

ASSESSMENT OF PELLET INJECTION FOR NET
PART IV:

An Estimate of the Effect of Energy Carriers
other than Thermal Electrons on the Ablation
of Pellets in Plasmas. An Extension of the
Electron Temperature Range Previously Considered

L. L. Lengyel

IPP 5/7

December 1985



MAX-PLANCK-INSTITUT FÜR PLASMAPHYSIK

8046 GARCHING BEI MÜNCHEN

MAX-PLANCK-INSTITUT FÜR PLASMAPHYSIK
GARCHING BEI MÜNCHEN

ASSESSMENT OF PELLET INJECTION FOR NET
PART IV:

An Estimate of the Effect of Energy Carriers
other than Thermal Electrons on the Ablation
of Pellets in Plasmas. An Extension of the
Electron Temperature Range Previously Considered

L. L. Lengyel

IPP 5/7

December 1985

*Die nachstehende Arbeit wurde im Rahmen des Vertrages zwischen dem
Max-Planck-Institut für Plasmaphysik und der Europäischen Atomgemeinschaft über
die Zusammenarbeit auf dem Gebiete der Plasmaphysik durchgeführt.*

Abstract

The effect of runaway electrons, NB ions and alpha particles is estimated by calculating the reduced ablation rates due to these particles in fusion plasmas and using the ablation rate induced by thermal electrons as reference quantity. Calculations were made for various energy content (i.e. beta) ratios and for a fusion-relevant electron temperature range (T_e up to 25 keV).

In a previous study [1], the effect of non-thermal particles that may be present in fusion plasmas on the ablation rate of pellets was estimated for the electron temperature range from 200 eV to 2 keV. It was found that the relative importance of all non-thermal species considered (NB ions, alpha particles, runaway electrons) rapidly decreases with increasing plasma electron temperature. Since runaways may affect pellet ablation quite substantially also at high temperatures, it became of interest to extend the calculations described in [1] to a fusion-relevant temperature range (for T_e up to 25 keV).

As in Ref. [1], the simplified ablation model of Vaslow [2] was applied. According to this model, the ratio of the ablation rates caused by species k and thermal electrons e can be expressed in terms of the energy fluxes Q carried by these particles to the pellet surface and their stopping lengths λ in the solid pellet:

$$\frac{\dot{N}_k}{\dot{N}_e} = \left(\frac{Q_k}{Q_e} \right)^{1/3} \left(\frac{\lambda_k}{\lambda_e} \right)^{2/3}.$$

The expressions used in calculating Q and λ are given in Ref. [1].

The ablation rate ratios \dot{N}_k/\dot{N}_e are given in Figs. 1 to 9 as functions of the (thermal) electron temperature for the temperature range $2 \text{ keV} \leq T_e \leq 25 \text{ keV}$, for different non-thermal particle energies E_k , and for different beta ratios $\beta^* \equiv \beta_k/\beta_e$. The following particle energies and beta ratios were considered:

NB ions	(Figs. 1-4): 80, 120, 160, 175 keV,	$0.2 \leq \beta^* \leq 1.0$;
Alpha particles	(Figs. 5-7): 1.0, 2.0, 3.5 MeV,	$0.2 \leq \beta^* \leq 0.5$;
Runaway electrons	(Figs. 8-9): 0.5 and 1.0 MeV,	$10^{-4} \leq \beta^* \leq 10^{-2}$.

For the sake of completeness, the results of Ref. [1] covering the electron temperature range $0.2 \text{ keV} \leq T_e \leq 2.0 \text{ keV}$ are reproduced in this report as well (see Figs. 10 to 18: Figs. 10 to 13 for NB ions, Figs. 14 to 16 for alpha particles, and Figs. 17 and 18 for runaway electrons).

As can be seen, the relative importance of the non-thermal particles increases with increasing particle energy and beta ratio, monotonically decreases with increasing bulk electron temperatures, and becomes negligible under thermonuclear plasma conditions. However, it should be noted that at intermediate electron temperatures the synergetic effect of the two particle species (k, e) may become important, an effect that is not taken into account in this estimate. Furthermore, the validity of the present approximation is limited to particle energy ranges in which the

condition of surface ablation is fulfilled: the penetration depths of the energetic particles must be small compared with the characteristic pellet dimension.

The results of these ablation rate ratio estimates can be summarized as follows:

- (a) **NB ions:** For $E_{bi} \geq 80$ keV one has $\dot{N}_{bi}/\dot{N}_e > 1$ in the temperature region $T_e \lesssim 1.3$ keV for all beta ratios considered. For $E_{bi} = 175$ keV and $\beta_{bi}/\beta_e \approx 0.6$ one obtains $\dot{N}_{bi}/\dot{N}_e \approx 1$ at $T_e \approx 2.5$ keV and ≈ 0.1 at $T_e \approx 12.5$ keV.
- (b) **Alpha particles:** For $E_\alpha = 3.5$ MeV, \dot{N}_α/\dot{N}_e was found to be unity for $\beta_\alpha/\beta_e = 0.2$ and 0.5 at $T_e = 3.7$ keV and 4.4 keV, respectively. With $E_\alpha = 1.0$ MeV, the ablation ratio becomes less than unity for $T_e \gtrsim 1$ keV for all beta ratios considered.
- (c) **Runaway electrons:** The results show that for $E_{ee} \geq 0.5$ MeV and $\beta_{ee}^*/\beta_e \geq 10^{-3}$ one has $\dot{N}_{ee}/\dot{N}_e \geq 500$ in the electron temperature range $T_e \lesssim 500$ eV (alternatively, if $\beta_{ee}/\beta_e \geq 10^{-2}$, or $E_{ee} \gtrsim 1$ MeV one has $\dot{N}_{ee}/\dot{N}_e \gtrsim 10^3$). At $T_e = 25$ keV and with $\beta_{ee}/\beta_e = 10^{-3}$ one still has $\dot{N}_{ee}/\dot{N}_e \approx 2.5$.

However, since the stopping range of 1 MeV electrons in condensed hydrogen is ≈ 25 mm (and ≈ 1.6 mm at $E_{ee} \approx 200$ keV), the validity of the results is limited to low runaway energies and large pellet sizes. At high energies and small pellet sizes one rather has volumetric heat deposition, which could lead to pellet disintegration as well as partial shine-through, neither of which phenomenon was taken into account in the model. Nevertheless, the results indicate that runaway electrons may have a significant effect on pellet ablation.

References

- [1] L.L. Lengyel, Assessment of Pellet Injection for NET, Part IV: An estimate of the effect of energy carriers other than thermal electrons on the ablation of pellets in plasmas. IPP Report 1/233, Sept.1984.
- [2] D.F. Vaslow, IEEE Trans. Plasma Sci., PS-5 (1977) 12.

LENNBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)= 80.00 KeV ; (NB-ION/TH.EL.)BETA RATIOS: .2/.4/.6/.8/1.0/

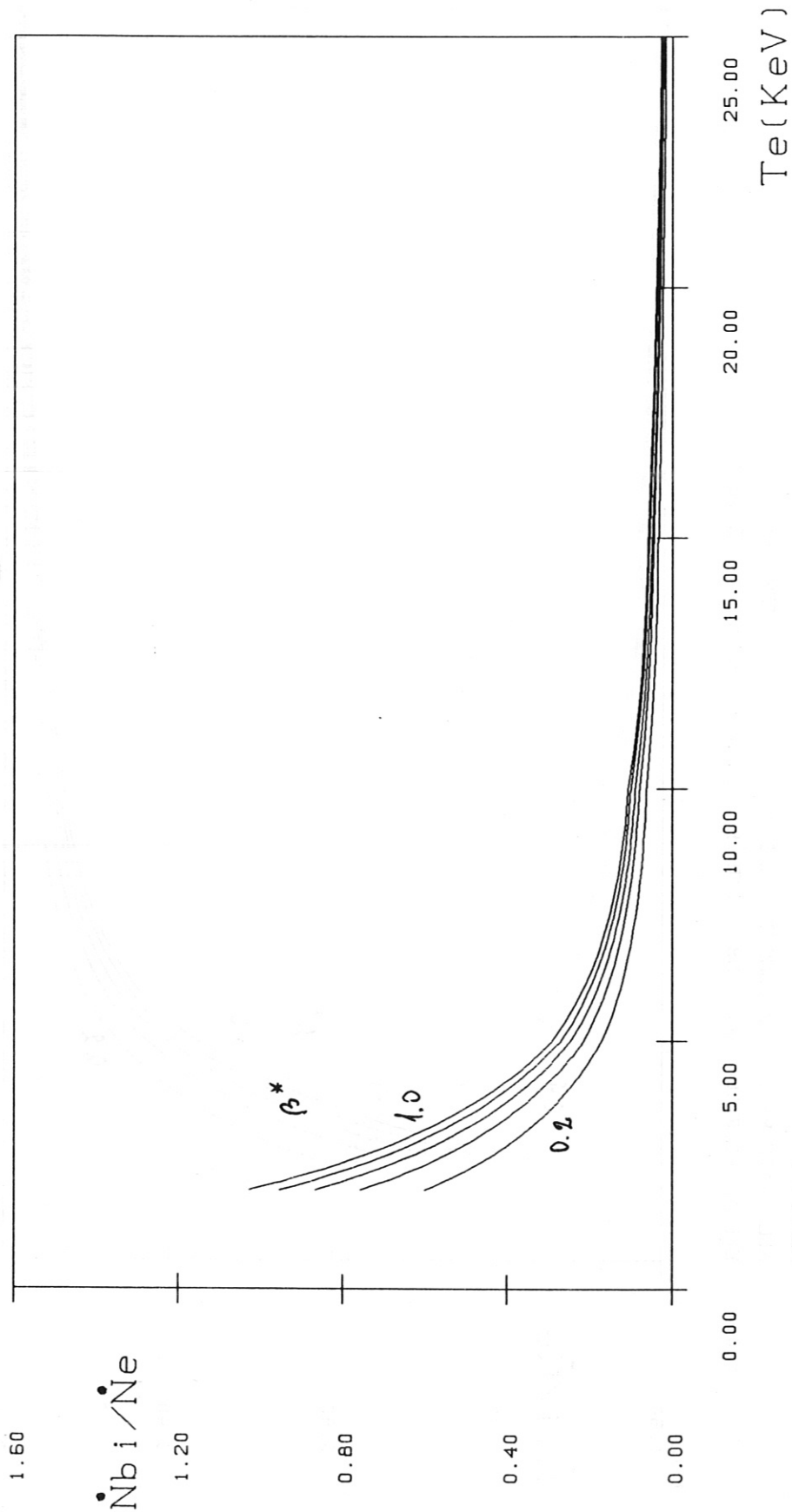


Fig.1

IPP--CMS 21/11/85 13.43:05 URR F2-06 004

LENNBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)=120.00 KeV ; (NB-ION/TH.EL.)BETA RATIOS:.2/.4/.6/.8/1.0/

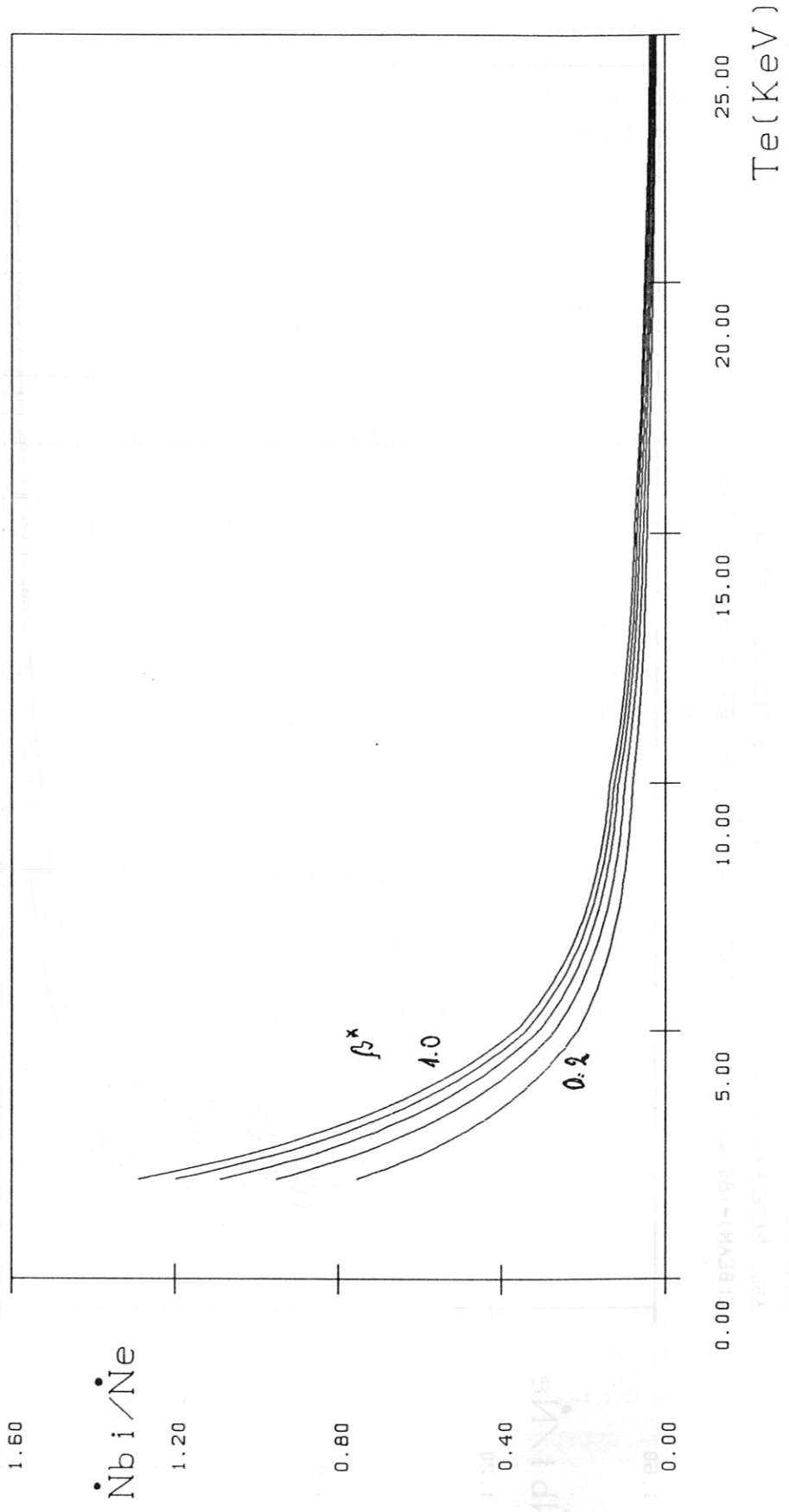


Fig.2

LENBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)=160.00 KeV ; (NB-ION/TH.EL.) BETA RATIOS: .2/.4/.6/.8/1.0/

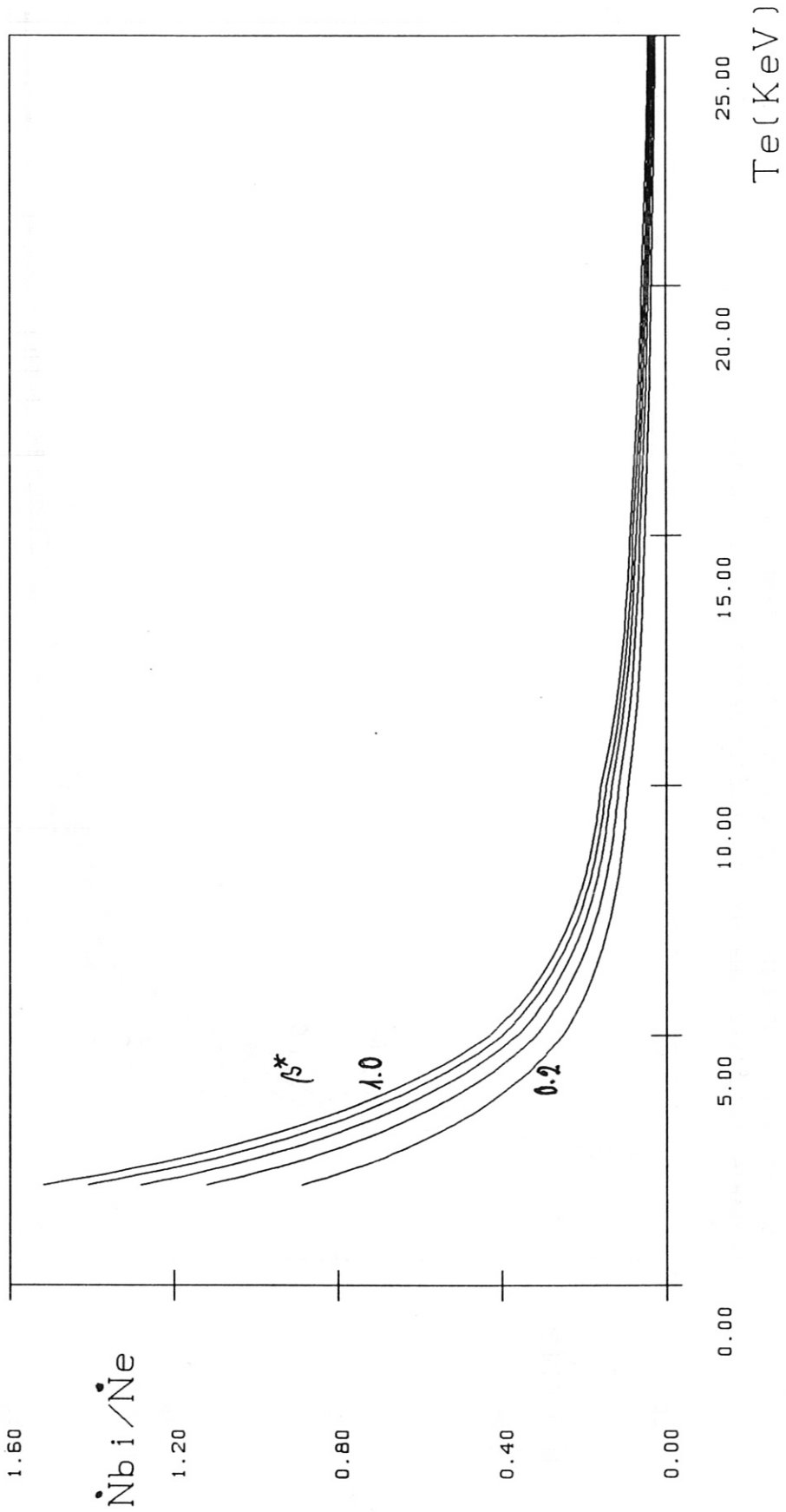


Fig.3

LENBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)=175.00 KeV ; (NB-ION/TH.EL.) BETA RATIOS: .2/.4/.6/.8/1.0/

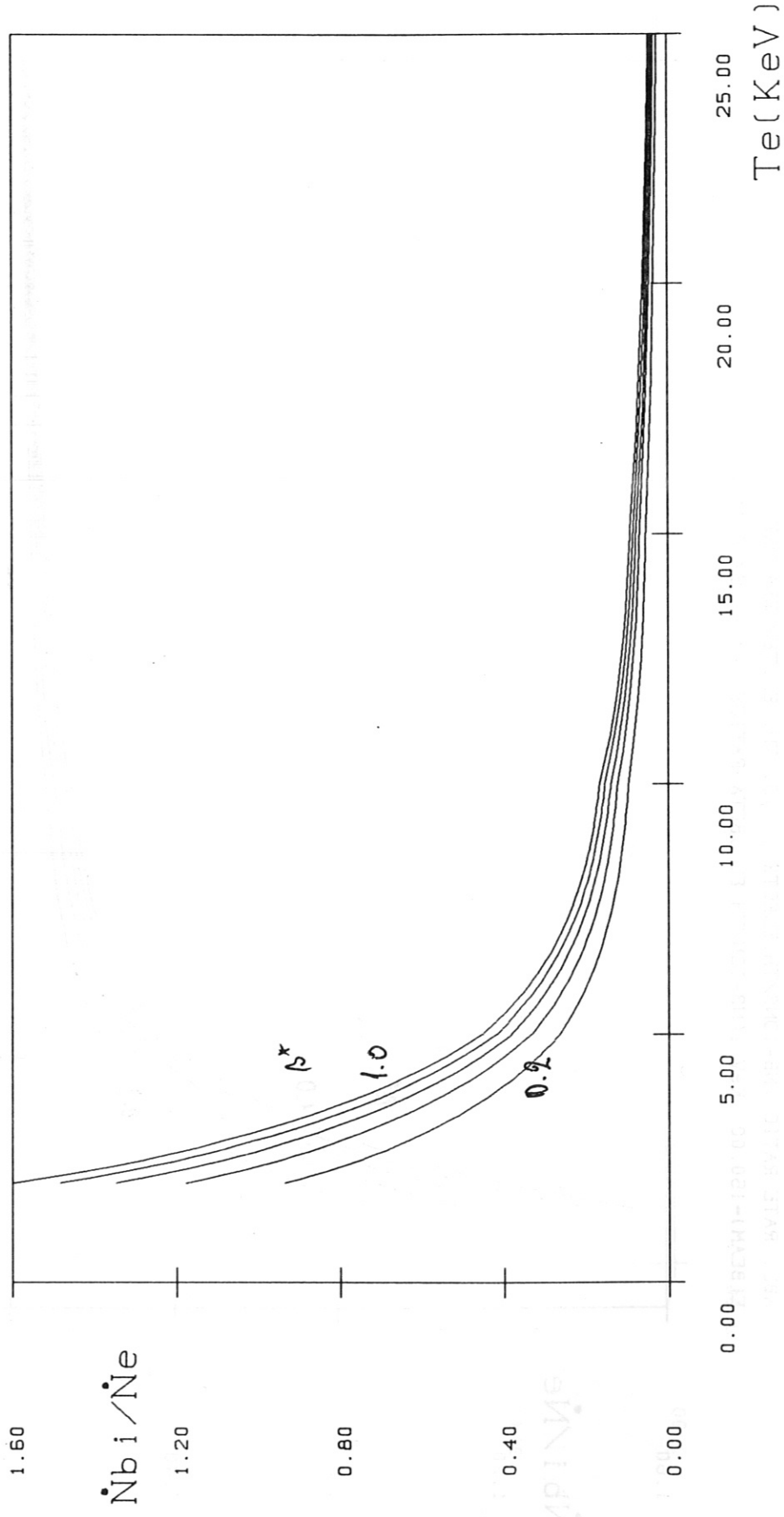


Fig.4

LENNANE
ABL. RATE RATIO (ALPHA/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.ALPHA= 1.0E+06(eV); (ALPH./EL.) BETA RATIOS: 0.2/0.3/0.4/0.5

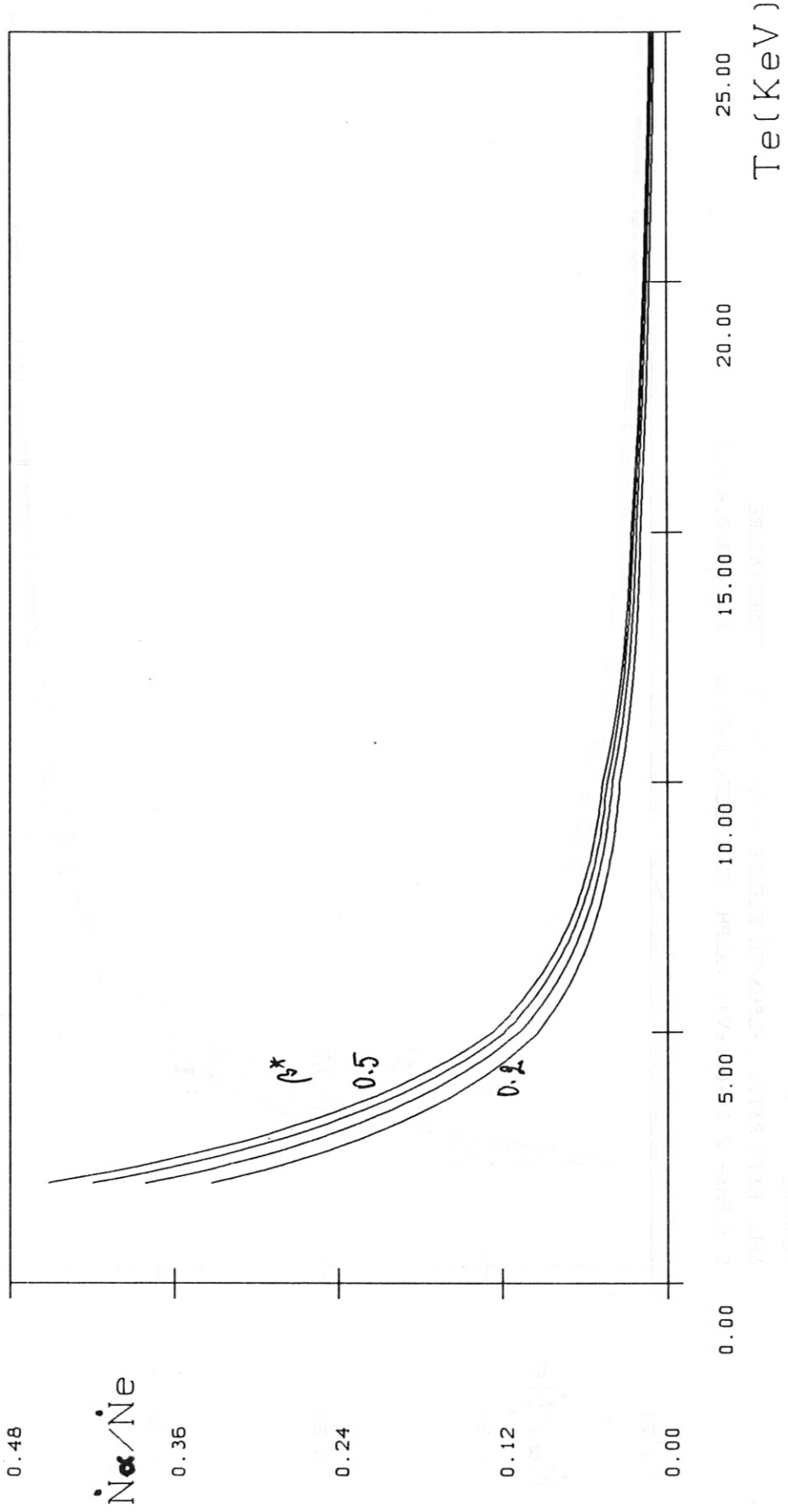


Fig.5

LENNANE
ABL. RATE RATIO (ALPHA/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.ALPHA= 2.0E+06(eV); (ALPH./EL.) BETA RATIOS: 0.2/0.3/0.4/0.5

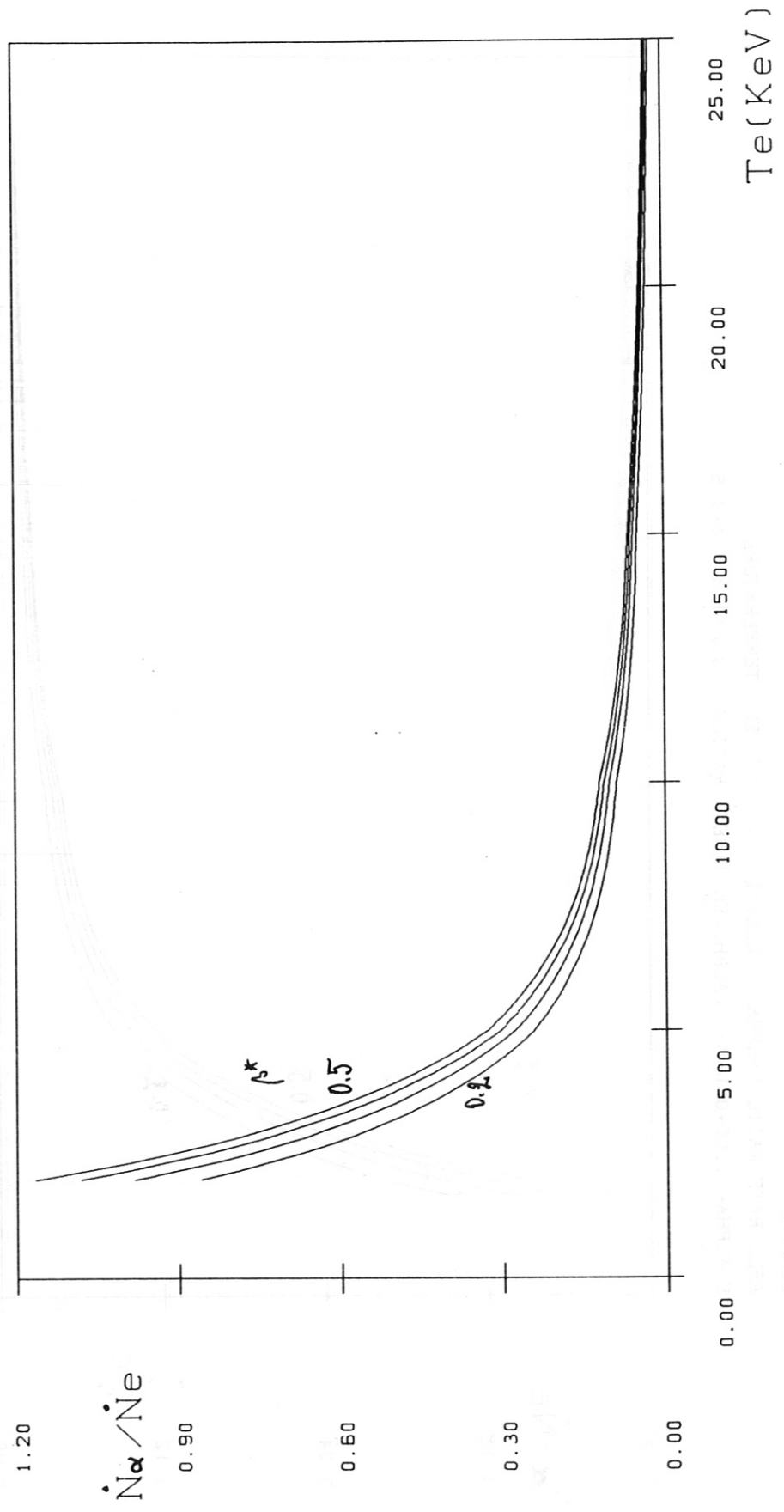


Fig.6

LENNANE
ABL. RATE RATIO (ALPHA/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.ALPHA= 3.5E+06(eV); (ALPH./EL.) BETA RATIOS: 0.2/0.3/0.4/0.5

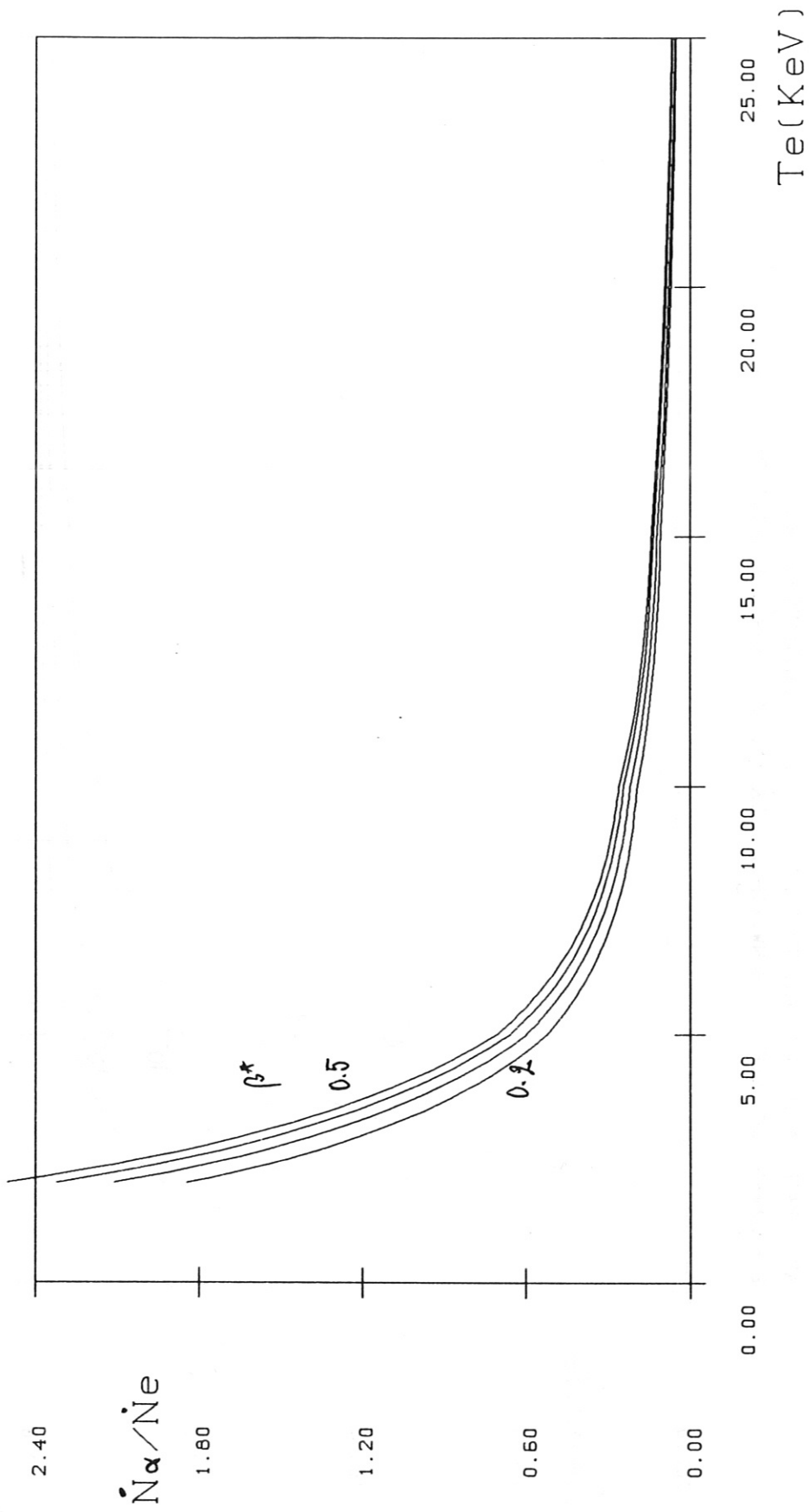


Fig.7

LENNAWAY
ABL. RATE RATIO (RUNAWAY/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.RUNAW=5.00E+05(EV); (RUNW./TH.) BETA RATIOS: 1.E-4/1.E-3/1.E-2/

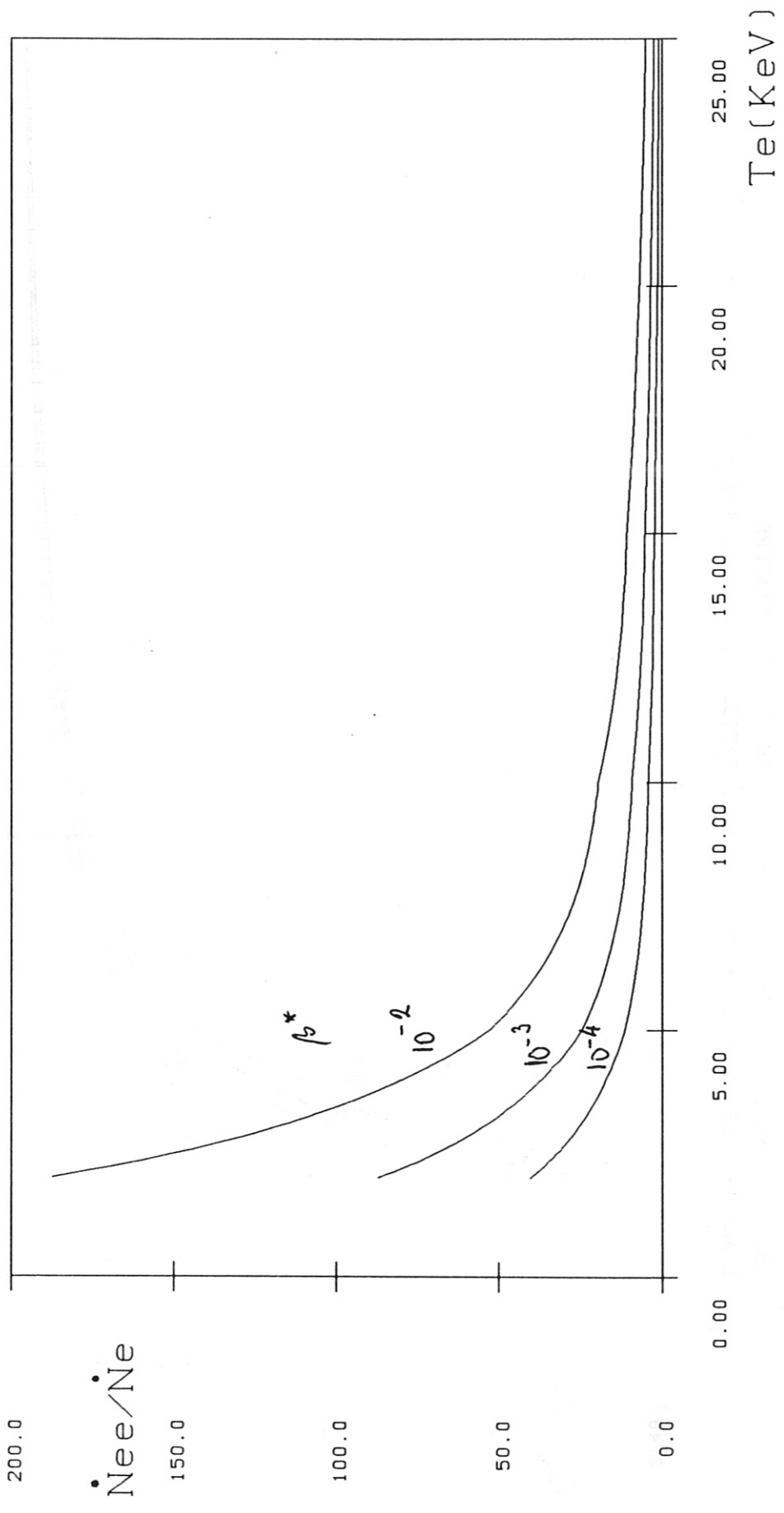


Fig. 8

LENNAWAY
ABL. RATE RATIO (RUNAWAY/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.RUNAW=1.00E+06(EV); (RUNW./TH.) BETA RATIOS:1.E-4/1.E-3/1.E-2/

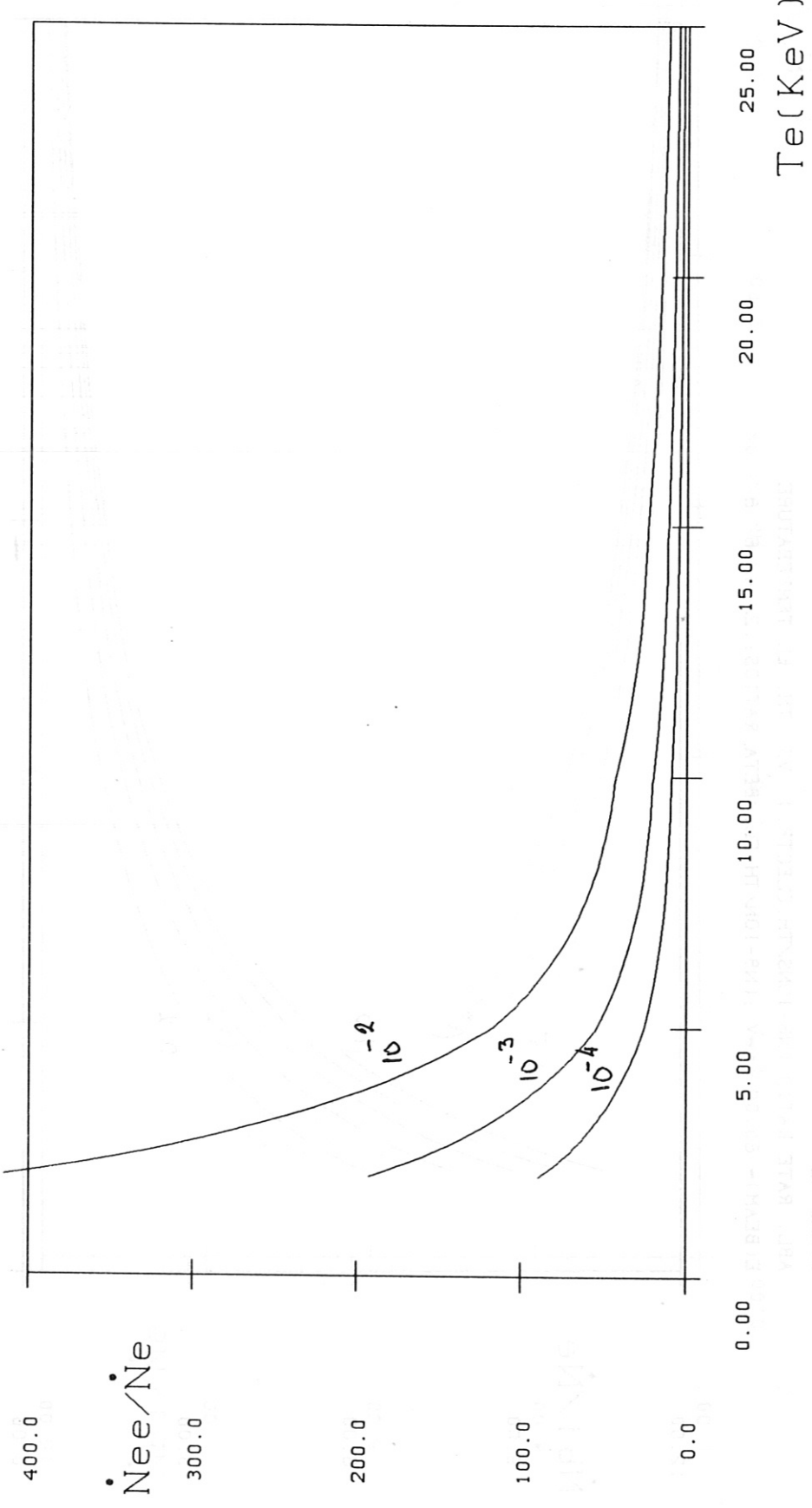


Fig.9

LENBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM) = 80.00 KeV ; (NB-ION/TH.EL.) BETA RATIOS : .2 / .4 / .6 / .8 / 1.0 /

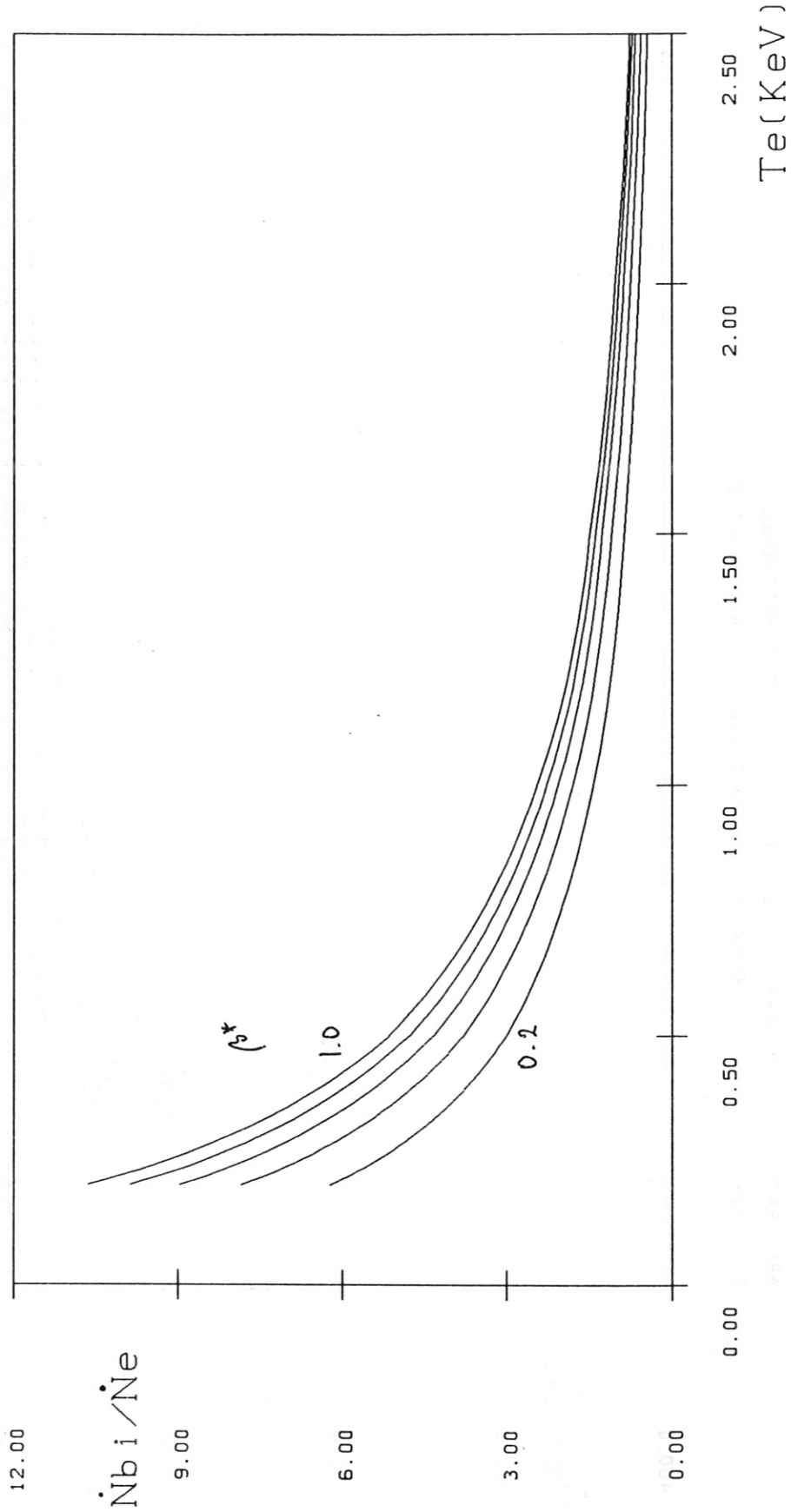


Fig. 10

LENBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)=120.00 KeV ; (NB-ION/TH.EL.) BETA RATIOS: 2/.4/.6/.8/1.0/

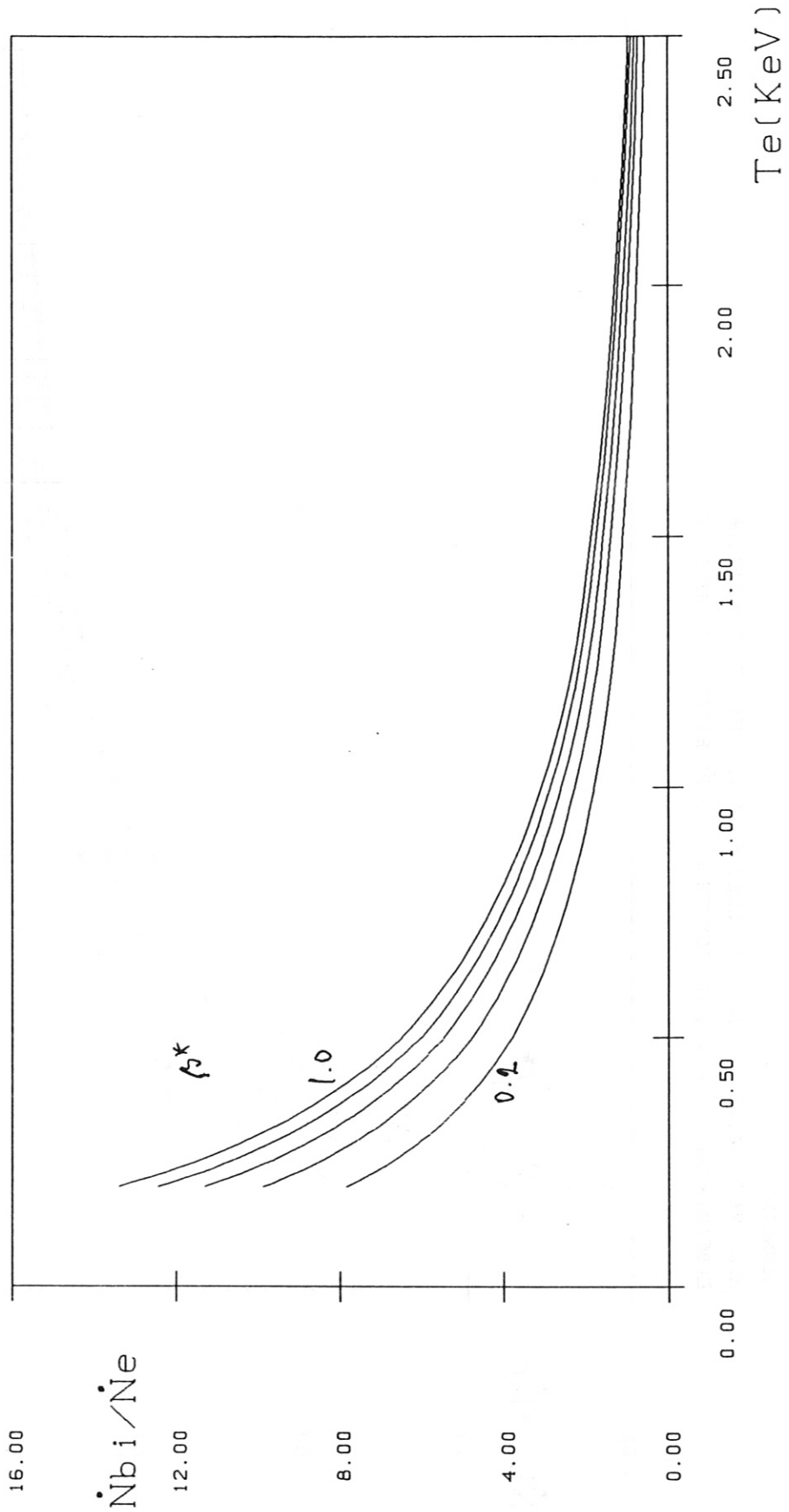


Fig. 11

LENNBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)-160.00 KeV ; (NB-ION/TH.EL.) BETA RATIOS: .2/.4/.6/.8/1.0/

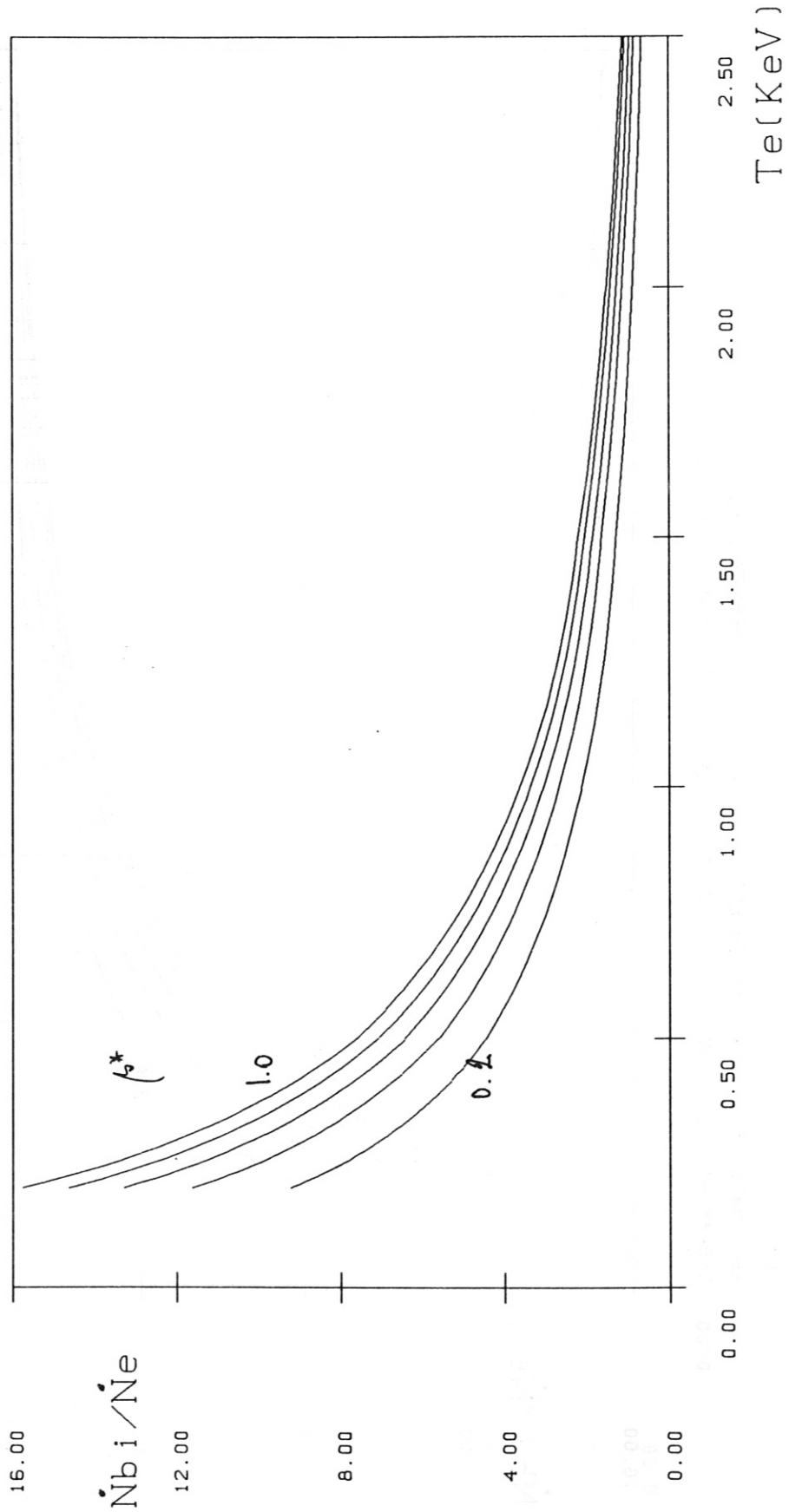


Fig.12

LENNBINE
ABL. RATE RATIO (NB-IONS/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E(BEAM)=175.00 KeV ; (NB-ION/TH.EL.)BETA RATIOS:.2/.4/.6/.8/1.0/

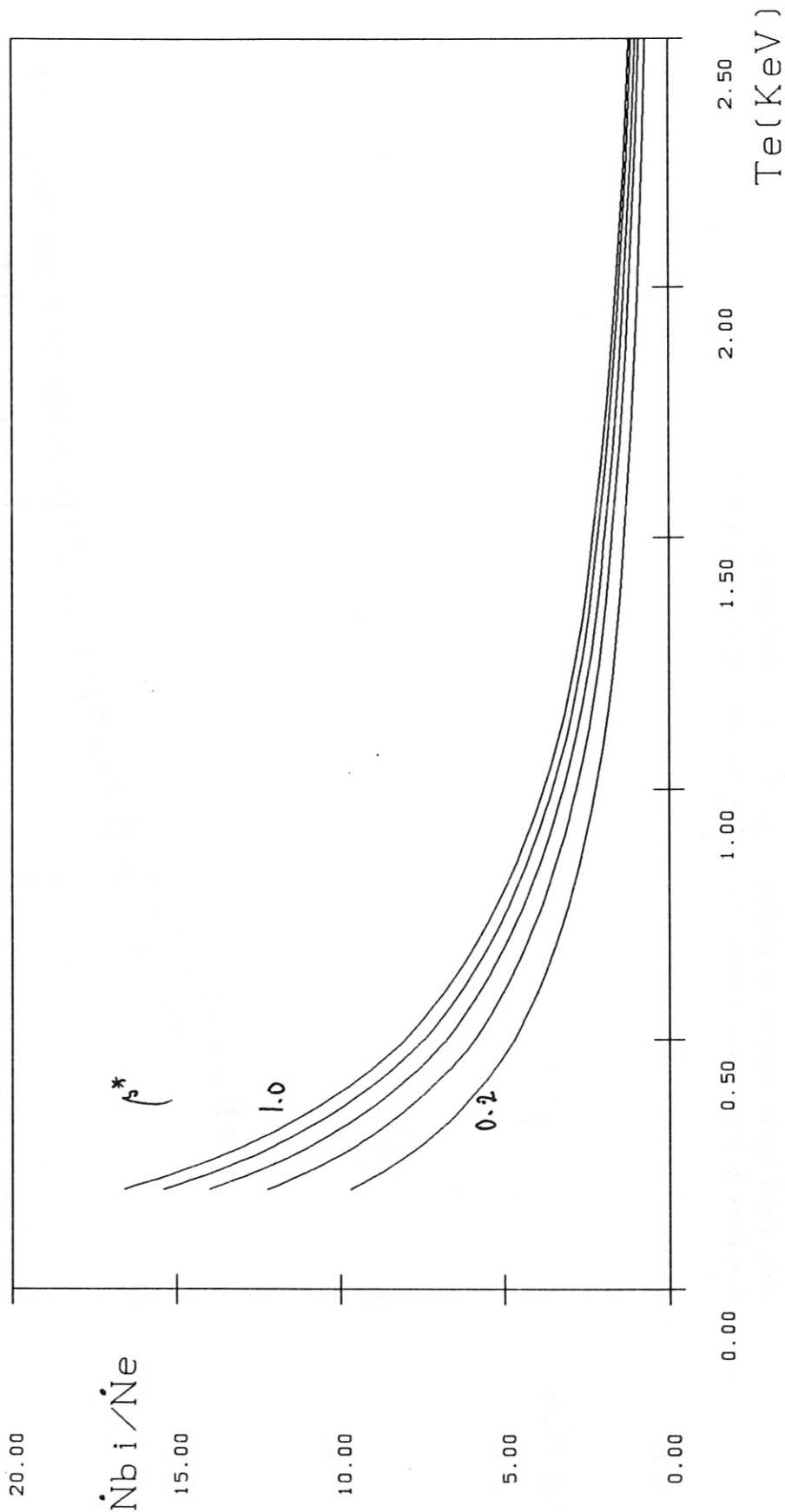


Fig.13

LENNANE
ABL. RATE RATIO (ALPHA/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.ALPHA= 1.0E+06(eV); (ALPH./EL.) BETA RATIOS: 0.2/0.3/0.4/0.5

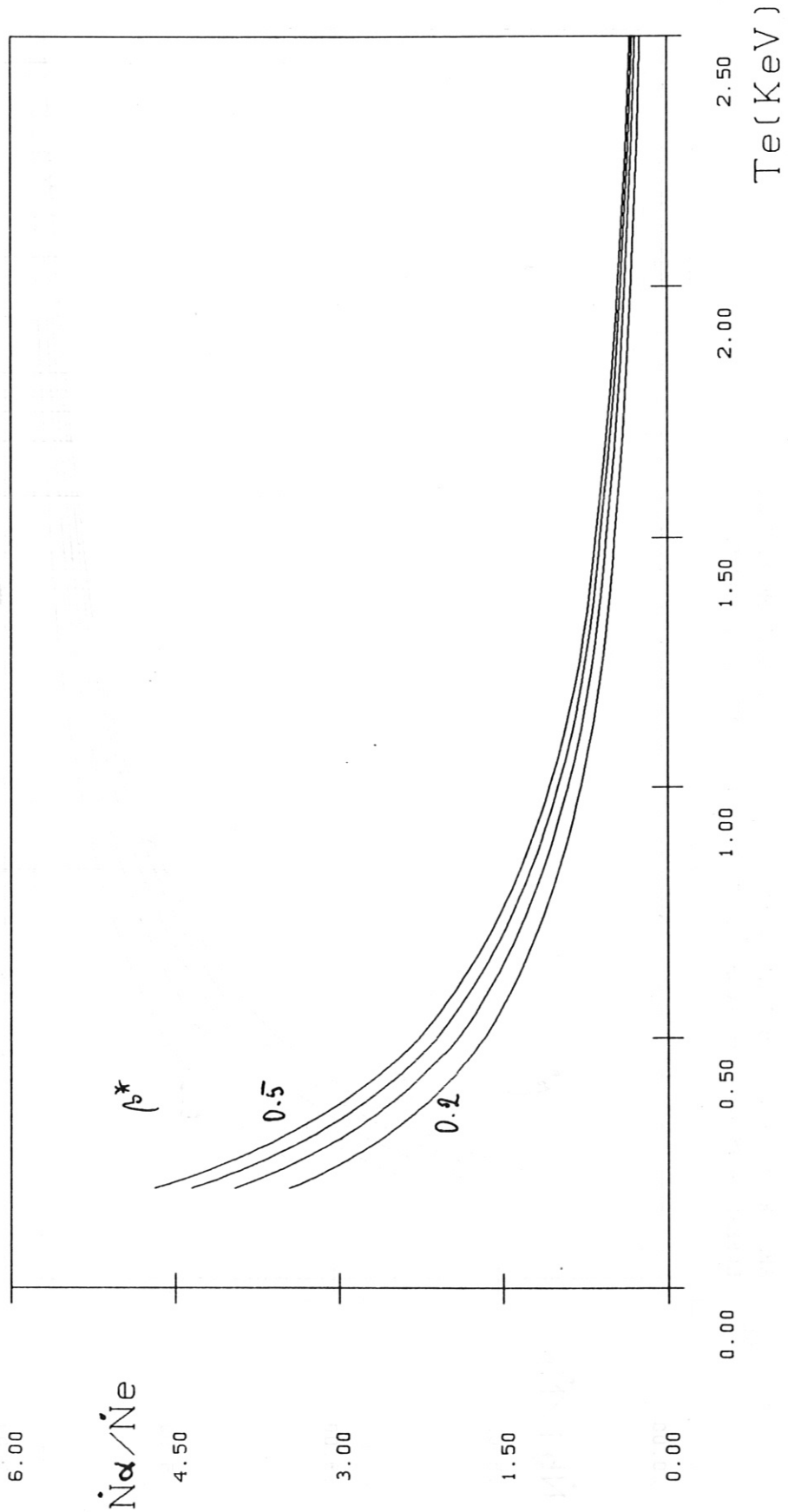


Fig. 14

LENNANE
ABL. RATE RATIO (ALPHA/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.ALPHA= 2.0E+06(eV); (ALPH./EL.) BETA RATIOS: 0.2/0.3/0.4/0.5

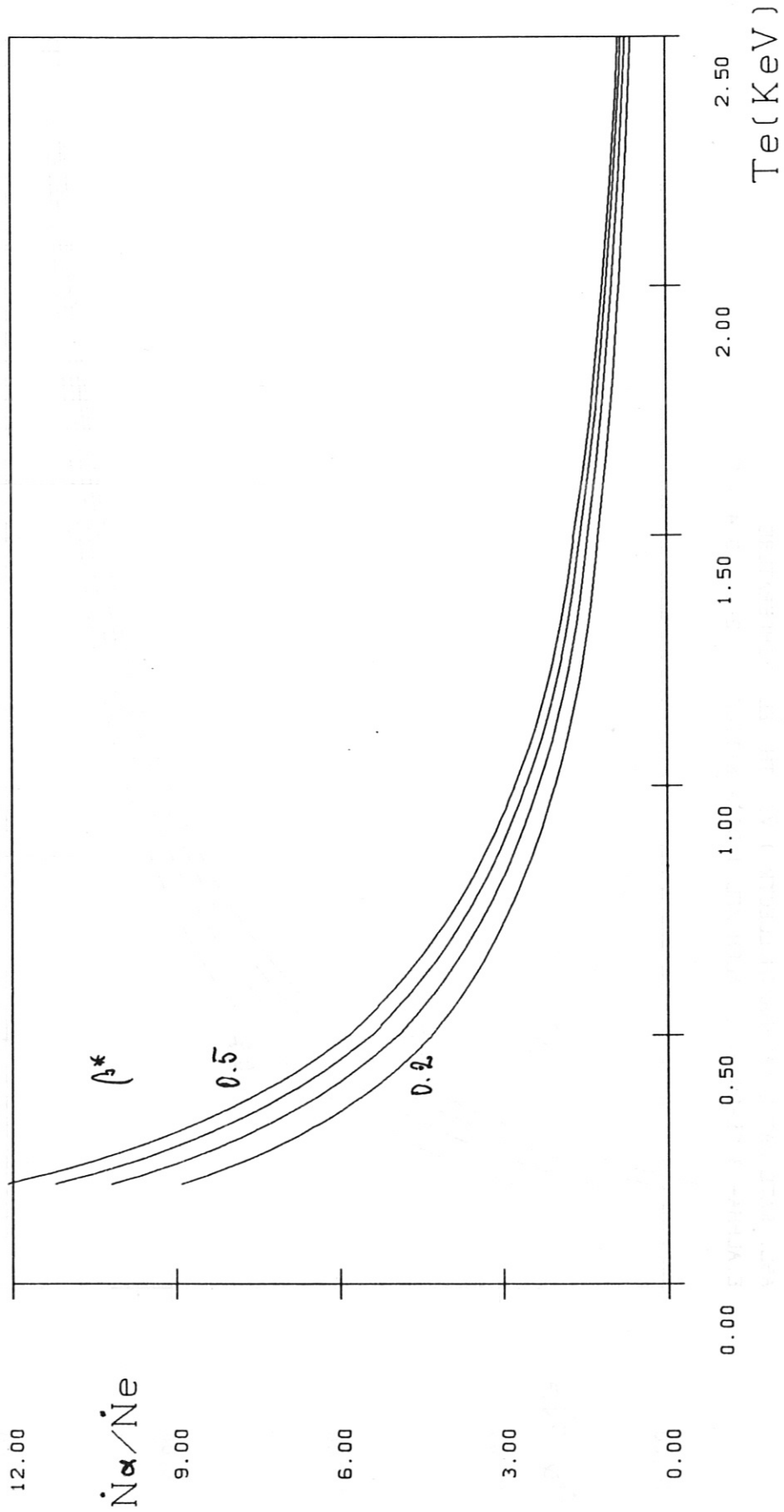


Fig.15

LENNANE
ABL. RATE RATIO (ALPHA/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.ALPHA= 3.5E+06(eV); (ALPH./EL.) BETA RATIOS: 0.2/0.3/0.4/0.5

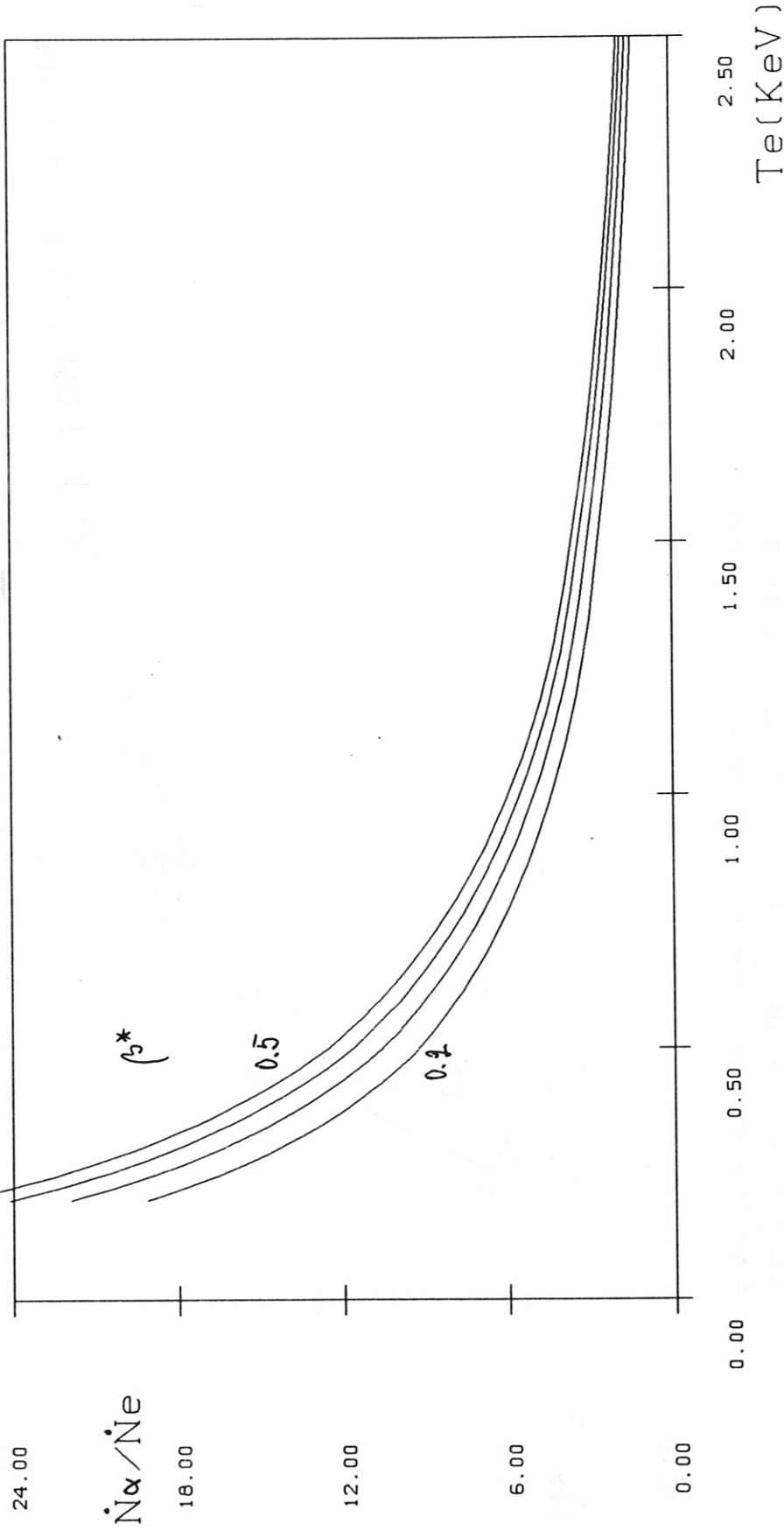


Fig.16

LENNAWAY
ABL. RATE RATIO (RUNAWAY/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.RUNAW=5.00E+05(EV); (RUNW./TH.) BETA RATIOS:1.E-4/1.E-3/1.E-2/

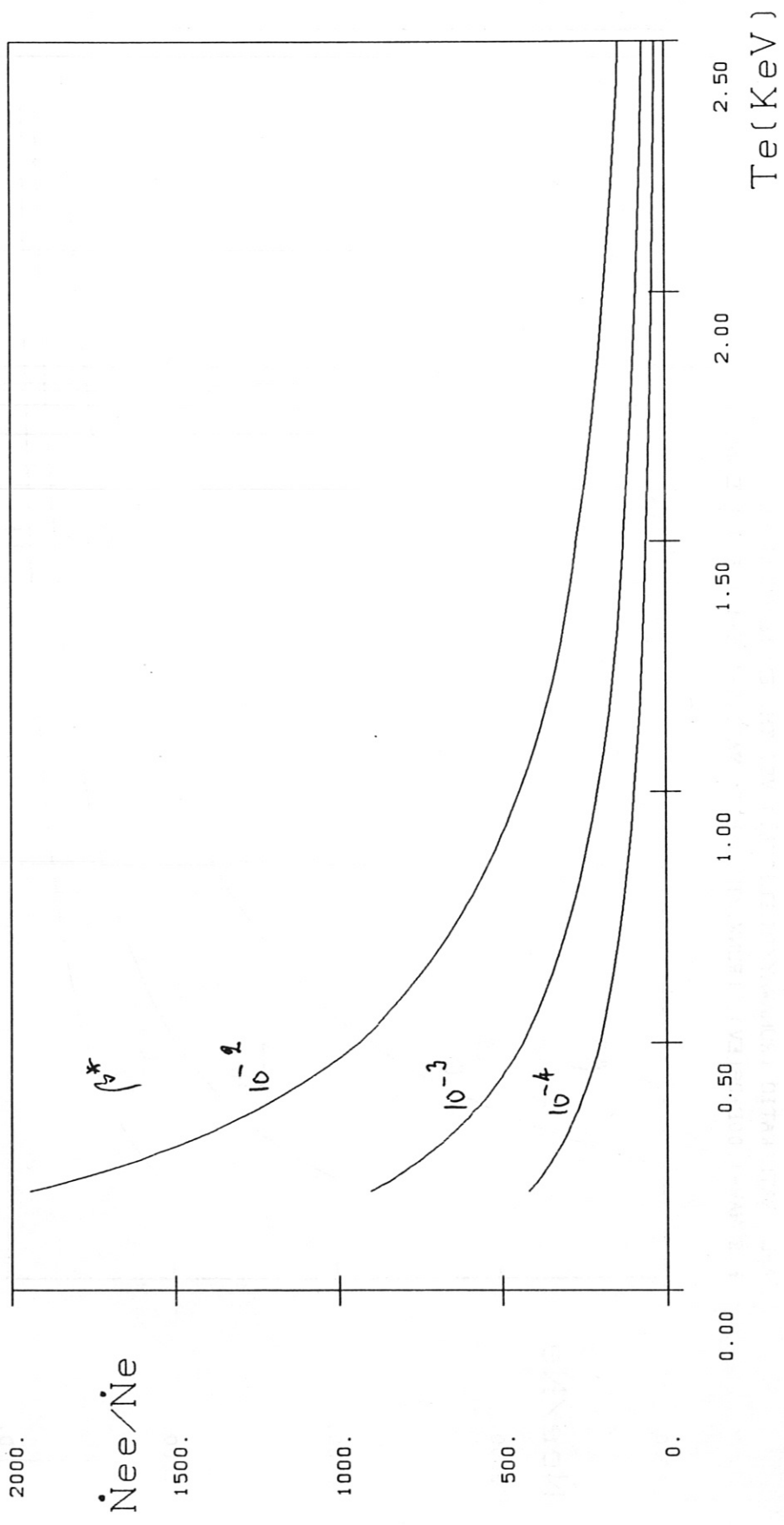


Fig.17

LENNAWAY
ABL. RATE RATIO (RUNAWAY/TH.ELECTR.) VS. TH. EL. TEMPERATURE
E.RUNAW=1.00E+06(EV); (RUNW./TH.) BETA RATIOS:1.E-4/1.E-3/1.E-2/

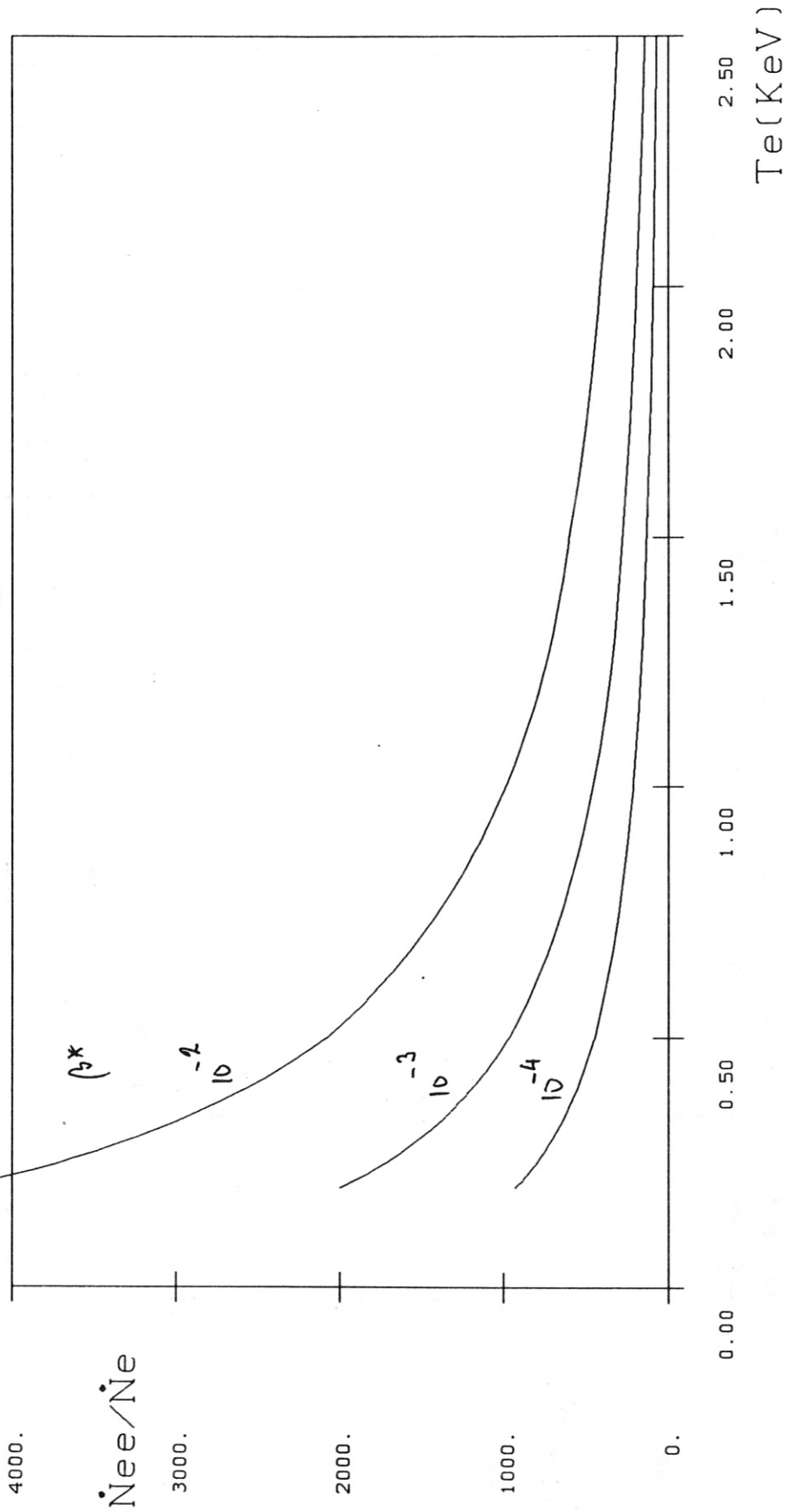


Fig.18