



- 1) Design of new Ti-based biomaterials by using ab-initio simulations, FEM, and experiments
- 2) Detailed analysis of an indent

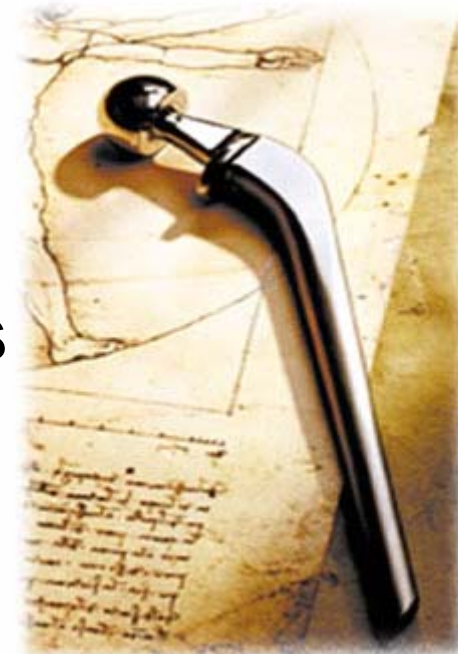


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N. Zaafarani, S. Zaefferer,
J. Neugebauer, D. Raabe
(d.raabe@mpie.de)

lecture, AICES – MIT conference at RWTH Aachen, 08. Oct. 2007

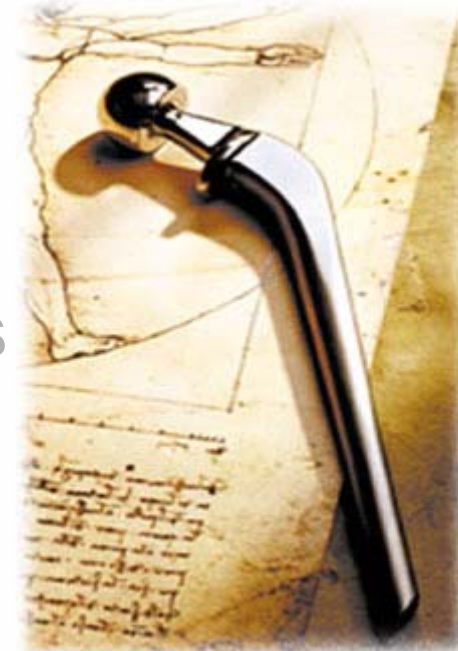


- **Motivation**
- **Theoretical methods**
- **Experimental methods**
- **Results**
- **Conclusions**





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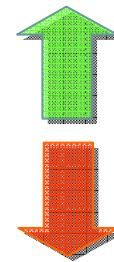


Motivation

- **Implant requirements:**

corrosion stability, fatigue resistance, strength-to-weight ratio, ductility, wear resistance

elastic modulus, cytotoxicity, allergic reactions



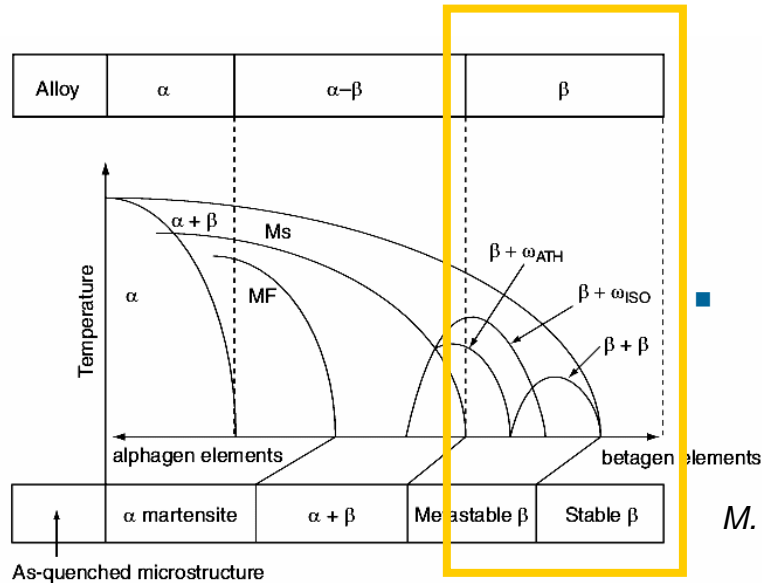
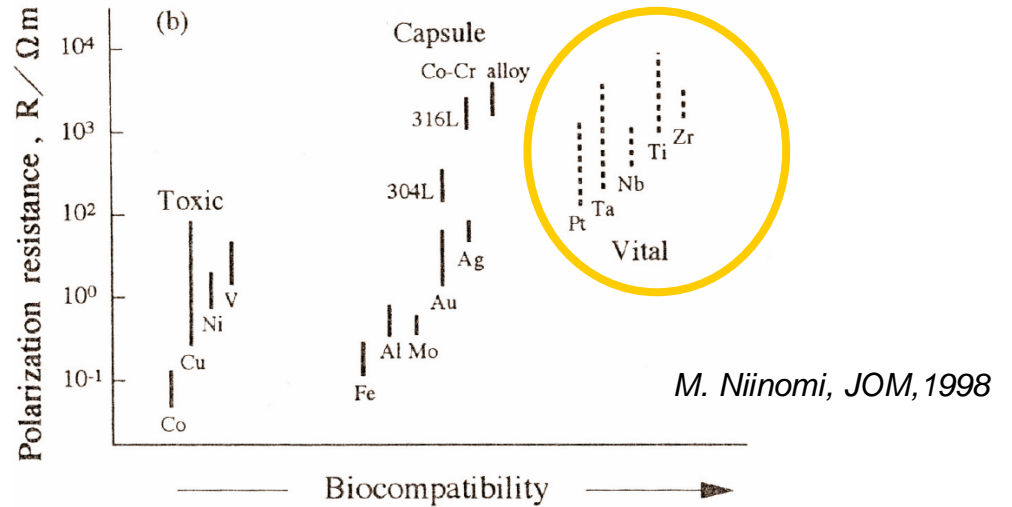
Aims

- **Stiffness closer to elastic modulus of human bone**
- **Stabilization of β -Ti**
- **Use only bio-compatible elements**

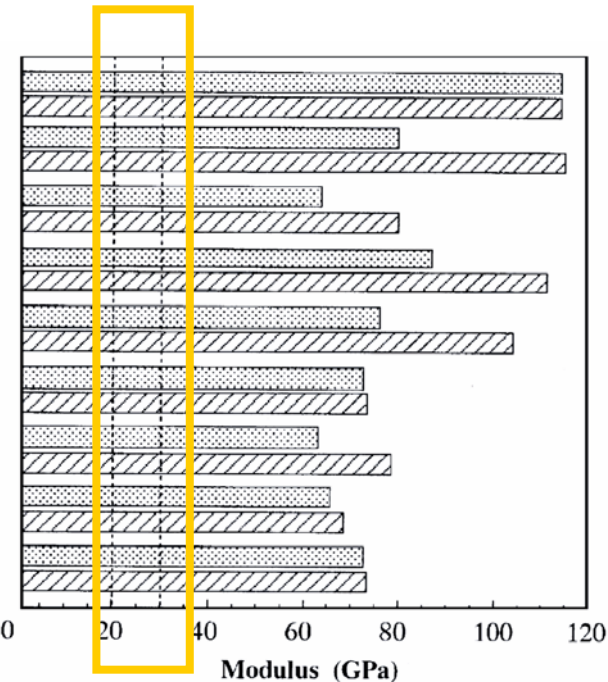
Boundary Conditions Considered – Some Numbers



- non-toxic elements



- stable β -phase



- reduced elastic stiffness

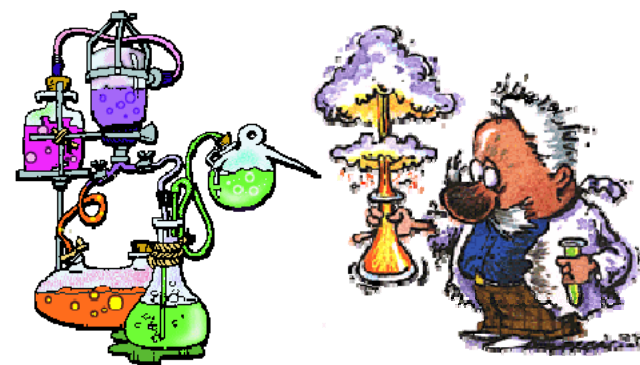
Challenge and Scientific Approach



- Theory – driven guidance in constrained alloy design (non-toxic; β -phase; reduced stiffness); replace phenomenological rules
- 2 binary alloy systems (Ti-Nb, Ti-Mo) and 2 engineering alloys (Ti-35wt.%Nb-7wt.%Zr-5wt.%Ta and a Ti-20wt.%Mo-7wt.%Zr-5wt.%Ta)
- Combination of ab-initio simulations and experiments

Density functional theory (DFT),
generalized gradient
approximation (GGA),
configurational and vibration
entropy

Casting, homogenization,
rolling, heat treatment,
recrystallization, grain
growth, microstructure,
mechanics





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- Free energy $F(x,c,T) = U - T \cdot S$
- U: density functional theory (DFT), generalized gradient approximation (GGA)
- S: Configurational (mixing) entropy
- Ti-Mo and Ti-Nb binary systems
- Elastic modulus calculation
- Polycrystal homogenization theory
- Crystal plasticity finite element method

Details: Plane wave pseudopotential approach (VASP), plane wave cutoff energy: 170 eV, 8×8×8 Monkhorst mesh to sample Brillouin zone, relaxation until cell stress free, supercells of 2×2×2 elementary cubic unit cells with a total of 16 atoms, variety of alloys by replacing Ti by either Nb or Mo (from 6.25 %, 1 Nb/Mo atom in a 16 atom supercell), variation of local arrangements: 48 bcc and 28 hcp configurations, further details on poster



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- Use ab-initio results as guideline for alloy composition
- 2 binary systems (Ti-Nb, Ti-Mo) and 2 engineering alloys (Ti-35wt.%Nb-7wt.%Zr-5wt.%Ta and a Ti-20wt.%Mo-7wt.%Zr-5wt.%Ta)
- Thermomechanical processing: electric arc furnace (Ar), 4 × repeated remelting and solidification, cast into copper mold (60mm×32,6mm×10mm), homogenization (1200°C), hot rolling (750°C), recrystallization treatment
- Characterization: OM, SEM, EBSD, EDX, XRD, ultrasonic resonance frequency, mechanical testing

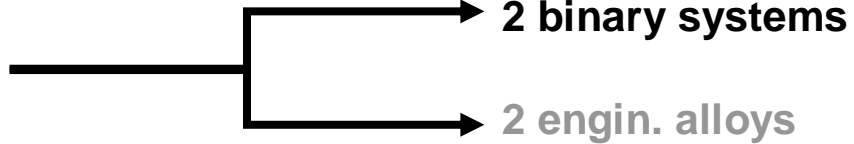
Details: furnace evacuated and flooded with Ar at 300 mbar; water cooled copper crucible; arc temperature 3000°C; melt at peak temperature 1830-1850°C; intense stirring; 30-60s melting time; solidification+tilting+remeltinged 4 times; all heat treatments under Ar or vacuum; SEM, EBDS, EDX: JEOL / ZEISS HR-SEM; XRD: Co-radiation



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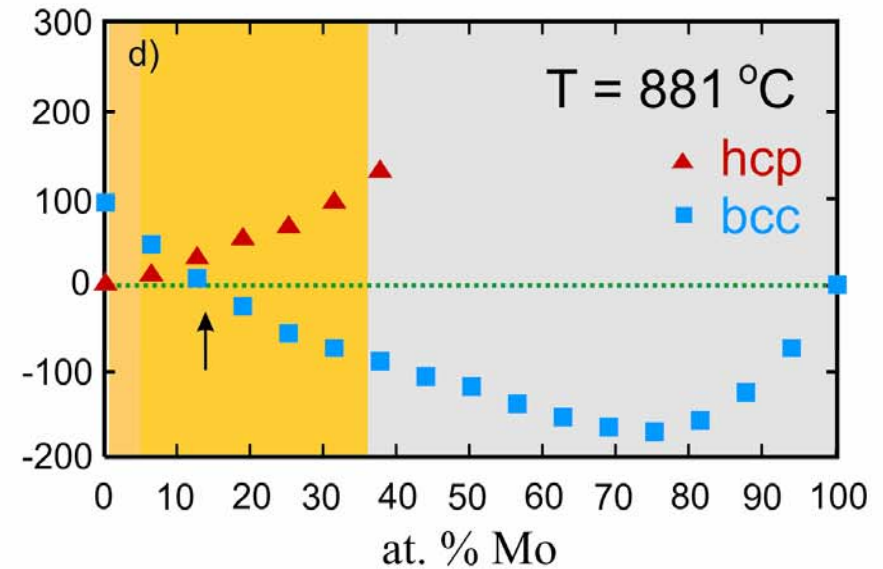
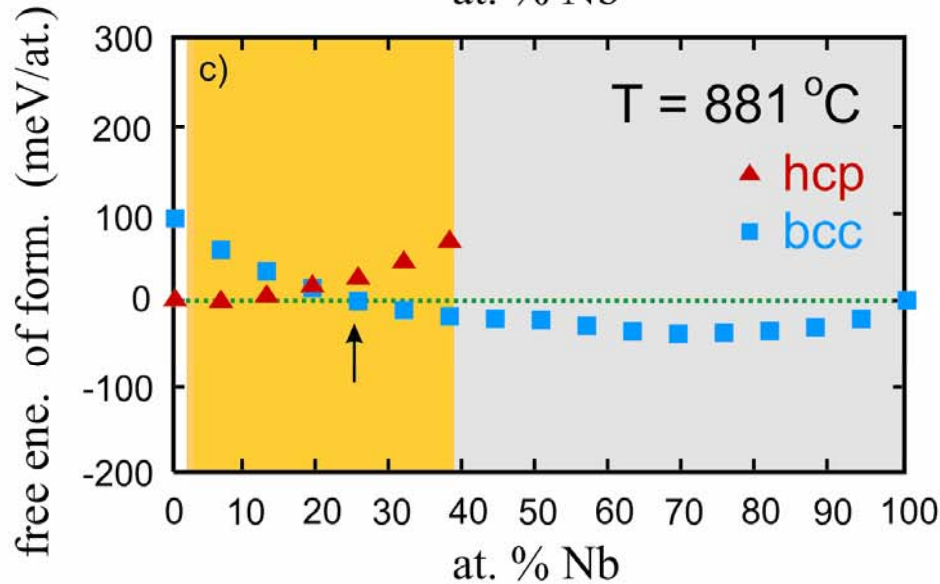
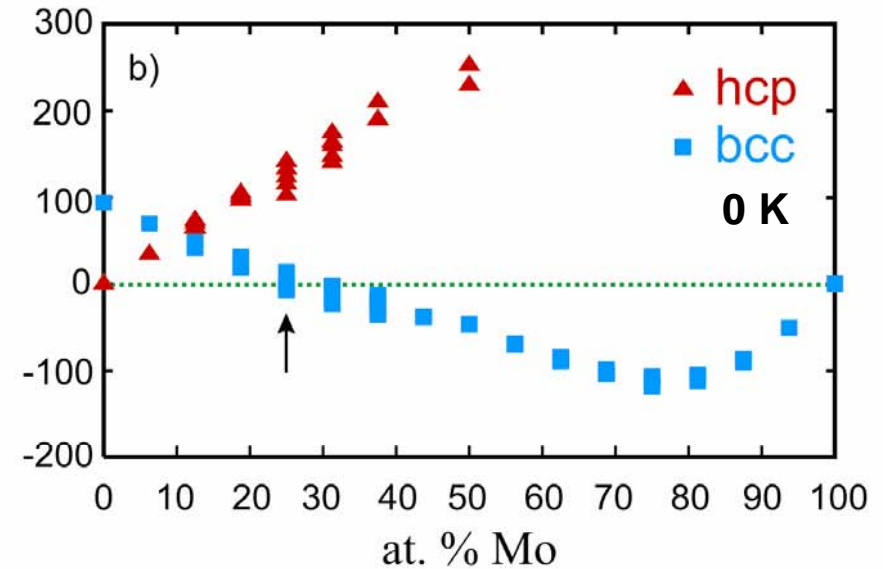
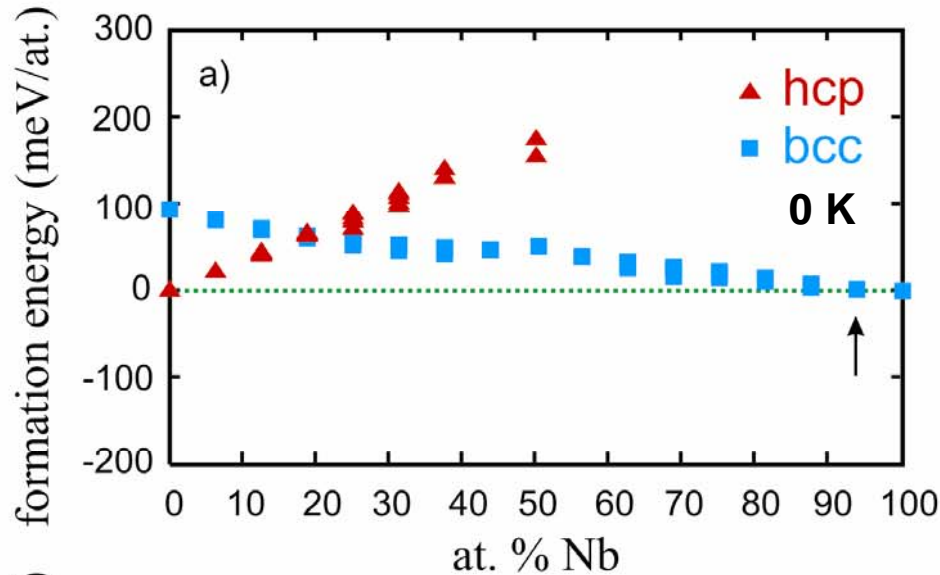




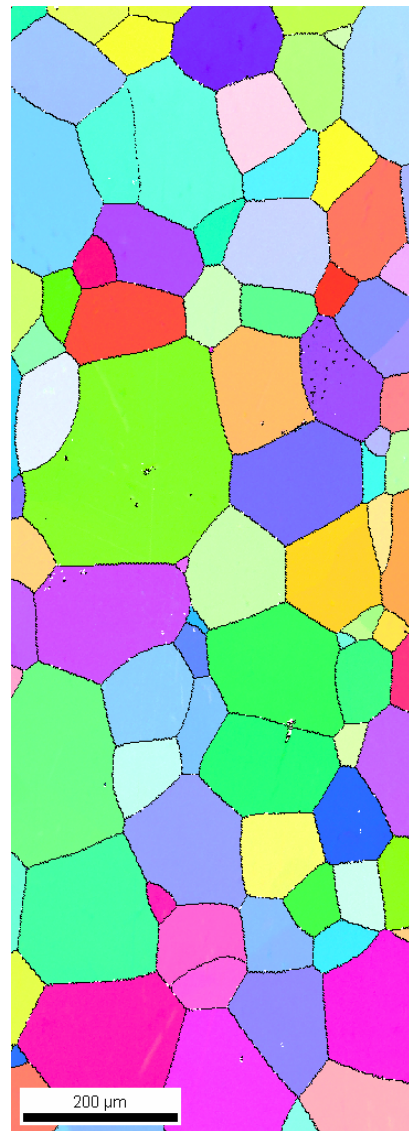
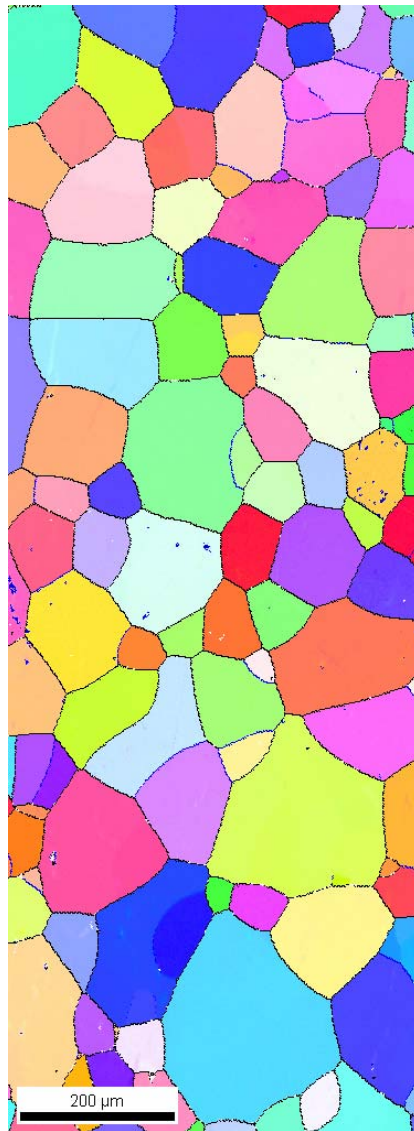
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graph LR; Results[Results] --> Binary[2 binary systems]; Results --> Alloys[2 engin. alloys];
```
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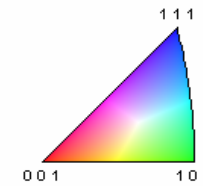
Results from theory – binary alloys



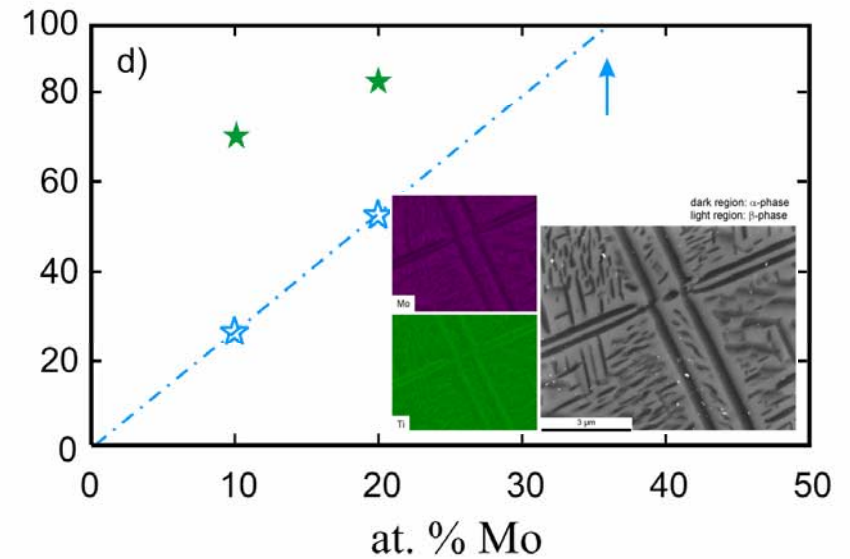
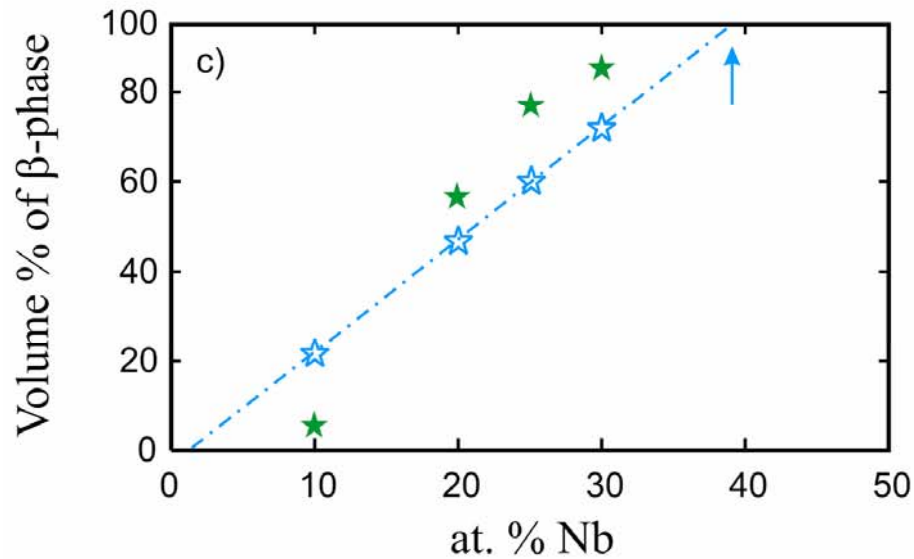
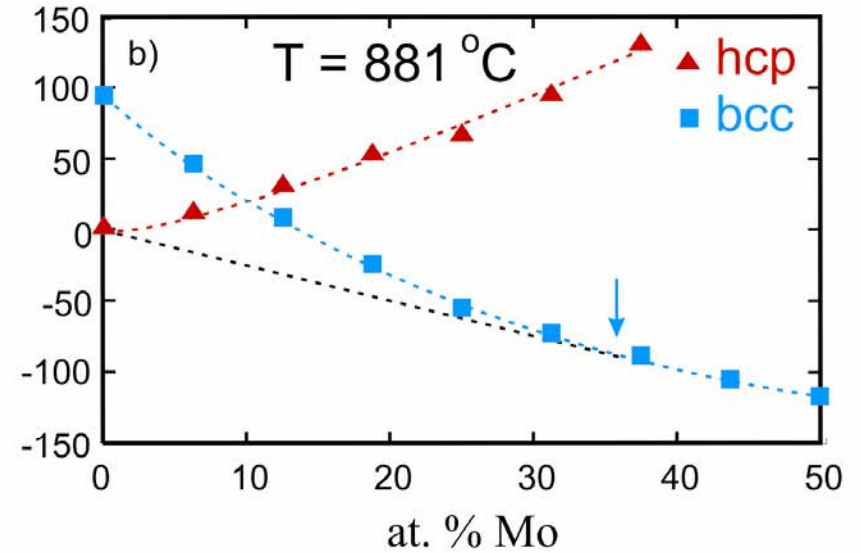
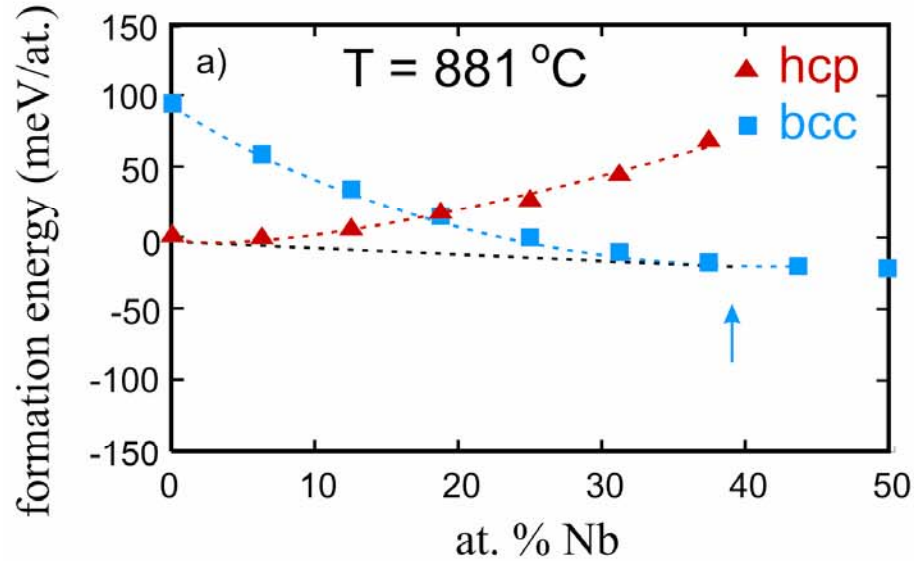
Experimental – results – microstructure, EBSD



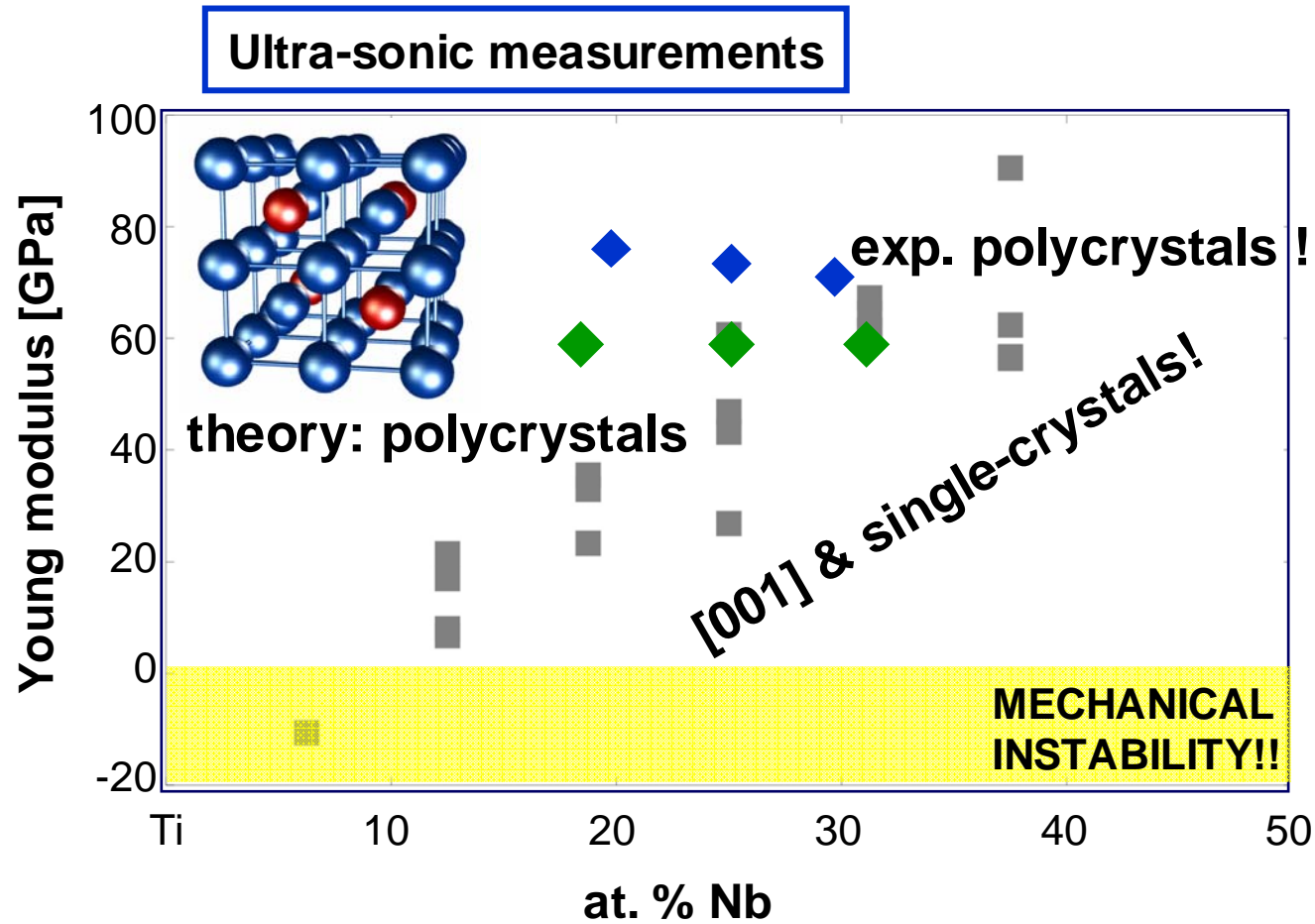
- **Ti-30at%Nb
(as cast)**



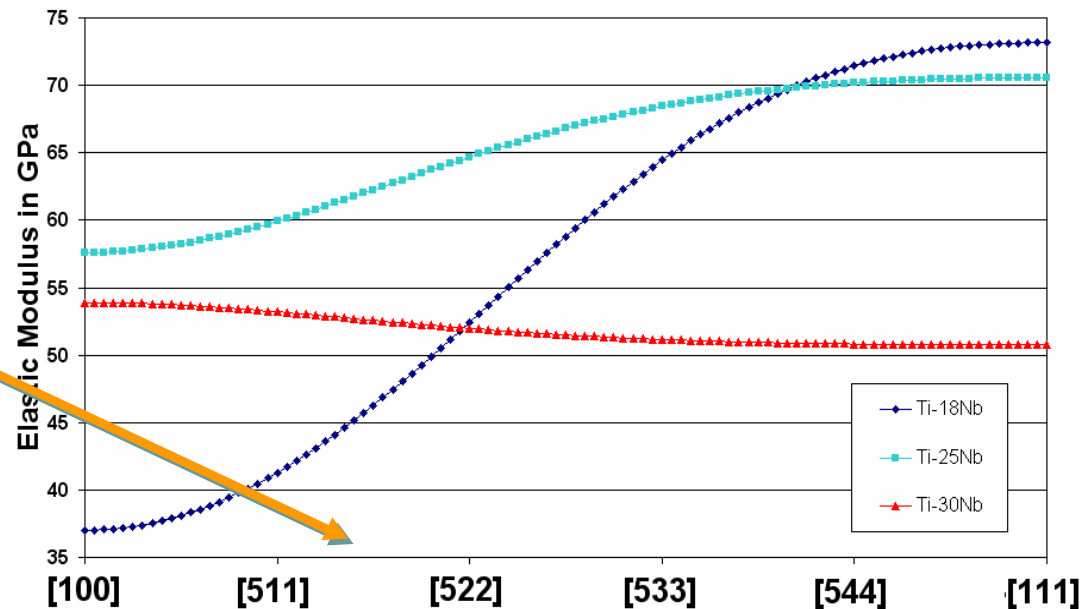
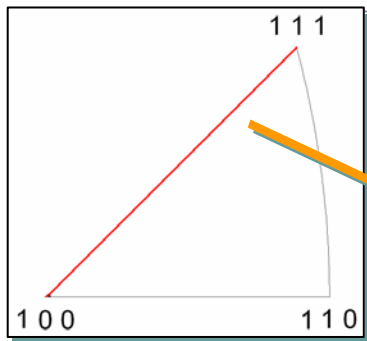
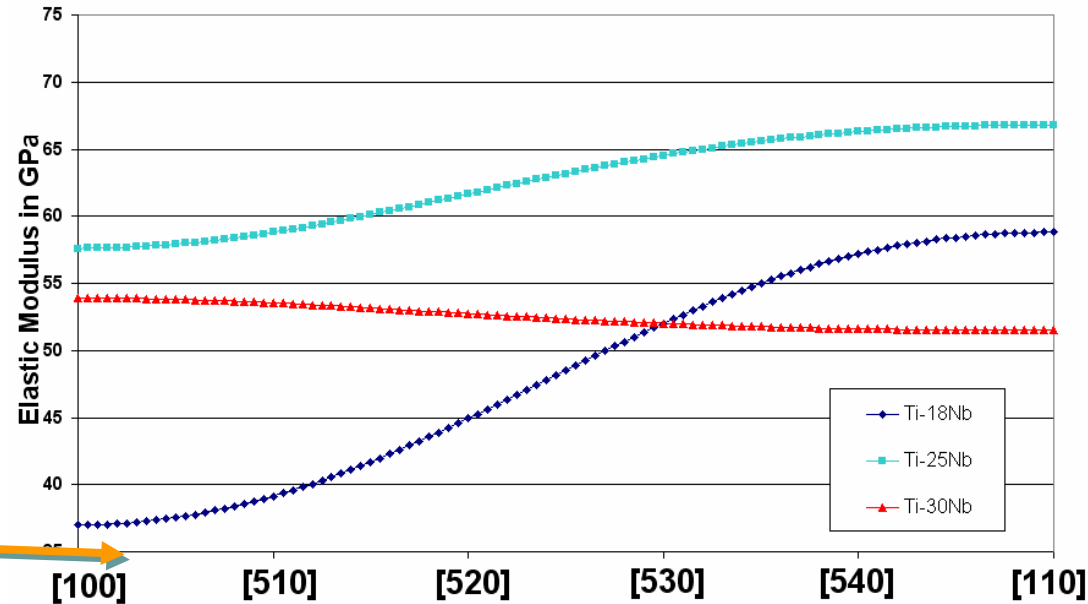
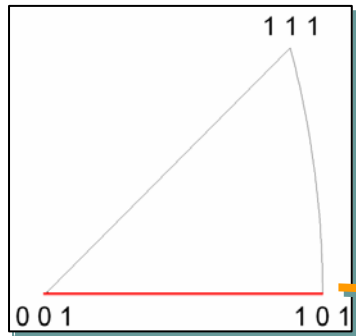
Ab initio inspired alloy design



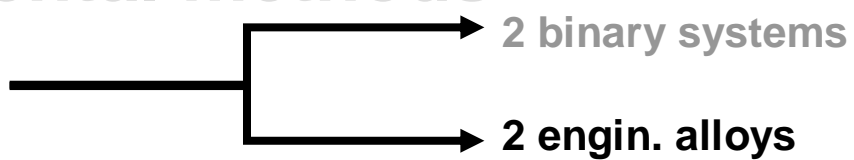
Results, theory and experiment – elastic modulus



Ab initio inspired alloy design: tensor (an)isotropy



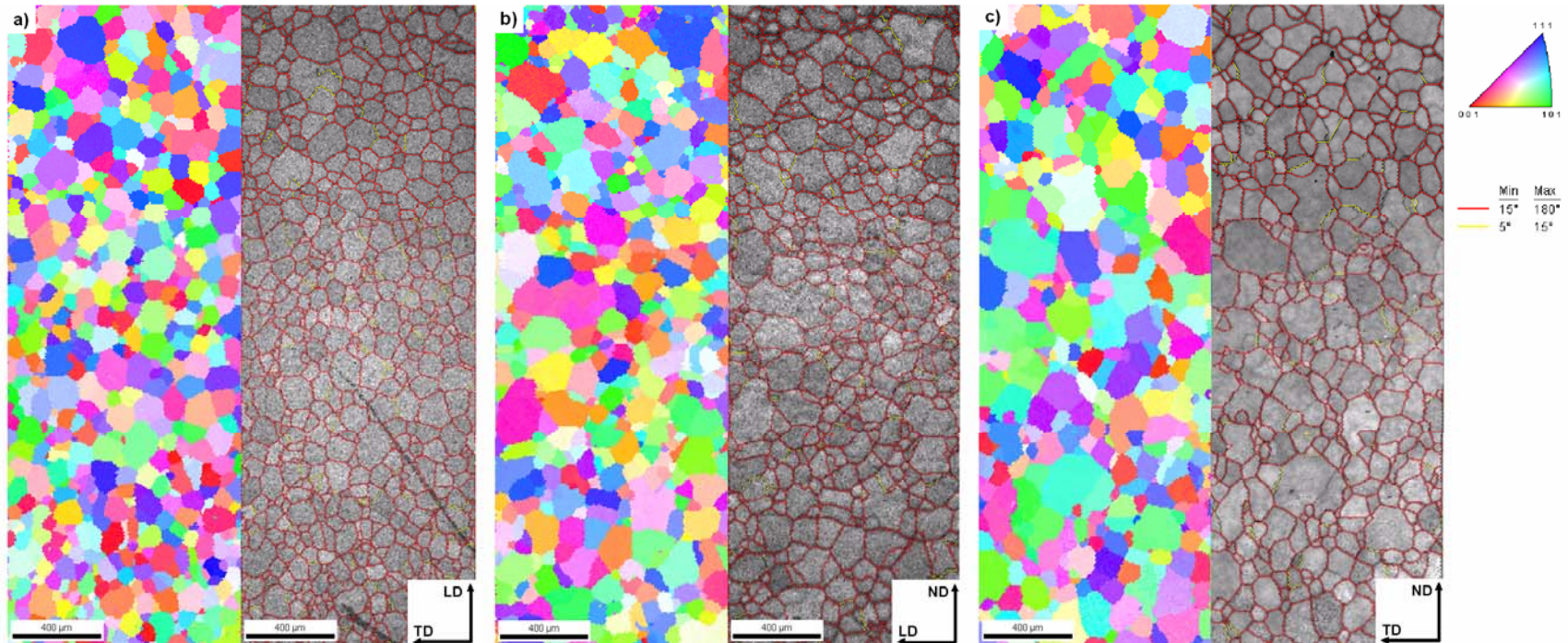


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graph LR; Results[Results] --> Binary[2 binary systems]; Results --> Alloys[2 engin. alloys];
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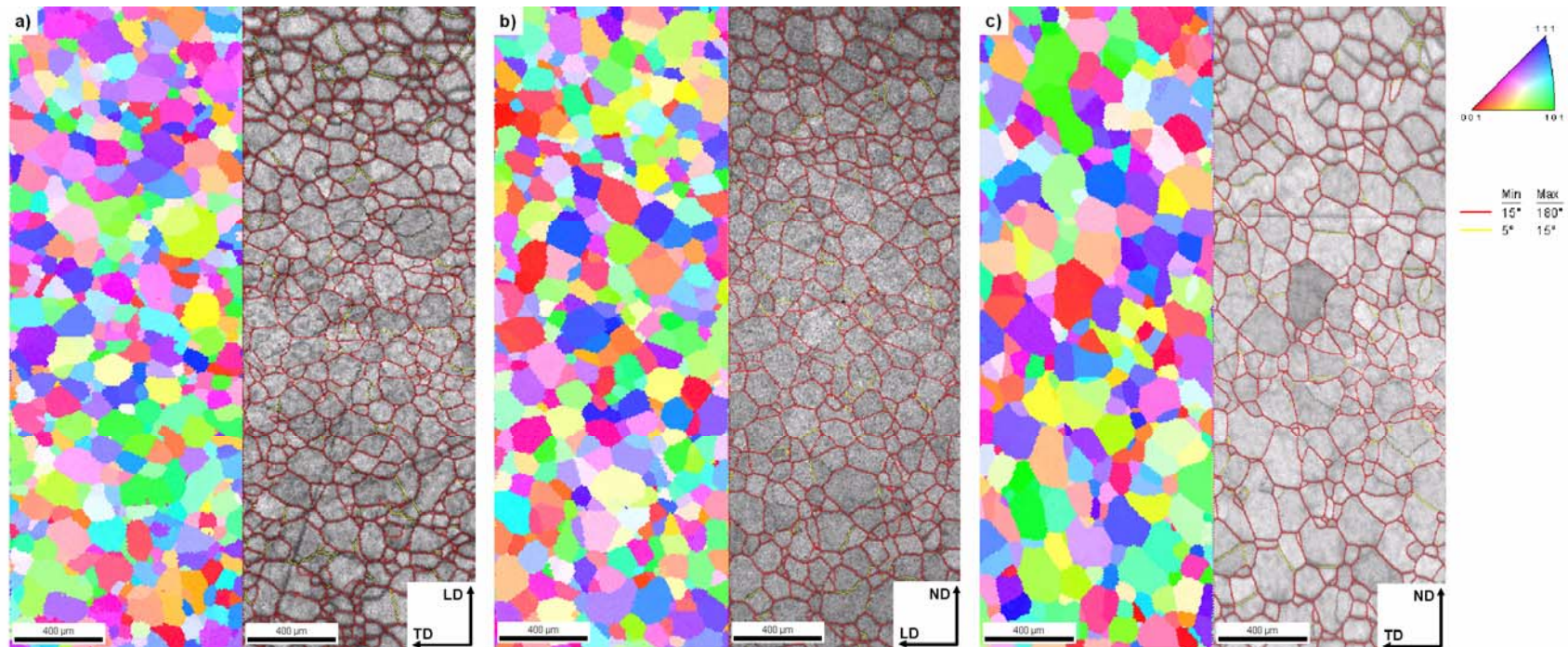
- **Ti-20wt.%Mo-7wt.%Zr-5wt.%Ta – as cast**



Experimental – results – microstructure Nb



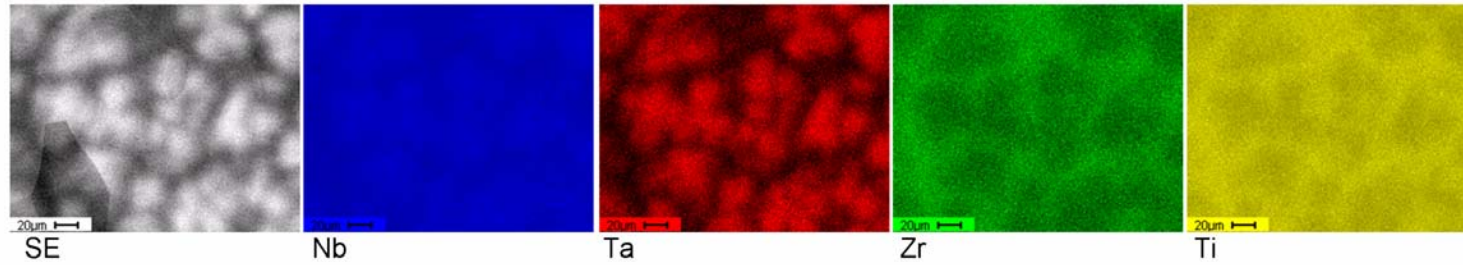
- **Ti-35wt.%Nb-7wt.%Zr-5wt.%Ta - as cast**



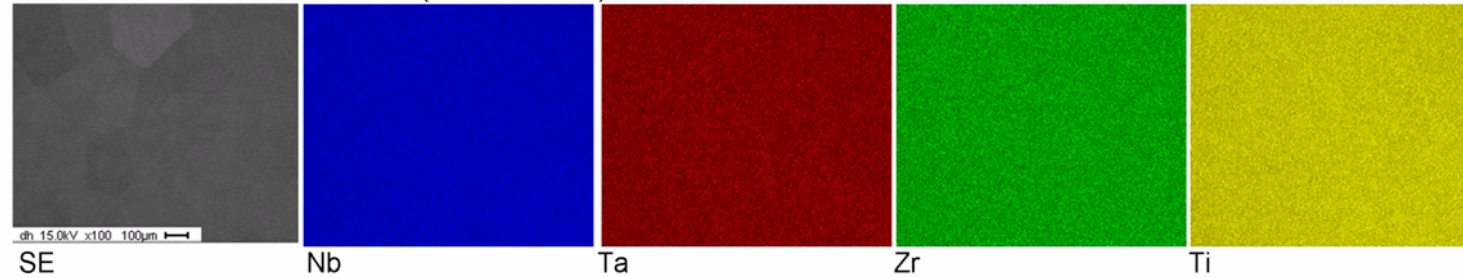
Experimental – Results – Microstructure, Segregation



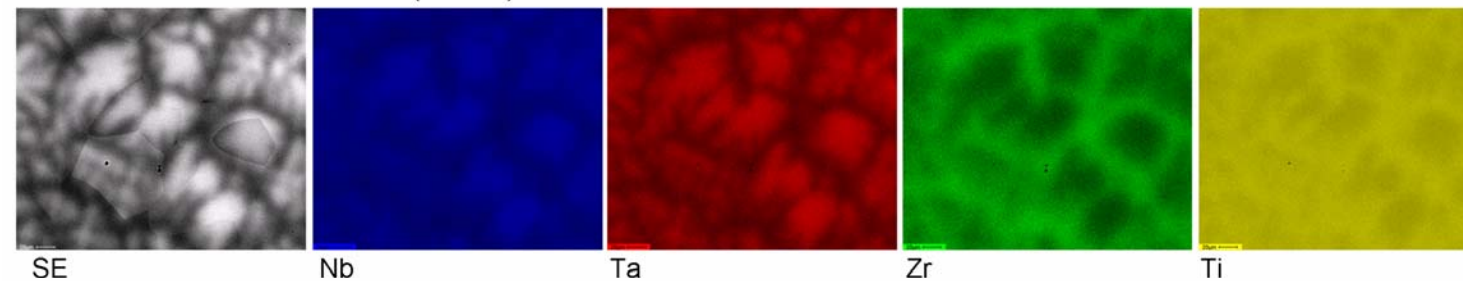
Ti-35wt.%Nb-7wt.%Zr-5wt.%Ta (as cast)



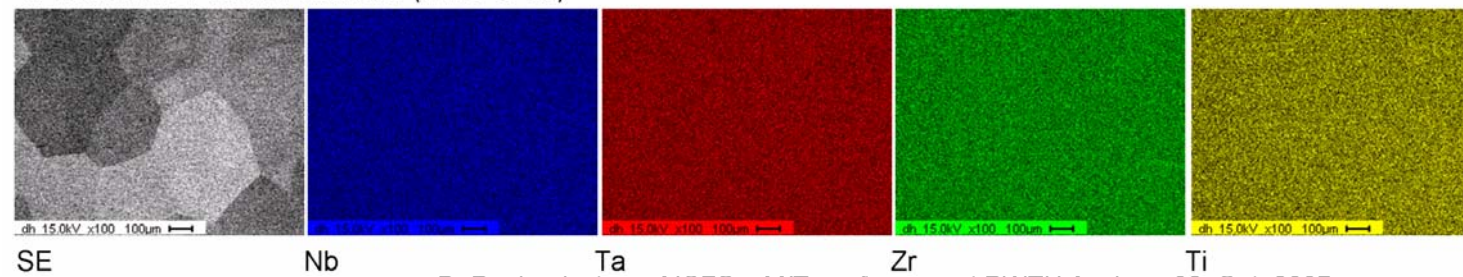
Ti-35wt.%Nb-7wt.%Zr-5wt.%Ta (1200°C for 4h)



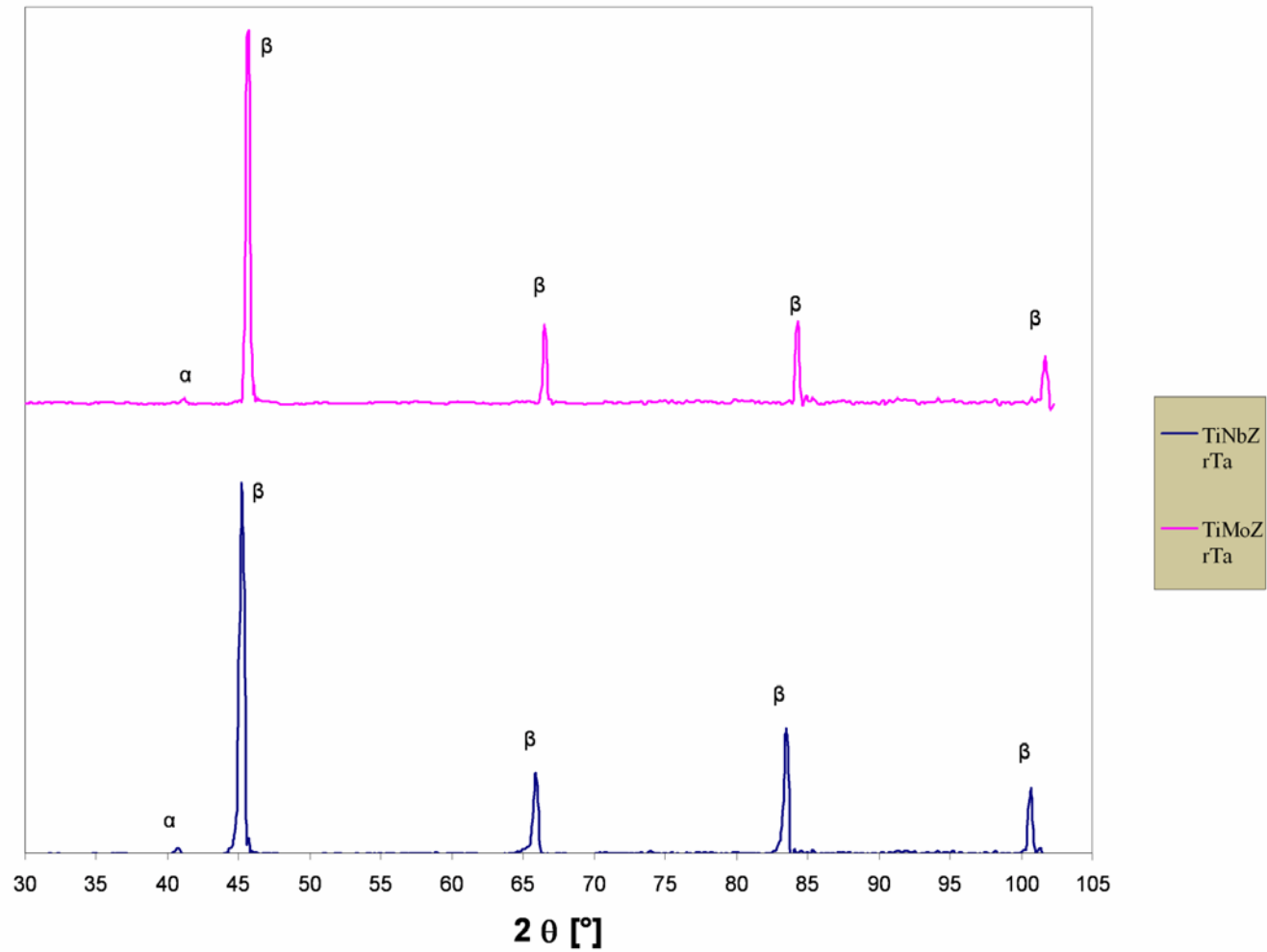
Ti-20wt.%Mo-7wt.%Zr-5wt.%Ta (as cast)



Ti-20wt.%Mo-7wt.%Zr-5wt.%Ta (1200°C 3h)



Experimental – Results – Phases

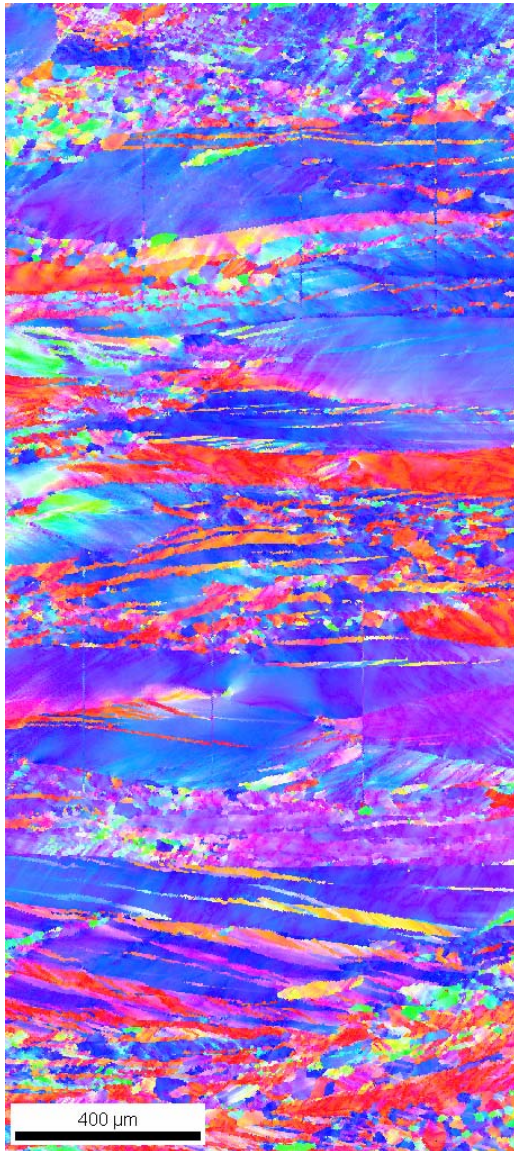


Experimental – results – microstructure

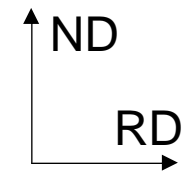
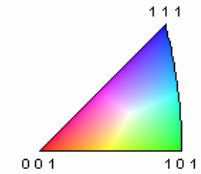
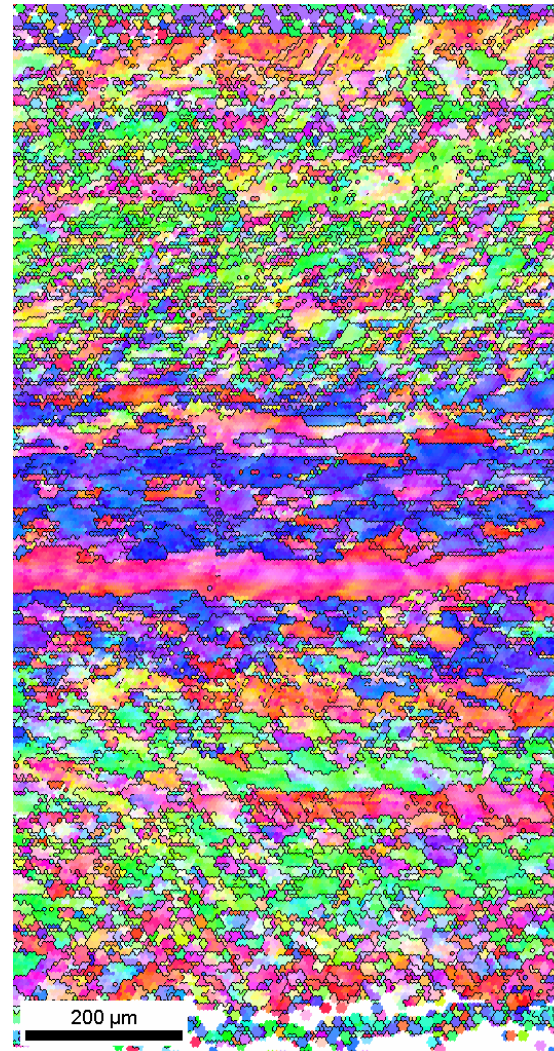


- Ti-35wt.%Nb-7wt.%-Zr-5wt.%-Ta (rolled at 750°C)

70%



90%





- **Ti: 114.7 GPa**
- **Ti-20wt.%Mo-7wt.%Zr-5wt.%Ta: 81.5 GPa**
- **Ti-35wt.%Nb-7wt.%Zr-5wt.%Ta: 59.9 GPa**



- **ab – initio prediction works (TD, modulus)**
- **Good fit between experiments and theory**
- **Next generation alloy design**
- **Ti, Steels, Mg, Chitin**

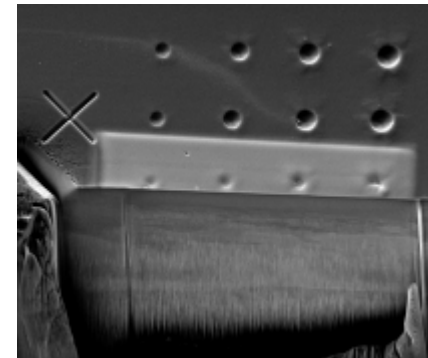
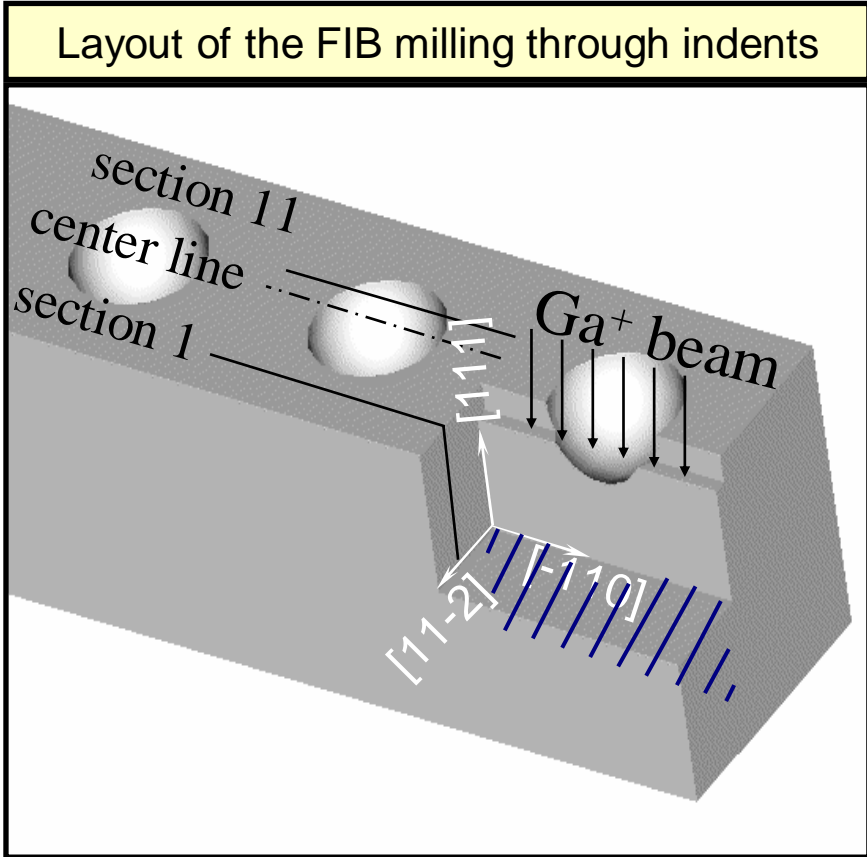
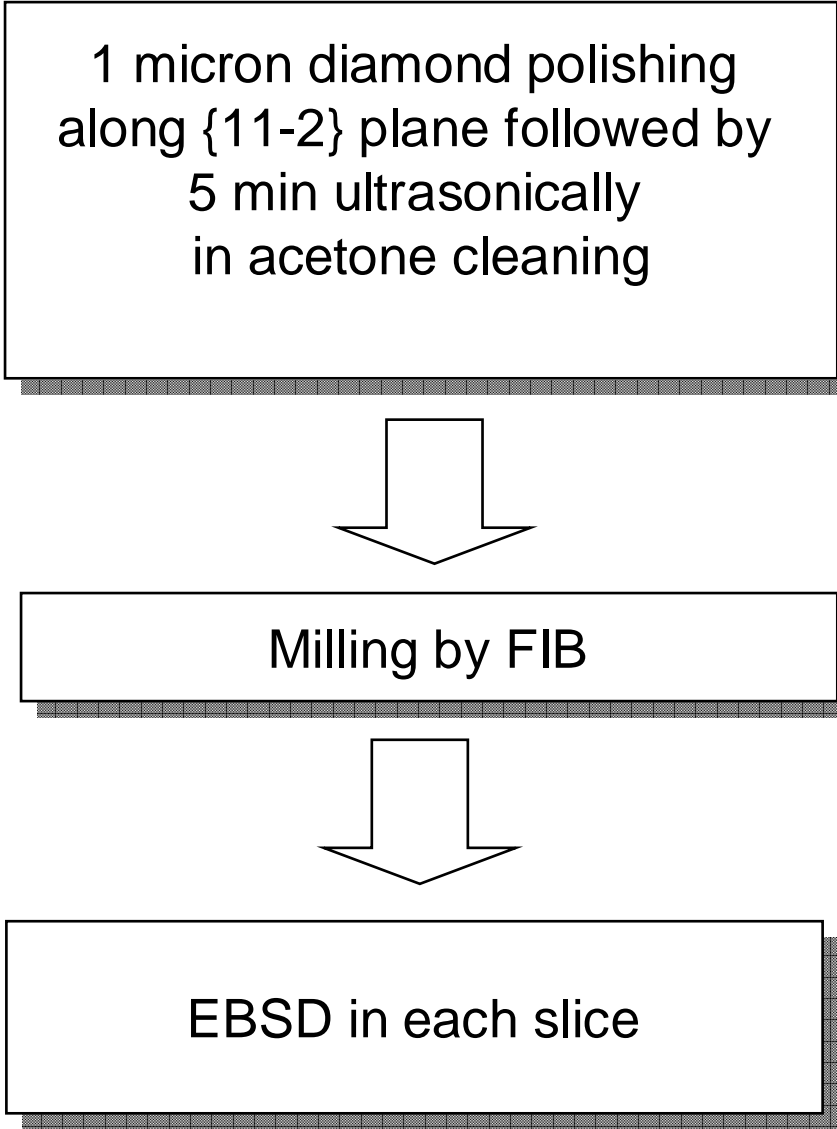




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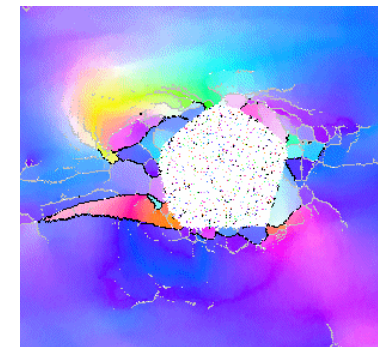
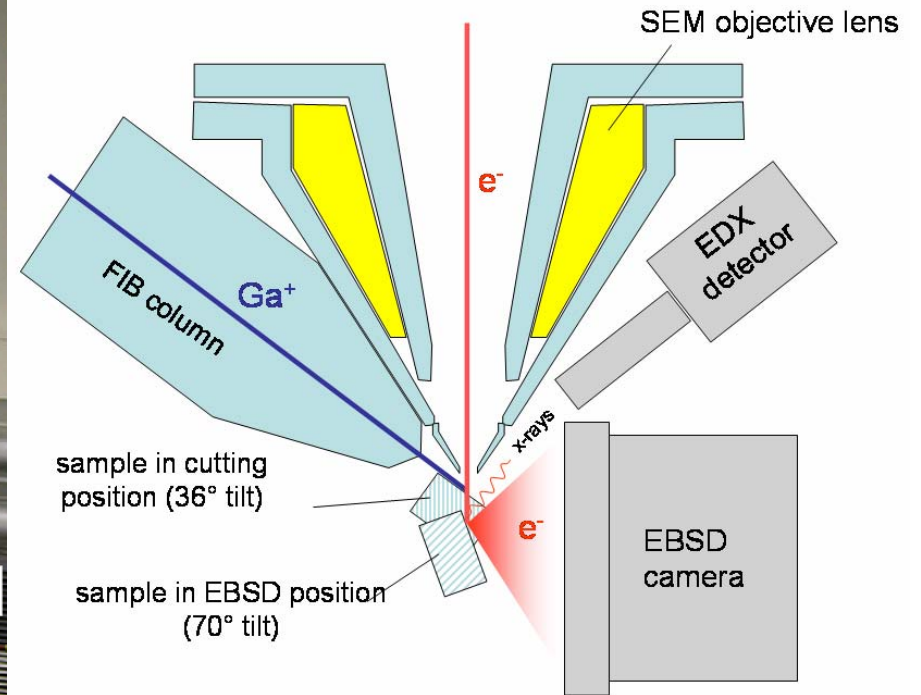
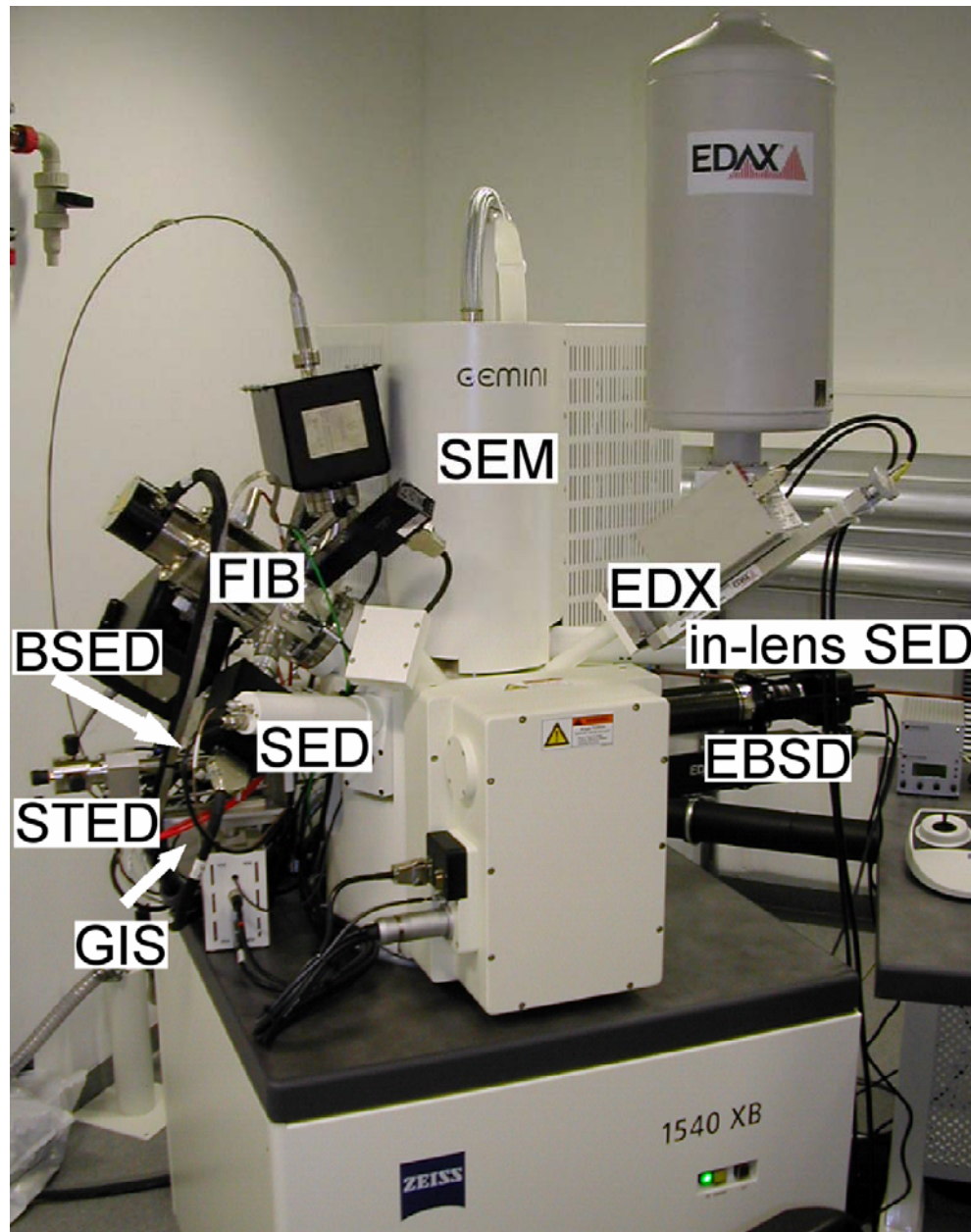


Experimental Procedure





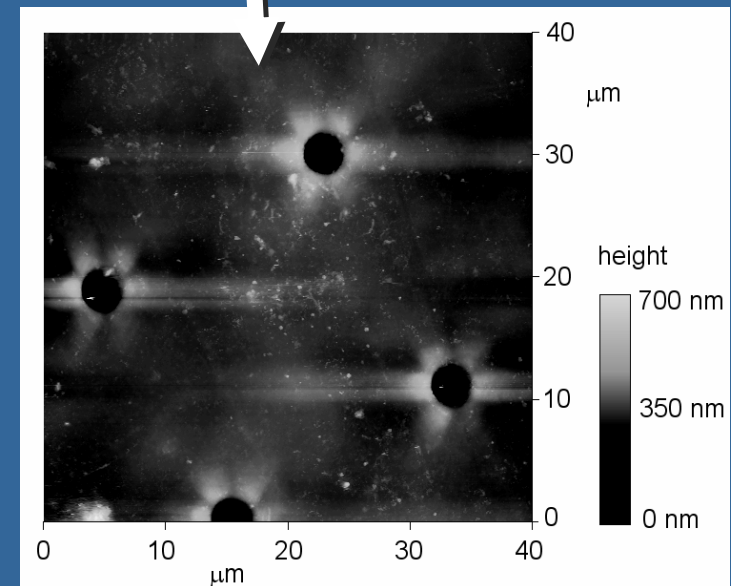
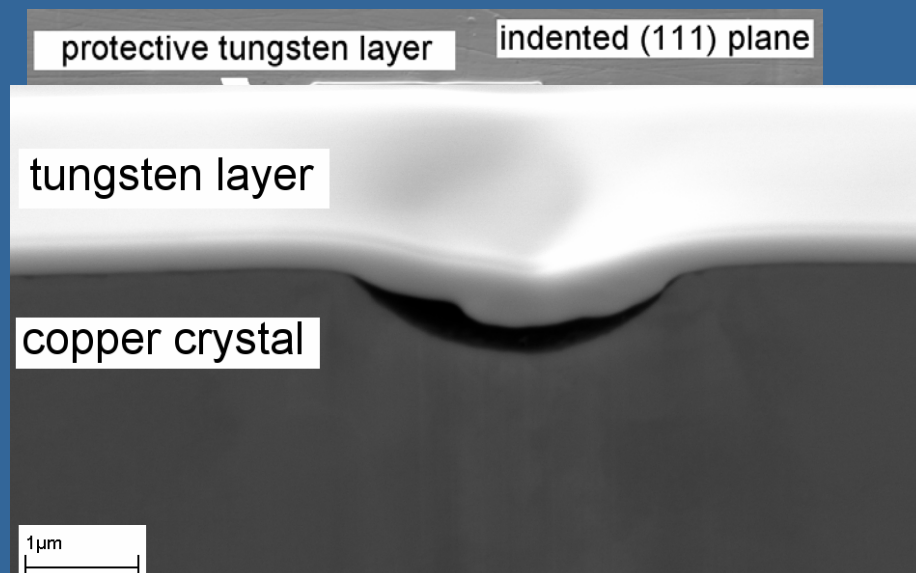
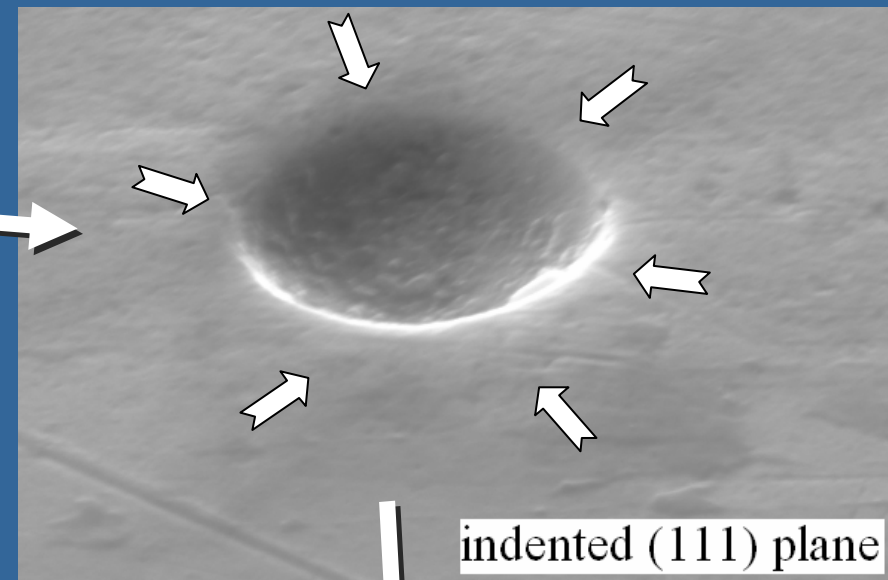
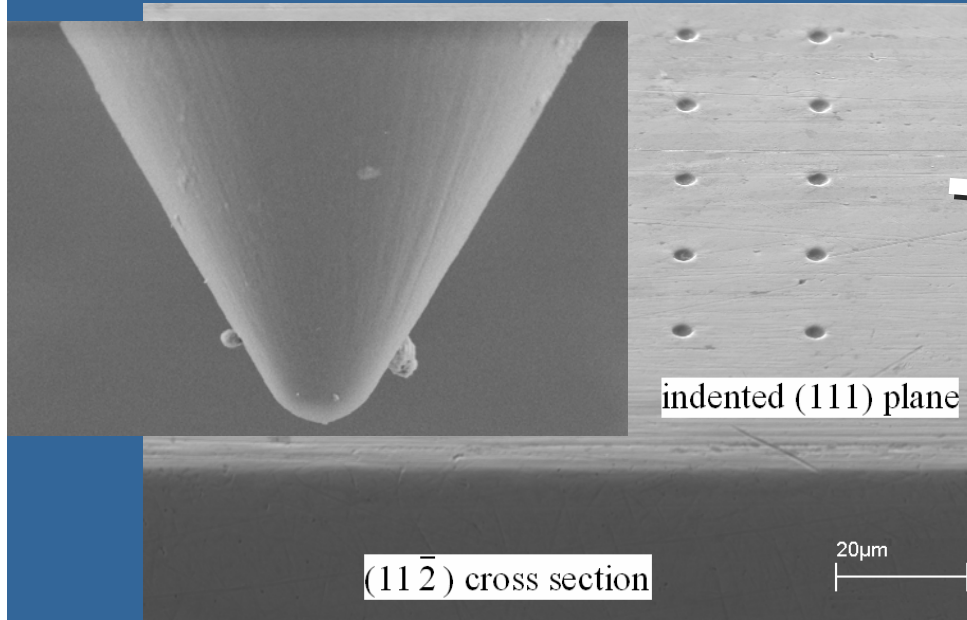
3D EBSD - electron orientation microscopy





Nanoindentation - 3D

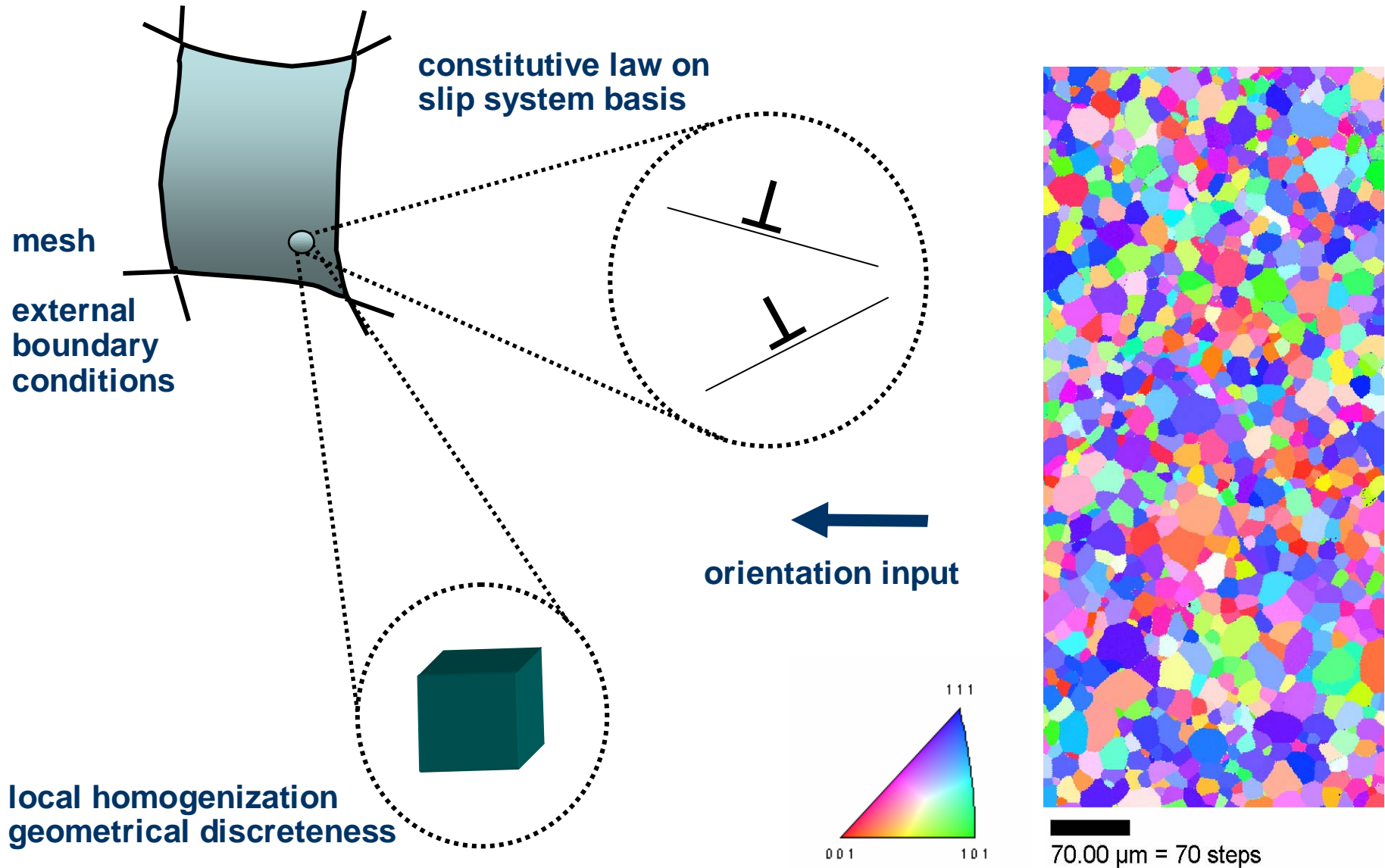
10 mN, no holding time, rate: 1.82 mN/s





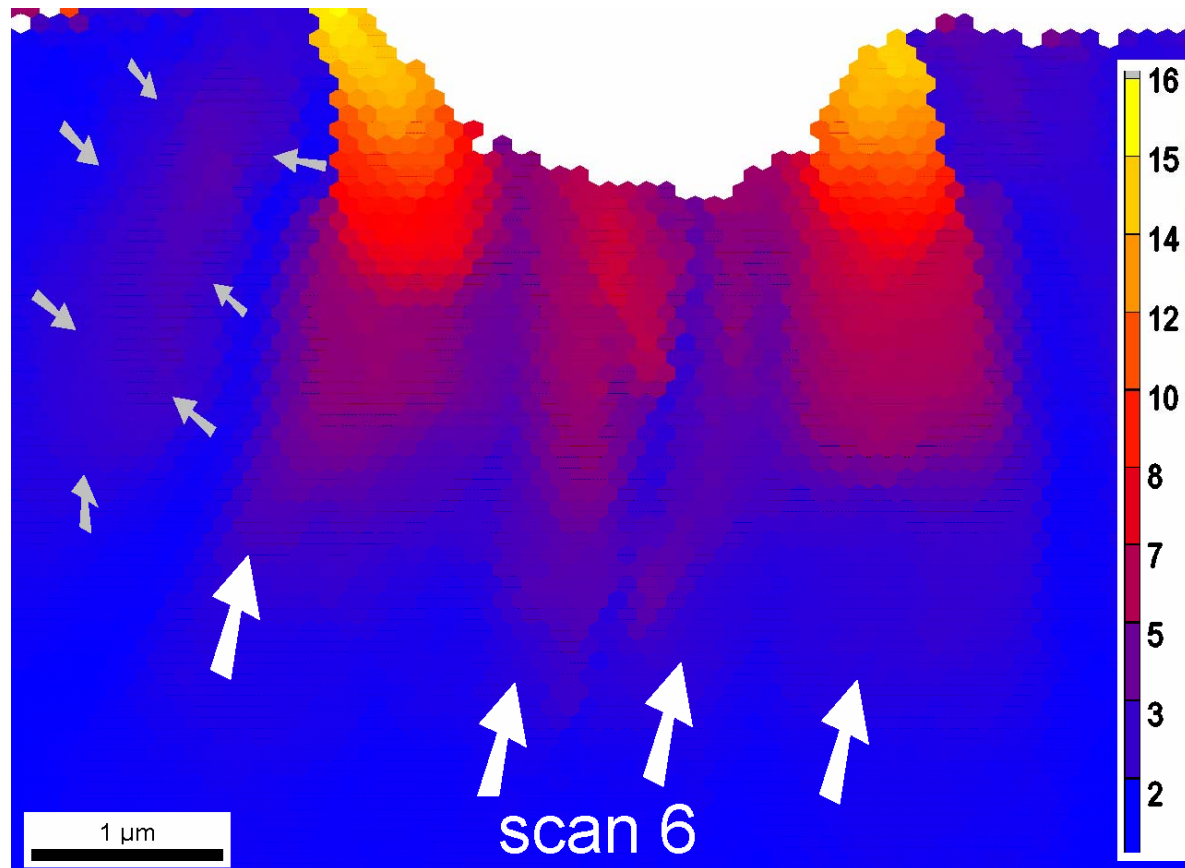
crystal mechanics FEM (general)

crystal plasticity FEM (CPFEM) - family



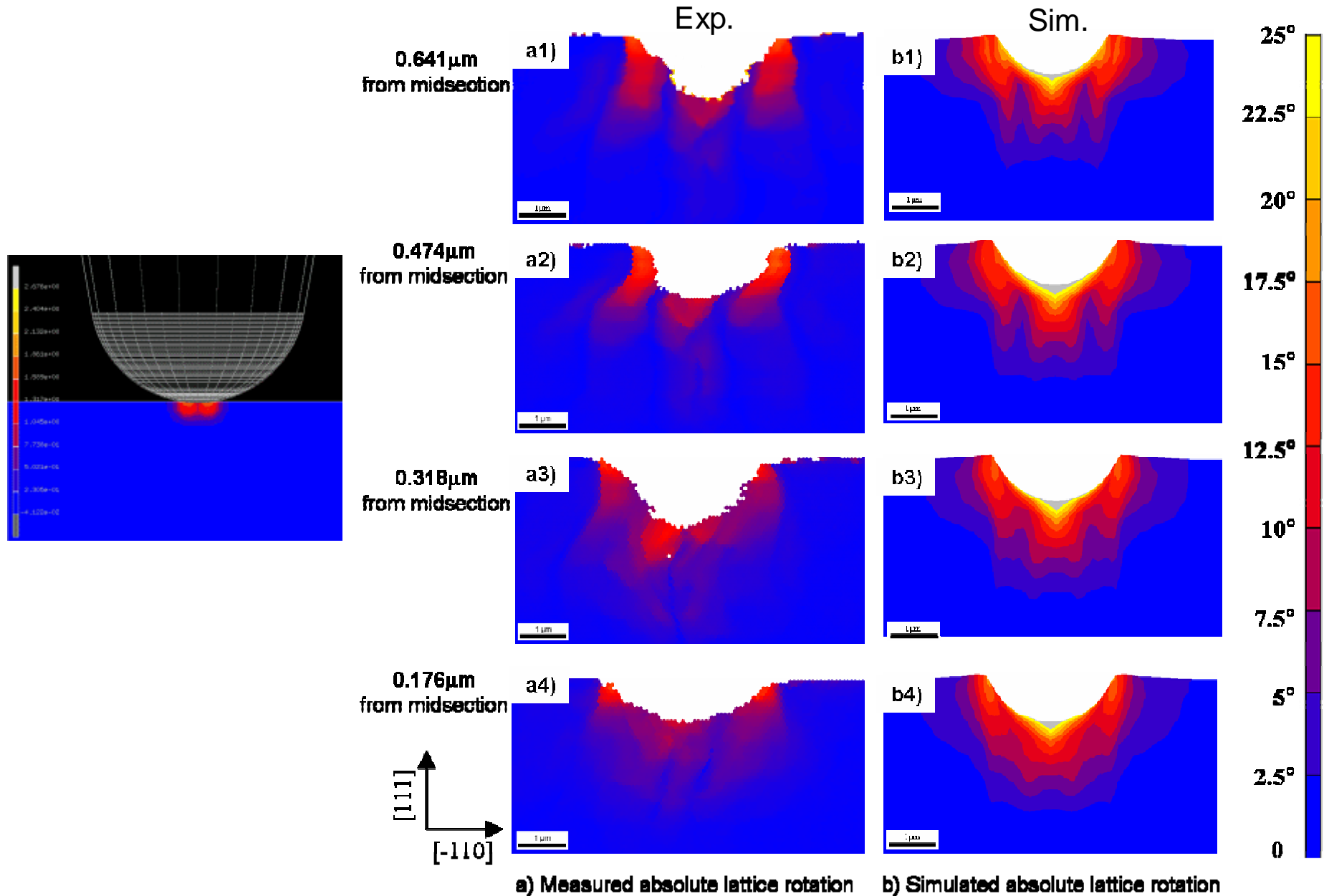


Misorientation map



Closer view of the experimentally observed pattern of the absolute values of the deformation-induced crystalline lattice rotations in $^{\circ}$ in the vicinity of the indent

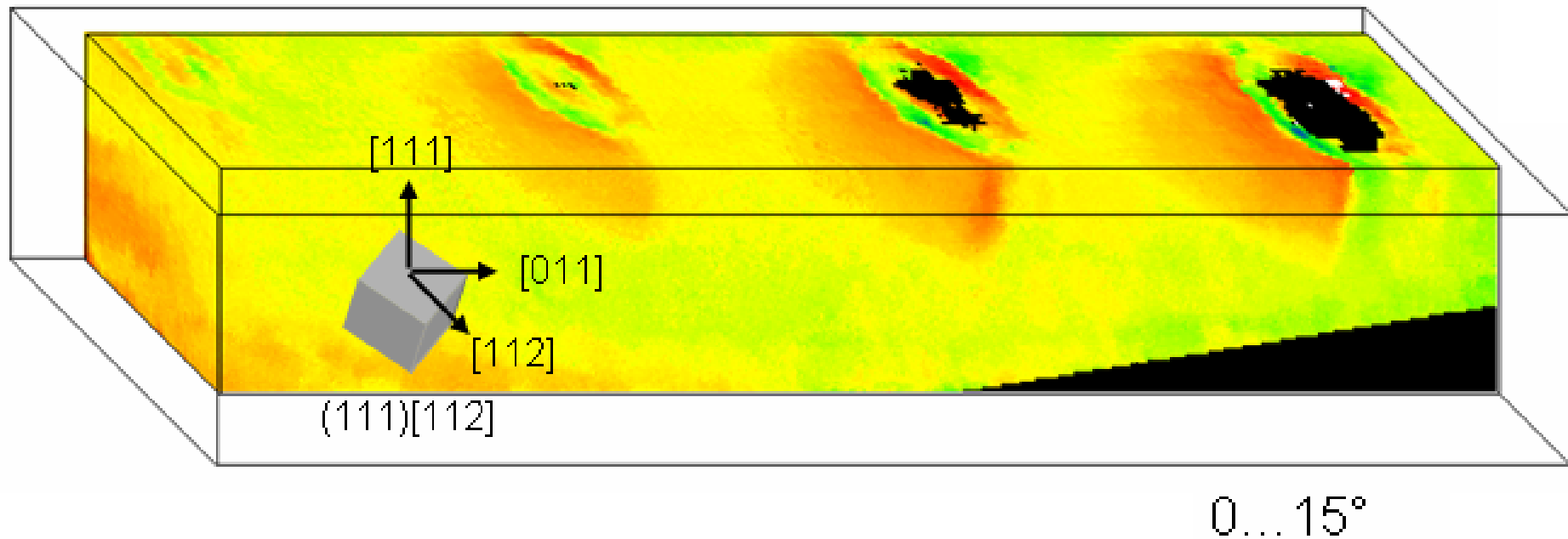
Comparison: magnitude of orientation changes





Experimental : Forces: 4, 6, 8, and 10 mN

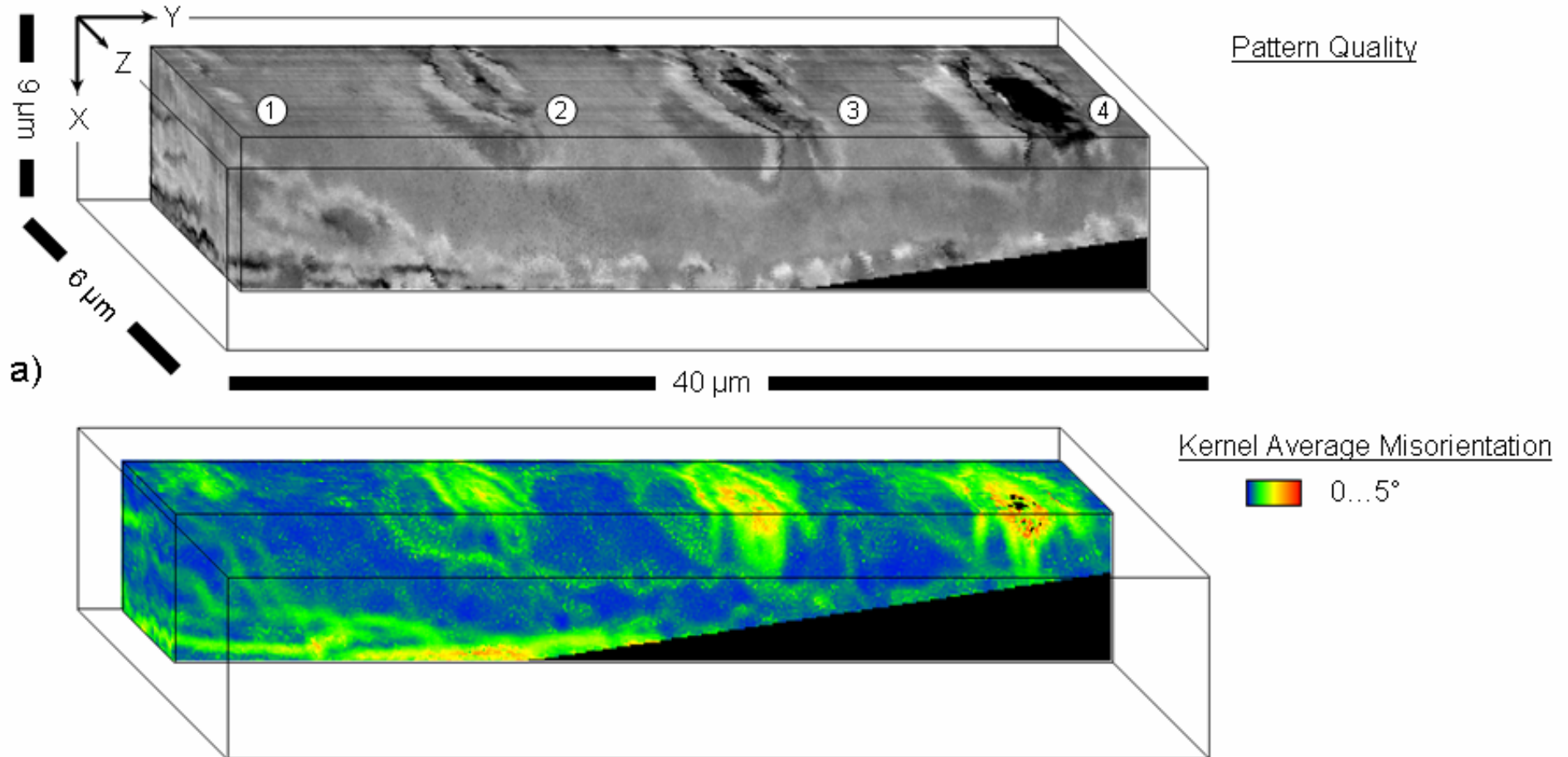
Gradual evolution during indentation ?
Experiment



self-similarity, same type of pattern from early beginning



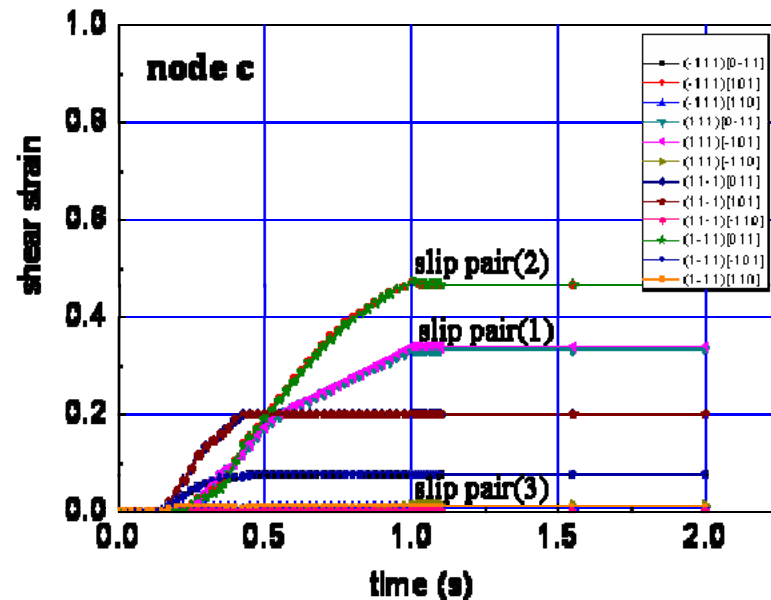
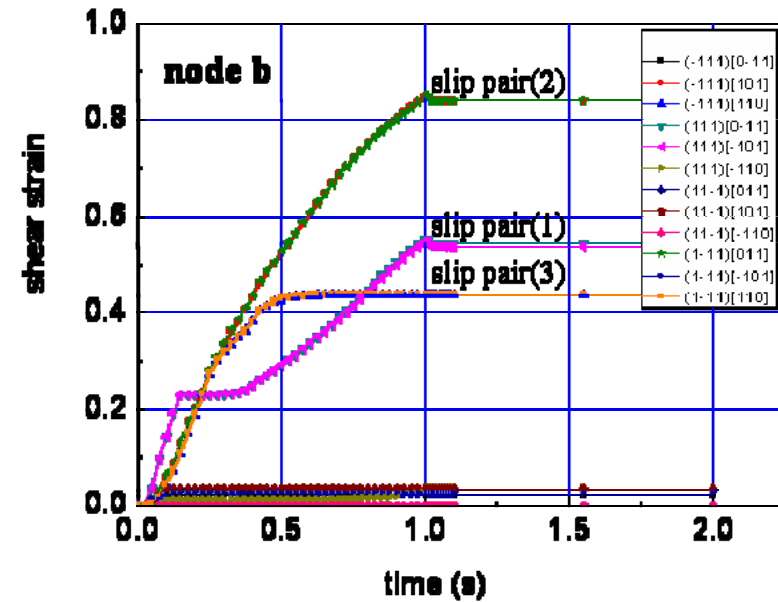
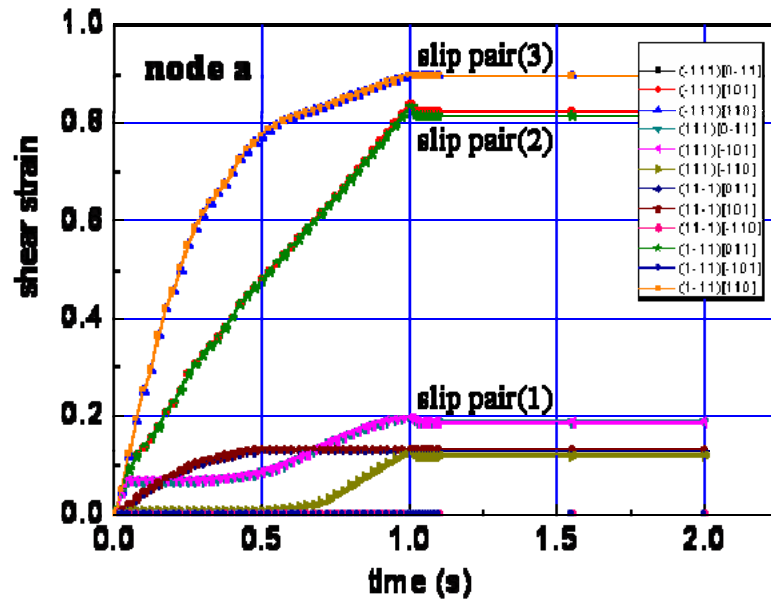
Experimental : Forces: 4, 6, 8, and 10 mN



local !! curvature seems NOT to be larger for very small indents



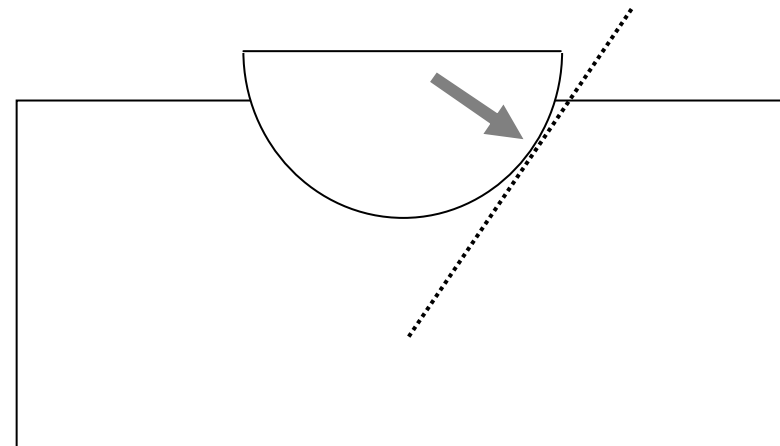
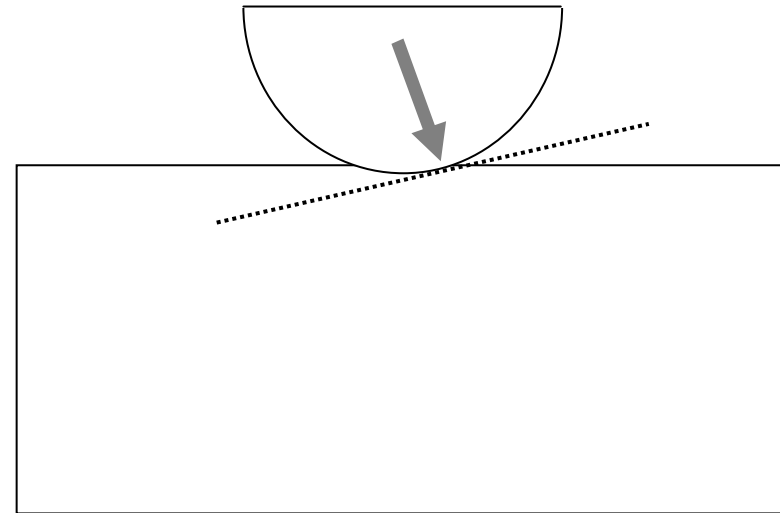
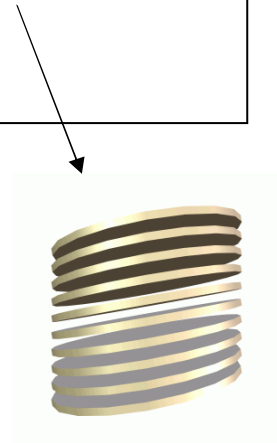
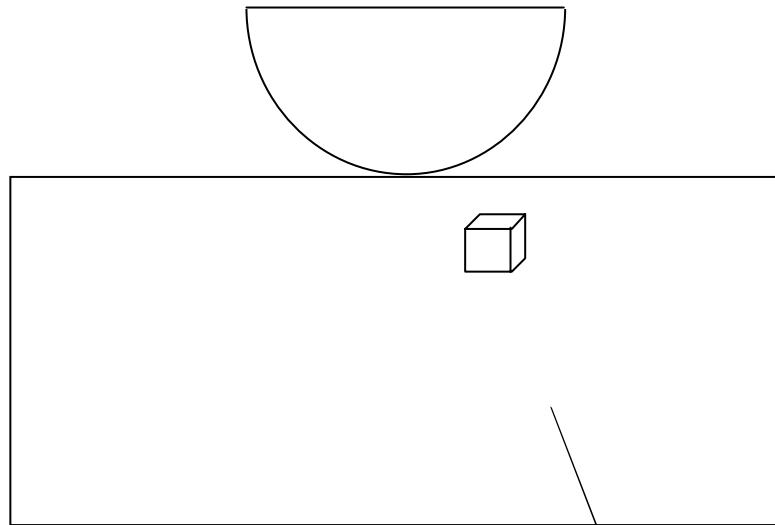
Local active slip systems (simulation)



The active slip systems during indentation at these nodes



Sachs case under compression tangential to contact



Simplify: single crystal kinematics for a Sachs case under compression tangential to local contact interface