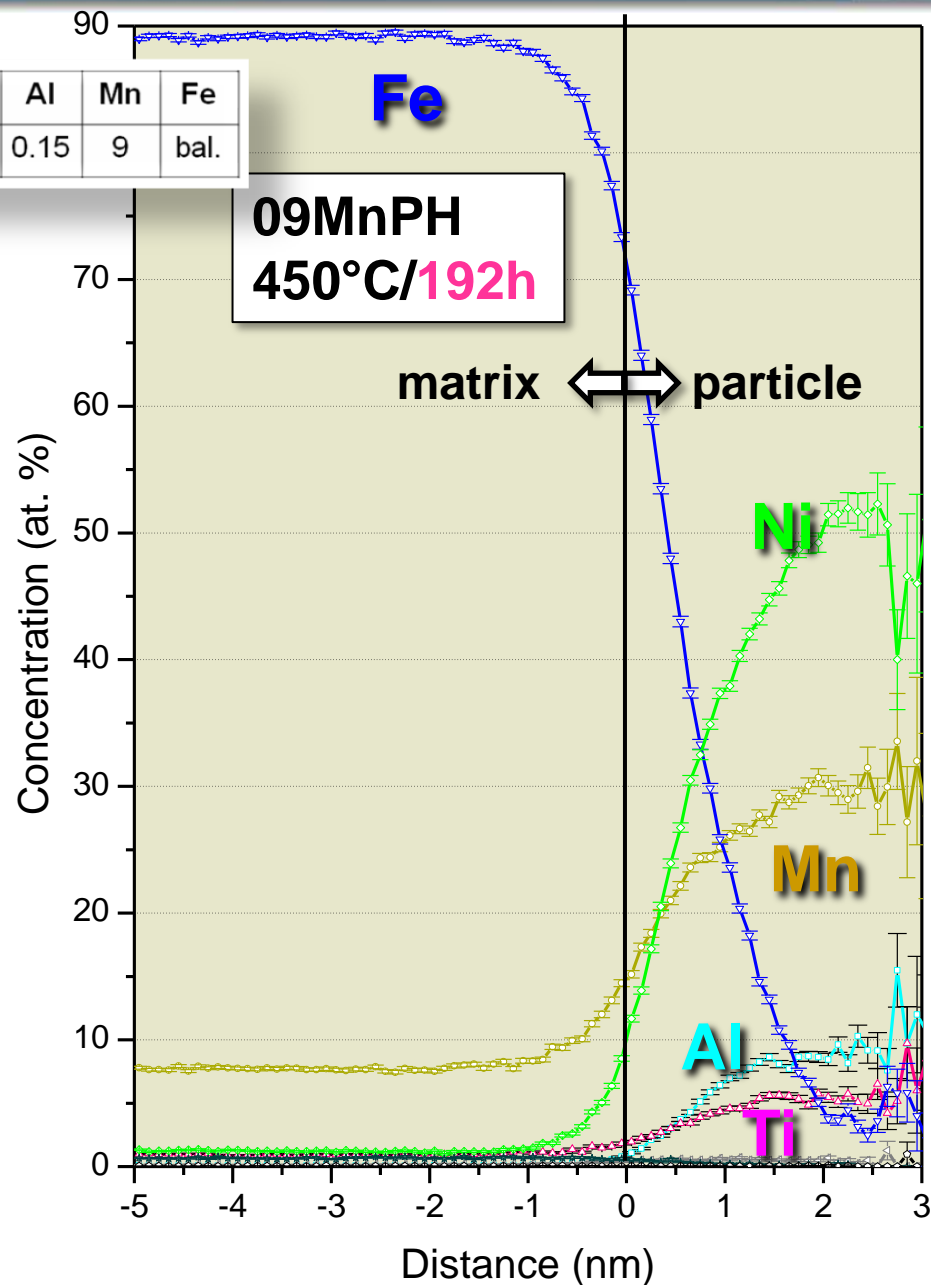
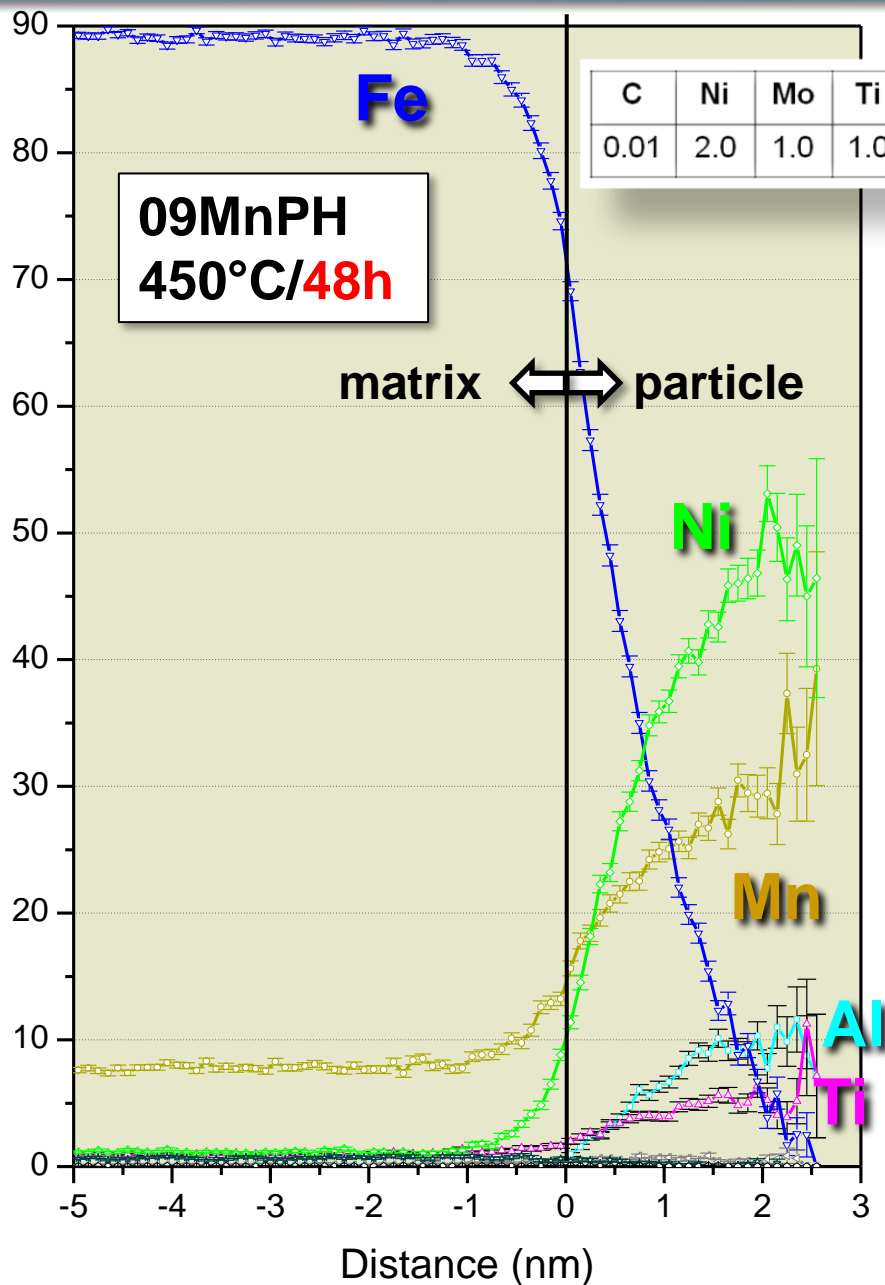
Atom Probe, 12MnPH aged (48h, 450°C)



Mn enrichment in interface ?



09MnPH aging at 450°C, Proxigrams





	at. % in particles	at. % in particles	
Ni	39.99	52.88	
Mn	24.70	32.66	} 47.11
Al	7.02	9.28	
Ti	3.91	5.17	
Fe	23.97	0	

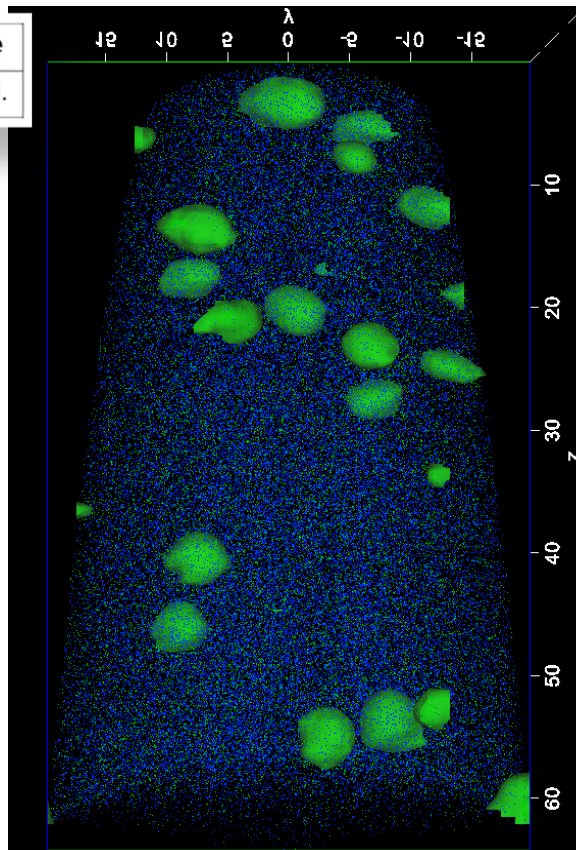
possible: $\text{Ni}_{50}(\text{Mn}, \text{Al}, \text{Ti})_{50}$

C	Ni	Mo	Ti	Al	Mn	Fe
0.01	2.0	1.0	1.0	0.15	9	bal.

Aging time at 450°C	48 hours	192 hours
Volume fraction of particles	1.5%	4.3%
Number density of particles (m ⁻³)	3.6x10 ²⁴	1.9x10 ²⁴
Mean diameter (nm)	4.7 ± 0.7	6.1 ± 2.2

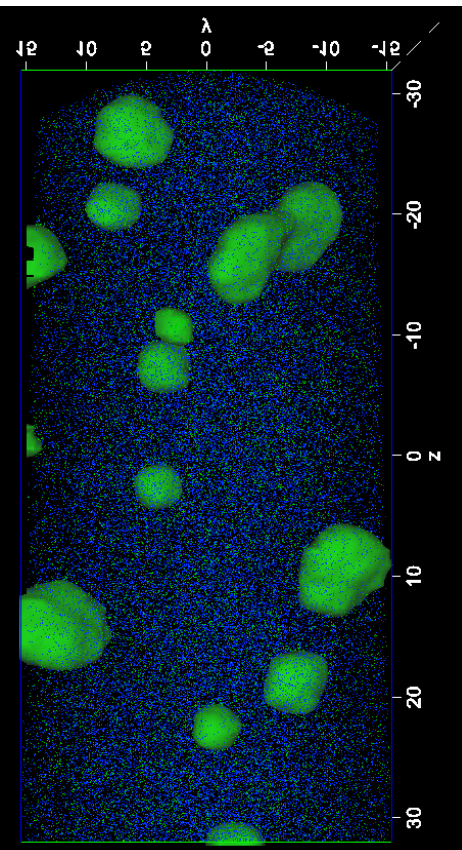
C	Ni	Mo	Ti	Al	Mn	Fe
0.01	2.0	1.0	1.0	0.15	9	bal.

48 hours



Iso-conc. surfaces:
14 at.% Ni
 only **Fe** and **Ni** shown

192 hours



10 nm

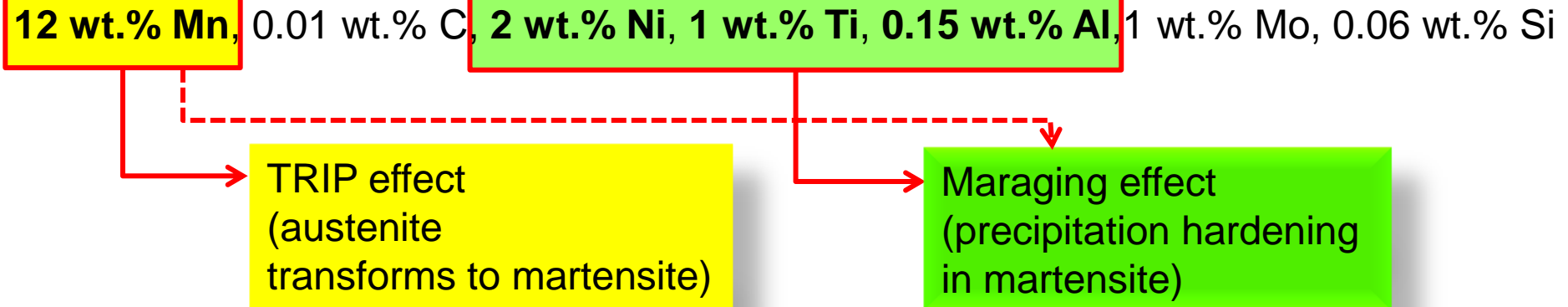


- After aging (48h 450°C) nanosized precipitations in martensite
($\emptyset \sim 5\text{nm}$; volume fraction $\sim 1.5\%$)

- Heusler Alloy (Ni_2MnAl)? B2 or L2_1 ? Coherent ?
Cut by dislocations ?

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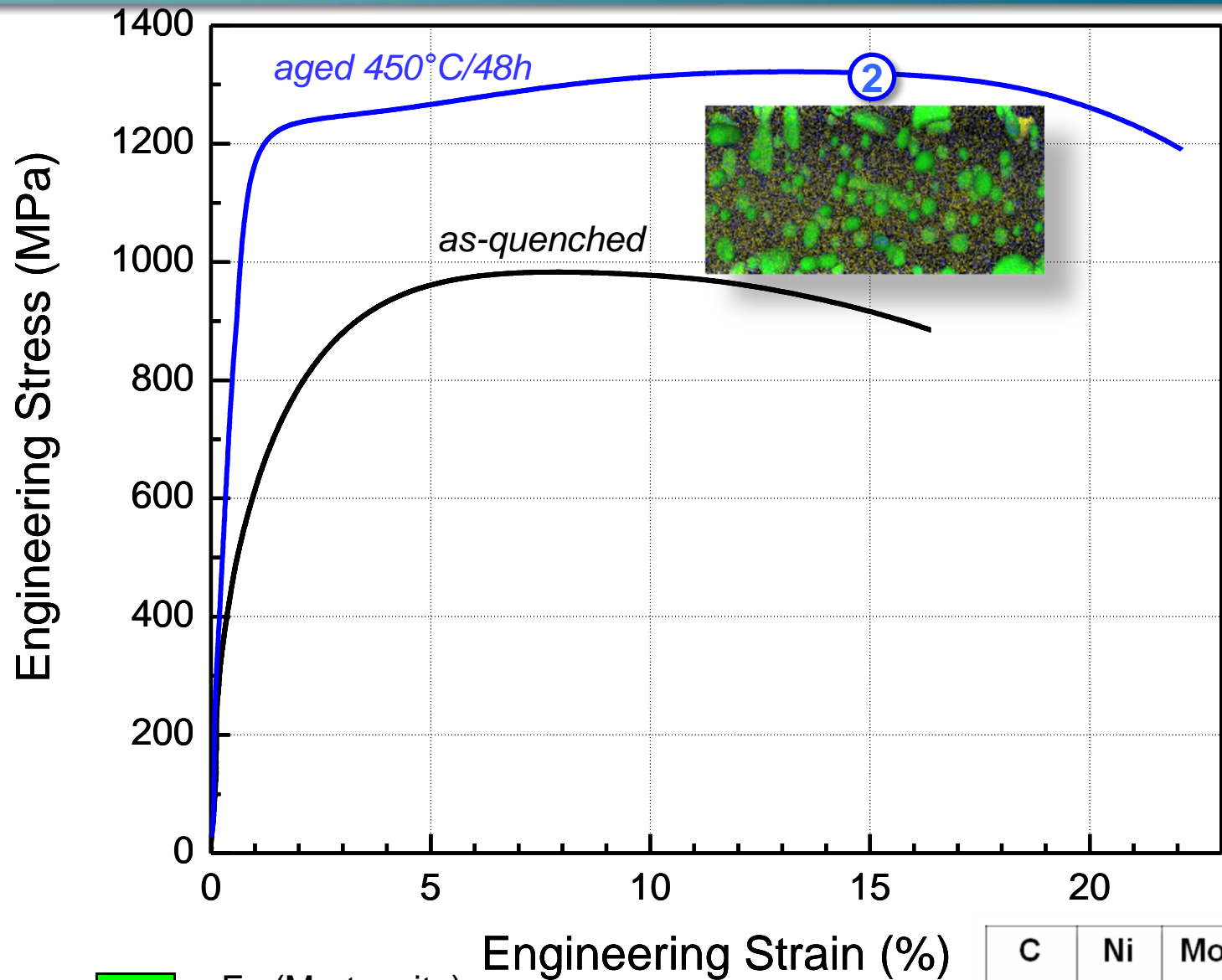
12MnPH



D. Raabe, D. Ponge, O. Dmitrieva, B. Sander, Scripta Mater. 60 (2009) 1141

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Effect of aging on ductility



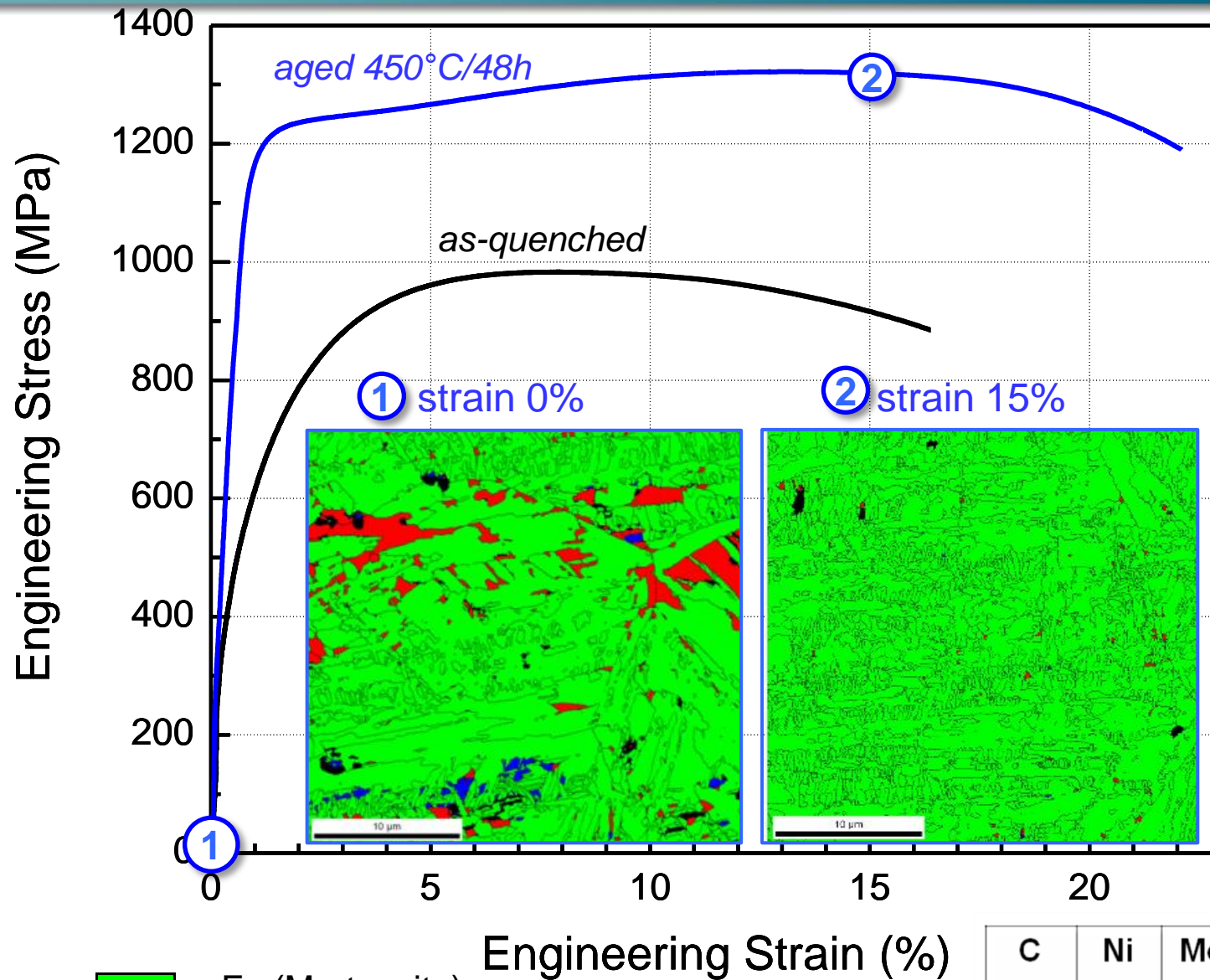
Precipitation hardening

increase of austenite fraction during aging

α -Fe (Martensite)
 γ -Fe (Austenite), vol. fraction 15-20%

C	Ni	Mo	Ti	Al	Mn	Fe
0.01	2.0	1.0	1.0	0.15	12	bal.

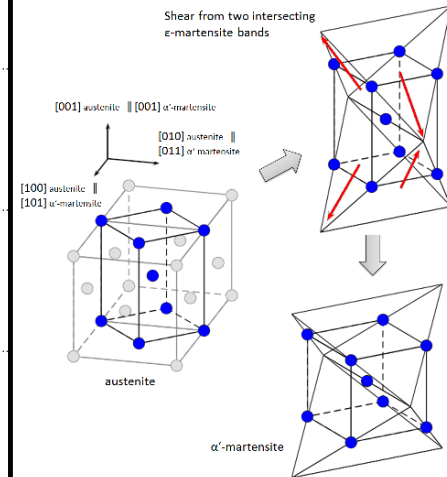
Effect of aging on ductility



Precipitation hardening

↑

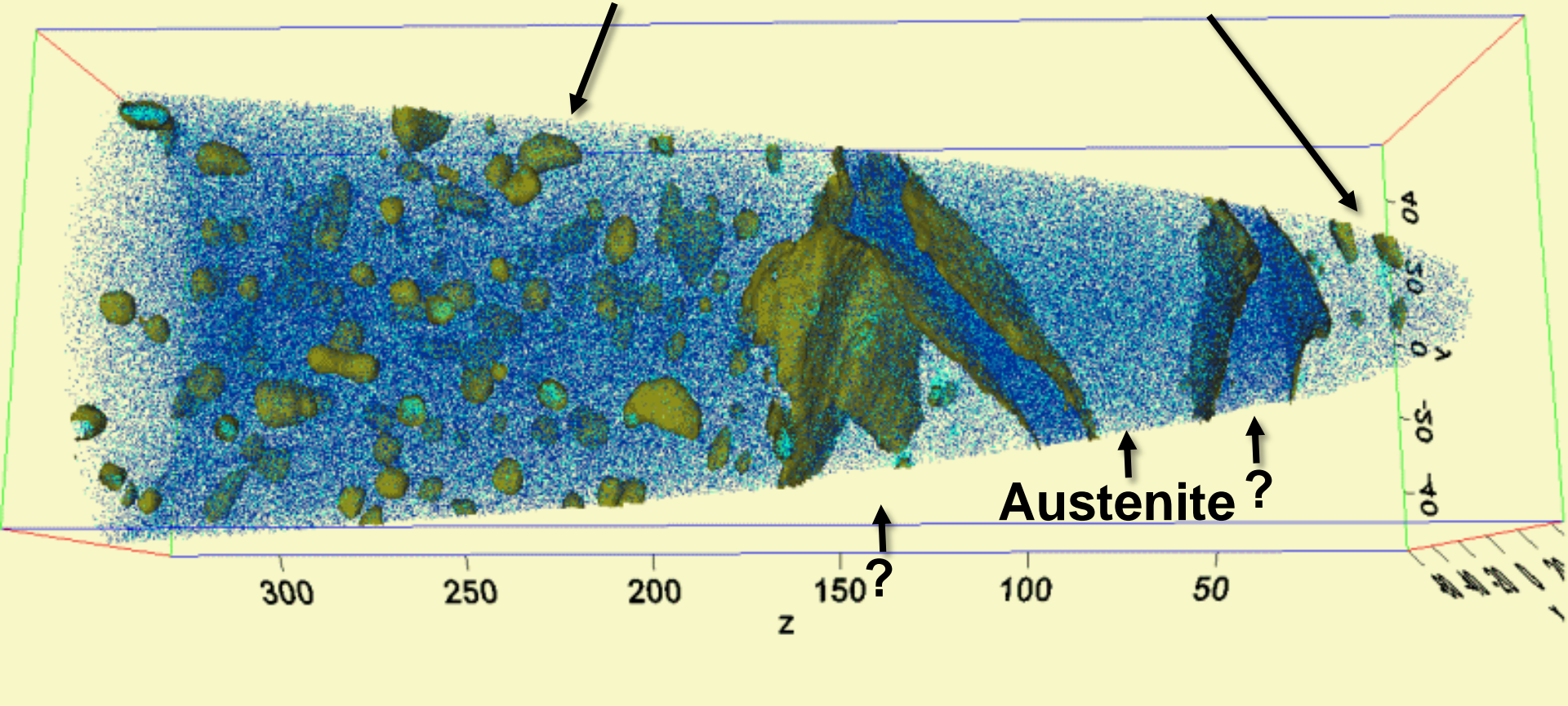
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Martensite decorated by precipitations



Austenite?

Mn atoms, Ni atoms
Mn iso-conc: 18 at.%

C	Ni	Mo	Ti	Al	Mn	Fe
0.01	2.0	1.0	1.0	0.15	12	bal.

70 million ions
Laser mode
(0.4nJ, 54K)

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Design of “Lean Maraging TRIP steel“

Precipitation hardening \Rightarrow Increase strength

Austenite (retained + new) \Rightarrow Increase ductility

- Martensitic Mn-steels ($\sim 0,01 \text{ wt}\% \text{C}$): good ductility
- + controlled amounts of Ni (2 wt%), Al (0.15 wt%), ... increase strength during aging by formation of nanosized precipitations without significant reduction of ductility
- By controlling the austenite stability (here by Mn) martensite can be refined and ductility can be further increased by retained and reverted austenite (TRIP)