

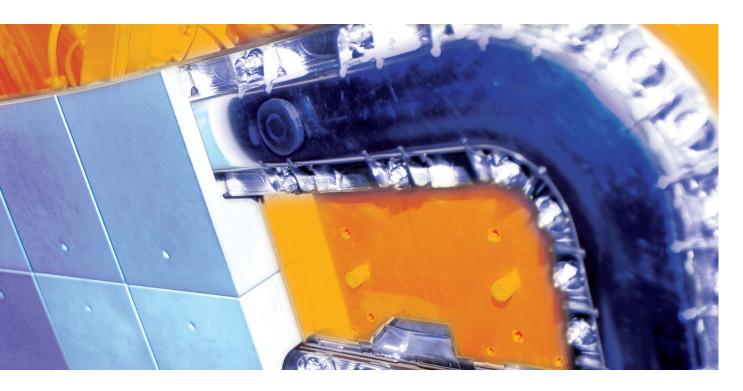
Annual Report 2010











Active inner vessel coil during assembly at the low-field side of the inner wall, partly with and without protection tiles. The first set of eight coils is operational. These coils are being used to mitigate ELMs and other detrimental MHD activities. The full set of coils will consist of 24 active coils.



Annual Report 2010

The Max-Planck-Institut für Plasmaphysik is an institute of the Max Planck Gesellschaft, part of the European Fusion Programme (Euratom) and an associate member of the Helmholtz-Gemeinschaft Deutscher Forschungszentren.



This year the Max Planck Institute for Plasma Physics (IPP) was able to look back on five decades of successful research work — with its foundation on 28 June 1960, it began a long-term programme with intensive basic research. The object under investigation, a high-temperature hydrogen plasma, proved to be considerably more complex than had been assumed by the founders of the institute. The plasma data attainable in the first stellarator and tokamak devices were equivalent to fusion powers of just a few milliwatts. Nowadays, for comparison, we have the world's record-breaking experiment of the European joint project, JET, which in 1997 attained a brief peak power of 16 megawatts. The ITER large-scale international test device, which is currently under construction, is now due to produce the first self-heating and energy-yielding plasma — an impressive development to which IPP has made significant contributions with its experimental and theoretical work. Though being 50, in its jubilee year IPP has continued to push scientific work on high level, as the paragraphs to follow show.

In 2010, the assembly of the superconducting magnetic field coils for Wendelstein 7-X was successfully completed. Providing the magnetic field which confines the hot fusion plasma, the 70 coils constitute the heart of the device. They are arranged in five similar modules, three of which have already been installed in their final positions in the experiment hall by the end of the year. The coils are enclosed by a cryostat vessel. Equipped with super-insulation, it acts as a huge Dewar vessel. Inside, the magnetic field coils will be operated close to absolute zero temperature. The superconductors can thus provide – almost without losses – the specially optimized magnetic field cage of Wendelstein 7-X. Special thanks go to our collaborators, who significantly contribute to the project's success. At the end of June the team at the Forschungszentrum Jülich was able to celebrate the successful development and construction of the bus bar system, which provides the electrical connection of the magnetic field coils. Another breakthrough was the successful prototype test and subsequent start of series production of the current leads, provided by the Karlsruhe Institute of Technology. The current leads connect the superconductors inside the cryostat to the normally conducting power supplies. While progress of the assembly work on Wendelstein 7-X can be perceived on a daily basis, the focus is now shifting to diagnostics and heating systems, which are necessary for successfully commissioning the device in 2014 and starting the scientific programme.

The ASDEX Upgrade tokamak was shut down for most of 2010 to allow the installation of a number of hardware upgrades. A modified ICRF antenna was installed, aiming at reduced impurity production during ICRF heating. The ECRH system was further upgraded and will allow more than 4 MW of power to be injected into the plasma, heating the electrons at a microwave frequency of 140 GHz. Finally, the first half of a set of 2 x 8 in-vessel coils was installed for studying the effect of resonant magnetic perturbations on the plasma, most notably the influence on Edge Localised Modes (ELMs). These MHD instabilities are a big worry for ITER, since they may lead to excessive transient power loads. In December 2010, ASDEX Upgrade resumed operation and has already been able to show that large ELM bursts can be suppressed by using the new coil set in a certain plasma parameter range. This important result is of great importance for ITER since further analysis and interpretation should lead to a better understanding of this effect, previously discovered on the DIII-D tokamak in San Diego. This clarification will allow for an educated decision whether to include such a coil set in the ITER design. The set of 2 x 8 coils will be completed during a shutdown in summer 2011, thus further increasing the experimental flexibility of these experiments.

JET has laid the foundations for the next cycle of its exploitation. The major shutdown, which started in 2009 for the installation of the ITER-like wall, is in its final phase and has to be considered as the largest modification of JET since the installation of the pumped divertor in the early 1990s. Preparation of the 2011-12 JET campaigns is nearing completion. The amount of work carried out by the Association staff within the JET Task Forces has been substantial with important contributions from IPP, in particular for the management of the JET Task Force E1. JET's future financial situation is still rather unclear.

Scientific exploitation of the new hardware is ensured for one year of operation only, but will hopefully be extended to the end of 2015. For the final step of operation with the ITER-like wall a deuterium-tritium campaign is currently being discussed with the Fusion Committees.

The ITER cooperation project at IPP is continuing its activities on the major topics: The ELISE test facility, a major step on the pathway to the ITER neutral beam injection system, is being built, R&D on the bolometer diagnostic for ITER continues, as does the work on the design of the ITER ICH antenna within the CYCLE Consortium. A major R&D task on fast switches for high power microwaves was finished successfully and on time. Additionally, IPP is contributing to various heating systems, diagnostics and, in particular, preparation of the physics basis through some direct contracts with ITER or F4E and a number of tasks within the EFDA work programme.

The aim of the work in theoretical plasma physics carried out at IPP's Garching and Greifswald sites is to understand the behaviour of tokamak and stellarator plasmas from first principles. In addition, there is a programme of collaboration with the Max Planck Institute for Solar System Research in Katlenburg-Lindau, where similar methods are being applied to the study of space plasmas. During the year, significant advances were made in the understanding of how fusion plasmas respond to magnetic perturbations. In tokamaks, such perturbations are applied with external coils and affect the density, temperature and rotation profiles as well as the MHD stability. These effects have opened a new research field, and first results were already achieved in 2010. In stellarators, small adjustments in the magnetic field can be used to manipulate the pressure-driven current and the confinement of fast ions as well as the thermal plasma components, which should be highly useful for operation of Wendelstein 7-X. The High Level Support Team of the European High Performance Computing initiative is now fully operational and has already made substantial contributions.

Researchers from edge plasma physics at ASDEX Upgrade and Wendelstein 7-X, from ITER Technology and from the materials research department collaborate in the "Plasma-facing Materials and Components" project, which for many years has provided a field of core competence at IPP with a worldwide reputation. In 2010, one highlight was the understanding of modification of plasma-facing tungsten and beryllium surfaces by nitrogen seed impurities as used in ASDEX Upgrade. In both cases, stable nitrides are formed, saturating at thicknesses comparable to the range of the incident ions. For tungsten the surface nitride layer strongly reduces the sputtering yield. The activities in this field are coordinated with the EU Task Force on Plasma-Wall Interactions, which in turn has been substantially managed by IPP personnel since 2002. Currently, the task force leader position and two special expert working group leader positions are taken by scientists from IPP. Furthermore, the project coordinates the EU coordination action, FEMaS (Fusion Energy Materials Science), as well as the Helmholtz Russia Joint Research Group, "Hydrogen Isotopes Retention in First-Wall Materials for ITER and Fusion Power Reactors".

On behalf of the Directorate and Scientific Board I would like to take this opportunity to thank all staff members for their substantial contribution to the success of fusion research at IPP in the past year.

Scientific Director Sibylle Günter

Content

Tokamak Research	University Contributions to IPP Programme
ASDEX Upgrade	Cooperation with Universities
Stellarator Research	University of Bayreuth
Wendelstein 7-X	Lehrstuhl für Theoretische Physik V
ITER	University of Stuttgart
ITER Cooperation Project	Institut für Plasmaforschung (IPF)11
Plasma-wall-interactions and Materials	Publications
riasina-wan-interactions and materials	Publications
Plasma-facing Materials and Components	Lectures
Plasma Theory	
	Appendix
Theoretical Plasma Physics	How to reach IPP in Garching
Supercomputing and other Research Fields	How to reach Greifswald Branch Institute of IPP 19 IPP in Figures
Computer Center Garching	TET III Tigules
Astrophysics and Laboratory Plasma Studies (ALPS)105	

Tokamak Research

ASDEX Upgrade

Head: Prof. Dr. Arne Kallenbach (Dr. Otto Gruber till July 2010)

1 Overview

1.1 Status of the Machine

The fusion experiment ASDEX Upgrade (AUG) is a medium size divertor tokamak (major radius R=1.65 m, minor radius a=0.5 m, plasma current I_p up to 1.4 MA, toroidal magnetic field B_t up to 3.1 T). It has a high shaping capability and versatile heating and current drive systems

comprising 20 MW neutral beam heating (NBI), an ion cyclotron resonance system (ICRF) with up to 6 MW coupled power and 5 MW installed power of electron cyclotron resonance heating (ECRH). The extension of the ECRH system was continued in 2010, resulting in presently 3 long pulse (10 s) gyrotrons of the ECRH II system installed. The system is equipped with fast steerable mirrors allowing for mode tracking in NTM stabilisation experiments or for fast changes of power deposition or current drive locations. The main enhancement of the ICRF system was the installation of an antenna with broad limiters, which is expected to allow code validation for the antenna design tools directed towards a reduction of tungsten sputtering caused by ICRF operation. AUG's fast integrated control and data acquisition system (CODAC) is being continuously extended in its real time control capabilities. Complementary, several diagnostics have been adapted to real time data processing and evaluation. The plasma facing components in AUG remained completely covered with tungsten, while feedback control of the divertor heat flux with impurity injection is fully embedded into standard high power operation. With the installation of an additional brake for the flywheel generator EZ4, full generator power and energy capability in routine operation has been re-established in December 2010. The newest element for advanced plasma control is the first set of 8 magnetic perturbation coils ('B-coils'), which have been installed during the 2010 vent. These coils have been initially used for ELM control studies, providing urgent results for the ITER decision on the installation of a corresponding coil system.

1.2 Recent Results from Data Analysis in 2010

Due to the substantial machine vent dedicated to hardware extensions from January to November, extensive data analysis of the 2009 experimental campaign was performed, which resulted in a number of important findings. Refinement of the spatial and temporal resolution of pedestal diagnostics allowed a better characterisation of the pedestal structure and gradient recovery during the ELM cycle. Current diffusion calculations revealed the subsequent ELM to occur with a significant delay compared to the edge current redistribution time,

The current ASDEX Upgrade program is directed towards physics input for ITER and a future DEMO design. During 2010, a major vent was undertaken from January till November. Meanwhile, data analysis of previous campaigns revealed important findings. First experiments with the newly installed magnetic perturbations coils showed a drastic reduction of the ELM size without any detrimental effects on plasma stored energy, density or impurity content.

suggesting a missing element in the peeling-ballooning model. Dedicated core transport studies with variations of ECRH deposition in NBI heated H-mode discharges allowed to test predictions of non-linear (GYRO) and quasi-linear (GS2) gyrokinetic modeling of electron and boron impurity density gradients in the core plasma. A key element of this study was the

use of experimental $T_{\rm e}/T_{\rm i}$, $R/L_{\rm T}$ and toroidal rotation values for the simulation, since their theoretical prediction is less accurate. A very good reproduction of the normalised electron density gradient was obtained, where the real frequency of the most unstable mode worked as almost perfect proxy of both measured and predicted $R/L_{\rm ne}$. The transport calculations revealed a transition of the dominant transport mechanism from ITG to TEM turbulence when central ECRH is applied. Concomitantly, a pronounced reduction of the toroidal plasma rotation and the ion temperature in the inner part of the plasma has been observed.

Further transport studies were devoted to reveal the origin of the improved energy confinement routinely observed with nitrogen seeding in AUG, an effect, which has not been obtained in other tokamaks so far. The improvement could be attributed to higher temperatures at the pedestal top, which then proceed to the plasma center via profile stiffness. Fuel dilution by nitrogen ions is supposed to be an important ingredient for the formation of higher pedestal temperatures. Hollow $Z_{\rm eff}$ profiles cause a reduction of the dilution towards the plasma center, which results in the positive effect on the total plasma pressure and energy.

Operational restrictions in case of a damaged tungsten divertor are an important question for the ITER program planning and risk analysis. Dedicated tungsten melting experiments with a pin inserted into the divertor plasma were analysed with the EMC3-Eirene code with regard to the penetration probability of evaporated tungsten into the core plasma. The AUG experiments revealed a very good divertor retention for evaporated tungsten atoms, which could be reproduced by the EMC3-Eirene calculations. Nevertheless, further experiments and modeling work will be required to strengthen the predictive capability of the calculations.

1.3 Experimental Programme in 2010/11 and Technical Enhancements

The AUG programme is directed towards physics input to remaining critical elements of the ITER design and the preparation of ITER operation, as well as addressing physics issues for a future DEMO design. The 2010/11 programme is coordinated by five Task forces, namely

- Improvement of H-mode and integrated scenarios
- Pedestal physics including tolerable ELMs
- SOL & divertor physics and first wall materials
- MHD instabilities and their active control
- Transport

The 2010/11 programme consists of 208 individual proposals led by 93 first authors from IPP as well as from 24 European associations and fusion labs in the US and Japan. A substantial fraction of the proposals is devoted to collaborative ITPA studies, EFDA tasks or experiments proposed by the EU PWI Task Force or EU Topical Groups. About one third of the requested discharges has an external proposal first author. Also one third of the AUG publications in refereed journals over the last years had an external first author.

The current experimental programme, which started in December 2010, gives priority to the exploitation of the newly installed hardware components. Experiments with the magnetic perturbation coils ('B-coils') mounted above and below the midplane aim at the characterisation and understanding of ELM mitigation by magnetic perturbations in order to improve the predictions for a corresponding system in ITER. The ECRH II enhancement brought in total 5 MW installed ECRH power at the end of 2010, which will give a high flexibility for transport studies, NTM stabilisation, operation with low momentum input and better central impurity control. ICRF studies, which are currently hampered by strong tungsten sputtering at the antenna limiters, are directed towards the development of an antenna, which is compatible with tungsten plasma facing components. In a step-wise approach, individual measures to reduce the tungsten source caused by ICRF operation were implemented, and, in parallel used to benchmark antenna design tools.

First AUG experiments in December 2010 were devoted to the characterisation of the plasma response to the B-coil operation, aiming predominantly at ELM control. Already during the conditioning phase for vessel and heating systems, first results on small ELM operation were obtained. A pronounced reduction of the ELM size in type-I ELMy H-mode has been obtained both for even and odd parity in n=2 coil configuration. No density pump-out or energy confinement degradation has been observed under these conditions, and the core tungsten content even slightly decreases. Upcoming experiments will be devoted to the characterisation and explanation of the physics mechanisms leading to the reduction of ELM size and to explore and widen the operational region where ELM mitigation is possible.

The technical enhancement of AUG will proceed in 2011. In completion of the ECRH II project, another gyrotron (with either 2 or 4 frequencies) will be installed in the second half of 2011. During the next machine vent, which is planned

from August till December 2011, another set of eight magnetic perturbation 'B'-coils will be installed. They will allow to investigate perturbations with mode numbers n=3 and n=4. Further modifications to ICRF antennas are foreseen, which should set the path towards full tungsten compatibility. Preparation work continues for the upcoming major hardware extensions, namely the massive tungsten outer divertor target (Divertor III, presently scheduled for autumn 2012) and a further set of 8 magnetic perturbation coils ('A-coils') in the midplane, which are designed for rotating field studies with frequencies up to 3 kHz.

In conclusion, the AUG programme heads towards the development of a high performance reactor scenario, integrated with optimised power and particle exhaust in a high-Z environment and active ELM mitigation.

2 Plasma Rotation with ECRH

The realisation of the connections between rotation and plasma stability and confinement has made the predictive capability and active control of the rotation profile a critical area of tokamak research. In particular, the impact of ion and electron cyclotron heating (I/ECRH) on plasma rotation is an important topic that is not yet understood. The following reports on the effect of ECRH on the toroidal rotation in low plasma current, NBI heated H-mode discharges. In these plasmas the core ion and electron temperatures tend to be quite similar.

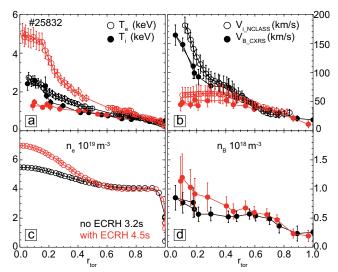


Figure 1: Plasma profiles from discharge # 25832. (a) ion (boron) and electron temperatures, (b) deuterium and boron toroidal rotations, (c) electron density, (d) boron density.

However, as shown in figure 1a, the addition of ECRH power decouples the profiles. Here, the core electron temperature and temperature gradient increase significantly concomitant with a drastic decrease and flattening of the ion temperature profile.

The electron and boron density profiles, (figure 1c&d) also react to the addition of the ECRH. The electron density profile, initially only moderately peaked, is observed to peak further with the largest change in the gradient around midradius. Similarly, the boron density profile is initially flat or slightly hollow at mid-radius and is observed to peak with ECRH increasing by of order 50 percent in the plasma core. A detailed analysis of the electron and boron particle transport at mid-radius in these plasmas show that the experimental behaviors are well described by the theoretical modeling (see section 3). The most dramatic change is seen in the toroidal rotation profile. In purely NBI heated discharges the plasma spins up in the co-current direction and forms peaked rotation profiles. When ECRH is added the rotation decreases significantly leading to flat and occasionally even slightly hollow profiles. An example of this rotation change is shown in figure 1b. The change in the core rotation can be as large as 100 km/s and the effect normally extends over more than half of the plasma radius. In the highest ECRH power cases $(P_{ECRH} \sim 2 \text{ MW})$ the change in rotation is observed to extend all the way to the top of the pedestal. However, for P_{ECRH} < 1.5 MW the edge profiles appear entirely unaffected. Based on these observations, this appears to be entirely a core effect. The rotation change is sensitive to both the amount of ECRH power as well as to the deposition location. The latter was tested using a series of three identical discharges, in which 1.1 MW of ECRH power were injected at different locations from mid-radius to on-axis. With the deposition at mid-radius no change was observed in the rotation profiles and when the ECRH deposition was moved further inward to $\rho_{tor} = 0.2$ only a slight decrease inside of the deposition radius was observed. However, when the power was placed on axis the rotation profile collapsed ($\Delta V_{\odot} > 80$ km/s). In these plasmas the increase in T_e and the decrease in T_i were smallest for the off-axis case and largest for the on-axis one. This suggests a link between the rotation and temperature changes most likely through corresponding changes in the plasma turbulence; with sufficiently high T_e/T_i the plasma moves from an ion temperature gradient (ITG) to a trapped electron mode (TEM) dominated regime. This hypothesis is also consistent with the rotation being a core effect localised to the area, in which the changes in the temperature profiles are greatest. A direct examination of the relationship between the temperature profiles and the rotation supports this hypothesis as it reveals a clear separation of peaked and flattened rotation profiles with increasing T_e. The flattest and most hollow rotation profiles occur for the highest values of T_e, T_e/T_i, and P_{ECRH}. A number of mechanisms that could help to explain the observed rotation behavior including an increase in momentum diffusivity, a change in the NBI torque deposition, a decrease in the Coriolis momentum pinch, an increase in the loss of fast ions, and the braking of the plasma

through the coupling of core modes with the wall, have been examined and rejected. In fact, several of the mechanisms considered, such as the Coriolis pinch and a change in torque deposition, act to increase the plasma rotation rather than decrease it. Altogether, the data suggest the presence of either an ECRH triggered outward convection of momentum or an intrinsic, counter-current directed torque. As there is no way for ECRH to impart significant momentum directly to the plasma, the physical mechanism behind the rotation change is presumed to be related to a Reynolds stress momentum flux triggered by the ECRH induced changes in the temperature profiles and plasma turbulence. The magnitude of the missing convection or torque can be estimated by using computed NBI torque density profiles and making reasonable assumptions on the other quantities in the momentum conservation equation.

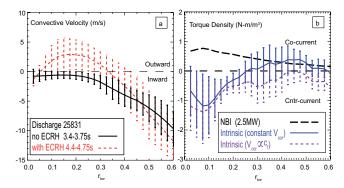


Figure 2: (a) Calculated convective velocities with and without ECRH. (b) NBI torque density profile and calculated intrinsic torque densities using two different assumptions for the convective velocity.

In figure 2a the convective velocities (V_c) calculated via this method for a non-ECRH and ECRH case are shown. Here, it is clear that with ECRH a core localised outward convection of momentum of a few m/s is required to explain the observed rotation profiles. Figure 2b shows the calculated intrinsic torque densities (S_{ECRH}) for the same ECRH case. Here, the intrinsic torque was calculated using two different assumptions for the convective velocity; first, V_C was assumed to remain unchanged from the NBI only case and second, it was assumed to scale with the ion thermal diffusivity. Both assumptions produce S_{ECRH} profiles that are effectively zero outside of ρ_{tor} = 0.4 and are negative in the core with magnitudes that are of the same order as the NBI delivered torque density. The intrinsic torques and convective velocities presented here do not necessarily represent the actual behavior occurring in the plasma discharges. Rather, they seek only estimate the magnitude and direction of additional terms in the momentum conservation equation that could describe the experimental observations. The results of these experiments suggest that in discharges with T_c>T_i an intrinsic momentum flux can exist, which is able to significantly alter the plasma rotation profile.

If $T_e > T_i$ is indeed a necessary condition then this effect will probably not contribute to the rotation profiles in large future devices since significant deviations between T_e and T_i will not be possible in these machines. However, as this effect can alter the rotation profile on present day tokamaks, it should be kept in mind when using data from these devices to extrapolate to future experiments.

3 Particle and Impurity Transport

An important aspect of particle and impurity transport research, relevant also for the prediction of a fusion reactor behaviour, is the effect of electron heating on the electron and impurity density. ECRH is an external means, by which electron and impurity density profiles can be modified. From the operational standpoint this has been used for preventing impurity accumulation, but it also offers the potential for controlling the electron density profile shape. From the physics point of view it is an important tool for identifying the main parameters, on which particle and impurity transport depend. During 2010 research on this topic focused on a set of complementary activities with the aim of investigating the impact of ECRH on both light and heavy impurities in L-mode and H-mode, as well as on the electron density profile. In addition, the potential of using ECRH as an actuator to control the shape of the density profile has been explored. As shown in figure 1 of section 2, applying central ECRH in low I_p , NBI heated, H-mode plasmas led simultaneously to an increase of the electron temperature, a flattening of the ion temperature and the toroidal rotation velocity profile, an increase in the electron density profile peaking, and a more moderate increase in the boron density profile peaking. These results confirm that central electron heating does not lead to "density pump-out" in all conditions. While density flattening in response to central ECRH is regularly observed in low density L-mode plasmas, increased profile peaking can occur at intermediate densities in both L-mode and H-mode plasmas, particularly when there is a significant increase in both the ratio of electron to ion temperature and their corresponding logarithmic gradients; as in these experiments. In addition, in these plasmas it is observed that around mid-radius the boron density profile is flat, or hollow, during the NBI only heated phase, but becomes moderately peaked with the addition of 2 MW of central ECRH. However, around mid-radius the logarithmic density gradient of boron always remains significantly smaller than the logarithmic electron density gradient. These experimental results have been modelled with local linear and nonlinear gyrokinetic simulations (see chapter "Theoretical Plasma Physics", paragraph "Transport Analysis Group"). Neoclassical transport has been included, but found to be negligible in these conditions at mid-radius. The resuts of the modelling are shown in figure 3, and compared to the corresponding experimental values. A satisfactory agreement between predictions and observations is found.

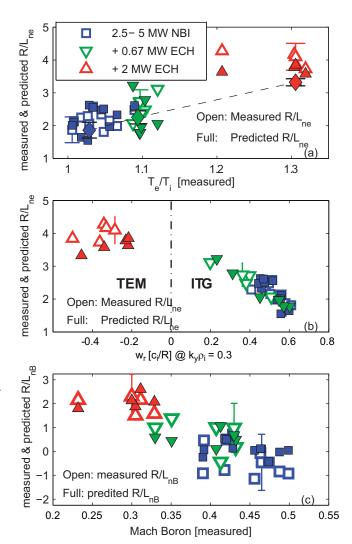


Figure 3: Analysis of representative cases of the three heating phases corresponding to plasma discharges described in section 2. a) Comparison of predicted quasi-linear GS2 (full symbols with squares, triangles pointing down and up), nonlinear GYRO (diamonds connected by a dashed line) and measured (open symbols) values of R/L_{ne} as a function of the temperature ratio T_e/T_c b) Real frequency of the most unstable mode at $k_s\rho_i=0.3$. c) Same comparison on the normalised logarithmic gradient of boron vs. the toroidal Mach number.

This allows the identification of the main parameters and related physical processes, which are responsible for the observed density profile behaviour. The increase in the density peaking with increasing central ECRH power is due to a combination of effects arising from an increase in the temperature ratio and their corresponding logarithmic gradients; with dominant TEM instabilities in the high ECRH power phase, and with ITG modes otherwise. The dependences of the logarithmic density gradient on all these parameters are revealed by the variation of the real frequency of the most unstable mode (which turns out to be a valid ordering parameter

over the entire dataset considered). The modelling of boron turbulent transport suggests that the toroidal rotation and its radial gradient are important ingredients to reproduce the observed boron density behaviour. "Roto-diffusion" is significant, particularly in the cases with NBI only, and allows the observed increase of the logarithmic boron density gradient with increasing ECRH power to be reproduced in the modelling. However, it appears not to be large enough to predict locally hollow density profiles in the phases with NBI only.

The effect of the ECRH deposition position on a medium Z impurity (Argon) has been studied in 0.8 MA ECRH L-modes. A new methodology for the experimental determination of the total impurity ion density produces transport coefficient profiles with high spatial resolution, thus resolving local effects not previously visible, as shown in figure 4.

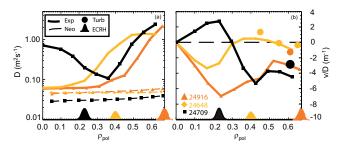


Figure 4: Profiles of D (a) and v/D (b) of Ar for three analysed discharges. Dashed lines in (a) are the neoclassical values calculated with NEOART, large dots in (b) are results from GS2 calculations.

Moving the ECRH deposition inward results in an increase in diffusivity up to one order of magnitude (figure 4a) and a transition of the convection from negative to positive (figure 4b) around the ECRH deposition radius. For deposition close to, or outside of the q=1 surface (localised at r/a=0.3-0.4) the central diffusivity is at neoclassical levels. Linear gyrokinetic calculations of the turbulent drift parameter v/D (figure 4 b) reproduce qualitatively the decrease of v/D with increasing radius outside of the intermediate deposition location. Since the positive drift parameter v/D is predicted to be approximately constant with increasing Z, the effect is expected to persist also for heavier impurities such as tungsten.

The response of the electron density profile to central ECRH enables this heating system to be used to control the shape of the plasma density profile. A real-time density profile reconstruction algorithm has been developed and active feedback control of the shape of the density profile using ECRH as an actuator has been demonstrated. Since the effect of ECRH on the density profile depends on plasma conditions, a controlled increase or decrease of the density peaking has been obtained by the application of central ECRH in L-modes at low or moderately high densities respectively.

4 Improved Confinement with N₂ Injection

To ensure the compatibility of a tungsten wall tokamak with high power advanced scenarios, radiative cooling by N_2 seeding at the plasma edge has proved to be efficient and reliable in reducing the heat load on the divertor plates, together with central ECRH to prevent impurity accumulation and density peaking. A positive side effect has been a systematic confinement enhancement, with H_{98} factors increasing by 10-20 % (figure 5).

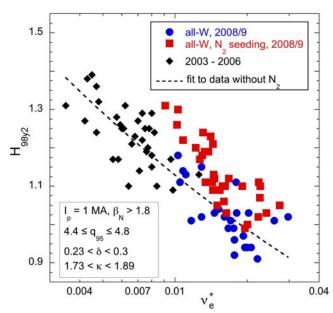


Figure 5: H_{98} as a function of collisionality for early heated improved H-modes. The seeded data points (red) have systematically higher confinement compared to the blue ones without nitrogen. Black triangles are from previous campaigns (before completing the W wall). The lower collisionality is not accessible in the all-W AUG so far.

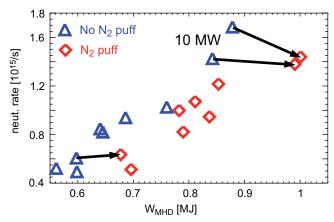


Figure 6: Neutron rate as a function of the plasma energy for pairs of similar discharges with (red) and without (blue) N_2 seeding. The arrows connect some of the pairs. The neutron rate is roughly constant, despite the improved confinement.

The improvement occurs in freshly boronised as well as in unboronised conditions. The neutron yield, however, shows less or no increase, a result of the higher impurity content, with N compensating the higher amount of fast beam ions due to the higher slowing down time of the seeded plasmas, as shown in figure 6.

To identify the causes of the high confinement the core transport has been analysed. The main contribution is provided by the increase of both temperature profiles, in the core and in the plasma edge (see figure 7).

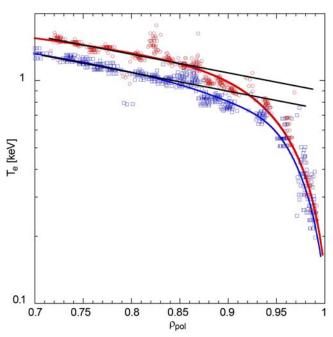


Figure 7: T_e profiles for the seeded (red) and unseeded (blue) cases, in semi-logarithmic scale. R/L_{Te} is constant within $\rho_{pol}=0.85$.

 $Z_{\rm eff}$ is higher in the seeded case, in particular at the plasma edge, as figure 8 shows. This implies that N does not penetrate too deep into the core, while radiating a significant amount of power in the divertor. An independent diagnostic for the

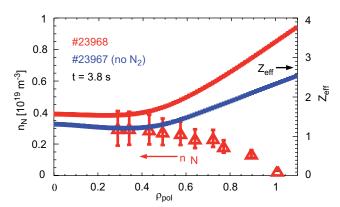


Figure 8: $Z_{\it eff}$ profile from bremsstrahlung for the seeded (red) and unseeded (blue) cases, and N density profile from CX.

nitrogen content is the charge exchange recombination spectroscopy (CX). The measurements are in the correct range but are not entirely consistent with the $Z_{\rm eff}$ deduced from Bremsstrahlung. In particular, the N density profiles from CX are usually not hollow, but rather flat or slightly peaked (see figure 8). Unfortunately N density profiles are available only for a few discharges. A definitive conclusion requires more experimental profiles in the forthcoming campaign. In figure 7 the temperature gradient length R/L_T appears

In figure 7 the temperature gradient length $R/L_{\rm T}$ appears to be unaffected by the N₂ seeding within $\rho_{\rm pol}=0.85$. In fact the core transport is almost unaffected by N; the dilution effect being compensated by higher $T_{\rm e}$ and hence stronger profile stiffness, as non-linear gyro-kinetic simulations in figure 9 show.

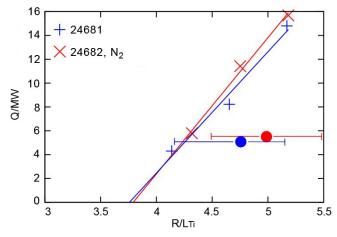


Figure 9: Gyrokinetic calculation of the heat flux as a function of $R/L_{\rm T}$ at half radius. The dilution effect on the ITG mode is compensated by stronger profile stiffness at higher $T_{\rm e}$. As a result, $R/L_{\rm T}$ is unchanged.

Between ELMs, R/L_T does change, however, outside $\rho_{pol}=0.85$, i.e. inside of the pedestal region. The ELM frequency roughly doubles in the seeded case, but the energy loss at each ELM crash is significantly reduced (see figure 10).

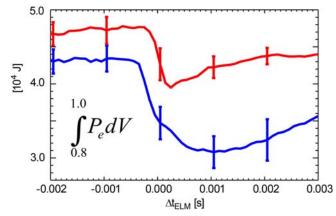


Figure 10: Pedestal energy loss per ELM in the seeded (red) and unseeded (blue) discharge. ELMs crashes are milder in the seeded case.

The fast energy content increases due to the longer slowing down time of the beam ions with higher $T_{\rm e}$, but, it accounts only for a small fraction of the improvement. It comes on top of an improved thermal confinement. The confinement degradation with power in N_2 seeded discharges can be reconciled with that for unseeded discharges by adding a $Z_{\rm eff}^{-0.6}$ dependence. The observed power dependence is lower than predicted by the IPB98(y,2) scaling (-0.54 instead of -0.69), which results in higher H_{98} factors, for both seeded and unseeded discharges, at higher $\beta_{\rm N}$.

5 Controlled Tungsten Pin Melting Experiments

Although AUG has operated successfully as a full-tungsten device for several years now, the fear that off-normal heat flux excursions or a small misalignment of divertor tile castellations in ITER could provoke melting of the material is still considered an argument against the use of tungsten as a plasma facing (divertor) material. In order to test the impact of such an event on the plasma performance a $1\times1\times3$ mm³ tungsten pin was introduced at the outer target plate by the divertor manipulator. By moving the strike point towards the pin melting was induced at a given moment (2.1 s) during the discharge. Weight measurements before and after the experiment showed that 20.6 mg or $N_{W,pin} = 6.7 \cdot 10^{19} \text{ W}$ atoms were lost during the plasma exposure. A first qualitative result was that the discharge is only little affected by this massive impurity event. The total radiation increases by only about 10 % during some 500 ms and consequently no notable effect is seen on either the line averaged density or the stored energy. The melting event was accompanied by the ejection of W droplets, which were observed and tracked by a fast framing camera equipped with an D_{α} rejection filter (figure 11).

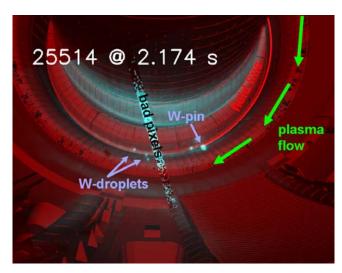


Figure 11: Ejection of droplets from a melting W pin in the divertor observed by a fast framing camera.

This diagnostic provided another important qualitative observation, namely that the droplets all move into the direction of the plasma flow, i.e. away from hot regions of the plasma. This macroscopic transport contributes efficiently to the expulsion of material by the plasma. In order to evaluate the impact on the core plasma quantitatively and to compare it to a main chamber source in the same discharge, $N_{W,LBO} = 4 \cdot 10^{17}$ W atoms were also injected into the edge plasma at the low field side close to the mid plane by means of laser ablation (LBO).

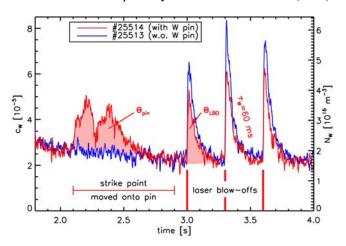


Figure 12: Spectroscopic measurement of the core W concentration during impurity events caused by the melting W pin and laser blow-off.

Simultaneously the core W concentration c_w was monitored spectroscopically as shown in figure 12. Multiplying c_w by the average electron density n_e and the core volume V_c immediately gives the total number of W atoms stored in the core $N_w = c_w n_e V_e$ at a given time (right scale of figure 11). Since the melting event (duration ~500 ms) and the LBO (laser duration 10 ns) occur on quite different time scales, the temporal behaviour of N_W has to be taken into account – here by using a simple 0D model $dN_W/dt = \Phi_{in} N_W/\tau_W$. For this model the total flux to the core is divided into an influx Φ_{in} and an outflux given by N_{in} divided by an average particle confinement time τ_{W} = 60 ms, which is determined directly from the decay time after the LBO. From this model and the measurement in figure 12 $\Phi_{\rm in}$ and also its temporal integral, the core throughput Θ can be determined. Subtracting the W influx from background sources measured during a reference discharge (blue curve) it is found that only $\Theta_{\text{pin}} = 7.9 \cdot 10^{16}$ of the eroded W atoms penetrate the core, which corresponds to a screening efficiency of $S=N_{W,pin}/\Theta_{pin}=850.$ In comparison to that a much higher fraction $\Theta_{LBO}^{-1} = 3.0 \cdot 10^{16}$ of the atoms originating from the LBO cross the separatrix, which reflects the much lower screening efficiency $S_{mc} = N_{W,LBO} / \Theta_{LBO} = 13$ for main chambers of the discrete state of the stat ber sources. An important parameter is also the divertor screening efficiency normalised to that of the main chamber $R = S_{div}/S_{mc} = 65$, the so-called retention factor.

R is a robust number since it does not depend on the absolute calibration of the spectroscopic measurement.

It has to be pointed out that although the nature of the sources in main chamber and divertor is quite different, in both cases the total number of W atoms was used to determine R. At least for the divertor source, however, it is known that a significant fraction of the material remains in the liquid state without ionizing. The fraction of material vaporizing and ionizing from the droplets was estimated from a model describing the power and the momentum balance of the droplet. Here, W is a particular material since above its melting temperature the blackbody radiation emitted from the droplet becomes the dominant energy loss channel. This self-cooling effect strongly suppresses the vaporisation and therefore the disintegration of the droplet. Assuming an ELM averaged parallel heat flux of 60 MW/m² and a number of droplets between 10 and 100 it was found that about 30 % of the material is ionised giving a retention for ionised W of $R_{W+} = 0.3 \cdot R = 20$. In this model, however, neither the possible poloidal motion of the droplet, nor the extreme interaction phase when an ELM interacts with the pin are taken into account. In addition to the experiments, simulations with the Edge Monte Carlo 3D (EMC3) - Eirene code package were performed to model the deuterium plasma as well as the W impurity and the neutral particle transport. An important result of this analysis was that R depends very sensitively on the source position relative to the strike point. At the strike point large gradients of the friction and thermal forces are found, which strongly affect the probability for the impurities to reach the main chamber. In particular the so called flow reversal phenomenon is responsible for this effect. In order to validate these theoretical results against the experiment, further discharges scanning the source to strike point distance are planned for 2011.

6 Technical Systems

2010 was dominated by a major venting to install the first set of magnetic perturbation coils. In-vessel work started on January 11th and was finished with the closing of the entrance port on Friday, 12th November. After leak detection and an extensive baking of about 7 days, the first plasma break-down could be achieved on Tuesday, 7th December. During the remaining 6 shot days in 2010, 101 discharges were started, 59 of them were useful for the physics program that was concentrated on exploring magnetic perturbation coil effects on ELMs. ELM suppression could be successfully demonstrated.

The in-vessel inspection immediately after the vessel opening revealed an excellent status of the machine. Local surface modifications from arcs burning in remote areas of the divertor and on selected components deep in the limiter shadow were observed.

6.1 B-coil Installation and Machine Modifications

During the 10 month of vessel opening the following main tasks had to be fulfilled: (i) Installation of 2×4 B-coils at the upper and lower PSL (figure 15) (ii) a modification of the outer divertor (figure 13) and the ICRH antenna limiter contour, (iii) modification of the pumping system to free space for the installation of current feed through for the lower B-coils and installation of a new vacuum system for the coil feed throughs, and (iv) modification and installation of new diagnostics.

In total 2×8 ELM control coils will be finally installed onto the upper and lower PSL, respectively, in 2010/2011. Forces, in particular during AC operation, require a solid fixing of the coils. Altogether, about 800 M6 and 400 M8 screw threads had to be manufactured inside the vessel and 16 cut outs had to be milled into the PSL.

The B-coil installation was organised in three phases. First, the vessel was prepared for machining of the PSL, i.e. the protection tiles of the PSL and the outer divertor were removed during the first month. This phase was followed by a 3 months machining period to prepare the fixing of all 2×8 coils. During this time, the vessel was wrapped in thick plastic foils to protect in vessel components against metal slivers. After an intensive cleaning of the inner vessel, the installation of the B-coils, the divertor and the diagnostics started in May. In September 2010 2×4 B-coils were installed and the conditioning of the PEEK insulation separating the vessel potential of the current feed through from the PSL potential of the coil casing and acting as CF gasket was done by applying routine baking procedures. Due to the strong and non-uniform shrinking, the baking had to be performed 3 times.

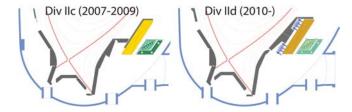


Figure 13: Modification of the outer divertor as a consequence of B-coil installation.

The installation of B-coil current feed throughs required a modification of pumping ducts. AUG is evacuated by 14 turbo molecular pumps (TMP) connected by special pumping ducts to 14 lower C-ports. A subset of 6 C-ports has to be used for the current feed through of the B-coils. The maximum length of a current feed through is 2.2 m, which allows installing them in the short version of pumping ducts. Long (> 3m) pumping ducts had to be reassembled to short versions. This was done for pumping ducts in sector 12 and 3 in 2009 and 2010, respectively. In addition, in sector 1 and 7 two current feed throughs are installed. Here, the pumping ducts were removed.

A third pumping duct in sector 14 will be removed in 2011. The removal of 3 TMP and the reduction of the conductance in the ports that are shared with current feed throughs result in an overall reduction of the effective pumping speed from $10 \text{ m}^3/\text{s}$ in 2008 to $8 \text{ m}^3/\text{s}$ in 2011/12.

The vessel opening was used to modify existing and to install new diagnostics. Diagnostic modification was necessary because for a few diagnostics located in the upper C-ports, the field of view was reduced due to the upper B-coils and the B-coil protections. The X-point manipulator located in the lower C-port in S10 had to be removed to free space for a current feed through. Here a new slim manipulator was designed, manufactured and installed. Further, a new valve for massive gas injection at the inner wall of the torus was designed and installed. The CXRS diagnostics were completed by a poloidal system and a system measuring at the high field side. A third fast ion loss detector was installed at the low field side in the upper part, about 0.5 m above the midplane, of the torus. The gas feeding system below the roof baffle was extended by 8 additional tubes.

6.2 Experimental Power Supply

The main achievement of the Experimental Power Supplies department was the installation and commissioning of a Mechanical Braking System for the flywheel generator EZ4. The goal is to have two independent braking possibilities for every generator in case of emergency. EZ4 has a combined motor/generator. Therefore the easy application of additional braking resistors at the generator side, as implemented previously at the generators EZ2 and EZ3, was not possible. Furthermore, the space available at the generator building is very limited. The solution is a combination of a 7 MW hydraulic dynamometer (water brake) for the speed range from 1650 down to 200 rpm and a 40 kNm disk brake engaged by a clutch at 200 rpm. This system allows a brake time below 10 minutes and thus within the lubrication capabilities of the oil tank, if all pumps would fail. The first step in spring 2010 was the extension of the generator foundation by a 14 tons supporting structure. The Mechanical Braking System has been installed in August, followed by the installation of the water cooling and the control system. To ensure a smooth work-flow and to reduce costs, the project management coordinating the various contractors and the complete design, installation and commissioning of the water cooling control system have been carried out by IPP staff. The commissioning of the complete system took place in December 2010. It turned out that some modifications of the disk brake assembly were necessary. Therefore the disk brake and clutch were disconnected. The dynamometer operates at the generator under experimental conditions without problems. The disk brake will be re-installed in spring 2011.

During the thorough maintenance of generator EZ2, the complete assembly has been dismantled, inspected and re-

assembled. Ultrasonic testing revealed a delamination of one of the generator bearings. The bearing had to be refurbished. Furthermore, damage of the flexible connections of the damper cage have been detected. At generator EZ3, improvements of the control and protection system, as previously implemented on generator EZ4 have been installed. Generator EZ4 has been re-balanced to reduce the vibration level.

The crossbar distributor of the high current power supplies has been extended to allow for a more flexible supply of the vertical coils. The required power and control facilities for the supply of the new saddle coils with 1 kA DC from an existing converter have been prepared.

The re-installation and modification of an old W7-AS high voltage power supply makes good progress. Most of the installation has been completed. The commissioning is scheduled for summer 2011. In addition, a driver stage for the ICRH has been enhanced and an additional "spare" driver stage for the new ICRH test facility has been commissioned.



Figure 14: Mechanical Braking System EZ4.

6.3 Neutral Beam Heating

The eleven months shut-down in 2010 for the installation of the first set of B-coils was used by the NBI group for extended maintenance and upgrades beyond the standard overhaul of the titanium sublimation pumps and a thorough cleaning and inspection of the interior of the two injectors. The biggest task was the replacement of the ageing S5 SIMATIC programmable logic controllers of injector I with up-to-date S7 systems and porting and/or rewriting of their software. Extensive early testing helped to reduce problems at the beginning of the new campaign to a minimum. The experience gained in this S5-to-S7 transition will be helpful to assure an even smoother upgrade of injector II during one of the next extended shut-down periods. Another important improvement was the replacement of the deceleration voltage safety interlock by a new hardware based solution.

This interlock ensures that beam extraction will be stopped if there is insufficient negative voltage at the deceleration grid to suppress back streaming electrons. The previous software based interlock had been a frequent source of erroneous pulse stops during modulated beam operation. The new interlock performs without these flaws.

In early 2009 a new water-cooled wall shielding in the duct was installed to replace its worn out predecessor. This new shielding is also a design prototype for the corresponding component on W7-X. The 2010 shut-down offered the first opportunity for inspection after one full campaign in use. The only minor problem detected was that a few screw hole plugs on the front surface had come out. This problem could be fixed with graphite glue.

Another W7-X component, a HF transformer, was tested on source 7 (Injector II). Despite a design identical to the transformers in use at AUG the test became necessary because the old cable and ferrite types were no longer available. Whereas the new cable proved suitable, the ferrites did not. At the end of November 2010, NBI went back into operation with all 8 sources fully operational and ready to deliver up to 20 MW of heating power.

In co-operation with IPR, India, one of the ASDEX/W7-AS

6.4 Ion Cyclotron Resonance Heating

the EIMAC tetrode.

generators was modified to use an EIMAC 4CK2.500KG tetrode. This type of tetrode is still commercially available, in contrast with the type built into the AUG generators, which is no longer being manufactured. The modification of one of the ASDEX/W7-AS generators allowed testing this tetrode without any risk for the operation of the AUG generators. Even though the modifications are not completed yet, the modified generator has already achieved one second pulses at 1.1 MW and 1.2 MW for 20 ms. Higher power levels and longer pulse length require a change to the external cooling system to fulfil the different requirements of the new tetrode and the modification of the HV power supply to allow different voltages to be applied to driver and final stage. Since all spare tetrodes of the AUG generators are currently in use,

In AUG, one of the antennas was changed to test some of the guiding principles and calculations according, to which antennas can be optimised to reduce impurity production. The limiters of this antenna were widened (see figure 15) and the antenna straps narrowed. Should the experiment confirm the calculations, more substantial modifications are envisaged for the antenna as the optimisation calculations shows that further significant reduction of the impurity production can be obtained.

it is essential to modify the generators step by step to accept

The limiters of the other three antennas were replaced from the equatorial plane up to the top of the antenna with limiters of larger depth, in order to provide protection for the new coils, which have been built into the machine. This increases the distance between the antenna strap and the front of the antenna and will decrease the coupling of the antenna.

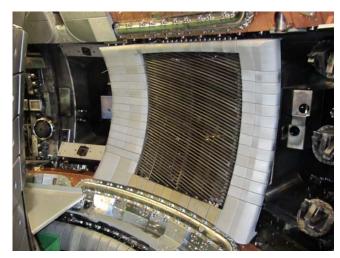


Figure 15: Modified antenna, with wider limiters on both sides, and reduced width antenna central conductors. B-coils are seen above and below the ICRF antenna.

IPP was able to get a steady state generator and coaxial components from the Bayerischer Rundfunk for a symbolic price. This generator has a frequency range of 3.9 MHz to 26.1 MHz, can operate in full steady state at 0.5 MW and at 0.75 MW for one hour and has a modulation bandwidth of 18 kHz. With its lower frequency range and very fast modulation, it provides new experimental options for AUG. Its steady state capability makes it ideal for testing steady state components for ITER or W7-X.

6.5 Electron Cyclotron Resonance Heating

Efforts with respect to ECRH were concentrated on the installation of new gyrotrons in the new ECRH system using the long shutdown. Status at the beginning of the year was one gyrotron absent for repair and one new gyrotron partially in operation but not fully accepted due to problems with the heater contact. In February 2010 the latter gyrotron was operated successfully using a rectifier in the heater supply and was accepted on the basis of an extended guarantee in case of a heater failure. It achieves 0.95 MW (specified: 1 MW) at 140 GHz and 0.85 MW (0.8 MW) at 105 GHz. The repaired gyrotron was delivered in July and accepted in October delivering 0.83 MW (140 GHz) and 0.65 MW (105 GHz), close to its performance before repair. A 3rd gyrotron was delivered in October and accepted in December operating at parameters similar to the one accepted in February. With the acceptance of these two gyrotrons, the second stage of the extension of the ECRH systems nears completion. These gyrotrons were financially assisted by EURATOM preferential support. The first stage, which in its contractual structure leaves more room for development, is not yet completed. The decision if the last gyrotron financed in this framework shall be a 2-frequency or 4-frequency system will be taken in early 2011. The decision depends on independent mechanical stress calculations by KIT, Karlsruhe and IAP, Nizhny Novgorod for the foreseen 4-f operation grooved diamond window, based on the existing samples provided by element-6, Cuijk, the Netherlands. Depending on the risk assessment, a grooved disk will be ordered or an existing flat disk will be used. In the latter case the corresponding 2-f gyrotron is expected to be operational at the end of 2011. A 4-f version with a new grooved disk could be ready in spring 2012. The extension of the new ECRH system in 2010 additionally included the final design of the matching-optics units (MOU) together with IPF Stuttgart.

IPP workshops (ITZ) were heavily involved in MOU production as well as in the completion of the HV-modulators. Further hardware installations concern the holographic reflector plates on the inner heat shield used for O2-heating. Together with IPF Stuttgart (see section 9), additional thermocouples have been integrated based on experimental results in 2009. In the 2011 campaign these thermocouples will be used for a real-time safety system, ensuring that the microwave beam either stays on the plate or is switched off. The beam moves owing to variations of the refractive index, which in turn depends on the electron density profile. Another major hardware system installed in the new part of the AUG-ECRH is the FADIS system developed at IPF, Stuttgart and TNO, Delft and tested in the ECRH installation of W7-X. The system allows switching power between two outputs either by mechanical tuning of the interference setup or by variation of the gyrotron frequency. An application foreseen for 2011 is to combine NTM stabilisation by a modulated beam (O-point heating) with central heating of the plasma. Such applications are especially interesting for devices with more beam lines than gyrotrons, as planned for ITER.

6.6 Data acquisition and computer infrastructure

The data acquisition and discharge control system was routinely operated. Two special topics are highlighted below.

- The Video Real-time Safety System (VRT)

The VRT for machine protection is based on analogue CCD/CMOS cameras installed in different ports covering nearly the whole in-vessel surface. All these cameras are recorded and archived as MPEG streams, some of them are used to detect possible overheating of built-in components and movable probes in real-time. The system is in standard operation for all discharges. A principal scheme of the realisation and implementation of the system is illustrated in figure 16. The connection to the discharge control system is implemented via a status signal, reporting periodically (40 ms) if local overheating of parts of the divertor is detected or if one of the inspected manipulators is glowing in the

pre-defined region of interest. If that occurs the discharge is terminated by a soft pulse stop. This happened for 2 % of the plasma discharges within the last campaign.

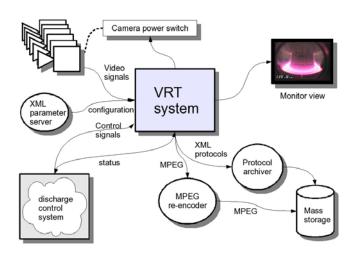


Figure 16: Data flow diagram of the real time video system.

- Infiniband for Real-time Feedback

Benchmarking MPI (Message Passing Interface) as a means to run data analysis codes in parallel on multiple computing nodes, has verified that this concept seems a promising way to speed up physics calculations and extend the normal size of control codes for real-time feedback. However, the communication latency over Ethernet was identified as a main bottleneck when trying to tune this sort of cluster applications for an integrated diagnostics and control environment. This led to setting-up a small Infiniband computing cluster to test possible advantages of this high-speed communication method over Ethernet. The tested cluster consists of two Solaris X86 eight-core nodes, a Sun Infiniband switch, and the Sun HPC implementation of the MPI software suite for Solaris. The overall communication latency for data buffer sizes varying from 64 to 8096 bytes over Ethernet was found to be 180 to 700 µs. In contrast latencies found with the same benchmark code just replacing Ethernet by Infiniband were 22 to 140 µs. This improvement in latency will allow real-time criteria to be better satisfied.

7 Core Plasma Physics

7.1 Energetic Particle Losses Induced by Alfvén Eigenmodes

Convective and diffusive energetic particle losses induced by shear Alfvén Eigenmodes (AE) have been recently observed in the AUG tokamak. Simulations with the full orbit code GOURDON and the guiding center drift orbit code HAGIS have been performed to better understand the orbit topology of the escaping ions and the nature of their interactions with the AE wave fields. Figure 17 shows the typical trajectory of a lost ion in the presence of AE.

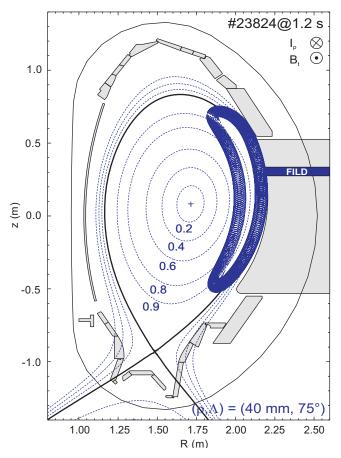


Figure 17: Typical trajectory of an escaping ion in the presence of AE.

7.2 Sawteeth Destabilisation of Fast Particle Stabilised Sawteeth with ECCD

It is often observed that large sawteeth trigger neoclassical tearing modes (NTM) well below the usual threshold for this instability. At the same time, fast particles in the plasma core stabilise sawteeth and make large crashes possible.

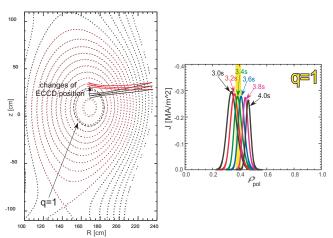


Figure 18: Changes of the electron cyclotron current drive position and shapes of the current related profiles.

This fast particle stabilisation effect will be much more important in ITER. The flexible heating system of AUG allows an ITER relevant demonstration of fast particle (NBI+ICRH) sawtooth stabilisation. Such sawteeth can then be destabilised by electron cyclotron current drive (ECCD) as foreseen in ITER. Results of first experiments show that moderate ECCD from a single gyrotron is able to destabilise the fast particle stabilised sawteeth. A reduction in sawtooth period by about 40 % was achieved in these experiments. The predicted sawtooth amplitude in ITER is about the critical size to trigger NTM. Thus, a 40 % reduction of the sawtooth period could be sufficient to avoid such triggering. Further experiments are planned to provide a solid basis for extrapolating to ITER conditions.

7.3 Hollow Central SXR Profiles and Inverse Crashes

Hollow soft X-ray radiation (SXR) profiles and repeated inverse crashes (IC), where profiles relax from hollow to flat, have been observed in H-mode discharges with central ECRH (see figure 19). As in the case of sawtooth crashes (SC), T_e profiles are flattened during IC with the inversion radius close to q=1. Both types of crashes have (1,1) precursors. Therefore, it is assumed that IC are plain SC with initially hollow SXR profiles. Since central n_a and T_a profiles are peaked, impurity densities must be hollow. The related central (unfolded) radiation can be up to 5 times lower than the maximum. Z_{eff} can hardly account for this variation, so hollow tungsten profiles must be assumed. Neither effects of plasma rotation nor turbulent transport with increased T_a gradients can account for the hollowness. The q=1 modes are observed with hollow SXR profiles and a radiation peak close to q=1. However, W snakes are not observed. In many discharges (also without ECRH) several (1,1) modes with different frequencies simultaneously at the same position are observed. Modes and profile shape are often correlated. SXR profiles are hollow only when a (1,1) mode with lower frequency is dominant.

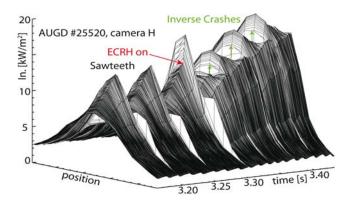


Figure 19: Line integrated SXR profiles changing from peaked to hollow before the crashes when ECRH is switched on.

7.4 ECCD Based NTM Control Using Real-time Computers

Advanced scenarios of tokamak operation are considered key to achieving efficient fusion power. These scenarios are prone to the occurrence of so-called magneto-hydrodynamic modes, which form magnetic islands. Neoclassical Tearing Modes (NTM) deteriorate the plasma confinement substantially. The method of choice for controlling and avoiding NTM is deposition of ECCD inside the magnetic island for stabilisation. In the newest approach, the ECCD deposition is controlled by a moveable mirror, which directs the ECRH beam. The magnetic equilibrium determines the location of rational surfaces where an instability may develop (usually m=2, n=1 or m=3, n=2) even before the island appears in the plasma. ECE measurements can make use of correlation analysis (T_a fluctuations and magnetic signals) to determine the actual mode location, when it is present. Both methods are compatible with real-time (RT) control.

The ECCD deposition location can be attained from correlating ECE signals by using a modulated ECRH beam, but for predictive calculation of the deposition, a real-time version of the TORBEAM code is used. RT-enabled diagnostics provide the input data to TORBEAM (equilibrium, electron temperature and density and actual mirror angle).

A proof of principle discharge with pre-programmed (feed-forward) mirror positions and sufficient heating to trigger an m=3, n=2 NTM was run successfully in December. Data analysis shows that the movement of the ECCD deposition by means of tilting the mirror was indeed the key parameter to stabilise the magnetic island, which was unaffected by the ECCD until the correct mirror angle was set by the control system. It was shown that an NTM could be stabilised by ECCD current drive. This is the first time at AUG, where this was achieved by moving the ECRH mirror instead of changing the ECRH resonance by ramping the magnetic field. Experiments closing the now possible control loop and thus demonstrating active control of NTMs by ECCD are planned for 2011.

7.5 Z_{eff} Profile Analysis

Effective ion charge $Z_{\rm eff}$ profiles are routinely analysed from the combined analysis of CXRS- and bremsstrahlung diagnostics applying the concept of Integrated Data Analysis (IDA) within the framework of Bayesian probability theory. The robust estimation technique applied to the complementary and redundant data allows one to resolve and mitigate data inconsistencies due to wall reflections, gas fuelling, passive or active line distortion of the bremsstrahlung background, and transient distortions. The estimation of $Z_{\rm eff}$ profiles relies on the knowledge of the electron density and temperature profiles, which are themselves obtained from an integrated analysis of the lithium beam, interferometry, and ECE diagnostics. The results are validated with low-impurity ($Z_{\rm eff} \cong 1.0$) and helium discharges ($Z_{\rm eff} \cong 2.0$).

With a temporal resolution of 50 ms, the correlation of the improved plasma confinement induced by nitrogen seeding with the increase of $Z_{\rm eff}$ can be studied. The enhancement of $Z_{\rm eff}$ with nitrogen seeding is stronger at the edge than in the core (see figure 20). According to the peeling-ballooning limit of the electron transport barrier an increased $Z_{\rm eff}$ at the edge results in an increased electron temperature due to the deuterium dilution. Profile stiffness results accordingly in an increased H-factor.

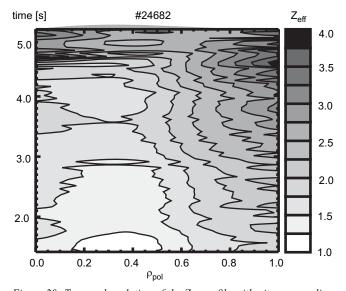


Figure 20: Temporal evolution of the $Z_{\rm eff}$ profile with nitrogen seeding starting at 1.7 s . Tungsten starts to accumulate at 4.6 s.

7.6 Disruption Analysis and Mitigation

The main achievements of the last year in the field of disruption studies can be summarised as follows:

- (1) The halo current can reach 50 % of the plasma current, independently of the disruption type, but this maximum value lasts a fraction of a ms. The question whether 2D MHD transport codes like DINA and TSC can reproduce this maximum is under investigation. Preliminary results are positive.
- (2) The toroidal halo current asymmetry is typically caused by a large magnetic perturbation with a toroidal mode number n=1 and appears at the maximum of the vertical displacement during the current quench. This perturbation lasts one millisecond. Long-life asymmetries are an exception in AUG. They neither exhibit a regular periodic structure nor are locked. Large horizontal forces on the vessel have not been observed.
- (3) A preliminary classification of disruption groups based on their physical cause, permits the application of discriminant analysis to find functions describing the boundary between each disruption group and the safe plasma states. Disruptions caused by edge cooling can be predicted by a simple linear or quadratic function of 3 to 5 plasma variables.

- Disruptions following β -limit and impurity accumulation are more unpredictable and additional precursors (MHD for example) must be used for their forecast.
- (4) The attainment of the critical density in our medium size tokamak seems to be technically and physically possible. Therefore a fast valve was designed, built and installed on the high field side. It is scheduled to go into operation at the beginning of 2011. The use of multiple valves is expected to favor the redistribution of the injected impurities around the torus, which would otherwise be prevented by the low ion temperature and mobility.

7.7 A Real-time Grad-Shafranov Solver

The magnetic equilibrium for a tokamak is described by the Grad-Shafranov equation in the poloidal flux, Ψ. The algorithm for the solution of Poisson's equation in cylindrical coordinates using discrete sine transforms, DST, along the Z axis and a tridiagonal solver has been adapted for solving this equation in real-time. This algorithm is an alternative to the commonly used cyclic reduction algorithm.

The Ψ generated by the external poloidal field coils is realised as a matrix-vector multiplication using pre-calculated factors from the Green's function for a current in a circular hoop. A calibration procedure involving the measurement responses to current in each poloidal field coil in the absence of plasma ensures that the probe positions and calibration factors were as accurate as possible.

The first step of the solver has zero as boundary conditions on the edges of the grid. For this solver step it is only necessary to compute those elements at grid point neighbors to the boundary. A special inverse DST can then be used to calculate only the needed elements of the grid rather than the inverse DST for the whole grid. The second step of the solver is carried out with boundary conditions from the first solver step but without current source terms on the right hand side of the Grad-Shafranov equation. Only the first and last elements of each row are non-zero so that a special DST that is significantly faster than the full DST can be used. The tridiagonal solver is applied to this second solver step and the results of the first and second solver steps are added. The solution of the Grad-Shafranov equation is then calculated by an inverse DST, realised as a matrix-matrix multiplication with pre-calculated factors. A weighted least squares fit to the magnetic probe and flux loop difference response yields three coefficients that scale the current profile form factors to give the current profile that is consistent with these measurements. The real-time Grad-Shafranov solver runs with a cycle time of 0.63 ms.

7.8 Magnetic Field Dependence of Pellet Injection

Cryogenic hydrogen isotope pellet injection is an effective particle refuelling method and, in addition, an established ELM control method at present fusion devices, foreseen for ITER as well. In both cases, the penetration depth of the pellet is a key parameter as the large fuelling pellets have to penetrate beyond the pedestal region for effective core fuelling, whereas small ELM pacing pellets have to reach far into the pedestal area for the prompt ELM triggering mechanism to take place.

At AUG an empirical penetration depth scaling had been established based on statistical model selection methods to determine the statistically important variables in pellet ablation based on the HFS-PAD pellet ablation data base. The scaling showed reasonable agreement with ablation theories, the neutral gas shielding model and the hybrid pellet ablation model regarding the electron temperature, pellet mass and velocity. The empirical scaling however indicated negative magnetic field dependence with an exponent of $-0.41(\pm 0.08)$ that was in strong disagreement (even regarding its sign) with our present theoretical understanding. This may play a significant role in ITER, as its foreseen toroidal magnetic field is 5.3 T compared to about 2.5 T of the measured depths in our data base. In order to resolve this discrepancy, dedicated experiments have to be carried out at AUG to investigate the magnetic field dependence in a single parameter scan especially covering higher toroidal magnetic fields. Recent experiments indicate a magnetic field dependence with exponent of $-0.63(\pm0.2)$ in agreement with the prior empirical scaling.

8 Edge and Divertor Physics

8.1 Characterisation of the Pedestal Width

The analysis of the edge pedestal relies on an accuracy, which is near the limits of plasma diagnostics. Therefore, it is important to eliminate all other sources of uncertainties. Pedestal information from different machines is often derived with different analysis codes, which may lead to small systematic deviations. In cross machine comparisons of pedestal parameters even such relative small deviations can result in unexpected discrepancies. An initial comparison of the AUG pedestal width with literature values from DIII-D showed systematically larger pedestal widths for AUG. This discrepancy could be resolved by analyzing data from both devices with the same code for pedestal characterisation. A two-line analysis yielded pedestal widths of the electron temperature $w_{Te} \sim 1.8 \pm 0.3$ cm and of the density w_{ne}~1.5±0.3 cm for both devices without significant deviations throughout the whole dataset.

8.2 Modelling of Divertor Detachment

The multi-fluid plasma edge code package coupled to a Monte-Carlo transport code for neutrals, SOLPS5.0, is used to simulate the SOL and divertor of AUG. The code validation effort against experimental data of Ohmic and L-mode discharges for He in forward only and for D fuelled in forward

and reversed B_t in lower single null configurations has been continued. As long as one of the two divertors is not strongly recombining and the other is at most in a medium recycling regime, satisfactory agreement between the results from simulations and experimental data can be achieved. Neither the experimentally observed high particle fluxes and densities in the far SOL of the inner divertor target at medium to high line averaged densities, nor the strong detachment along the inner vertical target plate, nor the ion flux densities close to the detachment threshold of the outer target can be simulated numerically.

8.3 ELM Resolved Edge Profiles

Profiles of the radial electric field in-between ELMs are inferred by analyzing the HeII line radiation at the plasma edge. First results are in agreement with neoclassical expectations. With dedicated edge diagnostics it is found that during the ELM crash the electron density (n_e) and temperature (T_e) profiles flatten and that the re-steepening of the T_e profile stagnates when the n_e profile starts to steepen. After the n_e and T_e profiles have gained their pre-ELM shape, no ELM appears then, but large scale fluctuations are observed. It cannot be confirmed that the delay in the recovery of the edge current density due to current diffusion sets the time for the next ELM.

8.4 Ion Temperatures in the Scrape Off Layer

Using the Retarding Field Analyser (RFA) technique, ion energies carried by ELM filaments have been measured for the first time in the far scrape-off layer (SOL). Energies, exceeding 160 eV have been found 5-6 cm outside the separatrix, with a decay length of about 2 cm. The measured ELM ion temperature (T_i) in the far SOL is in the range 50-80 eV, in good agreement with the predictions from two simple collisionless models of ELM parallel transport. In between ELMs, $T_i \approx T_e \approx 10$ eV is observed in the far SOL, consistent with relatively strong ion-electron thermal coupling in this region.

8.5 ELM Characteristics in Helium Discharges

To achieve sufficient confidence on the predictions for ITER on ELM behaviour and mitigation techniques it is important to compare the ELMs in He and D plasmas in present day experiments. In AUG helium H-mode discharges a similar ELM phenomenology as in deuterium is observed, showing both type-I and type-III like behaviour. A somewhat larger heating power in He than in D seems to be needed to enter reliably the type-I regime. The fraction of ELM energy losses (W_{loss}/W_{MHD}) lies in the same range as in D and scales similarly with confinement and ELM frequency (see figure 21). About 50 % of the energy loss reaches the targets. These first results indicate that the type-I ELM regime in helium is reached with $P_{tor}/P_{thr}(He) \geq 1.5$. Assuming for ITER about

70-80 MW available for heating and the predicted $P_{thr}(D)$ =53 MW, type-I ELM may be reached only if $P_{thr}(He) \approx P_{thr}(D)$ as observed at AUG. If the L-H power threshold is considerably higher as for example found in JET, type-I ELM in helium may be still obtained at reduced plasma current.

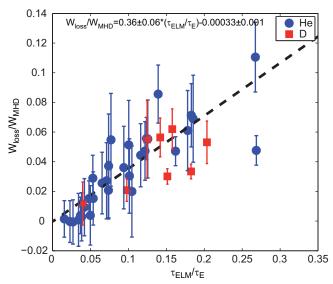


Figure 21: Energy loss fraction as a function of ELM period normalised to the energy confinement time for discharges with $\delta > 0.2$. The linear fit is shown with a dashed black line.

8.6 Type-II ELM Experiments

Edge localised modes with high frequency and low power (type-II ELMs) occur at high triangularity and close to double null in AUG with full tungsten plasma facing components. The transition from type-I to type-II ELMs was shown to occur above a collisionality threshold. For the first time a characteristic MHD feature around 40 kHz has been localised. The fluctuations are observed in a wide region from the pedestal inwards. Their amplitudes on the low field side of the plasma exhibit maxima above and below the mid-plane. The fluctuations move in the electron drift direction and lead to reduced edge electron temperature gradients. The reduction in edge pressure gradients is connected with these MHD fluctuations, which affect the T_e but not the n_e profiles.

8.7 Results on Impurity Seeded Discharges

Radiative cooling has been applied in a large variety of plasmas ranging from improved H-modes at intermediate density and heating power to discharges with very high heating power ($P_{aux} \approx 20$ MW) or high density and radiation fraction exploring the type-III ELM regime. Generally, the radiated power from the X-point and divertor region increased in N_2 seeded discharges by more than a factor of two, but the core radiation is almost unchanged.

In type I ELMy H-modes the ELM averaged radiation level increased from about 60 % of the input power in unseeded discharges and raises to 80 % in nitrogen seeded discharges. This increase is mainly in between ELMs, whereas the absolute value of the additional radiation during ELMs is nearly the same for both seeded and unseeded discharges. About 20-25 % of the ELM energy is found as radiation in unseeded discharges and 30-40 % in nitrogen seeded discharges, due to the smaller ELM size (see figure 22).

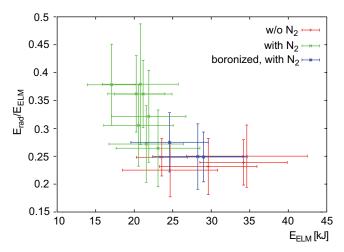


Figure 22: Normalised ELM radiation E_{rad}/E_{ELM} versus ELM energy E_{ELM} in unseeded and N, seeded (unboronised/boronised) discharges.

This value is comparable to the values found in former campaigns with mixed carbon and tungsten PFCs. Consequently, the power load to the divertor targets during and in between type-I ELMs drops significantly with nitrogen seeding. Even for discharges at highest heating power, good energy confinement could be obtained simultaneously with a low impurity content of the core plasma and efficient power control in the divertor. In seeded type-III ELMy discharges a strong increase of the confinement with plasma pressure was observed. In parallel, a very moderate power flux in the outer divertor and a strong suppression of the W influx could be achieved. Investigations using a mixture N_2/Ar as seeding gas revealed a change in central particle transport compared to discharges with N_2 seeding only.

8.8 Tungsten Sputtering during ICRH

ICRF operational experience with increasing coverage of the wall with W-coated PFCs is confirmed by the analysis of the rise of W concentration $c_{\rm W}$ during RF power application. Although such components as the upper PSL and the divertor horizontal plate, which connect to active antennas along magnetic field lines are non-negligible W sources, the antenna limiters are mostly responsible for the $c_{\rm W}$ rise. In recent experiments with rearranged antenna pairs a discrete operation of neighbouring antennas in a wide range of plasma

parameters could be performed. They revealed that the connection length of flux tubes starting at limiters can undergo a step-like change, which correlates to dramatic changes of the W sputtering patterns measured spectroscopically. This indicates that the local magnetic geometry is at least as important for the W sputtering as the distribution of RF near-fields at the antenna. The sputtering is also likely to be influenced by E×B density convection in front of the antenna, which is implied from the experiments comparing discharges with normal vs. reversed toroidal field. A modified ICRF antenna, which aims at reduction of the W sputtering has been installed in sector 12. The first results of antenna comparison are anticipated early 2011.

8.9 Transport of Tungsten in the Plasma Edge

The transport of tungsten in the plasma edge was investigated by the use of a modulated W-source at the low-field side. It was possible to observe the phase of the W-modulation at three radial positions ($\rho_{pol}=0.7,0.9,0.97$) and the amplitude of c_W at one position ($\rho_{pol}=0.7$). Additionally, a scan in upper triangularity and gas puffing was performed. A 1-D model (STRAHL) predicted changes in phase shifts in case of changed radial transport parameters. However, the observed phase shifts showed no correlation with neither triangularity nor gas puff. Therefore, radial transport appears to be unaltered by the scanned parameters. On the other hand, changed parallel transport in the SOL and prompt W-redeposition could explain the strong dependence of W-concentration on gas puffing observed in the experiments.

The transport in the edge transport barrier (ETB) is dominated by the effect of Coulomb collisions. W has an even higher collisional diffusion coefficient than the light elements, for which an agreement with purely collisional transport could be deduced from direct measurements. The collisional transport produces a strong inward pinch and a respective peaking of tungsten, which is relaxed during an ELM. When modelling the edge transport with the STRAHL code that treats the parallel losses in the SOL with volume loss rates, the impurity confinement time shows a strong decrease with increasing ELM frequency as experimentally observed. However, there is an equally strong dependence on the characteristic parallel loss time in the SOL, which is at present not well known and requires further measurements to restrict this parameter in the model (see above). The dependence on the diffusion coefficient in the SOL is very weak. In the ETB of ITER, the collisional impurity transport coefficients are about a factor of 20 smaller than in AUG. Thus the time to build up a strong edge gradient is substantially longer. In addition, the ELM frequency has to be kept high (around 20-30 Hz) in order to achieve small ELMs. Thus, the average edge gradient will be quite small, provided that the ELMs do not lead to a much smaller increase of the effective diffusion coefficient than used in the model (see figure 23).

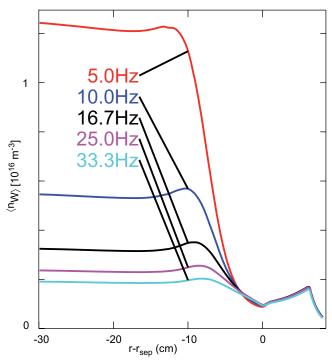


Figure 23: Modelled tungsten profiles in the ITER edge averaged over one ELM cycle. The profiles were calculated for different ELM frequencies and are normalised to the same effective source rate.

8.10 Characterisation of Arcs

The arcs observed in AUG can be categorised in arcs ignited at components in contact to the main/SOL plasma and arcs in remote areas, i.e. areas without field line contact to the main plasma. A systematic investigation of localised glow/arc events detected by the video system identified a preferential region above the upper PSL. Events at this position are found in discharges with plasma currents above 0.9 MA, mostly during phases with decreasing plasma stored energy. It turned out, that the events themselves are not the reason for the decay of the plasma stored energy, but a correlation with the ECR-sniffer probe reveals that they are due to a local cut-off for ECRH absorption. The resulting stray radiation is absorbed by PEEK insulators nearby resulting in local electrical fields and overheating. Detailed investigations were performed on the plasma induced, monopolar arcs. High resolution, fast camera observations show single arcing events and identify ELMs as possible initiating process of arcing.

As high Z PFCs show low physical sputtering other erosion mechanisms as for example arcing have to be taken into account to get the total erosion. Arc traces are observed locally in AUG, especially at the inner baffle region. The typical width of the arc tracks in the order of 10 μm requires the combination of different analysis techniques to yield the total erosion. High resolution photographs from complete tiles were taken to derive the total area affected by arcs.

A confocal laser scanning microscopy allowed measuring the erosion by single arcs and their details were studied by SEM. Strong erosion by arcing was always found if the surface conductance is poor, i.e. in deposition dominated regions, whereas at pure tungsten surfaces almost no erosion by arcing was determined.

8.11 Dust Investigations

2D dust particle trajectories were extracted from fast framing camera videos by a new time- and resource-efficient code developed at University Nancy. Using hybrid global and local intensity thresholding and linear trajectory extrapolation individual particles could be tracked up to 80 ms even under challenging conditions such as high particle density and strong vacuum vessel illumination. In parallel, dust has been trapped on five strategically positioned silicon wafer collectors. Characterisation of the outer morphology and determination of the elemental composition of 5·10⁴ particles were performed via automated SEM-EDX analysis resulting in the definition of a first preliminary dust classification scheme linking several classes to their most probable production sites.

8.12 Gas Balance Investigations

Gas balance measurements were repeated with extended discharge length, yielding to steady state phases up to 3.1 s, during which the gas inlet equals the amount of gas pumped. A series of equal discharges with different gas puffing levels confirms the importance of the amount of gas retained in the wall to reach this steady state phase. Obviously, the gas balance is dominated by dynamic wall loading and outgassing after the discharge. To investigate the out-gassing in detail, special discharges without active pumping and low gas puff rate were performed. In these discharges three components with a gas release on different time scales could be identified. The investigations show high relative gas retention similar to that reported from ALCATOR C-mod, but the absolute amount of gas retained is almost the same as in high density scenarios. This confirms the earlier observation of an absolute amount of gas loading necessary for dynamic wall saturation.

9 University of Stuttgart

9.1 Simulations on ECRH Propagation

The fullwave code IPF-FD3D was used to investigate the impact of fluctuations on ECRH beam quality. Several density profiles were taken from the shot database and were overlaid with random fluctuations or single blob structures at various radial positions. An ECRH beam in the standard central heating scenario was injected and its position and mode composition at the resonance layer was analysed. It was found that extreme fluctuation strengths or blob densities

lead to significant broadening and spatial deviation of the beam. In addition, the beam quality was seriously degraded by the appearance of higher Gaussian modes and a strong divergence. A given density blob's influence on the beam degradation depended only weakly on its radial position but strongly on its size and density. It is planned to incorporate experimental knowledge of fluctuation levels into the simulation to assess if there is any significant impact on ECRH in actual operations.

9.2 Langmuir Probe Enhancement

Electronic problems have been discovered in the probe system of the midplane manipulator. Investigations of plasma turbulence and intermittent density filaments in the scrapeoff layer have sometimes been dominated by cross-talking cables, electro-magnetic pickup and circuit oscillations. The cross talk amplitudes were reduced by more than three orders of magnitude after reconnection of the coaxial cables outer conductors at the manipulator exit. Furthermore, a reduction of electro-magnetic pick-up from the torus hall is expected. Cable low-pass characteristics and non-linear resonances in ϕ_{float} measurements could be suppressed by impedance transformation close to the probe tips. A newly designed passive filter will be available to suppress aliasing in future experiments. Some former physics results might need to be reviewed if they were based on fast measurements with the old probe setup to rule out systematic errors.

9.3 Holographic Mirrors for O2-mode Heating

In the last years, electron cyclotron heating scenarios were developed in order to overcome the X2-mode cutoff in ITER-like plasmas at high confinement and densities near the Greenwald limit in AUG. The O2 mode, which has twice the cutoff density of the X2 mode is one option, but suffers from incomplete absorption. To increase the absorption of this mode to non critical values, the shine through beam is reflected at two holographic mirrors, mounted at the inner wall, to ensure a second pass through the plasma core. For safety issues in these reflectors additional thermocouples have been integrated. In the 2011 campaign these thermocouples will be used for a real-time feedback system, ensuring that the microwave beam either stays on the plate or is switched off, as it moves due to variations of the refractive index depending on the density profile.

10 International & European Cooperations

10.1 IEA Implementing Agreement

The IEA Implementing Agreement on 'Cooperation of Tokamak Programs (CTP)' was created from a merger of the IEA Large Tokamak Agreement and IEA Polodial Divertor Agreement, which formally, after five years of discussion, was accomplished in June 2010. The objective of this

Agreement is to advance toroidal plasma physics and technologies by strengthening cooperation among tokamak programmes. The signatories of the agreement are EURATOM, Japan, Republic of Korea, and the United States. Both China and the Russian Federation have been invited to join the agreement. The exchange of information between parties comprises almost all experimental, theoretical and technical areas of fusion-oriented research. For IPP most important is that assignments of scientists, engineers and other technical experts to work at the facilities of the other contracting parties are covered by this agreement. In 2010 several of such visits took place and are reported in the following.

A multi-weeks stay of an IPP scientist at the Plasma Science & Fusion Centre at MIT, Cambridge, US gave an opportunity to exchange the experiences on plasma wall interaction physics and edge plasma physics. This included radiative cooling by impurity seeding, pedestal physics, plasma wall interaction in a high-Z environment during ICRF heating, operational limits of the I-mode, pedestal rotation signatures and charge-exchange with background deuterium. Special focus was put onto the active charge exchange spectroscopy system using a simple deuterium gas puff, which is operational at the inboard and outboard side of Alcator C-Mod. A similar system has been designed for AUG and design assumptions could be verified by a comparison. Using this system at Alcator C-Mod, the impurity transport at the H-mode pedestal was investigated. The discharges of interest were the enhanced D_{α} H-modes. First indications of the analysis confirm the observations from AUG that the impurity transport at the edge pedestal exhibits a strong inward convection.

The analysis of the edge pedestal relies on an accuracy, which is near the limits of plasma diagnosis. In particular, cross machine comparisons of pedestal parameters may suffer from small deviations resulting in unexpected discrepancies. An initial comparison of the AUG pedestal width with literature values from DIII-D showed systematically larger pedestal widths for AUG. By sending an IPP scientist to GA, this discrepancy could be resolved by analyzing data from both devices with the same code for pedestal characterisation (see section 8.1).

The understanding of apparent inconsistencies between the calculated distribution of neutral beam current density and measured changes in q-profile is important for predictions of q-profile evolution in future devices. In 2008, a series of plasmas have been done on JT60-U (JAEA, Naka, Japan) to better understand the localisation of NBCD. Those plasmas had 3 different phases, first an on-axis NBI phase to create a target plasma with a stable density and energy content. In the second phase, some of the on-axis NBI was replaced by off-axis injection to change the equilibrium q-profile by NBCD. The third phase served as a reference for the first one. As many parameters as possible were kept constant

during the experiment so that the MSE measurement only detects q-profile changes caused by off-axis NBCD. During a stay in Naka, Japan, an IPP scientist compared these JT60-U pulses with ASTRA simulations. The time dependence of MSE angles calculated with ASTRA does not agree with the time evolution measured with the MSE diagnostic. At the moment there is no apparent explanation for this discrepancy and further analysis will be necessary before conclusions on the localisation of off-axis NBCD in JT60-U can be drawn. The next step in the process to improve the understanding of off-axis NBCD will be joint JAEA - IPP experiments on AUG in 2011.

10.2 EURATOM Associations

2010 was a year devoted to analysis of experiments conducted in previous campaigns. 25 out of 70 AUG-related publications in refereed journals were written by external first-authors. Thus, the fraction of publications with an external first-author stayed at 35 % as in previous years since the AUG programme was opened, in particular to the EU fusion community. In the case of contributions to conferences this fractions reached even 42 %.

In 2010, also a call for participation in the 2010/11 AUG campaigns was launched. This call was answered with 208 experimental proposals requesting almost 2.300 discharges. Again 35% of these proposals were submitted by non-IPP scientists from 13 EU Associates: CCFE, CEA, CIEMAT, ENEA, FOM, FZ-J, GREECE, HAS, IPP-CZ, IST, OAW, RISØ and TEKES. In addition, we received proposals from IPP Greifswald, University of Stuttgart and from international labs like GA, ITER-IO, JAEA and PPPL. After appropriate discussion with the AUG team a prioritised programme was compiled and finally approved by the AUG Programme committee, which met in July 2010. The experiments will be conducted by 5 Task Forces (TF) mainly in the first half of 2011. Also for the period 2010/11 one TF will be led by another EU Associate. The TF IV "MHD instabilities and their active control" will be managed by a scientist from FZ-J. In the following, short reports are given for the 2010 contributions of a selection of EU Associates. Due to limitation in space such reports were not possible for all EU Associates involved in the 2010 AUG Programme. However, their contributions are documented in the staff list below and the section 'Publications'.

DCU — University College Cork

Progress made during 2010 in the context of the ongoing collaboration between IPP and University College Cork is summarised as follows: The FORTRAN 90 version of the CLISTE equilibrium code is now used for routine post-discharge equilibrium reconstruction. Processing of magnetic data within the code has been made machine-independent, and magnetic probe, PF coil and vacuum vessel geometry

data is now read in from the AUG Machine Description file. Work to remove AUG-specific data associated with non-magnetic diagnostics from the code is underway.

Work continued on the investigation of β -induced Alfvén eigenmodes (BAEs) using the CLISTE equilibrium code and a numerical solver for the kinetic ballooning mode dispersion relation. The effects of electron temperature gradient variations during the sawtooth cycle on the mode frequency evolution were studied. This work has been further expanded to include the effects of trapped particles on the frequency evolution of these modes.

Work has also begun on an investigation of reversed-shear Alfvén-eigenmodes (RSAEs) or chirping modes, so named because they often exhibit pronounced upward frequency chirping towards the end of the sawtooth cycle. The work in this area focused on how q-profile evolution near the magnetic axis can affect the behaviour of these modes.

Work commenced on an analysis of the evolution of the loop voltage profile during the ELM recovery cycle using the CLISTE code and high resolution edge kinetic data mapped to ELM phase.

FOM

ECE-Imaging diagnostic installed at AUG by FOM staff, provides a local, 2D measurement of the electron temperature and its dynamics. It measures the temperature in a 2D array of 8 (horizontal) by 16 (vertical) positions (128 channels total) in the poloidal plane, covering an area of 13 by 40 cm at a sampling rate up to 1 MHz.

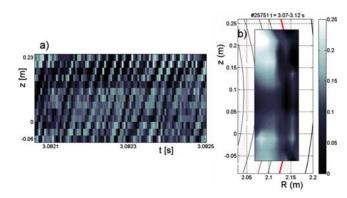


Figure 24: Type-II ELMs. a) Poloidal mode structure (radially averaged) versus time. b) 2D averaged mode amplitude.

As an example of data analysis performed in 2010, figure 24 shows data on type-II ELMs. Characteristic for this ELM regime is the appearance of a broad fluctuation band between 20 and 50 kHz. In figure a), the poloidal structure (at the low field side, averaged over the 8 radial ECE-Imaging channels) of this fluctuation is shown versus time, showing it's (upward) poloidal propagation and irregular frequency. In figure b), the averaged fluctuation amplitude is shown in 2D.

It shows that the fluctuations are localised just inside the separatrix, and that an unexpected poloidal asymmetry is present; the mode is strongest on the channels above and below the midplane. The interpretation of this effect is still ongoing (see also section 8.6).

HAS - KFKI RMKI, Budapest

The ongoing collaboration between IPP and EURATOM HAS resulted in the following main advances in 2010: The hardware development of the Event Detection Intelligent Camera (EDICAM, maximum frame rate: 100 kHz) for pellet observation was finished in 2010. In order to get a direct view of the AUG interior, two ports have been modified to be able to accommodate the small-sized EDICAM in the plasma facing end of the ports. Port 5Co (radial view) will be used to see the pellet-plasma interaction volume of the cryogenic pellets. Port 1Co (tangential view) will be applied to investigate ELM filament interaction with plasma facing components (typically antenna limiters) of the outboard wall. The first EDICAM was installed to perform pellet tracking using a tangentially viewing image guide, and commissioning was successfully finished in the AUG restart in November 2010.

A major change/upgrade of the optical observation system of the Li-beam diagnostic was started. The new optical setup is necessitated by two factors: The A-coils (to be installed after 2013) will block the existing observation views and therefore new observation optics must be built. An increase of the number of detectable photons for fluctuation measurements is required as well. The new optic head will have 30 channels and the number of detectable photon will increase by one order of magnitude.

Sawtooth precursor activity, namely the interaction of the main kink mode and a lower frequency mode was studied in detail. Both bandpower-correlation and bicoherence analysis indicate a non-linear interaction between the two modes. Wavelet-based methods developed to determine mode numbers of core modes found both spatial structures with a (1,1) characteristic.

National Technical University of Athens (NTUA), Greece

A guest from NTUA developed together with members of IPP divisions E1 and TOK a model describing the stabilisation of tearing modes by ECCD through the change in equilibrium current profile in the presence of a magnetic island. This work extends previous work that neglected the island. Implications for NTM stabilisation on AUG are still under discussion and may result in an experimental proposal for the 2011 campaign.

IST - Centro de Fusão Nuclear

In 2010 a continuous effort was dedicated to the implementation of the real-time density profiles. Significant progress

was achieved: the acquisition system's functionality and low level system software were completed and fully tested. The new system hardware was commissioned at AUG and Level 0 software integration in the RT AUG network completed. Level-0 RT operation was tested during the 2010 experimental campaign with full operation (low and highfield-side profiles and boundary position time trace at 1 ms intervals) in early 2011. An automatic procedure was developed for measurement validation (e.g. during ELMs) and to give position estimate confidence values. First results give confidence that reflectometry data can be incorporated into the AUG plasma position control loop during ELMy H-modes. Investigations were made to find a non magnetic indicator of the plasma separatrix position from the frequency variance of the FM-CW (Frequency Modulation of a Continuous Wave) signals. Preliminary results are promising but technique validation is ongoing. The planned refurbishment of the FM-CW system was delayed due to funding. Only repairs and minor modifications were undertaken. A major improvement was the implementation of a novel technique to generate reference signals without the in-vessel directional coupler loads, which has led to significant hardening of the HFS channels against excess stray ECRH radiation, thus keeping the unique HFS/LFS capability of the profile system.

The fluctuation channels have been equipped with a new Hotlink/SIO system from IPP enabling to measure density fluctuations up to 1 MHz. Control software has been developed and full operation is expected shortly. Further data analysis tools were developed to improve density profile accuracy, specifically the application of the reassigned spectrogram technique to increase the time-frequency resolution of the classic spectrogram. Excellent progress has been made in integrating the reflectometry data into the IDA package. A forward model has been built using the (partially processed) level-1 group-delay signal as input rather than the raw 'phase' data. The inclusion of the reflectometer data has a major impact on the resulting IDA profile both in terms of pedestal position and edge gradients.

Several plasma physics studies were performed. (i) Fast particle/MHD modes: The radial structure of the AE cascades has been obtained from the cross-correlation of reflectometer, ECEI and SXR signals. Resulting experimental coherence profiles are in good agreement with simulated radial eigenfunction by CASTOR code. Energetic particle modes have also been investigated via SXR and reflectometry correlation. (ii) Edge profile and fluctuation studies: The search for robust filament signatures shows clear reflectometer phase perturbations towards the bottom of the pedestal. Signal correlation with Langmuir probe data will continue in 2011, particularly during edge ergodisation experiments with the RMP coils. (iii) Density profiles and fluctuation measurements from reflectometry have also

contributed to the characterisation of the edge pedestal, analysis of triggering mechanisms of the edge transport barrier formation; characterisation and comparison of the kinetic edge profiles in nitrogen seeded discharges.

Regarding theory and simulation studies, the results obtained with the 2D FDTD code could already support the interpretation of unprecedented reflectometry experiments without reflecting layer where Alfvén cascades located at the plasma centre were detected. Significant progress has been also made on integrating GEMR turbulence simulation data into the 2D FDTD reflectometer code.

RISØ

A design for a major upgrade of the collective Thomson scattering (CTS) diagnostic on AUG has been carried out in 2010. Presently, the CTS is coupled to the ECRH transmission line via moveable quasi-optic mirrors located in the matching optics unit located in the gyrotron hall. The new design directly couples to the ECRH waveguides via RF switches designed by RISØ in collaboration with the ECRH group at IPP Greifswald and the plasma research group at the University of Stuttgart. The complete CTS hardware will be relocated to a section of the NBI control room where the waveguides are easily accessible. In addition to a more robust quasi-optic design, one of the many advantages of this upgrade is the added flexibility to easily change the receiver transmission line allowing different scattering geometries. This also enables the CTS to be independent to one particular gyrotron as its probing source. Furthermore, an additional receiver (formally located at TEXTOR) will be installed allowing two simultaneous measurements of the fast ion distribution at different locations in the plasma. The RF switches and the new quasi-optics components are scheduled to be completed in 2011.

ÖAW - IAP, TU Vienna

OAW supported the enhancement and technical improvement of the AUG lithium beam diagnostic by designing a new observation system and by building up a new data acquisition based on the SIO technology. The new observation head is currently been manufactured and will be installed in AUG during the 2011 shutdown. The SIO data acquisition system was tested and will soon replace the current CAMAC system once all remaining technical problems are solved.

At the end of the year, the restart of the lithium beam diagnostic was cumbersome, mainly caused by aging of many technical components. Finally, we were able to measure the edge electron density profile during the first plasma discharges of the 2010 AUG campaign. Especially, the effect of the new RMP coils, on the edge electron density profile could be studied.

In addition, the preparation of experiments concerning the H-mode pedestal profile evolution following L-H and H-L transitions, proposed for the 2010/11 AUG campaign proceeded. This included the analysis of pedestal profiles close to either the L-H or H-L transition from previous campaigns.

TEKES

In 2010, TEKES contributed to the research efforts at IPP on two distinct frontiers: fast ion physics and plasma-wall interactions (PWI). In PWI, SIMS measurements were carried out at VTT, Finland, to determine the deposition profiles from ¹³C puffing experiments. RBS, NRA, and also SIMS were used to study erosion of W and Ni in divertor tiles with special marker coatings as well as re-deposition of these two elements. In addition, the poloidal deposition profiles of B, C, and D on different substrate materials were determined on the same tiles.

¹³C puffing experiments were also modelled using DIVIMP, ERO and ASCOT-PWI codes and the results were reported in 3 different contributions at the 2010 PSI conference and were published in journals. For this purpose, the ASCOT code, originally used for fast ion physics, was upgraded to include background flows essential for impurity migration. The task of converting CAD drawings of the AUG wall into 3D wall structure usable by ASCOT was also completed. Using this new capability, we were already able to show that ¹³C simulations using only a 2D wall representation give misleading results. The new ASCOT-PWI is now capable to perform impurity studies using 3D magnetic and wall geometries. Both the toroidal ripple and 3D wall elements were found to affect the ¹³C deposition.

For fast ion physics, ASCOT simulations to determine the potential of an 'active' NPA system utilizing neutrals generated from beam-beam interactions were carried out after developing an NBI neutral cloud model for ASCOT. In this context, also the ADAS database was adopted in ASCOT. The simulations indicate that a refurbished NPA could be used to monitor the fast ion population from tangential NBI lines.

In collaboration with IPP's TOK division, ASCOT was also equipped with a numerical model for NTM-type islands, so that their effect on NBI current drive can be studied. The extension of this model to 3D magnetic fields was started in collaboration with TOK.

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Introduction

During 2010 JET laid the foundations for the next cycle of its exploitation. The current EP2 shutdown for installation of a Be wall and a W divertor is in its final phase. Replacement of the in-vessel components has turned out to be more difficult than expected owing to the large number of in-vessel anomalies

encountered. Preparation of the 2011-12 campaigns has also been finalised. The amount of work carried out by the Association staff within the JET Task Forces has been substantial and of high quality. Wide consultation with the JET stakeholders (Associations, EFDA Task Forces and Topical Groups, Fusion for Energy and the ITER Organisation) took place throughout the year, with two General Planning Meetings. More than 15 IPP scientists participated in these meetings. A senior IPP scientist is leading JET Task Force E1, which is responsible for a safe and efficient scientific exploitation of JET with its new wall. Characterisation of the latter will start already with the first plasma during the JET restart in 2011. Such first attempts of plasma operation are envisaged for the end of July 2011.

IPP continued its contributions to several JET enhancement projects. A new project for the installation of two additional IR cameras was launched. At the end of 2010 a kick-off meeting for a Fusion Technology task with the aim of installing AUG-type dust collectors in JET took place. Two IPP scientists attended the JET Session Leader Training and qualified for the practical part of the training during the coming 2011 campaigns.

Seven long-term secondments of IPP staff to the Close Support Unit (2), the JET CODAS group (1) and to the JET Operator (JOC, 4) were active in 2010. IPP staff seconded to JOC has been responsible for visible imaging diagnostics, ECE diagnostics, spectroscopic measurements of impurity influx and maintenance and development of codes for data analysis.

Edge modelling activities were performed in 2010 as well. The CARRE grid generator was extended to create fully orthogonal grids up to the target plates combined with a cutcell approach at material boundaries. This approach will improve the numerical accuracy of edge modelling codes and will allow automatic creation of field-aligned grids covering the whole in-vessel domain. EDGE2D modelling of JET divertor plasmas were performed to study the effect of neutrals on the power decay length at the outer divertor target plate.

Selected examples of scientific results as well as contributions to JET enhancement activities are given in the following.

JET continued its major shutdown, started in 2009, for installation of the ITER-like wall. This shutdown is the largest modification of JET since installation of the pumped divertor in the early 90s. In parallel, preparation of the 2011-12 campaigns proceeded, with IPP transferring its experience gained with the fully tungsten-clad ASDEX Upgrade to the forthcoming JET operation with beryllium wall and tungsten divertor.

Fast Particle Physics

During 2010 work with the scintillator probe for fast ion losses in JET (KA3 diagnostic) focussed on two areas: (a) upgrading of specific components, during the ILW shutdown, to improve the time response of the diagnostic, and (b) continuation of its scientific exploitation by analysis of data collected in previous campaigns.

Motivated by the experience obtained on ASDEX Upgrade, IPP contucted a small enhancement project to exchange the scintillator coating of the detector head from P56 (Y₂O₂:Eu³⁺, 2ms decay time) to the much faster responding TG-Green (SrGa₂S₄:Eu²⁺, 400ns decay time). The task involved remanufacturing key components (plate substrate, a Faraday cable plug and holding structure) and carrying out stopping power computations (SRIM code) for fusion-relevant ion species to determine an adequate scintillator material coating thickness. The plate substrates were coated at Sarnoff Co. (USA) and delivered to JET in October 2010. Vacuum compatibility tests were successfully performed and the new components are envisaged for installation on the probe head, in time for its deployment in the next JET campaigns. The scintillator exchange was supplemented by the recent purchase of a new CCD camera by Princeton Plasma Physics Laboratory. Compared with the CCD camera used so far (~20 Hz frame rate), the new camera (Photron Ultima APX-i2) offers 4000 times faster data acquisition.

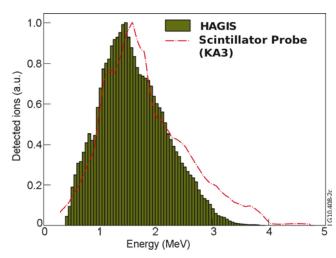


Figure 1: Energy distribution of fast ion losses measured with the KA3 diagnostic and compared with results from HAGIS simulation.

For scientific exploitation of the KA3 diagnostic, a synthetic diagnostic model for simulation of 2D scintillation-type detectors was developed and integrated into the HAGIS drift orbit following code. The model was subsequently tested on a

JET discharge, which exhibited fast ion loss bursts caused by fishbones. Thanks to the improved geometrical treatment within the simulations and to an accurate consideration of the instrument function of the diagnostic, the simulated energy (see figure 1) and pitch angle distributions at the detector are found to be in excellent agreement with the measurements.

Divertor Heat Loads

The divertor outer target heat flux profiles in JET were analysed with a high-resolution IR camera for 63 deuterium plasmas and 4.383 single ELMs in Type-I ELMy H-mode discharges. The data base includes discharges with plasma currents from 1.0 to 3.5 MA, q_{os} =2.8-5.6, triangularity of 0.28-0.4 and gas puff scans. The inter-ELM profiles are taken prior to ELM onset in a time window of about 10 ms when the strike line is found to stay constant. The ELM profiles are averaged in time from ELM onset until a value of 1/e after the ELM heat flux peak value (~1 ms) is reached. It was observed that divertor heat flux decay lengths time-averaged over the discharge duration gives too large inter-ELM values due to strike point movements. Two different quantities are employed to characterise the power fall-off length: first, the target power decay length λ_{target} using the integral value of the heat flux divided by the peak heat flux; second, an e-folding length at the divertor entrance ($\lambda_{\text{entrance}}$), derived from fitting the target heat flux profiles by a convolution of a Gaussian function with an exponential function to take into account diffusive transport into the private-flux region. It is found that $\lambda_{target} \approx 2 \cdot \lambda_{entrance}$ for inter-ELM periods. The inter-ELM scaling reveals an inverse dependence on the plasma current:

$$\lambda_{t \arg et}^{\inf er-ELM} \propto B_{tor}^{-0.38 \pm 0.24} \cdot P_{NBI}^{-0.09 \pm 0.12} \cdot I_{p}^{-0.86 \pm 0.23}$$

The smallest inter-ELM target decay lengths found are in the range of 3 mm when mapped to the midplane for discharges at 3.5 MA and q_{95} values of 2.8. The inter-ELM exponential decay lengths give smallest values of about 1.5 mm in this case. Largest values for the mapped inter-ELM target decay lengths are $\sim\!\!7$ mm at 1 MA and $q_{95}\!\!=\!\!3.5$. ELM broadening values (ratio between ELM and inter-ELM values) are found to vary between 1.5 and about 5, systematically increasing with larger ELM loss energies normalised to the plasma stored energy (E_{ELM}). A residual diagnostic artefact arising from codeposited surface layers cause large scatter for a given normalised ELM loss energy. Neglecting this, we found a scaling for the ELM power profile width $\lambda_{target}^{ELM}\!\!\sim\!\!\!B_{tor}^{0.35}\cdot I_p^{-0.19}\cdot E_{ELM}^{-0.18}$.

Contributions to the ITER-like Wall Project

In 2010 installation of the ITER-like wall (ILW) commenced. Tungsten coating of a total of about 1.700 CFC tiles – covering nearly 50 m² of JET's first wall – was finished at the 'National Institute for Laser, Plasma and Radiation Physics'

(NILPRP), Bucharest. The main focus at IPP, consequently, was completion of the quality assurance high heat flux tests in GLADIS, which were started in September 2008. After testing of nearly 170 samples, mostly larger divertor tiles, the quality assurance goal of testing a fraction of approximately 10 % of the production was achieved in mid-2010. Marginal defects occurred on only four tiles, which led to an overall failure rate of less than 2.5 %. After six years IPP's involvement in the development and quality assurance of tungsten coatings on CFC tiles for the ILW was successfully completed in 2010. Investigations on another topic were initiated: During operation in JET some tiles will undergo phases of high surface temperature. Carbon from the tiles can then diffuse into the metal coating and convert it into a brittle metal carbide. This will ultimately limit the thermomechanical performance of the coatings. First experiments to investigate the lifetime limits of the coatings were performed in GLADIS by high heat flux testing of coated tiles after dedicated heat treatment. Clear threshold behaviour with respect to the thickness of the carbidised layer was observed, indicating that the effect can be controlled by restricting the peak surface temperatures accordingly.

Specially developed molybdenum/tungsten marker layers for investigation of tungsten erosion and redeposition in the JET divertor were coated on 15 divertor tiles and on 10 lamellas of bulk tungsten tile 5 at the NILPRP in Bucharest (Romania). The thicknesses of the marker layers were determined at IPP using ion beam analysis with incident high-energy protons. The tiles were delivered to JET. In total, two sets of marked tiles were produced in 2009 and 2010: The first set is currently being installed, while the second is envisaged for installation in 2012. Special deposition monitors for measuring material deposition in remote areas of the divertor were manufactured and delivered to JET. Sachet samples for measuring beryllium and tungsten erosion at the inner main chamber wall were coated with tungsten and beryllium marker layers. The initial thicknesses of these marker coatings were measured by ion beam analysis methods, and two sets of these sachet samples were delivered to JET.

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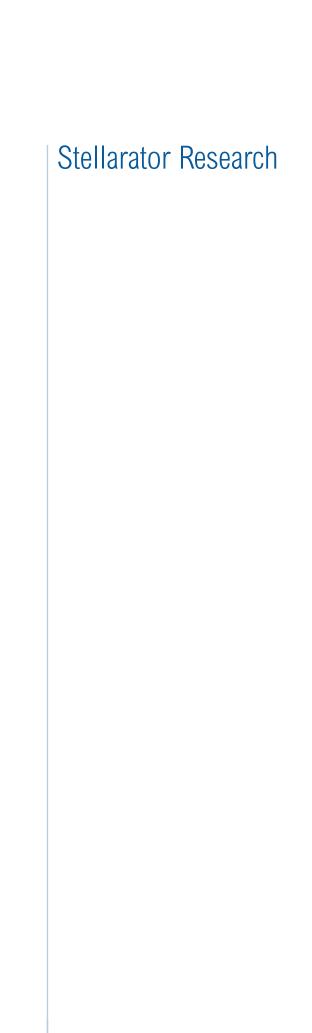
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Wendelstein 7-X

Heads: Dr. Remmelt Haange, Prof. Dr. Thomas Klinger

1 Introduction

In 2009 the organisation of the project Wendelstein 7-X remained mostly fixed. In spring of 2010 the department dealing with the superconducting coils was dissolved and its responsibilities were taken over by the department for the magnet power supplies. In the sub-division for in-vessel components, the tasks

of the two departments were redistributed and the departments were correspondingly renamed in "first wall" and "divertor". Within the Physics sub-division a new department "diagnostics engineering" has been established. This department under the lead of an experienced engineer will support the construction of the W7-X diagnostics. In September 2010 the department head "Quality management" retired and this position was taken over by an experienced engineer from this department.

Design and manufacturing of the different components of the basic device have considerably progressed, as described in chapters 2 to 4. The accompanying efforts of the engineering subdivision (chapter 5) and the design and configuration control (chapter 6) are still indispensable. The assembly of

In 2010, considerable progress was achieved in the construction of Wendelstein 7-X. Fabrication of most of the major components has been finished. For the remaining components design and manufacturing continued according to schedule. Assembly of the device progressed very well and by the end of 2010 the first three magnet modules have been installed in their final position in the cryostat module and work is progressing well on all five modules of Wendelstein 7-X.

the stellarator device and the development of the related technologies have made great progress, as described in chapter 7. Diagnostics developments (chapter 8) and the set-up of heating systems (chapter 9) as well as the development of control systems have continued. The Wendelstein 7-X device consists of five identical modules (M1 to M5), each of them con-

sisting of two flip-symmetric half-modules. Assembly started with module 5; the assembly sequence is M5-M1-M4-M2-M3.

Quality Management

The Quality Management (QM) department reports directly to the project directors via the associate director coordination. The department organises the QM system within the project W7-X and supports the supervision of all external contractors. It has taken over responsibilities for quality assurance during the assembly phase of Wendelstein 7-X. At the end of 2010 the QM system of Wendelstein 7-X has been supervised by the TÜV NORD CERT according to the DIN EN ISO 9001. TÜV NORD CERT certified an improvement of the system, no obligations were given.

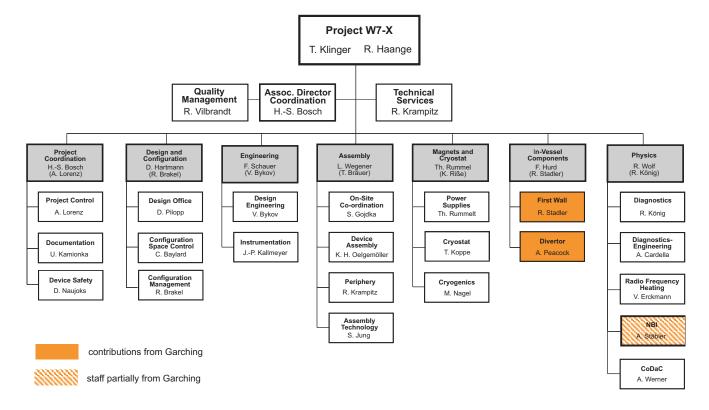


Figure 1: Organigramme of Wendelstein 7-X project as of 31 December, 2010.

Project Coordination

This subdivision comprises three departments dealing with coordination activities for the project Wendelstein 7-X:

(I) The project control department (PC-PS) is responsible for the financial planning of the project, for the control of the expenditures and for the time planning and coordination of all activities within the project as well as of the external contracts. The department monitors and co-ordinates component delivery and assembly schedules, supports the component responsible officers in the handling of industry contracts; it deals with organisational aspects of the project and is responsible for the reporting to all external supervising bodies, especially the supervising body of the financing institutions (Project Council).

A new Integrated Planning Tool (IPT), based on MS Project 2007, had been developed up to the end of 2009. In 2010 its use within the project Wendelstein 7-X has been enforced and to date the IPT has become a routinely used tool for the responsible officers, their supervisors, but also for the financial reporting to both the management and the supervising bodies. The concept of establishing links between all subprojects in a stable and reliable way has been implemented. The interlinked processes within the project are now monitored and controlled by a control WBS, which compares the delivery milestones of components with the dates when these components are required for assembly preparation or for other work processes in a different department/sub-division. (II) The documentation department (PC-DO) is responsible for an independent check of all technical drawings and CAD-models and for archiving all documents relevant to the project. An electronic documentation system (agile-PLM) is used for archiving documents and CAD models (in CADDS5-format). Because of the increased use of CATIA v5 for design and collision investigations, in 2009 an interface between PLM and CATIA v5 has implemented. In 2010 additional tools have been implemented for this interface to allow a daily automatic export of new models in the archive into a working directory of all W7-X models, the so-called "W7-X assembly". This allows concurrent engineering within a full W7-X CAD model for all designers and also allows keeping track of changes in the part models via a daily "baseline". In November 2010 the implementation and test phase of these additional tools was finished and this "CATIA assembly" replaced the former "CADDS5 assembly". With this switch to the CATIA assembly, the change of the main CAD tool (from CADDS5 to CATIA v5) was completed. (III) The device safety department (PC-DS) plans, implements and leads the processes that are required to ensure safe operation of the Wendelstein 7-X device with its interacting components and supply systems. In 2010, a number of hazard events (currently 32), which could occur on the W7-X stellarator have been analysed. The way of detecting the events is described as well as the associated technical and control safety measures; administrative procedures and the resulting actions. Systems and components that are important for personnel or public safety are identified considering their functional importance in the overall plant safety. To each global hazard event, the corresponding reports and references are given.

All control components and systems foreseen for the supervision of W7-X operation have been compiled and assessed regarding their importance for analysis purposes, operation requirements, and for personnel and device safety issues.

The specification of fire protection in the W7-X torus hall has been finalised in 2010 and the realisation of the defined technical measures (amongst them fire detection sensors, a mobile water mist station, and a central high-pressure water mist system) was started.

The successful collaboration with the Lithuanian Institute of Energy (under the EFDA agreement – Association Work Programme) on the topic of Loss of Coolant Accidents (thermo-hydraulic modeling, analysis of the water hammer phenomenon, structural analysis, leak-before-break studies) has been continued.

Schedule

Also in 2010, the time schedule of the co-called "scenario 3" (developed in fall of 2007) was followed. All five milestones scheduled in 2010, have been achieved in 2010, four of them in (or ahead of) time, the other one with a delay of five weeks. The experiences gained with port assembly in the first module resulted in a planning revision as these processes turned out to require more time than planned before. However, the revised schedule did not introduce any delay to the assembly end date due to a reorganisation of the use of the port assembly ramp. The end of assembly and start of commissioning is still scheduled for August 2014. By the end of 2010, the first three magnet modules were installed in their respective cryostat vessel modules. In the first module, all ports have been insulated and inserted, welding is under way. In the second module, insertion of the ports is still ongoing. On the last two modules, the busbars and cryo-piping are being installed. The detailed planning of assembly packages for the peripheral installations such as supply systems, diagnostics and heating systems has begun in summer 2010.

2 Magnets and Cryostat

2.1 Magnet System

2.1.1 Coils

W7-X has a superconducting magnet system consisting of 50 non-planar coils and 20 planar coils. The procurement contracts for the coils were formally closed in spring 2010. Meanwhile all coils are assembled. In addition to the superconducting coils, which will produce the main stellarator

field, normal conductive coils were developed to fine tune the magnetic field and to increase the physically flexibility of the magnetic field configuration. The five trim coils will be located at the outer side of the cryostat and have a size of 3.6 m×3.3 m and 2.8 m×2 m, respectively. In the frame of an international cooperation the US partners Princeton Plasma Physics Laboratory (PPPL), Oak Ridge Laboratories (ORNL) and the Los Alamos National Laboratories (LANL) got a three years DOE funding program to support the stellarator research at IPP. The US partners PPPL and ORNL will contribute the five trim coils within the frame of this support program. The cooperation started in the mid of November 2010. The delivery of the first coil is scheduled for 2012.

2.1.2 Coil Support Structure and Cryo Legs

The support of magnet system is composed of the central support ring, the inter coil supports and the cryo legs. The central support ring consists of ten identical sectors (half-modules) with a total weight of 72 t. It is made from steel plates, cast flanges and cast extensions, which are welded together to one half module. The contract was successfully finished in 2009. For the assembly of the modules to a ring, connection elements between the module flange are necessary. These connection elements are composed of several 3-D shims, diamond foils and special bolts. The bolts for all five connections are delivered. Special measurement tools were developed for the fabrication of the shims and the first connection was measured. The associated shims are drawn and the manufacturing process is running according to the schedule.



Figure 2: Magnet module 4 inside the lower OV shell.

The coil support structure is vertically supported by ten cryo legs. The delivery of the prototype and the ten regular cryo legs was finished. IPP has reworked the base-plates and installed the instrumentation for measurement of vertical forces.

The cryo legs of three modules have already been installed between central support ring and the W7X-machine base. Also the associated bellows were welded. The remaining cryo legs and bellows will be assembled according to the schedule in 2011.

2.1.3 Inter-coil Supports and Connection Elements

Different types of support elements connect the coils with each other. The narrow support elements (NSE) between non-planar coils on the inner side of the torus take up pressure loads while simultaneously allowing sliding and tilting. Meanwhile all NSE were produced and assembled. The welded lateral support elements (LSE) join the non-planar coils on the outer side of the torus. The semi products of all LSE's (with exception of the LSE-D06 at the module separation plane) have been manufactured. The final measurement, custom-machining and assembly were successfully completed. For LSE-D06 a new design was created and a mock-up was successfully tested. The semi-finished parts were specified and delivered in 2010. The new design includes some diamond foils, a call for tender is planned for 2011. For the fabrication of the LSE-D06 mono block a call for tender is running. The connection elements like bolts and super nuts were also delivered in 2010. The planar support elements (PSE) connect the planar coils to the non-planar coils. Two types of the PSE had to be pre machined and afterwards E-beam welded. After the welding the final shape had to be realised after a measurement of the real geometry. Most of the PSE were fabricated and assembled. The remaining PSE-B3 of the fourth module at the module section will be assembled in spring 2011. Two sorts of contact elements (CE) support the non-planar coils at the halfmodule separation plane and at the module separation plane. They take up pressure loads while simultaneously allowing sliding and tilting. Each contact elements consists of two machined steel blocks, padframes, pads and sliding plates.



Figure 3: CE330

All smaller contact elements (CE 330) were machined, assembled and installed at the half module separation plane. The steel blocks for the module connection (CE 540) are machined and assembled except one part for assembly tests. All the pad frames, pads and sliding plates are prepared. After final measurements of the modules in their final position, the pad frames will be adapted. The first assembly of the pad frame and pads is planned for spring 2011. All bolts, super-nuts, round-nuts, sleeves, spherical washers, shims and wedges for the supports of the magnetic system are listed as connection elements. The shims and wedges are machined after a special measurement by IPP. The contractor Tempelmann and the Swiss subcontractor P & S Vorspannsysteme AG delivered all the different bolts and nuts by the end of 2010.

2.2 Vessel, Cryostat and Ports

The plasma is surrounded by the Plasma vessel, which follows the plasma contour and constitutes the first ultra-high-vacuum barrier. The entire superconducting coil system is assembled between the Plasma vessel and the Outer vessel. Their function is to create a cryostat keeping the magnet system at cryogenic temperature and constitute the boundary between the W7-X main device and the external environment. 254 ports give access to the Plasma vessel for diagnostics, additional heating and supply lines. MAN Diesel & Turbo (MAN DT), Germany, is responsible for manufacturing the Plasma vessel, the Outer vessel and the thermal insulation of Plasma vessel, the Outer vessel and ports. Romabau Gerinox (Swiss) was responsible for manufacturing of the ports.

2.2.1 Plasma Vessel

The maximum outer diameter of the helical twisted Plasma vessel torus is approximately 12 m; the minimum inner diameter is 8 m. The Plasma vessel is made of the austenitic steel 1.4429 (X2CrNiMoN17-13-3) and has a wall thickness of 17 mm. The openings for the 254 ports are distributed evenly around the Plasma vessel torus. The shape of the Plasma vessel cross-section changes within each module from a triangular to a bean form and back again to a triangular form. The Plasma vessel (PV) is composed of ten halfmodules, which are divided into two sectors to allow stringing of the innermost coil during assembly. Manufacture of all ten half-modules was completed in 2005 and installation of the thermal insulation has been nearly finished. In each case two sectors forming the half-modules were welded with very low distortion. The cooling pipe inlet and outlet lines of these four half-modules have been manufactured and assembled. All main brackets of the PV-modules are assembled. All 15 vertical supports of the Plasma vessel were delivered by MAN DT. The vertical supports for the first four modules were welded successfully to the lower

shell of Outer vessel by IPP in 2009 and 2010. The assembly for the last module is planned for middle 2011. For the horizontal support/centering system the design, the calculation of horizontal adjustment (University of Rostock; Germany) and the technical specifications were completed. The standard parts have been manufactured by IPP. The additional brackets to the five ports AEU by TRINOS were welded successfully in 2010.

2.2.2 Outer Vessel

The Outer vessel is designed as a torus with an outer diameter of approximately 16 m. The internal diameter of the cross section is 4.4 m. It is made of austenitic steel 1.4429, the same material as the Plasma vessel. The nominal wall thickness of the shell is 25 mm. The Outer vessel is made of five modules; each module is divided into an upper and a lower shell. The Outer vessel is designed to have 524 domes for ports, supply lines, access ports, instrumentation feed through and magnetic diagnostics. All modules passed the works acceptance check and were delivered to IPP. The finalisation of the remaining domes is on track by MAN DT according to the time schedule. Several port elongations especially for the cryo valves were manufactured by the German company Trinos. A further Italian supplier Simic manufactured 20 port elongations for the water pipes of the Plasma vessel and 10 Quench detection and 10 instrumentation port elongations. Romabau reworked nine coil connection domes because of collisions. The upper and lower shells of the first two modules have been welded. In the fourth module, assembly of the thermal insulation is almost finished.

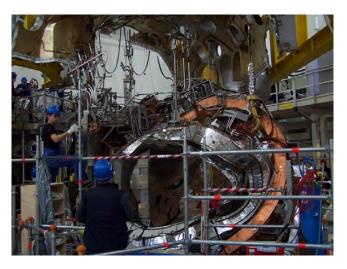


Figure 4: OV upper shell above module 4.

The preassembly and measurement is done. For the last module the insulation is running according to schedule. Further at the first two modules the port elongations for the cryo valves have been welded.

2.2.3 Ports

A total of 254 ports will be used to evacuate the Plasma vessel, for plasma diagnostics and heating, as well as for supply lines and sensor cables. The cross sections of the ports range between 100 mm circular up to 400×1000 mm² square and are equipped with bellows to compensate deformations and displacements of the Plasma vessel with respect to the Outer vessel. All ports are surrounded by water pipes in the bellow-area to control their temperature. All the ports and their fixing tools were delivered in 2007. Ten ports had to be elongated, and have been successfully reworked by the contractor Trinos. Because of collisions all water pipes at port tubes have to be reworked. At some special ports additional copper stripes between cooling pipes and ports where installed for a better heat transfer. The routing of water pipes in the bellow area has been corrected for the first three modules. Because of misalignment of ports an enlargement of dome plates was partially necessary. The needed additional sickle plates were designed and tested. For the first module all plates have been delivered and assembled. For the second module the manufacturing is on track according to the time schedule. During the assembly preparation of the ports four damaged bellows were found. Romabau in collaboration with the sub-contractor Kompaflex renewed the four bellows in 2010. The two special ports AEK-V2 for the neutral beam injection have to be reworked to allow assembly with the small tolerances required. Therefore a dummy was manufactured to simulate the revision. The rework is on track according to the time schedule. The delivery is planned for April 2011.



Figure 5: Port assembly preparation.

2.2.4 Cryo-pipes

The cryo-pipes of W7-X distribute the cold helium within the cryostat with pipe diameters ranging from $\emptyset13\times1.1$ to $\emptyset50\times3$. They start at the Helium port in the cryostat and end

in the individual feeders of the cold components, i.e. the coils, the central support structure, the thermal shields, etc.. The very restricted space inside the cryostat resulted in a complex, three dimensional pipe routing. Geometrical problems with the pipes consisting of flexible hoses could be solved. At first, no length change of the flexible hoses was taken into account during the production. This change was caused during pressurizing the pipes after the glow-process. As a consequence the lengths of the flexible hoses were observed carefully during the different manufacturing steps and additional correction steps were implemented. In most cases an accuracy of about +/-10 mm could be achieved for the pipe length. The cryo pipe header located inside the cryostat and the process feed/return-pipes running from the helium refrigerator to the cryostat have to be connected at the helium-port. A design for the connection of both pipe groups was developed and collision checks were carried out to confirm the routing. The very narrow available space required an enlargement of a dome opening, which is located at the module separation plane between the last two modules. After finishing the design of the pipe connection at the heliumport the final pipe routing was sent to Romabau where the modified pipes were manufactured, tested, and finally sent to IPP. The contract with Romabau - Gerinox could be completed in 2010. About 1000 pipes were bent, welded, geometrically checked with a FARO- measuring tool and finally leak tested. About 740 supports made of stainless steel frames and glass-fiber inlays were manufactured and delivered. In the meantime a new assembly concept for the current leads (CL) was developed. This concept required new temporary supports that hit the He-supply pipes for the current leads. Therefore a new pipe routing was required. The design has been developed for four modules. Collision control will be carried out after the fixing box design has been finished. After finalizing the design for all five modules it will be decided whether IPP or an external company will bend and weld the new pipes.

2.2.5 Thermal Insulation

The thermal insulation of the Wendelstein 7-X cryostat is fixed at warm cryostat surfaces and protects the cold components against heat loads from the warm surfaces. The thermal insulation consists of multi-layer insulation (MLI) and a thermal shield. The shield is cooled by helium gas flowing in pipes, which are attached to the shields via copper strips or braids.

Engineering and manufacturing

The preparation of the CAD-models made further progress for the outer vessel insulation. All shield models like outer vessel panels, cooling pipes and dome shields for the last two modules were sent to MAN DT. The manufacturing models were created by MAN DT and finally approved by IPP.

The outer vessel insulation was manufactured for the fourth module and is in work for the last module according to schedule. The CAD-data for the port insulation were sent to MAN DT for the second and third module. All port insulations of the first two modules were manufactured. Additionally 20 port shields were fabricated for the third module. Scans of the ports AEE and AEA in the first three modules showed geometrical deviations that do not fit to the port shield geometry. Individual solutions for each port were elaborated. Whereever possible the outer diameters of the port shields were increased. In some cases the copper strips on the ports had to be removed partially to fulfil the geometrical requirements. It was tried to use the same ports shields for the same port types that are located in different modules starting the procedure from the second module. This required a collision control of a port shield in all relevant modules. Deviations in the as-built geometry of the coils, however, required different cut outs for port shields of the same type that are located in different modules. Finally, a port shield geometry was created that fulfilled all the requirements in the different modules. This procedure reduced the engineering work and the manufacturing documents for the manufacturer. 26 port-types were identified as candidates for this procedure.

Assembly

The insulation of the outer vessel half shells continued in Lubmin. Meanwhile, the second and the third module have been insulated successfully. The lower half shell of the fourth module was also insulated. Work in the upper shell of Mthis module is in progress. Dome shields and panels are installed.

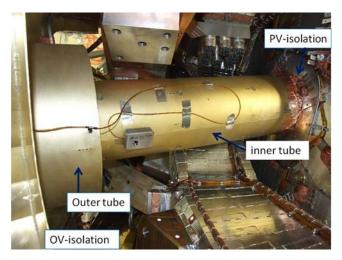


Figure 6: View on a port insulation.

The cooling pipes were adjusted to the panel geometry and welded together. On site welding seams were leak tested. The soldering of the pipes to the copper strips of the panels has been started.

The port insulation generally consists of two major components, the outer tube insulating the bellow area and the inner tube insulating the lower port tube (see figure 5). The inner tube is axially fixed on the PV and is supported on the ports in radial direction with Torlon-pins. The outer tube is welded to the outer vessel (OV) shield. The assembly of the port insulation is closely connected to the port assembly process. In a first step the outer tubes are welded on the OV-shields in the cryostat. Then the inner tube is threaded over the port and fixed. The shields are positioned on the ports with an accuracy of +/-3.5 mm (including manufacturing and assembly tolerances). Then the port is transported with attached insulation to the cryostat and clamped to the port assembly device. After that the port is threaded with the insulation through the port dome in the OV-shell into the cryostat and inserted in the corresponding whole of the plasma vessel (PV). The port shield is axially positioned with an accuracy of +/-5 mm compared to the nominal position. The port MLI-layers are connected to the PV-MLI and to the OV-MLI during the threading process. Copper tresses are riveted and soldered to the adjoining shields. The assembly of the port insulation started end of March 2010 with the first module. In October 2010 this process was finished and work on the insulation assembly of the second module has started. 42 ports of the first and 27 ports of the second module have already been insulated. The close interaction between port assembly and port insulation required a very close cooperation of the workers from MAN DT and IPP.

2.3 Current Leads

The current leads (CL) are the electrical connection between the superconducting magnet system inside of the cryostat and the power supplies outside of the cryostat, operated at room temperature. The main challenge in W7-X is the socalled upside-down orientation of the CL, i.e. the cold end is on top and the warm end is at the bottom. The development and production is being performed by the Karlsruhe Institute of Technology (KIT). In 2010 significant progress has been achieved in the production as well as in the field of testing. The production of the two current lead prototypes has been finished in spring 2010. In parallel the work for the refurbishment of the TOSKA test facility has been finished, too. The two current leads were installed in the test cryostat and all the instrumentation was connected to investigate the thermal, hydraulic and electrical behaviour of the current leads. The interconnection between the current leads inside the test cryostat, consisting of about one meter of NbTi superconductor of the W7-X type, was connected and pre tested. Then the current lead prototypes were tested in two test campaigns. After a thorough check under room temperature the whole test arrangement was cooled down to cryogenic temperature with a cooling speed of approx 10 K/h. After the hydraulic and thermal stabilisation the current leads were successfully loaded up to the maximum current of 18.2 kA several times. Also an overload test up to 20 kA was performed to check the margin in terms of the current. A steady state test at 18.2 kA over six hours did not show any problems. Also the test of a loss-of-Helium-flow accident showed sufficient time to de-energise the W7-X magnet system slowly, until a quench will occur. In the test campaigns also the safety margin of the superconducting parts was tested by induced quenches. The margin between the operating conditions and the achieved quench temperature meet the requirements. The necessary helium mass flow rates to operate the current leads fit to the expectations. The high voltage strength of the test arrangement was improved between the two test campaigns to overcome problems observed at higher voltages.



Figure 7: Current lead (left) and current lead prototype test arrangement at KIT.

In parallel to the test at KIT, tests on the mechanical stability of the two GRP-flanges have been finished successfully. Flange test mock-ups were loaded with up to 150 % of the forces and moment, which will be acting during the W7-X operation. The tests were done at room temperature as well as at cryogenic temperature at the test facility of the company IMA in Dresden, Germany. In conclusion of the several tests it can be stated that the development of the current leads was successfully finished and that the worldwide unique upside down operation of current leads is manageable. On the basis of the test results the series production was released by IPP.

In order to make the best use of the knowledge at KIT gained during the development and production of the prototypes it was commonly decided to produce the 14 series current leads at KIT as an in-house fabrication with only a few tasks done externally by a few key sub suppliers. The production has been started in the middle of 2010. Most of the material has been ordered and the production of main components is well advanced. By the end of 2010 the components for the first four current leads have been manufactured and assembly of the first two current leads was underway. The overall schedule for the production and test of the current leads is in agreement with the assembly schedule of Wendelstein 7-X.

2.3.1 Current Leads Mechanical Support

Mechanical supports of Current Leads are needed to support the current leads itself at the section between warm and cold side while allowing all the movements coming from the operation. Simultaneously they will be needed to support the bus system up to the central support ring. They consist of two main parts, which will be manufactured in different steps. Firstly the bearing at the central support ring with the connected horizontal rods to join the coil support structure with the fixing box. In the second step, the fixing box itself with the bearings for the current leads and the bellows is built. Because later there is no access possible, the supports and rods have to be installed first. The manufacturing for all bearings and rods is finished. Beside the last module, all the bearings and rods have been assembled in 2010. Because of a reduced access during the assembly of the fixing box, a mock-up was manufactured in 2010, too. With the first results the design was partial reworked and finally finished for the fixing box, the bellows, the bearings for the current leads and the connected bus supports. The first rectangular pipes for the fixing box have been manufactured. A specification for the bellows is finished; a call for tender is prepared. The assembly is on track according to the time schedule.

3 Supply Systems

3.1 Helium Refrigerator

The helium refrigerator produces and distributes the cold helium mass required to cool the cold components of W7-X. The commissioning of the refrigerator is in progress. The installation and testing of test boxes 1 & 2 containing the main test heaters were completed. The oil heat exchanger was replaced with a bigger type because the maximum oil temperature was exceeded. Wrong bearing material for the pump shafts resulted in scratches on the pump shafts. Although Linde Kryotechnik (LKT) has replaced the bearing materials, the problems persisted; therefore LKT has decided to change these pumps with another type of pumps.

After the mounting of cold machines i.e. cold compressors and cold pumps the commissioning of these machines was started. Both the cold compressors were operated in manual mode, the start-up in automatic mode was carried out for the first one, further work is continuing. The manual start-up of cold pumps is also continuing in parallel. The change of the control program from FUP to PCS7 for all the 3 SPS units was completed; further refrigerator operation was carried out with the new program. The integral leak test of boxes and transfer lines with vacuum enclosures were completed, the leak tests of warm piping are planned for the near future. LKT has announced further delay in completion of commissioning and documentation with a finalisation date of May 2011. Meanwhile, LKT delivered and integrated a fourth cold pump that is needed to run the cryo-vacuum-pumps. Additionally seven spare cartridges were delivered for the seven turbines.

3.2 Magnet Power Supply

The superconducting magnet system is divided into seven electrical circuits, containing five circuits with ten non planar coils each and two circuits with 10 planar coils each. Seven independent power supplies provide direct currents of up to 20 kA at voltages of up to 30 V. Fast and reliable discharge of the superconducting magnets in case of quenching or severe faults is realised by fast circuit switches, which shortcircuit the coils and dump the magnetic energy into resistors. After the declaration of the acceptance in mid 2007, several test campaigns were performed to train the staff and to identify possible weak points. Over the time the failure rate tends to increase. Intensive negotiations with the main contractor ABB turned out to be necessary to find a common solution in terms of repair, warranty, payment and spare parts. As one result ABB started the repair mid of 2010 with the aim to demonstrate the proper operation of the system in an eight hour steady state test. By end of 2010 several repair measures has been done and most of the spare parts have been delivered.

3.3 Quench Detection System

The quench detection system of W7-X will permanently check the differential voltages across the double layers of the coils, all sectors of the bus system and the superconducting part of the current leads. The system has to reliably detect millivolt signals in a broadband noise environment and operate at high voltages during a rapid shutdown of the magnets. In order to provide a redundancy in the quench detection, it was decided to install a back-up quench detection system. It runs in parallel to the original system, but allows as an additional feature to detect symmetric quenches in adjacent double layers of the coils. Due to a slightly different cabling concept the number of necessary units is less than in the original quench detection system. In total 560

quench detection units are necessary. The quench detection units will be put into ten so called subsystems. One subsystem contains up to 64 quench detection units and is equipped with an internal AC/DC power supply combined with an uninterruptible power supply to secure the independent operation of the subsystem. For control and data acquisition an internal controller is installed to evaluate and to transmit the quench signals to the magnet safety system and to allow a fully remote control. The fabrication of the prototype subsystem has been finished in 2010. In a steady state test over several weeks the error free operation was demonstrated. All the components of the subsystem have to withstand the magnetic field strengths. Therefore the components as well as the finished subsystem were tested in a magnetic field up to 30 mT successfully. Due to the good results the prototype subsystem will be used as the first series subsystem. The production of the remaining subsystems has been started in IPP.

4 In-vessel Components

The in-vessel components consist of the divertor target plates, baffles, panels and heat shields, control coils, cryopumps, port protection and special port liners for the NBI and DNBI and the complex system of cooling water supply lines. Plansee SE is manufacturing the High Heat Flux (HHF) target elements and MAN DT the wall protection panels. The horizontal and vertical target modules of the HHF divertor are designed to withstand power fluxes of up to 10 MW/m². The baffles, which prevent the neutrals from re-entering the main plasma chamber, receive power fluxes of up to 0.5 MW/m². The remaining first wall components are subject to neutral particles and plasma radiation of up to 0.3 MW/m². In 2007 it was decided to start operation of Wendelstein 7-X with a test divertor unit (TDU) without water cooling. The TDU is designed for short pulses of 6.25 seconds at a maximum heating power of 8 MW. The recovery time between pulses at maximum load shall be 20 minutes. The design, manufacture and assembly is managed by the In-vessel component division in Garching. Assembly of the target modules from target elements for both the TDU and HHF divertors, much of the fabrication of the TDU frames and module structures, baffles, heat shields, the cryo-pumps and of the supply lines is performed by the Integrated Technic Center of IPP in Garching or the Technical Services in Greifswald. Specialised companies are used to perform the vacuum brazing, pipe bending, specialist welding processes and machining. All in-vessel components are tested in Garching (geometry, He-leak tests and hydraulic tests) before delivery to Greifswald. For the first operational period with the TDU it is foreseen to operate with a limited number of cooled components. These include the control coils and some special areas close to diagnostics and heating systems.

However, in order to reduce the length of the subsequent shut down, all the other components and their cooling circuits necessary for long pulse operation will be installed. Only the cryo-pump, the HHF divertor and their water supply lines will be omitted for this first operation phase. The input parameters for the cooling requirements during the first operation period are presently assessed in detail and fixed by a working group.

4.1 Target Modules

The ten divertor units of the HHF target are designed to remove 10 MW convective stationary power load. The ten units consist of two main areas: the first, an area of 19 m², which can be loaded up to 10 MW/m² and the second with an area of 5.4 m², which can be loaded up to 1 MW/m². Each divertor unit is assembled from 12 separate target modules. The highly loaded target modules are assembled from sets of bar-like target elements, which are supplied with cooling water in parallel and fixed on a common frame. The supports of these modules are adjustable within a range of a few millimetres to allow for compensation of manufacturing and assembly tolerances of the plasma vessel or uneven heat-loading during plasma operation. For the higherloaded area 890 target elements are required. Their surface closely follows the 3-D shape of the plasma boundary and will be machined before assembly of a module. The decision to introduce the TDU in the first operation period has meant significant additional design and testing. The TDU will have the same surface contour as the HHF divertor. Some of the mounting frames and the intermediate area modules will be the same components to save time and cost. The TDU will use un-cooled fine grain graphite elements and is expected to withstand up to 8 MW/m² for 6.25 seconds. A total energy input limit of 50 MJ has been set for the design phase. The detailed design of the TDU including a prototype module test to qualify the design and fine grain graphite material was completed in 2009. During 2010 the 3D machining of the TDU elements, the Vertical support frames and vertical module frames have been completed, contracts for the first sets of horizontal support frames have been placed. The procurement of the divertor modules of the lower loaded area was started in 2010 using a design similar to the Baffles and will be included in the TDU phase. In 2010 the detailed design of the HHF divertor modules has continued. In the HHF divertor 8 mm thick CFC tiles made of SEPCARB® NB31, produced by SNECMA Propulsion Solide, are joined to a water-cooled CuCrZr heat sink. These tests have shown the improvement in the technology by the introduction of a compliant copper layer between the AMC® interlayer and the CuCrZr heat sink. In collaboration with the materials research division in Garching further lifetime and increased power loads have confirmed the robustness of the manufacturing technology. In 2010 a standard element with known

defects has been used to correlate the infrared measurements carried out in the ARGUS facility of Plansee SE with possible defects. With the support of the BMBF a pre-series of long elements is continuing to qualify the end tile and long cooling structure technology.

4.2 Baffle Modules

The baffle modules prevent back-streaming of the neutralised gas from the target plates into the main plasma and protect the water manifolds of the target modules. The design uses graphite tiles, which are clamped onto a cooling structure made of CuCrZr. Water cooling is achieved by stainless steel tubes, which are vacuum brazed to the back-side of the heat sink. The fixing screws for the graphite tiles are made from a molybdenum alloy (TZM). In total there are 170 Baffle modules, 150 of the cooling structures are completed or in manufacture by the IPP workshop in Garching, the ordering of the graphite tiles runs in parallel to the cooling structure manufacture.

4.3. Wall Protection

About 70 m² of the plasma vessel surface is covered by doublewall stainless steel panels with integrated water-cooling. In total over 320 panels have been delivered, including panels for the protection of the plasma vessel behind the pumping gap and an additional 50 panels required due to the Scenario 3 changes have been delivered by MAN DT. The majority has been tested and accepted. Additionally other areas of the inner wall of the plasma vessel are protected by heat shields. These heat shields use graphite tiles, which are clamped to a cooling structure using a similar design to the baffles. The design integrates several plasma diagnostic components as well as a NBI beam dump and mirrors for ECR heating. By the end of 2010 a total of 160 of the 162 heat shield cooling structures are completed or in manufacture in the IPP workshops. In 2010 a set of 4 heat shields were installed in a plasma vessel sector in collaboration with the assembly division The procurement of the graphite tiles runs in parallel to the cooling structure manufacture. During steady state and full power plasma operation, the inner surfaces of the ports need to be protected in the same way as the plasma vessel. For budgetary reasons, the detail design of the port protection panes has been delayed, nevertheless, the qualification of the technology and definition of interfaces has continued. Since the space behind the wall protection is very restricted, all port protection panels will be later supplied with water from outside via port. The NBI ports as well as the port for the diagnostic injector need to be protected against energetic particles by CFC and graphite tiles from the beginning. In 2010 the manufacture of the first assemblies was completed. Due to new data the beam dump area is being re-designed to increase the cooled area and its thermal load capability.

4.4. Cryo-pumps

Ten cryo-pumps are located behind the target plates to increase the pumping capacity for hydrogen and deuterium up to 75m²/s during high-density plasma discharges. The cryo-pumps are composed of a cryo-panel cooled with single phase helium, a Chevron baffle cooled with liquid nitrogen and an additional water cooled baffle. Fabrication of the cryo-pumps is well advanced, however, the cryo-pumps will be installed only after the first operation phase. Due to possible high ECRH stray radiation a special absorbing coating has been developed and tested in MISTRAL.

4.5 Control Coils

Ten control coils will be installed behind the baffle plates. These coils will be used to correct small field errors at the plasma edge, to optimise the position and extent of the islands and dynamically sweep the power across the target plate. The coils have been fabricated by the company BNG. Each coil is made of eight turns of a hollow copper conductor and is water cooled. All control coils have been tested and accepted. All ten control coils have been delivered to Greifswald. During 2010 assembly trials have been carried out in collaboration with the assembly division.

The control coils are supplied by power supplies, which are able to provide direct currents of up to 2500 A and alternating currents up to 625 A with frequencies between one and 20 Hertz in parallel. In 2010 the operation of a power supply together with the associated control coil was performed successfully. The coil was operated up to the maximum direct and alternating current several times to check the electrical and thermal performance. Also the quality of the closed loop controller was checked successfully.

4.6 Water Supply Lines inside the Plasma Vessel

Cooling for the in-vessel components is provided from the main water system through 80 supply ports in the different W7-X modules. The interface between the supply lines and the cooling loops inside the plasma vessel is achieved by so called plug-ins, which are groups of pipes and cables that can be installed as a single assembly with the port flange. The water cooling loops inside the plasma vessel form a very complex network of pipes with a total length of about 4000 m. Routing of the water pipes has to take account of the 3D-shape of the plasma vessel, avoid the diagnostics and heating systems port openings, take into account the restricted space behind the wall protection panels and identify appropriate attachment points. In addition, the design of the cooling circuits has to consider many interfaces with the diagnostics and heating systems. The design was qualified by the installation of a prototype in a sector of the plasma vessel. The design, manufacture, assembly and testing the main cooling circuits is complete. Some cooling circuits have been modified to take account of changes required by other divisions and this work is progressing. A prototype plug-in, including a special thermal shield required for port protection and the diagnostic cable routing and protection, has been manufactured to qualify the technology and the design of the other seven variants. This has also been tested in MISTRAL to assess ECRH effects on the integrated diagnostic cables.

4.7 Glow Discharge Electrodes

The conditioning of the W7-X plasma vessel will be performed by glow discharges. Ten glow discharge electrodes will be permanently placed inside the vessel. These electrodes are ready and available for installation in W7-X. One prototype was tested in ASDEX Upgrade and was operated successfully for four months. Some small design changes will be made to the fixation of the glow discharge cathode. A second test in 2009 was also successful.

Each glow discharge electrode is supplied by a separate power supply delivering a voltage of up to 3 kV and a current of up to 3 A. The power supplies have to be combined in one system with one central control unit. The contract for the development, production and test of the power supply system was awarded to the company Puls Plasmatechnik Dortmund. The whole system was produced, delivered to IPP and finally tested. In 2010 the test campaigns under different operating conditions were continued.

5 Engineering

The sub-division Engineering (EN) provides engineering support to the Wendelstein 7-X project. EN is now organised in two departments: Design Engineering (DE) and Instrumentation (IN). The department Development and Test (DT) was closed on July 9, 2010.

5.1 Design Engineering

5.1.1 Structural Analysis and Design

Design of the "basic machine", i.e. without in-vessel components, diagnostics and periphery, is largely completed, structural parameters such as bolt preload, initial conditions for contact elements, etc., are defined. Therefore, the focus is shifting towards fast analyses of non-conformities, deformations as input for collision checks, and changes in the assembly procedure. This assembly-related work is expected to continue until commissioning of the machine, however, with decreasing intensity. In parallel the analyses for invessel components, diagnostics and periphery, as well as exploration of operational limits of the as-built machine are increasing. In addition, initiation of design activities on a relevant level at least for the mechanical structure and cryostat of a HELIAS stellarator reactor is considered indispensable in order to arrive at a competitive decision base for a DEMO-Reactor.

5.1.1.1 Magnet System Global Analysis

The magnet system global model (GM) encompasses the non-planar and planar coils (NPC and PLC, resp.), the central support structure (CSS), and the inter-coil support structure. The latter comprises the narrow and lateral support elements (NSE and LSE, resp.) between the NPCs, the contact elements (CE) between the half-modules and modules, and the planar support elements (PSE) between NPCs and PLCs. The NSE and part of the PSE as well as the CE basically consist of sliding aluminium bronze pads and corresponding sliding steel counter-faces. The highly loaded interfaces between the CSS and the coils, the so-called central support elements (CSE), comprise the bolted and wedged flange connections, which partially open during operation. Two GM variants are routinely in use: The 36°-GM with flipsymmetric boundary conditions encompasses one halfmodule for quick simulations of bolt loads, cool-down, and magnetic loads. For loads not in accordance with the stellarator symmetry like gravity and cryo-leg forces, a more involved 72°-GM with cyclic boundary conditions is needed. For loads not complying with the five-fold torus symmetry, like forces from auxiliary supports during assembly, module misalignments, or trim coil fields, a complete 360° model or part of it is required (figure 8).

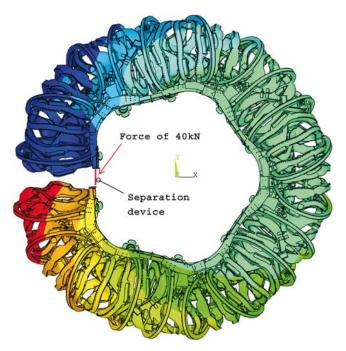


Figure 8: Evaluation of torus spreading of 2×0.25 mm for assembly of the last module using the 360° global model. Deformation is shown highly exaggerated, forces are ≈ 40 kN.

Due to the non-linearity of the structure, the GM is very sensitive to variations of initial parameters and boundary conditions. For sufficient confidence, at least two independent

global FE-models are indispensable. Actually, three independent FE-GMs were created: The ANSYS GM with fully operational 36° and 72° variants as well as a simplified 360° model, the ABAQUS GM in 36° and 72° variants, and a completely independent and more detailed 36° ADINA GM, which was used to benchmark the other two. Now and in future only the ANSYS and ABAQUS models are in use. Continuous improvements as well as updating corresponding to the as-built geometry and real materials are still ongoing. The 36° and 72° ANSYS models are the workhorses, which are heavily used for all kind of magnet system analyses. The ABAQUS GM 36°- and 72°-variants, originally created by LTC (Italy), are now continuously operated and updated by IPP. They are used for benchmarking, comparative studies of special structural questions, and for tasks, for which ABAQUS is better suited (e.g. dynamic analyses, friction studies of cryo-legs, large deformations, limit analyses, serration effects). Major GM applications during the reporting period are listed in the following:

- Studies concerning operational limits based on as-built NSE gap tolerances have been started. The real gaps are about twice as large as previously assumed, therefore, significantly higher loads, particularly on the CSE and NSE, have now to be taken as design loads. In the worst case some extreme 3 T configurations might not be completely accessible.
- The 36° global models were extended from elastic to ideal elastic-plastic material properties, which yield better load distributions. Limit analyses are now possible resulting in large load scaling factors >2 before collapse of the magnet system.
- The structure concept of a HSR5 reactor with ≈12 T at the coil was further developed using a simplified 72° FE-model. Figure 9 shows that most of the stress intensity in the double shell inter-coil structure is far below the allowable limits for steel, and that in the next step the structural mass can be greatly reduced. No CSS is required. It was also shown that stress and deformation levels in winding pack components (cable jacket and insulation) are comparable to the ones of ITER.
- Temporary supports at the interfaces between modules impede installation of the current leads. In order to accelerate the W7-X assembly, an early removal of these supports would be advantageous. The corresponding FE-analyses were completed with the result that premature temporary support removal is possible without inacceptable deformations of the magnet system.
- For moving the last module into the gap between the already aligned other four modules, this space has to be widened by 0.25 mm on each side for installation of flange shims with friction-enhancing foils. An assessment using the 360 degree FE GM (figure 8) gave a moderate spreading force of approx. four tons.

- The PLC case is a bolted and pinned structure with some highly loaded pins and surrounding case plate regions. The cyclic behaviour of the PLC case was analysed iteratively with the ABAQUS GM. The conservative analysis showed that even in case of complete breakage of a few pins there is no danger of excessive deformation and overloading of the winding pack.
- Dynamic FE studies were continued and finished for final evaluation of the "MQ-test" performed on a non-planar coil in the course of the acceptance tests at Saclay. The energised coil was hit with different impact energies in order to simulate stick-slip events within the W7-X magnet structure. Aim was to investigate the stability of the superconductor with respect to mechanical disturbances. The experiment and theoretical calculations confirmed that no loss of superconductivity has to be expected due to worst case stick slip events.

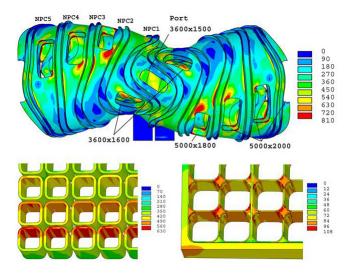


Figure 9: Stress intensity distributions in HELIAS reactor magnet system (top), conductor jackets (bottom left) and WP insulation (bottom right); units: mm and MPa.

5.1.1.2 Detailed Analysis of Magnet System Components

Development, refinement and updating of the numerous local structure models for detailed analyses was done mainly at IPP. Cooperation existed with FZJ (bus system), Warsaw Technical University (CSEs and LSE 5-5), and with LTC (NSE limit analysis). Besides the accompanying calculations for W7-X assembly, other major tasks are listed in the following:

- The parametric FE-models created by WUT for all 14 CSE-connections were re-analysed with updated loads resulting from as-built NSE gaps. Three connections showed critical results and have to be further investigated using a less conservative, more accurate approach. This activity is ongoing.

- Limit analyses were performed by WUT on the CSE coil extension welds based on the updated loads and taking into account serration effects. Three coil extensions require further consideration with a less conservative approach. The most critical extension is currently under analysis.
- The design of the bolted LSE 5-5 was completed as a "mono-block" bridge without wedges but with friction-enhancing foils at the contact surfaces under direct bolt load. The bridge has to be adaptable within a wide range to the finally adjusted module positions. Extreme worst case configurations were confirmed with a 3D FE-model created by WUT.
- FE analyses of the module interfaces comprising adaptable shims and friction-enhancing foils were performed.
 Tolerances, requirements for flange preparation as well as recommendations for the assembly procedure were derived.
- The updated FE-models of the bus system, provided by FZJ, were checked and bus deformations extracted and prepared for collision control. At the interfaces to coils and current leads some reinforcements and design changes were necessary.
- In preparation of the trim coil specification the loads on the outer vessel as well as deformations were determined.

5.1.1.3 Fracture mechanics

The acceptance criteria for surface cracks in the LSE weld influence zones were re-evaluated using different analysis tools. It was confirmed that the crack tip plastic zone of cracks in the maximally stressed regions are sufficiently small such that the linear-elastic approach is justified. Conservative crack propagation estimates show that the foreseen cycle numbers are by a safety factor of >10 below critical values.

5.1.1.4 Cryo-piping

FE-modelling of the cryo-piping was completed for all five modules. The analyses were performed iteratively hand in hand with the design of the pipes and their supports. Modifications due to non-conformities, re-design of components, re-routing of the pipes, etc., are continuously implemented in FE models and re-analysed.

5.1.1.5 Cryostat

Main application of the ANSYS cryostat GM was to provide input for local analyses, particularly forces/moments in port welds and OV supports, local deformations under Trim coil loads, diagnostic port movements/deformations, etc. The current outer vessel FE model is based on a CAD design, which is outdated by now due to many modifications during manufacture and assembly. Activities were started to collect all changes and assess them in view of implementation in an updated OV model. Evaluation of module 5 is completed.

Sufficient safety factors were taken into account in recent calculations so that no serious consequences due to the inaccuracy of the model geometry concerning strength, deformations and port movements are expected. For analysis of the significantly changed cryo-supply dome a local model was created with the help of IGN comp., Germany.

Further activities in the reporting period are listed in the following:

- Work on the port welds at the PV continued. The new weld design, created by AS in cooperation with EN, was analysed with semi-analytical methods. The majority of the ports could be released for welding with the new standard weld seam, and a few ones required stronger seams. For special ports, and in cases of doubt, laborious 3D FE analyses were initiated, including limit analysis. First results show that the planned welds are adequate with sufficient safety factors.
- PV deformation and port sag after tack welding and removal of supporting assembly tools was evaluated. Deformations and displacements of Type 1 ports are within acceptable limits, the Type 2 ("supply") ports need to be fixed temporarily with simple methods.
- Mainly due to tolerance deviations, several OV dome plates had to be split into two parts, and some plate welds had to be changed during assembly. Based on FE analyses of typical domes these weld seams were defined.
- In order to compensate for weld shrinkage, the OV and PV modules have to be shifted apart by 6 mm before welding. FE analysis showed that sliding back of the cryostat supports to the target positions due to the weld shrinkage is not assured. In order to minimise residual stresses and forces, the supports bottom plates thus have to be moved back separately.
- Analysis of the planned OV leg fixation on the machine base revealed overload of the bolts due to thermal expansion during PV/port baking and consequential heating of the OV. An appropriate re-design was developed in collaboration with Assembly dept.

5.1.1.6 In-vessel Components (KIP) and Diagnostics

Analysis activities supporting the design of KIP components and diagnostics grew considerably, major examples are listed in the following:

- Thermal stresses and deformations of HHF divertor tiles were evaluated for overloads and realistic tolerances as achieved in production.
- The influence of thermal shields of the diamagnetic loops on their measurement signals was analysed. Cuts in the shielding were defined in order to limit signal attenuation.
- Two variants of the support structure of the Thomson radiation diagnostic were dynamically analysed with the conclusion that they are similar with regard to vibration response. For both structures it is expected that damping

- measures have to be adopted, depending on the real vibration spectrum of the ground floor during W7-X operation.
- Shielding against plasma radiation in front of some diagnostic ports was analysed resulting in proposals for improvements.
- Thermo-mechanical analyses of retroreflector designs for interferometry and polarimetry was done for several fixation options. The poster presenting these analyses at the SOFT 2010 conference got the "Best Poster Award" in the category "Diagnostics, Data Acquisition and Remote Participation".
- Re-evaluation of all thermal loads within the plasma vessel has been continued.

5.1.2 Magnetic Field Analyses

In order to compensate for the influence of accumulated construction errors on the stellarator field configuration, the module positions have to be corrected accordingly. The corresponding software was developed further. A target function, based on weighted field error components, was defined to be minimised for an optimal module position. The first three modules were placed on such optimised coordinates taking also into account the latest assembly state and measurements of all five modules. It was also shown that the influence of machine base sag during assembly is negligible and further corrections of the already placed modules are not necessary. As a recurrent task, calculations of fields and vector potentials, as well as eddy currents and the consequential mechanical loads were performed on request as design bases for components and diagnostics.

5.1.3 Thermal Stress Analyses

Due to the extremely restricted space, the port cooling/ heating (C/H) pipes were removed on all ports except at the large rectangular ones. This deterioration of temperature control was compensated by better C/H of the PV-sided flanges between the port tubes and bellows. On the rectangular ports some of the copper stripes providing the thermal contact between the C/H -pipes and the port walls had to be partially removed due to potential collisions. Thermal FE analyses provided decision bases for all these modifications. Another issue was insufficient thermal contact of the bellows middle section to cooling/heating pipes of the large ports, and insufficient flexibility of these pipes to follow the bellows deformations. Based on FE analyses, necessary design changes for both the pipe routing and reinforcement of thermal coupling were developed. Removal of the C/H pipes cause the port wall temperatures to increase during hot-liner operation in those ports, which contain hot water heating pipes. FE analyses revealed that all wall temperatures stay below the allowable level except in one port. For this a special internal wall shield was proposed and developed in collaboration with KiP dept OV heating during PV/port baking at 150 °C as well as the corresponding heat flow into the torus hall were analysed (figure 10).

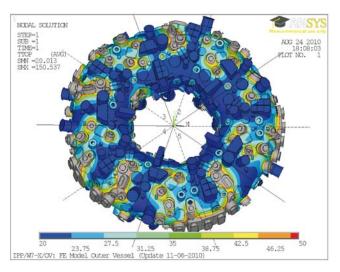


Figure 10: Outer vessel temperature distribution during PV/port baking at 150° C. Gray colour represents regions with temperature above 50° C.

It turned out that the average temperature of the OV body remains below the maximally allowable value of 50°C by natural air convection. However, the heat load on the torus hall becomes up to 200 kW, which has to be taken into account for climate control.

5.2 Instrumentation

Main activities were the creation of work instructions for instrumentation applications on the W7-X cold structure and development of signal transfer and processing. Remaining detail development work concerning special applications and clarification of measurement accuracies was completed. Some applied sensors were already used during assembly steps and assembly qualification procedures.

5.2.1 Sensors

Application of magnet structure sensors within all five modules of the cryostat is finished to 97 %. These are the strain gauges (SG) on the PSEs, LSEs and CSEs as well as on all highly stressed CSE bolts. The SGs on the bolted LSE 5-5-bridges will be applied after module connection. All cantilevers to monitor the critical CSE flange openings and displacements between the NPCs and PLCs were installed. A solution was found for a SG-based system to monitor the loads on the cryo-legs. The idea is to measure the circumferential compression of the ring-shaped spherical cryo-leg bearing with six SGs (figure 11). FE-analysis showed that the SG signal is almost linear with respect to the cryo-leg load. All bearings are furnished by now at their inside openings with SGs. They are used already for cryo-leg load measurements each time a module is placed onto its

final position. Approximately 20 positions per module are instrumented with electrical contacts to monitor the cold structure for collisions. These sensors, consisting of self adhesive tapes requiring only one signal wire per contact, can easily be adapted to all kinds of component surfaces, even to the surface of multi-layer insulation packs. Modules 5, 1, 4 and 2 are fully instrumented by now, the positions in Module 3 are known and described in a work instruction.

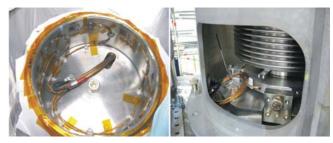


Figure 11: Cryo-leg bearing ring opening instrumented with 6 SGs (left). Instrumentation cable fed through the bearing base plate (right).

5.2.2 Signal Transfer and Processing

Much work was devoted to find out the best shielding and grounding system for the instrumentation cables and electronics. Advantage was also taken from experiences gained at ASDEX-Upgrade. A prototype of the whole cryogenic measuring chain consisting of sensor, cryogenic cable, feedthrough, torus hall cable, and cubicle has been built in the lab. Strains and displacements can be simulated under well defined grounding conditions. Investigations using disturbing signal generators and intentionally created power grid disturbances revealed that acceptable signal noise levels can only be achieved with doubly screened cables in a special grounding arrangement. The corresponding cable specification was prepared. A modular cubicle concept was developed. A cubicle consists of the boards with electronics, the power supply module, the line power connection with filter, and the mechanical structure. Based on thermal experiments, a cubicle cooling system was developed using only internal fans and air streams.

5.2.3 Extended Instrumentation Group

The extended instrumentation team is composed of members from all divisions and chaired by the EN-IN department head. Its task is to coordinate all instrumentation activities of the project, and it meets at intervals of about six to eight weeks. Main achievement in the reporting period was the final I-Port (cryo-instrumentation feedthrough port) design. A prototype was leak tested, and manufacturing has started. The I-port pinning for Module 1 and 5 has been agreed. The originally planned soldering of the sensor cables to the feedthrough contacts at the cold side was changed to crimping for easier and quicker assembly.

5.3 Development and Test

Task of the department EN-DT was development and test of special components of the W7-X magnet system. This work was very successfully completed and EN-DT was closed down in summer 2010. The staff of the department was distributed to EN-DE and the new department Diagnostic Engineering of the sub-division W7-X Physics.

5.3.1 Coil Support Elements

EN-DT helped to prepare and update work instructions for support elements and the CSS, and was heavily involved in evaluating achieved tolerances and non-conformities. Furthermore, MoS₂ layer applications and coil spreading for LSE assembly were supervised. Another routine work was to check and release drawings of connection elements. The systematic NSE MoS₂ layer ageing experiments were finished and summarised in a report. A long time exposure experiment of reference NSEs was started in the torus hall of W7-X in order to allow evaluation of the NSE lubricant layers condition – which are exposed to the torus hall air during the W7-X assembly phase – over the next years.

5.3.2 Module Connections

At the bolted connections of the CSS and the LSE 5-5 high shear forces have to be transmitted. The steel friction factor (FF) has to be significantly increased. Therefore, a qualification program was performed for commercially available friction foils to be inserted between the contact surfaces. After extended test series at room, LN₂, and LHe temperatures the optimal foil with a FF=0.5 was selected. In addition, cyclic load experiments were performed in LN₂. The required FF >0.5 was confirmed for the relevant case of dynamic loads without sliding.

5.3.3 Coil Quench Experiment (MQ Test)

Aim of the MQ test was to explore whether dynamic loads originating from stick slips within the magnet structure are able to trigger large enough elastic energy releases within the superconducting cable to cause quenches. The impact loads were applied by a pendulum via a transfer rod to the casing of the cold and energised coil within the test cryostat in Saclay. No quench could be triggered even with the maximal impact energy of about 200 J, corresponding to the worst estimated disturbance within W7-X, and at coil operation conditions with the lowest superconductor stability margin. The data of the successful MQ test were further evaluated and finally documented, the main results were published.

5.3.4 Potential Breaker

The mechanical strength of the potential breakers in the He supply lines for the coil cables is not explicitly specified. They are connected to flexible cryo-pipes, which are not supposed to transmit significant forces, moments and torsions

during W7-X cool-down and operation. However, such loads on moderate levels are unavoidable. Therefore, experiments at ≈ 85 K were performed to check structural integrity and leak-tightness of the breakers under torsion and tension, and an internal He gas pressure of 10 bar. It was found that the potential breakers withstand, without leaks or mechanical defects, about 10 times the loads expected in W7-X.

5.3.5. Materials

Maintenance and supplementation of the material data base (MDB) was brought to an end. The MDB is a collection of thermal and mechanical property data of all kind of cryogenic materials within W7-X, including all test results from the materials qualification programmes. A summary of the evaluated data was published.

6 Design and Configuration

The subdivision "Design & Configuration" is responsible for configuration management of W7-X, for configuration control of the components in the cryostat, the plasma vessel and the components in the experimental area and for providing design solutions and fabrications drawings for many components of W7-X. These tasks are taken care of in the three departments "Configuration Management", "Configuration Control" and "Design Office".

6.1 Configuration Management

The department Configuration Management (CM) is responsible for providing the complete and up-to-date system identification of all components of W7-X and to ensure proper change and deviation management. This then allows the determination of the present design or implementation status of all components of W7-X and provides detailed information on the history of any design changes. The system identification of all components and documents related to design, installation and operation of W7-X is stored in individual documents, the so called "Ringbuch" documents that either provide the information or refer to the most up-to-date information. Of those, interface documents describe in detail the nature and agreed upon specifics of all interfaces between pairs of components and change notes describe changes in the design that were adopted after the initial design had been released. The product lifecycle management (PLM) system is simultaneously used as a documentation data base, as a navigation platform to the specification of W7-X and its components and for notification on new releases of CM-relevant documents. Permanent control of the various CM processes is supported by specific process data bases, e.g. status and open issues of change requests, quality deviation reports and interface descriptions, are monitored. Well-established procedures are being followed to counteract any delays of in the change note processes or to assist particularly critical issues.

By now the configuration management for system identification, change and deviation management, interface coordination are routinely applied. Currently, 862 design change requests are registered in the change data base. 83 % of the requests have been accepted, 6 % are in the decision process and 11 % have either been rejected, withdrawn or became obsolete by revision. 75 % of the accepted change requests have been closed, i.e. the relevant design and assembly documents, computer aided design (CAD) models and drawings have been revised or created according to the change. Highest priority has been given to changes, which may directly affect the progress of W7-X assembly.

The W7-X interface matrix is currently built up of about 70 components. 192 pairs of them have identified interfaces, which are followed up by the interface coordination process. 51 % of the interface descriptions has been released, 44 % are being processed. For the remaining 5 % the design process of at least one of the components and thus the interface definition is pending. 15 % of the interfaces are fully defined, i.e. the interface descriptions have been released and there are no open issues left.

6.2 Configuration Control

The department Configuration Control (CC) is responsible for ensuring collision-free operation of W7-X during all modes of operation and for coordinating the space requests of peripheral components in the torus hall and adjacent buildings. In 2007, tools and procedures were established, to enable detailed and accurate investigations taking into account as-built geometries, in-operation deformation, etc. In 2008, procedures and interfaces with others department were defined or improved and the global strategy for configuration control was defined with the W7-X-board. Due to missing or late information on the deformation of those components and a lack of engineers able to perform the sophisticated investigations, it was necessary to take some risk management decisions: no configuration control for cryopipes was being done, the tolerance chains were reduced (average value instead of worst case). In 2009, the number of engineers in the department was temporarily doubled from 17 to 34 to cope with the workload and deadline of the thermal insulation configuration control. This required a change in the organisation: the group leaders were replaced by a team of projects leaders, and tasks were organised in projects. The department also performed a global check of the first module before the assembly in the outer-vessel. This check was a success: problems (resp. corresponding corrective actions) have been early enough discovered (resp. realised) to ensure the assembly of the module without any problems. It was therefore decided to perform the same check also for the other modules. In 2010, the department performed the global check of the second and the third module. The configuration control of components in cryostat (thermal insulation, bus system, cable trays, etc.) has been pursued and completed (only a few components still need to be investigated in 2011). Space reservation and design activities in the torus hall have also been pursued, for instance routing of cooling system, vacuum system, space reservation of heating devices, escape paths. The team devoted to this activity was very small during the first semester, but the completion in time (and sometimes ahead of schedule) of the configuration control tasks allowed the department to start to increase the staffing of the team during the second semester. The department "configuration control" continuously improves existing tools and establishes new ones. In 2010, the templates for issuing configuration control reports were further refined to better fit the demands and improve the tracking of changes in the CAD models. Excel tables and databases were implemented to provide complete information on all relevant issues. The CAD database tool Smarteam has been successfully implemented for the group System Layout and specific tools (export, collision reports, etc.) have been developed. The department also played a major role in the change of the assembly procedure of the ports. The first step of this procedure (performed "manually" by AS for the first module) was completely replaced by a new procedure. This new procedure consists in the measurement (scan) of the plasma vessel openings and the computer assisted creation of stencils and requirement sheets. These documents can then be used by AS to perform the cutting and assembly of the port without any additional preparation step. These documents were created for most of ports of module 1. This task required the development of specific tools and procedures inside the department and a lot of common work and coordination with AS.

6.3 Design Office

The tasks of the department Design Office are developing design solutions and providing fabrication drawings for components, supports, and tools for W7-X in close cooperation with the responsible officers of other departments. Additional tasks are defining and implementing design guidelines for working with CAD programmes and maintaining a proper structure of the CAD models in the data base. The design office is organised in four groups that focus on different design tasks: The Cryostat group, the Structural Elements group, the Components-In-Plasma-Vessel group and the Diagnostics group. In this way it is possible to coordinate related work packages, to maintain the same standards and design characteristics, to ensure simultaneous engineering, to adopt the design resources quickly to the extent of the design tasks, to effectively train new personnel. Most of the components of W7-X were originally designed using the CAD tool CADDS5. In recent years the transition was continued to use the design tool CATIA V5 instead unless the components were already such much

advanced that the conversion to CATIA would have been inefficient. Simultaneous engineering was made feasible by maintaining two identical overall assemblies of all components of W7-X both in CATIA V5 and CADDS 5. The leading assembly for most of the year 2010 was still CADDS 5, since the end of 2010 with the availability of the corresponding data base systems the leading assembly is being maintained in CATIA V5. The group Structural Elements group mainly provided design solutions for various structural components in the cryostat: Here the remaining fabrication drawings for the structural support elements were provided on the basis of measurements of the attachment flanges. Port, outer vessel dome and outer vessel surface models and drawings were modified according to a number of change notes that became necessary to mitigate collisions with the thermal insulation inside of the cryostat or to accommodate the increased space required for in-vessel components. The group Cryostat completed the design of the thermal insulation, of the cryogenic helium supply pipes and of various supports for permanent or temporary use within the cryostat. By now all components inside of the cryostat have been designed. Some modifications, however, are necessary for the cryogenic pipes in the vicinity of the attachment supports of the current leads. The Components-In-Plasma-Vessel group completed the design of the heat shield, of the covers of the diamagnetic loops, of the water cooling pipes and of the wall panels in the plasma vessel based on the design requirements of the initial phase of operation. The Diagnostics group focussed on the design of those diagnostics that need to be installed first or that require the longest time of development and fabrication. The remaining work load is substantial therefore care is being taken to completely specify the design requirements to limit the need for later-on iterations and to monitor the work progress closely in order to receive early warning the predicted completion dates tend to move after the required completion dates.

7 Assembly

In 2010 the preparations of assembly equipment and extensive assembly trials have been continued. The fifth and last magnet module passed successfully the mechanical preassembly. The first three magnet modules are put into their outer vessel modules on the final positions in the experimental hall. The alignment accuracy achieved is still much better than originally expected. The fourth magnet module was completed with the helium pipe system and the bus-bar system. The bus-bar system is being installed at the last magnet module. Further complex assembly devices for the final assembly (assembly ramps, vessel rigs) were put into operation and optimised. The manufacturing of the bus-bar system (co-operation with FZ Jülich) was accomplished successfully. The manufacturing sit at FZ Jülich was dis-

mantled. All pre-assembly work runs smoothly and without essential problems. The preparation of plasma-vessel (PV) sectors and coils and support structures were finished and the associated assembly equipment dismantled. Both the mechanical preparation of the outer vessel shells (including the complex plasma vessel supports) and the installation work of their thermal insulation still run routinely. The main focus in 2010 was the implementation of the port assembly. With large effort and additional resources this challenging task could be coped with. Indeed the process time needed for the port installation had to be extended noticeably however the schedule could be kept constant through increased work density, optimisation of the technology and restructuring of work packages. Both assembly and welding procedures for special ports were developed to minimise the welding-shrinkage. The assembly sequence and technology for current leads were conceptionally finished with the assistance of the PPPL and ORNL in Princeton and Oak Ridge. A 1:1 mock-up was built to qualify the associated technologies in detail. The challenging assembly process-planning, process documentation and work safety system run reliably.

7.1 BUS System

The manufacturing of bus-bars and the associated complex mechanical supports were accomplished. Works on the first four modules are complete; the fifth module was started with. All work inclusive the insulation at the busbar joints runs still routinely and without major problems. The process time was shortened accordingly. Developmentworks for the electrical connection of bus-bars and current leads were continued. A detailed and comprehensive assembly sequence was compiled and reviewed. The technological concepts were developed by the ORNL in Oak Ridge and the PPPL in Princeton. These concepts passed successfully the final design review (FDR). The entire sequence will be tested with dummies in a 1:1 mock-up, which has been built in 2010. First trials showed promising results. The cooperation with IFJ in Krakow was fruitful as in the years before. IFJ provides a major part of the technicians and the responsible line management for the daily works. In conjunction with the decrease of work in this assembly area (no further developments needed) the staff was reduced accordingly.

7.2 Vacuum Technology

The work packages of the vacuum technology group in 2010 were continued as in the years before. Main tasks were: leak detection on single components and on the cryo piping of thermal insulation; Paschen tests on coils and on the bus-bar system during the coil preparation and the assembly. Local leak tests with diverse test chambers for superconductor connections and cooling pipes at room temperature and at 77 K (if technically necessary) are routinely used during assembly.

The design of these test-chambers as well as the qualification of the practise was further continued. Design works on the vacuum systems were continued; first components have been ordered. The procurement contract for fast piezo valves for the gas-inlet was finalised.

7.3 W7-X Assembly

7.3.1 Component Preparation

The work at the preparation of coils, plasma vessel sectors and support structures has accomplished. Works at the last four outer vessel shells and ports are continued as planned. The preparation work on ports meanwhile runs also routinely. The development and implementation of the detailed procedures required 50% more resources than originally planned. Particularly the precise definition of the 3D cutcontour was very challenging. Moreover, the practical alignment of prepared ports is possible within about 2 mm but the high precision welding procedure requires accuracies of less than 0.5 mm. By rework these discrepancies have to be balanced. The minimisation of this rework through refined preparation processes was one main task in 2010. During the running work the preparation sites were changed to reduce costs. Internal hall space became free since the coil preparation was accomplished and the contracts therefore could be cancelled for external hall space. Despite the more and more optimised technology for the port assembly more process-time was needed than considered in the project schedule. One way out was to omit the trial-assembly of the ports, which lasts about two months per module. With that, the real contour of the PV opening should directly on the port be transferred. Instead, a theoretical procedure was successfully introduced, which bases on metrology data that are converted to a theoretical cut contour through the back office. This process runs completely in advance and in parallel to the practical works on site. A second counter measure was the utilisation of idle times by increasing the work density in the torus hall. Also these improvements were successfully implemented. With all counter measures the original schedule milestones could be kept. First ideas for the preparation of KiP components were developed. Suitable hall space was made up for these works.

7.3.2 Pre-assembly

All magnet modules have been completed mechanically in the pre-assembly. The associated complex assembly equipment was dismantled. The hall space is used now for installing the thermal insulation on ports. The first three modules are positioned onto the machine base in their final co-ordinates. The fourth module is ready for being transported onto its final position. The fifth module gets its bus-bar and helium-pipe system at the moment with all mechanical, electrical and hydraulic connections. These works are running smoothly and routinely and they are slightly in advance of the schedule.

Since here the work load is decreasing and no further qualification and development work is needed, the staff was reduced accordingly.

7.3.3 Final Assembly

In the final assembly the construction work at the first module of W7-X is nearly accomplished. In this module all ports have been installed, welded and leak tested. In the second module the port installation is finalised whereas in the third module these works are just started. The overall accuracy at the port installation is a bit worse than expected but still compatible with the later use of the ports. The implementation of the complex assembly technology was more time and resource consuming than planned (see chapter "component preparation"). Almost all technology resources of the assembly subdivision were allotted to these work packages. Also the assembly bridge and ramps had to be optimised a few times.



Figure 12: The port assembly ramp in operation from the floor.

After ten very work-intensive months in 2010 the technology is now running routinely. Only the highly accurate port AEK-V2, which is used by the ECRH heating still requires the development of a special technology. The precise welding

prehensive qualification in advance the port welding and leak inspection are running without special problems or delays. The quality of these welds is excellent up to now. Six additional welders who are highly qualified were hired from the industry to cover the work system with 88 hours per week. This is another example for the good and longstanding co-operation with our partner firms. The optimisation of the ports assembly is ongoing but with less recourses. The installation of the thermal insulation (TI) in parallel to the port installation runs also very smoothly meanwhile. These works are made by MAN DT. Still open is the issue of harmonizing the different shift systems between IPP and MAN DT. The solution of that issue could save further time and shall be traced again in 2011. The shipment of the fourth module to the experiment hall lies ahead briefly. The insertion into the outer vessel shells is expected to run as smoothly as with the former three modules. Probably these works will start a bit earlier than assumed in our schedule. The preparation of the outer vessel shells for the last module runs without any problems and within the schedule. One main work package in the assembly technology was the further development of the assembly sequence for the module separation plane (MSP). 3D shims (wedges) are used to bridge the gap between neighbouring modules of the magnet structure. The modules of the structure can relative be tilted, shifted and twisted to each other. That result from the final alignment of the individual magnet modules within the W7-X co-ordinate system, which is made independently for every module (minimisation of the resulting field error). Eight shims in total are needed per MSP. Each shim weighs about 20 kg. Every shim must be customised with an accuracy of better than 1/10 mm, which forms a practical limit. Together with the shims diamond-coated friction foils are inserted into the gap between the neighbouring modules. The determination of the gap dimension is made by means of steel-templates and measure machine. The associated procedures were successfully qualified. Another very comprehensive development was made for the lateral supports at the MSP. These supports connect the coils at the adjacent modules. Each support weighs about 50 kg and must be precisely installed through the quite narrow gap between the outer vessel modules. For the positioning and tightening of the bolts the technician must work in the interior of the module in a narrow assembly duct. The support itself represents a complex twisted wedge construction. It must fit into the counter supports at the coil housings with a formlock better than 1/10 mm. To achieve that accuracy the individual 3D shape of the coil supports is laser scanned. After that the position of two respectively opposite supports is determined with the photogrammetric. Both data sets the scanning and the photogrammetric are then combined forming the base for the manufacturing of an aluminium dummy.

process particularly is qualified at present. Thanks to a com-

This dummy is trial installed and as long as reworked until the remaining gap is smaller than 5/100 mm. The aluminium dummy is the base for the consecutively manufacturing of the original steel support, which is made from steel 1.4429. This procedure shall be repeated for every support. The soundness of this procedure was proven using several mockups and trials. Procedures for the connection of the vessels inclusive its thermal insulation at the MSP were agreed with the company MAN DT. The assembly procedure for the current leads (CL) was the third development work package in 2010 for the final assembly. Much assistance was given by the ORNL in Oak Ridge and the PPPL in Princeton to find conceptional solutions for the various complex details. Particularly a doable solution for the temporary support structure was worked out, which is situated in the interior of the cryostat in the narrow vicinity of coils, pipes, bus-bars and ports. The pair of CL (each weighs 250 kg) will hang at this structure temporarily during the assembly process. The upper end of the CL must be positioned precisely in front of the aligned bus-bar joints to ensure that the electrical connection between CL and joint has got a resistance value of not more than about 10 nOhm. In addition, any misalignment will result in residual stresses, in the associated ends of the bus-bars, their insulation and welds. After the assembly the dead weight of the CL is taken by pivot supports at the bottom side of the CL. The critical step is when the dead weight is being transferred from the temporary support at the upper end on the pivot support at the bottom side. The CL must not inadmissibly tilt or set during this operation to avoid an overstress of the sensitive welds and insulation-connections.

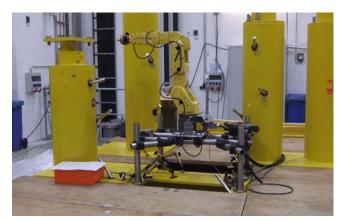


Figure 13: The manipulator during the acceptance test.

A whole set of alignment tools and support was designed and will be tested to realise these requirements. A major tool will be a modified assembly ramp, which is already used during the port assembly. This ramp will allow the precise assembly of the CL but also the associated heavy domes (part of the outer vessel) and pivot supports. In addition this third ramp can be used for the assembly of ports either. This shall help to minimise idle times. The delivery of this ramp was contracted to the Fantini Company in Italy, which delivered already the first two ramps. For it a comprehensive set of manufacturing-drawings was provided by the ORNL. With the use of the above technologies the five individual modules can be connected with each other and the torus of the base machine of Wendelstein 7-X will be accomplished. According to the present planning the first MSP will be closed in summer 2011. But first part-works have already started.

The co-operation with the KiP division in Garching at the field of conceptual planning of the assembly of the KiP has been continued in 2010. Trial assemblies with wall panels, heat shields and sweep coils have been continued successfully. The system of platforms and cranes for the handling of components was developed further. A manipulator for the precise 3D-alignment of supports and bolts in the interior of the PV was delivered meanwhile. The manufacturing and necessary improvements for achieving the specified accuracies of that system lasted much longer than the supplier and the IPP were expecting. The target co-ordinates for this manipulator are being deduced from the CAD data of the associated models. In the final acceptance test it was proven that the positioning accuracy of the manipulator is approximately within half a millimetre. The technology development in terms of logistics, tooling and procedures is continued as planned.

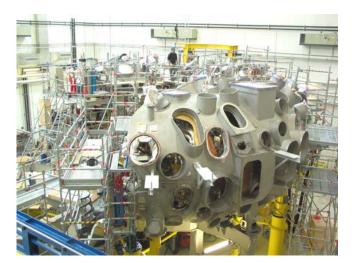


Figure 14: Three out of five modules in the torus hall.

In the periphery, the work on cryo instrumentation in conjunction with the work at the bus-bar systems has been further continued. Installation works of the extension of the low voltage power supply system are continued. The conceptual planning for the realisation of the Electro-Magnetic Compatibility (EMC) during the construction of the periphery was continued. The first construction stage of the cooling system is complete. The planning work on the second stage

is ongoing as planned. The assembly control and the planning work routinely as before. The advanced weekly and 4-weekly plans are used as standardised tools. The preparation of the assembly documentation (QAAP, work and test instructions) is ongoing without any severe problems. In 2010 a further refined resource planning was made. Quality deviations are reliably handled as in the years before. The assembly schedule was slightly updated. The planning for the final periphery (cables, cooling pipes, vacuum lines, and platforms) was further refined. The details here will become a highlight in the year 2011. The commissioning date was kept constant on the middle of 2014 but the work density during the final assembly was increased further. Staff for the assembly was adapted to the changing work packages (mechanics, insulation specialists, welders) with personnel from the industry. More responsible officers took up their employment. Again external staff was included to ensure the partial two-shift-system and extended working times in the assembly. Additional engineering staff started the work for the development and qualification of technologies for the final assembly. The co-operation with engineers and technicians of the Polish Academy of Sciences was continued. Altogether, assembly has reached the planned progress in 2010. Further new assembly technologies were qualified and successfully tested. The preparation of coils, plasma vessels and structural components was accomplished. The same applies to the mechanical pre-assembly of magnet modules. The assembly technologies for the ports were concludingly defined. The device assembly ran continuously and speedily as planned. Resources for engineering tasks and technicians for assembly works were adapted to cope with the changing work packages and needed work capacities. The port assembly technology was completely implemented. The detailed technology for the assembly of module separation planes (magnets, vessels, ports, current leads) was comprehensively developed and complemented. The assembly control with the planning and the documentation of assembly was further refined and works furthermore experienced and reliably. The co-operation with external partners who provide skilled and well-trained technicians and engineers for the realisation of the assembly work on W7-X works stabile and smoothly.

8 DIAGNOSTICS

8.1 Overview

The work concentrates on the "start-up diagnostics" set necessary for safe operation and control of the machine and those diagnostics adapted to and being indispensable during the initial operation phases of the experiment. The diagnostics department consists of three expert groups and a temporary working group, which is developing and testing solutions for ECRH stray radiation shielding of in-vessel components. The following sections briefly summarise the main activities within the expert groups of the project.

8.1.1 Edge/Divertor and Magnetics Configuration Diagnostics

A design optimisation of the flush mounted Langmuir probe array for the Test Divertor Unit (TDU) with respect to manufacturability has been carried out and a new mock-up for testing this design in GLADIS manufactured and assembled. For the first time two of the probe tips were wired and a realistic cable routing implemented. In parallel the electrical connector unit at the end of the divertor module as well as the routing to the plasma vessel and along the vessel wall into the port till the electrical vacuum feed throughs has been completed. The principal design of a resonant piezo step-driver for linearly movable probes required for the pop-up probe array for the actively cooled High Heat Flux (HHF)-divertor has been finished, so that the high-temperature piezo-material can be ordered now. The short prototype of a manometer cannula for W7-X has been successfully tested on WEGA and a number of possible further improvements identified. The mechanical tests of a long prototype showed a small cross-deformation of about 3 mm from bending of the 2.30 m cannula under its own weight, asking for an additional support of the head inside the machine. Using the short prototype the required reduction of the noise with the re-designed digital electronics has been successfully demonstrated on WEGA. The H_a-diagnostic for W7-X will be installed in all 10 AEF ports, together with the infrared-thermography cameras, for monitoring the divertor plasma in the upper and lower divertor modules with mm-spatial resolution. The design study for a long pulse compatible endoscope system with a cooled entrance pinhole and a mirror system mapping the light from the divertor view onto different detection branches equipped with filters and cameras sensitive for visible and two different IR-regions has been finalised and the specifications for an international call for tender are being prepared. For cost reasons, during the TDU-phase only two such endoscope systems will be installed, while the other eight ports will be equipped with a simple immersion tube system sealed with IR and visible vacuum windows and a shutter for protection during plasma wall conditioning. A cradle containing the IR camera, a visible camera with a wide angle objective equipped with an interference filter (IF) and a third channel for either a further camera system or a fibre optic for spectroscopy, mounts directly behind the window flange to maximise the field of view. The cradle system is at atmosphere and can be unhinged from the immersion tube to service the cameras. With the IFs selection of certain wavelengths bands (e.g. H_{α} , H_{γ} , C II or C III line radiation) in front of the visible cameras particular physics questions and scenarios will be addressed. Furthermore a third H_a-diagnostic system employs single-line-of-sight views at various ports collecting the radiation with simple lens systems into fibre-bundles for

spectroscopic investigations. The micro bolometer IR-camera sitting in the cradle has been especially hardened for operation in strong magnetic fields (up to 3 T). The system contains a state-of-the-art infrared detector with 640×480 pixels and has a Gigabit Ethernet interface. It features a temperature range of 0 °C to 1800 °C, a special wide-angle lens with FOV of 116°×82°, a pneumatically driven shutter and consists of two boxes. The first one includes the sensor housing with parts not sensitive to the magnetic field. The second one is the electronics box, which contains all parts expected to fail in high magnetic fields. Both the sensor housing and the electronics box are sealed to IP54 standard with a rugged housing that holds up well in environments where water and dust resistance is required. Screened cable connections between them provide protection from alien cross-talk and electromagnetic interference. The video diagnostic is being developed by HAS (Budapest, Hungary). A prototype of the video diagnostic system has been manufactured and used for a complete mechanical and thermal in-vacuum test at IPP-Greifswald. Besides the test of the camera docking mechanism the complete system's behavior was tested simulating the different heating scenarios (baking, various plasma operation scenarios) by using an infrared heater. The air cooling (both camera capsule and objective) and the water cooling (pin-hole part) efficiency was found to be sufficient: at the maximum expected temperatures the cooling systems were able to decrease the temperature to an acceptable level in a sufficiently short time span, so that the design of the mechanical part of the diagnostic could be closed. The test of the optics, specially designed for observation through the pinhole, has demonstrated that it performs up to its specifications. The first fully functional control software package (v1.0) for the EDICAM v2.0 fast camera has been completed. The software features all fast camera functionalities, such as a very flexible region of interest (ROI) selection, a wide range of exposure times (25 ns - 100 s), frame rates up to 100 kHz, and triggering capability. The development of the firmware for the intelligent camera operation has been continued in 2010 and the first results are expected in 2011. Reference designs for the in-vessel cabling of the magnetic diagnostics and for the ECR stray radiation shielding of the in-vessel Rogowski and segmented Rogowski coils as well as the diamagnetic loops were chosen. Vacuum tests of outgassing, stray radiation shielding as well as modeling and tests of the electromagnetic behavior, in particular of the effect of eddy currents in the stray radiation shielding, were initiated. The present status of the in-vessel magnetics was reviewed in the framework of a design review in order to identify open points. A concept for the temperature surveillance of the in-vessel Rogowski coils, the segmented Rogowski coils and the diamagnetic loops has been developed. Several material options for the Mirnov coils were considered and first prototypes of these coils been ordered from industry.

The signal cable routing inside the plasma vessel and within the ports was designed for the magnetic diagnostics. The cabling and rack layout in the experimental hall outside the vessel and the definition of the interface to the data acquisition systems has been started.

The design of the manipulators (for the electron gun and the fluorescence rods) and shutters for the flux surface diagnostic made significant progress. The electron gun based on LaB₆ electron emitter material was successfully tested up to a magnetic field strength of 3T in a gyrotron magnet and utilised during magnetic field line visualization experiments on WEGA. In order to provide well defined geometrical reference points inside the W7-X plasma vessel, within the plane of the fluorescence rods, for the AEQ port video observation cameras, copper coated quartz fibres, which will be integrated into the graphite tiles of the wall protecting elements and which can be illuminated from outside the plasma vessel will be used. The ECRH stray radiation compatibility of fibres has been qualified during a test campaign in the MISTRAL chamber. The fibres can be continuously operated at temperatures of up to 700 °C. For the data analysis of the helium beam diagnostic a Bayesian inversion model has been implemented. Simulations for high density and low temperature detached divertor plasma operation show the necessity of an absolute intensity calibration of the detection system to achieve acceptable density measurement errors levels. An application of white light interferometry for insitu measurement of diagnostic window transmission losses due to plasma deposition in the visible spectral range is being investigated. First Bayesian inversion based simulations suggest the possibility to derive the thickness and absorption coefficient of a coatings building up on the windows from a measured reflection spectrum.

8.1.2 Microwave and Laser Based Diagnostics

The classical microwave and laser diagnostics are being prepared aiming at the measurement of electron density and – temperature in the plasma core, namely Thomson scattering, interferometry, polarimetry, reflectometry, and ECE. The design of most in-vessel components has been finished. For the ECE system the Gaussian in-vessel optics consisting of stainless steel mirrors, with the first mirrors actively being cooled, has been manufactured and alignment tests started in the laboratory. The periphery, control- and data acquisition needs have been defined. For the YAG Thomson scattering system the observation optics for the first port has been delivered and tested successfully and the optics for the second port been ordered. The design of both optics was part of the training program Engineering of Optical Diagnostics for ITER. The design of the laser launching port with its Brewster windows and cooling capabilities is close to completion. Long term tests of the cooled port shutter showed fatigue in the flexible hose for water supply; alternatives have been found and vacuum tests are now being prepared. Series production and assembly of the 30 polychromator boxes for OP1 has started at the Institute for Nuclear Physics in Krakow (INP, Poland) and runs on schedule. The spectral characteristics of the polychromator filters were measured together with the AUG Thomson scattering group. In the experiment hall a massive support structure in the torus centre will serve as support for the Thomson observation optics as well as for the retro-reflector of the single channel interferometer, which shares its line-of-sight with the Thomson laser, making it ideal for cross calibration. A stability analysis of the support structure has been conducted by the engineering department and a mechanically most robust design for this structure has been selected. The interferometer development was reviewed in the 3rd Workshop on Interferometry for Steady State Fusion Devices organised in Greifswald with participants from external cooperation partners and beyond. Issues were options for advanced line average density measurements with improved reliability under high-density steady-state conditions such as dispersion interferometry, polarimetry and high-resolution two coloured interferometry. A modular multichannel Dispersion Interferometer (DI) is being studied by a Post Doc at TEXTOR, Jülich. The system has been delivered by an FZJ contract partner, the Budker-Institute of Nuclear Physics (BINP), Nowosibirsk. The four commissioned DI channels are being operated successfully since summer. Improvements with respect to their long-pulse capability are ongoing. Dispersion interferometry allows for a compact optical system without need for a reference line and therefore is intrinsically less prone to vibrations and drifts but also is tolerant against intermittent loss of signal – an advantage in particular for quasi-continuous operation. As a robust fallback solution a classical single-channel two-colour CO₂-CO interferometer has been set-up, tested and qualified in the laboratory. A fast steady-state phase measurement based on an FPGA has been developed within the framework of a PhD thesis in cooperation with CIEMAT, Madrid. For comparison of both interferometer systems vibration tests were conducted with a piezo controlled retro-reflector. It has been suggested to build both W7-X interferometers – the multichannel interferometer and the single-channel Thomson sightline one – based on Dispersion Interferometry; the final decision on this will be taken by early 2011. In the torus hall mechanically challenging components are the two optical benches for the single- and the multichannel interferometer. Their basic design including laser safety aspects and maximizing mechanical stability has been finished; however, a final decision on the table board material is still missing due to activations risks possibly arising from the desired Granite materials. Granite material composition from different sites is presently being analysed. For long-pulse operation all laser diagnostics need active laser beam position control to

cope with thermal drifts. A first prototype of a system based on a SIEMATIC control unit has been set-up and tested in the laboratory. As a redundant measurement technique for density feedback control of high-density discharges, a feasibility and sensitivity study for a single-channel Cotton-Mouton polarimeter in the specific magnetic geometry of W7-X has been conducted and published together with the Akademia Morska, Szczecin, Poland.

However, due to restricted resources the realisation of this diagnostic has been postponed. The diagnostic group also operates the MIcrowave STray RAdiation Launch facility (MISTRAL) together with the diagnostic engineering department and the ECRH group. The MISTAL chamber is used to qualify diagnostic and other in-vessel components for operation in a high background of 140 GHz microwave stray radiation as expected during O2 and OXB mode ECRH heating of high density plasmas. Suitable diagnostics for 140 GHz stray radiation measurements and its spatial distribution e.g. in W7-X ports, have been specially developed in cooperation with the technical University of Eindhoven. Studies of the spatial distribution and homogenity of the stray radiation inside the MISTRAL chamber were performed by a trainee (home institution CIEMAT) of the program "Microwave Diagnostics Engineering for ITER", which was part of the European Fusion Training Scheme. Apart from the necessary detection and characterisation of the stray radiation itself, the focus of the work was on the development of stray radiation shields for critical in-vessel components. E.g., the actively cooled radiation shield in front of the cryopumps – the so called water chevrons – have been successfully coated with an ECRH absorbing Al₂O₂-TiO₂ ceramic layer at the University of Stuttgart. Another focus has been on the shielding of microwave absorbing cable isolations and entire components, coils, connectors and feedthroughs of the magnetic diagnostics. All in-vessel cables need to be enclosed in Cu tubes. For vacuum pump-down the pipes need to be perforated with a sufficiently large number of holes with diameter significantly smaller than half the wavelength. Finding a suitable compromise between vacuum and ECRH shielding requirements still is an ongoing process.

8.1.3 Core Spectroscopy

The construction of the Russian Diagnostic Injector for W7-X (RuDI-X), which is needed for active CXRS and CX-NPA measurements is progressing. The injector tank has almost been completed, with helium leak testing presently ongoing. Furthermore, almost all power supplies have been completed and will next be put through their acceptance tests. The calorimeter is 80 % ready, only the ion source with its sophisticated extraction grid design still requires significant developments during the next months. Two closed-loop cryo-pumps have been delivered to W7-X and tested and presently the S7-control-electronics system is

being set up. The design of the support platform for the RuDI-X in the torus hall has been completed, as well. Numerous tests of vacuum gauges, a mass spectrometer system, a turbo pump system and electronics were successfully performed in the local magnetic field test rig, providing information, on which components can be operated in the permanent magnetic field on W7-X. For the CXRS observation system, the concept and outline design of the immersion tube has been completed. A spectral Motional Stark Effect (MSE) diagnostic has been implemented at ASDEX Upgrade. Data analysis tools have been developed and also used to build a virtual diagnostic. Simulations for Wendelstein 7-X have been performed using predictive transport simulations and pre-calculated equilibria, also properly accounting for partially elliptically polarised light emission due to charge exchange emission and the MSE multiple (supported within the EFDA work program 2010). The general design of the CX-NPA has been finished with exception of its support structure. Presently, the proposed solution with one extension arm for supporting the three analyser is checked by structural analysis calculations. Detailed stability calculations of the support structure and calculations of the load onto the outer vessel in the proximity of the AEN 41 port have been started. Studies of the influence of magnetic stray fields on the performance of the NPAs have been performed on MAST by measuring the outer magnetic field components using a fast 3D-Hall probe during typical discharges. The CAD model for the support structure of the high-efficiency XUV overview spectrometer system (HEXOS) including all set-up modifications due to the special W7-X requirements has been almost designed while the system is still running on TEXTOR-DED (FZ Jülich) for testing purposes. According to a new schedule concerning the preparation of the assembly at W7-X, the HEXOS system should be transferred into the final W7-X support structure in summer 2011 and again mounted to TEXTOR till summer 2012. During this time the control and data acquisition will be adapted to W7-X standards by the ZAT (FZ-Jülich) and the CodaC group (IPP-Greifswald), and in parallel the system will join the scientific program at TEXTOR. In the framework of the cooperation between IPP and University Opole (Poland) the conceptual design of the C/O monitor has been finished and the design work packages fixed during a design review. The TlAP crystal for O VIII has been ordered and for the three MLMs for B V, C VI and N VII the tendering procedure has been started. An appropriate detector foil has been selected and already delivered. For the bulk plasma bolometer system in the triangular plane, a prototype of the shutter system for the horizontal camera in port AEU30 has been manufactured and tested in the laboratory. The design of the vertical camera in port AEV21 has been completed. Manufacturing drawings for a shutter prototype, being different from the one of the

horizontal bolometer camera, have been made. Manufacturing details for the water-cooled detector holder, which needs to be made of highly thermally conducting CuCrZr are presently being discussed with a manufacturer. The impact of non-absorbed 140GHz microwave stray radiation on the bolometer signal has been further investigated in the MISTRAL chamber using a gold-foil type detector. By coating the inner surface of the camera enclosure with TiO₂/Al₂O₃, an ECRH absorbing ceramic layer, significant damping of the microwave multi-path-reflections has been achieved. In this way the microwave induced signal has been reduced by a factor 10, in line with the expected value deduced from power balance calculations inside the bolometer housing. By installing a suitable metal-mesh (d90µm/ w236µm) in front of the detector head, it was possible to reduce the microwave impact by a factor 30. By applying both techniques simultaneously a suppression of the impact of the microwave radiation by a factor 300 has been achieved. In this way the microwave induced signal becomes less that 1 % of the expected signal level from plasma radiation (50 kW/m²). This concept will be adopted in the W7-X bolometer designs. For the in-vessel soft X-ray multi-camera tomography system (XMCTS), the shutter could be improved further to achieve a sufficient long term operation reliability. A prototype multi-channel preamplifier board has been manufactured, tested and remaining signal to noise ratio problems identified. The cooling requirements of the pre-amplifiers in the secondary vacuum were assessed and it was found that a simple contact cooling to the surrounding cooled electronic box is sufficient. The manufacturing of the electronic box made from CuCrZr material, considered for improved cooling, remains a challenge in conjunction with the custom-made multi-pin vacuum feedthroughs. The design was improved further by avoiding weldseams. Different joining technologies for the electrical feedthroughs (glass, ceramics, epoxy) are under consideration and a collaboration with the Köhler Institute in Jena was started. In the scope of the ongoing collaboration with IST/Portugal a feasibility study of support vector machines as method for online tomographic inversion has begun. The design of the pulse height analysis system (PHA) being built by IPPLM Warsaw to monitor the X-radiation emitted from the core plasma has been trimmed to fit into a single beam pipe with the piezo-driven slits, a set of filter-foils and three silicon drift detectors for simultaneous high-efficiency observation in three X-ray energy regions. The PHA detectors and the detector arrays for the multi-filter foil system (MFS) are on order. In collaboration with PTB Braunschweig MCNP modelling of the neutron counters has been started to define their material composition and geometry. The neutron counters are based on the NPL long counter principle (National Physical Laboratory, Teddington, U.K.), but will be equipped with up to five parallel arranged counter tubes.

Some improvements are expected from further optimisation calculations regarding the opening angle and the energy response function of the monitors during the next six months. In addition, first experimental studies with selected counter tubes have been performed. The basic concept for data acquisition system has been worked out taking into account the requirements given by the authorisation agency on one hand and diagnostic purposes on the other.

8.2 Collaborations

The diagnostics are being developed in close collaboration with FZ-Jülich. In particular in case of the HEXOS VUV spectrometer and the development of the diagnostic neutral beam FZ-J is heading the projects. The Budker Institute in Novosibirsk, Russia, is developing and constructing the diagnostic neutral beam injection system, EURATOM HAS in Budapest, Hungary, is developing and constructing the video diagnostic systems for W7-X, IPPLM, Warsaw is developing a pulse height analysis (PHA) system and a multifoil spectroscopy (MFS) system, the university of Opole, Poland is preparing a C/O monitor diagnostic and the Akademia Morska, Szczecin, Poland and the Szczecin University of Technology are investigating the sightline of the Interfero-Polarimeter and different microwave based polarimeter and interferometer methods, CIEMAT investigates potential and components for CO₂-Intefererometry, IST/CFN, Lisbon participates in developing fast tomographic inversion methods and is developing ADC/DAQ stations being linked to XDV, PTB Braunschweig is working on the development of a Neutron-Counter System for W7-X and IOFFE Institute St. Petersburg, the Culham Centre for Fusion Energy (CCFE) and CIEMAT in Madrid are collaborating in the field of CX-Neutral Particle Analysis and the Technical University of Eindhoven, The Netherlands, is contributing to the development of ECRH stray radiation detectors.

9 Heating

9.1 Project Microwave Heating for W7-X (PMW)

The 10 MW Electron-Cyclotron-Resonance-Heating (ECRH)-system for W7-X is designed for continuous wave (CW) operation (30 min) at 140 GHz, which is resonant with the W7-X magnetic field of 2.5 T. The total power is generated by ten gyrotrons and is transmitted to the plasma by a low loss quasi-optical transmission line and versatile in-vessel launchers for both, high field side and low field side launch. ECRH will support also W7-X operation at reduced magnetic field, because the gyrotrons can be tuned to 103.6 GHz radiation emission with about half the output power. This is of particular importance during the commissioning phase of W7-X and for confinement studies. The ECRH-system is being developed and built by the "Karlsruher Institut für Technologie" (KIT) as a joint project with IPP and IPF Stuttgart.

The "Project Microwave Heating for W7-X" (PMW) coordinates all engineering and scientific activities in the collaborating laboratories and in industry and is responsible for the entire ECRH system. PMW is strongly involved in advanced and ITER related R&D activities for ECRH and CD-Systems with even higher power, efficiency, and flexibility. This activity is partly organised within the frame of the virtual institute "Advanced ECRH for ITER" (collaboration between IPP Garching and Greifswald, KIT, IPF Stuttgart, IAP Nizhny Novgorod, and IFP Milano), which is supported by the "Helmholtz-Gemeinschaft deutscher Forschungszentren". The virtual institute was terminated on schedule by end of 2010.

9.1.1 The W7-X Gyrotrons (KIT)

The production of the seven series gyrotrons at THALES started in 2004, the first gyrotron SN1 was delivered and tested successfully in 2005 with an output power of 920 kW for 1800 s. This gyrotron was sealed to keep the warranty, whereas the two prototype gyrotrons were routinely used for experiments and component tests. The reproduction of the SN1 performance turned out to be difficult and the following series gyrotrons failed to meet specifications. A careful analysis indicated, that parasitic oscillations are excited in the beam tunnel region, which lead to an excessive heating of the beam tunnel components, in particular of the absorbing ceramic rings. The inspection of gyrotrons, which were re-opened in the factory after operation showed significant damages due to overheating at the ceramic rings and the brazing of the rings. The series production was put on hold in agreement with THALES and a new beam tunnel was designed, manufactured and validated in experimental high power campaigns with two modular short pulse test gyrotrons in 2009 at KIT. As the main difference to the usual beam tunnel this design features corrugations in the copper rings, which handicap the excitation of parasitic modes. The SN 4 (repair) gyrotron was the first series gyrotron, which was equipped with this improved beam tunnel, and delivered to KIT in early 2010 for Factory Acceptance Test (FAT). During the tests no parasitic oscillations originating from the beam tunnel region were observed and the maximum power could be extended to 820 kW. The gyrotron, however, showed an unstable behaviour and mode loss was limiting the achievable pulse duration to several 10 s of seconds. The limitations could be removed by a careful mechanical adjustment of the gyrotron in the magnet (tilted installation) and by improving the high voltage capability. A reliable operation with up to 870 kW was achieved for 3 min pulses (test stand limit). The thermal power dissipation measured in the beam tunnel, cavity and launcher cooling circuits is as expected with no excessive heat load. The measurement and analysis of the output beam gave a Gaussian content as high as 97 % indicating,

that the mode converter and the internal optics operate as designed. A saturation of the output power on beam current was observed, however, beyond 40 A, which is below the currents observed in previous tubes. The gyrotron will be shipped to IPP for Site Acceptance Test in January 2011, where the activity shall focus on the extension of the pulses and the improvement of the efficiency. The FAT of the SN 3(repair) gyrotron at KIT was performed early 2010 and completed in March. As this gyrotron was still equipped with the old beam tunnel, it was decided to perform the tests at reduced output power, well below the threshold for excitation of the parasitic oscillations. A safe operation of the tube was achieved with an output power << 700 kW without oscillations in the beam tunnel. The operation of the gyrotron beyond this limit is usually associated with unstable operation, enhanced stray radiation and an increased amount of absorbed RF power in the beam tunnel region, which may result in a thermal overload. Thermographic measurement and analysis of the output beam gave a TEM00 content of 97 %, which confirms the high quality of the internal converter and mirror system. Long pulses up to 3 minutes were performed during FAT at KIT with 700 kW and an efficiency of 37 % in depressed collector mode for energy recovery. All gyrotrons must pass a reliability test as a standard procedure in consecutive full power, 3 min, pulses.

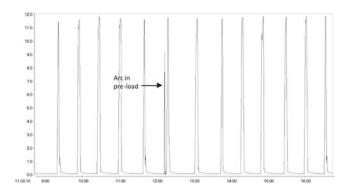


Figure 15: Repetitive operation of the SN3 gyrotron with 3 min pulses at a duty cycle of 10 %. The output power is plotted versus time during one operation day. One short pulse was due to an arc in the pre-load.

Figure 15 shows the repetitive operation during this reliability study for a full day with a duty cycle of 10 % (power supply limit at KIT). All pulses were successful; one pulse was pre-terminated due to an arc in the pre-load. After shipment to Greifswald, the Site Acceptance Test at IPP was performed in parallel to the SN 4 (repair) tests at KIT and completed after only 6 weeks of testing in June 2010 while extending the pulses towards 27 min at the same power. The gyrotron is in regular operation at IPP Greifswald now for tests of advanced ECRH-components.

9.1.2 Transmission System (IPF)

The power transmission from the gyrotrons to the plasma is provided by a quasi-optical mirror based system, which operates under atmospheric pressure. It consists of single-beam waveguide and multi-beam waveguide (MBWG) elements. The single-beam lines provide the beam conditioning, i.e. the matching of the gyrotron beams to the parameters of the transmission system, and the adjustment of the polarisation for optimum absorption of the radiation in the plasma. Two symmetrically arranged MBWGs transmit the combined power of all gyrotrons to the experimental hall. At the output planes of the MBWGs situated in the torus hall, two mirror arrays separate the beams again and distribute them via two other mirrors and CVD-diamond vacuum barrier windows to individually movable antennas (launchers) in the torus. The manufacturing and installation of the components of the basic transmission system (112 reflectors for transmission plus 32 reflectors for switching and diagnostics) is completed now. The rf-beam characterisation of the SN 3(repair) gyrotron and the subsequent design and manufacturing of the surfaces of the two matching mirrors for this tube were performed. The beam parameters of the SN 4 (repair) gyrotron, which is presently under test at KIT Karlsruhe have been measured also, the design and manufacture of the related matching mirrors is under way. Standard methods use heat targets, which tolerate only short high-power pulses of a few ms. The W7-X gyrotrons (like others) exhibit, however, a frequency chirp during the first second after switching on, which is caused by the thermal expansion of the cavity, and it is an open question, whether the output beam parameters change significantly during the chirp. We have thus performed measurements on the Maquette gyrotron beam with a thermographically imaged high-temperature Si3N4 target at various locations in front of the CCR load. A noticeable shift of the beam was observed during the pulse of typically 500 ms pulse duration. The target would, in principle, tolerate longer pulses, but the pulse length was limited by arcing at the target surface. A new technique using thin foil beam splitters is now considered. Several materials have been subjected to 100 ms long pulses and a usable material has been identified. Further remaining work includes diagnostics and power measurement of the gyrotron beams. The receivers attributed to the directional couplers on the mirrors M14 have been designed, and are under fabrication; related alignment control is in development. Industrial high power cw dummy loads, which are based on thin absorbing layers on metallic cooling structures shows a long-term destruction of the coating and a related degradation of the power handling capability. This long-term experience has triggered the development of uncoated metallic absorbers. For module 1, a water-cooled version of the 'Long Load', which consists of a 22 m long absorbing stainless-steel waveguide, was constructed and

delivered in December 2010. The power distribution along the load shows pronounced minima and maxima due to interference of the propagating modes as seen in figure 16. The load consists of four segments; the first two segments have the same diameter as seen from figure 16 (top) to keep the power loading at an acceptable level. The next segments are connected with linear tapers in areas, where the wall currents and thus the power deposition have a minimum to avoid arcing problems. The total length is chosen to fit into the beam duct at W7-X. The remaining power at the exit of the load is about 25 % of the incident power, which can be easily absorbed and calorimetrically determined. In this arrangement, the Long Load would serve as a calibrated pre-attenuator. Commissioning of this load is scheduled for beginning of 2011.

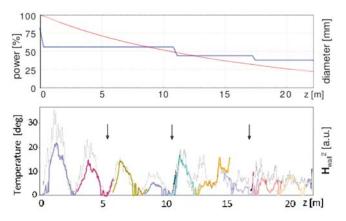


Figure 16: Top: Calculated rf-power and waveguide diameter as a function of the length z. Bottom: Calculated distribution of the temperature rise and field intensity $H_{wall}^{\ \ \ \ \ \ \ \ \ \ \ }^2$ as a function of the length z. The arrows indicate locations of minimum absorption, where the different segments are connected.

In module 5, an industrial compact cylindrical stainless-steel load from GYCOM was installed, and the system of coupling mirrors was upgraded to allow routing of the power beam either to the CCR load or to the GYCOM load. Within the parameters used up to now (700 kW, 15 min), the GYCOM load performs well, further tests are planned.

9.1.3 High-field Side Launch with Remote Steering (IPF)

The scientific programme of ECRH and ECCD at W7-X includes confinement studies with high field side launch. Two out of the ten rf-beams can be switched to N-ports, which give access to the plasma from the high field side with a weak gradient of the magnetic field. Front steering launchers as used in the A and E ports will not fit into these narrow ports and thus "remote-steering" launchers (RSL) are foreseen. The further investigation of the RSL-concept is of high importance also in view of future applications of ECRH in radioactive environment e.g. in DEMO. The area of the plasma facing ECRH-launcher front end can be minimised

and movable parts and steering mechanisms are avoided in the hostile environment of a burning plasma. The remotesteering properties are based on multi-mode interference in a square waveguide leading to imaging effects: For a proper length of the waveguide, a microwave beam at the input of the waveguide (with a defined direction set by a mirror system outside of the plasma vacuum) will exit the waveguide (near the plasma) under the same angle as seen from the principle sketch in figure 17. For W7-X, the vacuum window, a vacuum valve as well as a mitre bend must be incorporated into the 4.6 m long waveguide. For the RSlaunchers a conceptual design as shown in figure 17 was developed, which is specified for 1 MW, cw, low-loss rftransmission. The waveguide has corrugated walls and will be fabricated by an electroforming process, thereby integrating the water-cooling channels. In support of the mechanical design, calculations of fields and wall currents at various locations were carried out to estimate the cooling requirements. Also the effect of a bending of the waveguide due to movement of the vacuum vessel and gravitational sag was investigated and found to be uncritical.

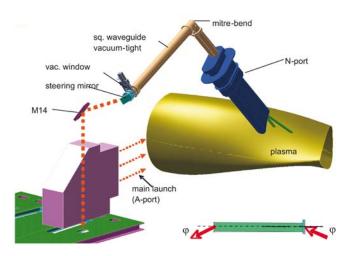


Figure 17: Conceptual design of the remote steering launcher for the Module 5 N-port. The insert at the bottom, right, shows a principle sketch of the remote steering launcher.

To enlarge the steering range, the investigation of small deformations for the basically square corrugated waveguide were continued to find an optimised cross-section. The finite-difference code IPF-FD3D has been adapted to this problem by reducing it to finding the resonance frequency of purely perpendicular modes in the waveguide cross section. This transforms it to a 2D problem, which can be solved with the available computing resources. A number of techniques have been implemented to excite the desired modes in the resonator and find their resonance frequency. As a first result, previous work by a different group was reproduced for an ITER remote steering waveguide, and an

improved (but not yet optimal) waveguide shape was found for W7-X. The results cannot simply be scaled from ITER to W7-X, because the ratio of wavelength to waveguide size, which is relevant here, is different for the two cases. The work will be continued and a suitably deformed waveguide will be built and tested at low power. Furthermore, non-rectangular shapes that ease manufacturing, like rounded instead of sharp corners, will be explored. Preferably the vacuum valve will be shifted from the waveguide entrance towards the mitre bend to increase the angular steering range. Calculations of the losses in the gap needed for installation of the vacuum valve were therefore continued, taking optimised waveguide shapes into account. In conjunction with the optimised waveguide cross-section, a significant reduction of the gap losses especially for larger scanning angles is expected. Low-power experimental investigations on a prototype waveguide have been started at IPF Stuttgart to benchmark the calculations.

9.1.4 In-vessel Beam Control and ECA (IPP, IPF)

Four front steering ECRH-antennas in the outboard midplane A- and E-type ports are designed to comply with the different operation scenarios such as plasma start-up, O- and X- mode heating and current drive at 103.6 and 140 GHz. During plasma density ramp-up beyond the X2 cut-off density, a well-controlled transition from the strongly absorbed X2-mode to a multi-pass second harmonic ordinary mode (O2) heating scenario is required. The single pass absorption for O2 is expected to be between 60 and 80% in that case. Therefore the beams must hit specially designed reflector tiles, which are integrated in the heat shield opposite to the ECRH antennas and a reflector liner in between the A- and E-type Ports in two W7-X moduls. The reflecting stainless steel liner will be polished for higher microwave reflection.

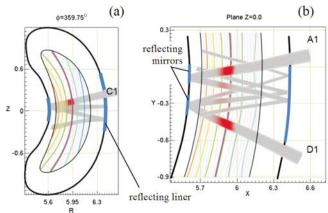


Figure 18: Ray trajectories for multi-pass O2 heating with different ECRH-Beams for the poloidal (a) and toroidal (b) cross section. Three controlled passes can be implemented by reflector tiles at the high field side and a reflector liner at the low field side between the A- and E-type ECRH ports.

Some ray trajectories for the multi-pass heating scheme are shown in figure 18. These sophisticated 10 MW ECRH-scenarios can only operate safely, if the ECRH-launchers are absolutely reliable and precisely controlled. To avoid any possible damage, a set of ECRH-protective diagnostics is being prepared to detect any peculiarity credibly.

The non-absorbed power as well as the beam position and its polarisation at the ECRH heat shield will be measured by an array of altogether 126 small pick-up antennas. This electron cyclotron absorption (ECA) diagnostic consists of circular mono-mode waveguides, which are integrated in the graphite tiles of the heat shield structure. A prototype bundle was successfully test assembled into the heat shield tiles in the W7-X vessel as shown in figure 19. The in-vessel waveguide bundle will be connected with a bundle, which is fed through the B-Port. The four B-Port plug-ins and the vacuum interfaces have been assembled completely and are currently leak-tested.



Figure 19: Test assembly of the copper waveguide bundle for the multichannel ECA-diagnostics in the W7-X vacuum vessel.

The ECA probes allow monitoring the correct adjustment of the launch angle. The motor drives for the front steering mirrors have been installed and tested. The control back-end and the end-point switches of the motor drives have been put into operation and were used for cyclic tests of the launcher unit within the allowable range. The integration of the launcher control into the central ECRH control is under way. The front steering antennas showed some weakness in the driving mechanism during cyclic fatigue tests and were sent back to TID-DGT (former BTI) at the KIT for enforcement. The first of them was refurbished by end of 2010 and went though intensive mechanical tests successfully. No problems with the bearings were found any more. The launcher was laser tracked and its new dimensions provide the specified clearance of 12 mm on each side with respect to its dedicated port. Finally it passed the vacuum leak test and is presently being mothballed until W7-X assembly completion. The remaining three Launchers will be finished step by step in the next months.

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9.2. Neutral Beam Injection

The NBI system under construction for Wendelstein 7-X consists of two injectors, positioned close to each other on Module 2. In a first phase of W7-X operation each injector box will be equipped with two beam sources providing a total heating power of up to 7 MW in hydrogen and 10 MW in deuterium, respectively. In a later stage two additional ion sources per injector are planned to double the heating power. The NBI project is supposed to be realised in close co-operation with partners from Polish research institutes. One partner, IPJ Swierk, has got approval and funding from the Polish government at the end of this year to build and provide NBI components like cooling systems, ion deflection magnets, torus valves and injector support structures. The project will be started very soon in the next year and will run over more than 3 years. The second partner, WTP Wroclaw, interested in delivering the cryo-sorption pumps and cryo supply has not yet reached such an advanced state and will submit their proposal for approval by the Polish government in the next year. Discussions have been started meanwhile about alternative fast pumping systems (like cryo-condensation pumps or titanium evaporators) in case this proposal is not being

accepted or not compatible with the required schedule. The procurement of various other components have proceeded as planned during the past year. The assembly of the first ion source flange is being completed, i.e. neutralisers and ion dumps are mounted on its inner side, source valves and beam steering units on its outer side. Figure 20 shows this ion source flange assembled on box 21 with mounted source valves and beam steering units. In addition, the procurement of the calorimeter components is almost finished and the assembly is under way. Design work on the torus adapter unit, consisting of a box exit scraper, assembly bellows and duct protection elements is proceeding. The design of the pipe work and water manifolds for the low pressure cooling cycle is completed, the instrumentation is in house and the manufacturing has been agreed to be done within the W7-X Assembly group in the next year. The magnetic shielding concept to reduce the stellerator stray magnetic field inside the injectors down to an acceptable value has been optimised with respect to minimizing the magnetic material mass. The detail design work on this component is close to completion. Progress has been made in the manufacturing of RF and high voltage cages, which are the first parts of the NBI systems to be installed inside the torus hall as soon as the corresponding space there is not required anymore for machine assembly.



Figure 20: NBI 21 with assembled ion source flange showing source valves and beam steering units on the upper two source positions and a temporary vacuum system on one of the lower source ports.

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WEGA, VINETA and Further Activities

WEGA

Head: Dr. Matthias Otte

Utilizing a 2D Langmuir probe array turbulence studies in the vicinity of magnetic islands were studied. At minor radii smaller than the island location long range correlations of floating potential fluctuations at about 5 kHz both in toroidal and poloidal direction were found. This correlation

appears to be interrupted by the island separatrix. A comparative study at magnetic configurations without major resonances has shown that the potential fluctuations have a toroidal m=0, and poloidal n=0 mode structure. The magnetic topology was again investigated by flux surface measurements. In general a good agreement with former results was found. Beside an already known m=1 error field component a m=4 component could be detected resulting into magnetic islands. Furthermore, the distortion of the stray field of the transformer coils on the magnetic structure could be qualitatively determined. For the flux surface diagnostic of W7-X a prototype electron gun with a LaB₆ based electron emitter was successfully tested up to 3.5 T. A highly sensitive magnetic diagnostic including Rogowski-coils, diamagnetic loops as well as compensation coils allowed the detection of a plasma energy of below 1 J and a current of about 5 A during electron Bernstein wave (EBW) heated plasma scenarios at 0.5 T operation. Furthermore, a current of up to 1.2 kA could be measured during lower hybrid (LH) heating scenarios. The characterisation of soft X-ray emission originated by a fast electron component during EBW as well as LH plasma heating experiments was tested with a new silicon drift detector provided by the Garching group "Astrophysics and Laboratory-Plasma-Studies". Perturbative heat transport experiments have been carried out by ECRH power modulation and monitored by a 16-channel fast bolometer (Si-diode array). Furthermore, the electron thermal diffusivity and the two dimensional plasma radiation have been investigated with the bolometer. For EBW emission experiments an optimised steerable quasi-optic antenna system and a corrugated broad band horn antenna were developed. In cooperation with IPP Garching and IPF Stuttgart a new microwave notch filter was developed to suppress the ECRH gyrotron frequency of 28 GHz at minimum damping of other frequencies.

During 2010 the experiment control was switched over to the prototype of the W7-X control system. More sophisticated plasma experiments and event detection have been performed.

International Stellarator/Heliotron Database

The Stellarator/Heliotron database has been maintained within an international collaboration (NIFS, CIEMAT, U-Kyoto, ANU, PPPL, U-Wisconsin, U-Auburn, U-Charkov, U-Stuttgart, and

On WEGA experiments were focused on turbulence studies in the vicinity of magnetic islands, magnetic flux surface measurements and electron Bernstein wave heating. The international Stellarator/Heliotron database and the assessment of ELM control by resonant magnetic perturbations have been continued. The research focus in VINETA has been the kinetic wave damping, turbulent fluctuations, and the plasma profiles in magnetic field inhomogeneities.

IPP). First comparative studies of H-mode (LHD, TJ-II, Heliotron-J, W7-AS) discharges in 3D-devices revealed robust similarities (profile gradients and radial electric field) but also indicate configuration dependencies (e.g. influence of shear and edge iota). First comparative studies of edge fluctuations have been performed also involving tokamak devices (TJ-K, AUG, MAST, URAGAN

3M, HSX, WEGA, W7-AS). The studies were to assess similarities and scaling in fluctuation spectra with regard to blob transport. Discharge documentations for the validation of neoclassical transport models have been started (W7-AS, LHD, TJ-II).

ELM Control by Resonant Magnetic Perturbations (RMP)

The effect of 3D edge perturbation (RMP) of tokamak magnetic fields has been refined and documented by time resolved infrared imaging (collaboration with GA, San Diego). The beneficial effect of RMPs is due to a significant reduction of power load densities for small ELMs (see figure 1) or elimination of larger ELMs. A similar result was found at the JET tokamak (separate collaboration with EFDA-JET). Moreover, the wetted area increases linearly with deposited power in type-I ELMs without RMPs. This finding partly mitigates concerns for the lifetime of the divertor of ITER.

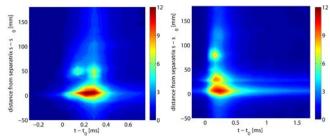


Figure 1: Power loads due to type-I ELMs (in MW m^{-2}) to DIII-D divertor.

Study of Heat Flux Pattern in Different Beta Discharges

An infrared imaging diagnostic was set up in collaboration with NIFS at LHD. Experiments focused on the time evolution of 2D temperature measurements during comparable discharges at different plasma beta. First results indicate structural changes of observed patterns that could be linked to an altering magnetic edge topology due to the nonlinear interaction with plasma currents.

Scientific Staff

H. Ahrens, E. Chlechowitz, A. Dinklage, P. Drewelow, M. Glaubitz, M. Jakubowski, A. Kus, H. P. Laqua, S. Marsen, E. Müller, M. Otte, R. Reimer, A. Rodatos, T. Stange, F. Wagner, R. Wolf, D. Zhang.

VINETA

Head: Prof. Dr. Olaf Grulke

Wave Dynamics and Turbulent Fluctuations

Electromagnetic wave propagation, particularly for whistler and Alfvén waves, has been a focus of the research at VINETA for several years. The waves have been identified in terms of their respective dispersion relation and its dependency on plasma parameter variation. In high density helicon plasmas those waves are generally dominated by collisional damping. By specific shaping of the plasma profiles kinetic damping, i.e. electron cyclotron and Landau damping, has been studied. For whistler waves excellent agreement has been obtained between the measurements of the critical frequency, at which cyclotron damping represents the dominant damping mechanisms, and linear Vlasov dispersion calculations for a wide range of plasma-β, shown in figure 2.

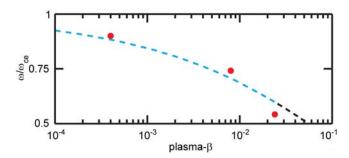


Figure 2: Comparison of measurements of the critical frequency for cyclotron damping of whistler waves (circles) with Vlasov calculation (dashed line).

The observation of a rather complicated whistler wave propagation pattern could be shown to be mainly caused by the wave excitation geometry and the radial plasma density profile, which leads to ducting of the wave energy. Those observations are in good agreement with full wave code calculation specifically tailored to the experimental situations, which were performed in collaboration with the University of Stuttgart. Landau and cyclotron damping of Alfvén waves is observed in axial magnetic field gradients, which cause also axial gradients of the plasma pressure. As for whistler waves the results are in agreement with linear dispersion calculations.

The work on fluctuations and structure propagation in drift wave turbulence has been continued. The experimental results have been compared to fully nonlinear three-dimensional fluid simulation, which are performed in collaboration with the Technical University of Denmark, Risø. In addition to previous results about the radial propagation of turbulent structures, the spatial region of formation of those structures has been shown to correlate with a strong increase of the Reynolds stress in experiment and simulation, suggesting a shear-layer drive of the structure formation.

Plasma Profiles in Magnetic X-point Configuration

In preparation to investigations in dynamically driven magnetic X-points the evolution of the profiles in rf heated plasmas in a static azimuthally symmetric X-point configuration was studied. In contrast to independent investigations, in which an increased plasma pressure was observed at the X-point and interpreted as either stochastic heating due to ergodisation of particle orbits or increased dissipation of helicon wave energy, the electron temperature is observed to remain flat. However, a local peaking of the plasma density close to the X-point region is observed and could be explained by particle trapping in the strongly inhomogeneous magnetic field. Calculation of the electron density for a capacitive discharge with a hollow radial density source profile due to particle trajectories in the inhomogeneous magnetic field configuration is shown in figure 3.

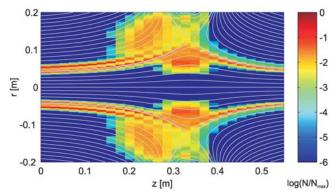


Figure 3: Calculated plasma density in a radial-axial plane for a hollow density source profile (at z=0) and an azimuthally symmetric magnetic X-point configuration. The magnetic field lines are superimposed in light gray.

The investigation will be extended from the static to a dynamic investigation during magnetic reconnection. The VINETA setup is currently changed by adding one additional large magnetised vacuum module, which will be used for the reconnection studies. Magnetic reconnection is planned to be driven by a pair of axial conductors carrying a large fluctuating current, which drive reconnection at the X-point in the plasma center. The focus of the studies will be the plasma dynamics and particle kinetics in response to the topological rearrangement of the magnetic field in the presence of boundaries. Finalisation of the setup and diagnostic equipment is envisaged for mid 2011.

Scientific Staff

H. Bohlin, C. Brandt, F. Braunmüller, J. Brunner, O. Grulke, T. Klinger, D. Niemczyk, K. Rahbrania, C. Rapson, T. Schröder, A. Stark, A. von Stechow, T. Windisch, M. Wisotzky.

Part of the VINETA program was carried out under the auspices of an EFDA Fusion Researcher Fellowship.

ITER

ITER Cooperation Project Head: Dr. Hans Meister

Introduction

2010 brought major changes to the ITER Project. After controversial discussions, the ITER baseline was accepted in July. In parallel, Osamu Motojima was appointed new director general and proposed a new organisational structure to accompany activities aimed at preventing any further cost increases.

The IPP contributes to the ITER Project in a wide range of activities. Tasks range from R&D for heating systems and diagnostics to development of integrated plasma scenarios. In addition, the IPP is playing a leading role in contributing to the ITER physics definition and objectives via contributions to the International Tokamak Physics Activity and by participating in the various Task Forces and Topical Groups of the EFDA Workprogramme.

of the ITER neutral beam system. Most of the components are ordered and in manufacturing; some (source flange, source valve, HV insulator) have been delivered. The assembly is proceeding; a big step was the final assembly of the neutron shield (figure 1). The integrated commissioning with the first pulses is still expected in fall 2011.

Remmelt Haange was appointed as his deputy and head of the new ITER Project department in November. Fusion for Energy (F4E), the European Domestic Agency, started a restructuring process, too, in order to increase effectiveness and to adapt to the requirements of the ITER baseline. The new budget for ITER has been accepted by the European Commission. However, the European contribution was capped to 6.6 B€ and adoption by the Parliament is still pending. Nonetheless, until end of 2010 procurement contracts worth about 60 % of the European budget have been placed. One visible effect is that construction on the ITER site continued and the first concrete columns rise out of the ground.

The ITER cooperation project at IPP continues its activities along the major topics: The test facility ELISE, a major step on the way to the ITER neutral beam injection system, is being built, R&D on the bolometer diagnostic for ITER continues as does the work on the design of the ITER ICH antenna within the CYCLE consortium. A major R&D task on fast switches for high power microwaves could be finished successfully and on time.

Additionally, IPP is contributing to various heating systems, diagnostics and in particular the preparation of the physics basis through some direct contracts with ITER or F4E and a number of tasks within the EFDA Workprogramme.

Heating Systems

Development of RF Driven Negative Hydrogen Ion Sources for ITER

The development of the IPP RF source – being since 2007 the ITER reference source – was ongoing in 2010 with the construction of the new ELISE test facility, the continuation of long pulse experiments at MANITU, basic experiments regarding the magnetic filter field and the influence of the source temperature at BATMAN and with ITER relevant RF experiments at RADI.

ELISE, being supported by a 4 M€ F4E service contract, is an important intermediate step between the small IPP prototype sources and the large ITER source. Therefore ELISE is now an integral part of the F4E and ITER roadmap for the development



Figure 1: View into the L7 experimental hall with the concrete neutron shield assembly for ELISE.

The early operation of ELISE is important for the success of the neutral beam injector test plant (PRIMA) in Padova, Italy, consisting of two test facilities: a full power, 1 MV test facility (MITICA, planned to be operating end of 2016) and a low power, 100 kV ion source test facility (SPIDER, operating end of 2013) as input for the design of the MITICA ion source, which is planned to be frozen in 2013, is essential. Furthermore, IPP continued to contribute to PRIMA in the design of the full size RF source, the RF circuit and the layout of source and beam diagnostics, also by training of PRIMA personnel at the present IPP test facilities. An example is a dedicated material test (thermal parameters, stress) of electrodeposited copper that has been performed in collaboration with RFX Padova. The results of this test went already into the design of the extraction grids of ELISE and PRIMA. Although long pulses (several 100 seconds) with 80 kW power are now possible at the test facility MANITU, the ITER requirements have not been met yet. The reason is still the increasing electron current during a long pulse. Hence, RF power and extraction voltage are limited in order to

avoid damage of the extraction grid. This limitation is even

more pronounced in deuterium operation due to the much

larger ratio of co-extracted electrons. Nevertheless, stable deuterium pulses of some hundreds of seconds with an extracted ion current density of 10-15 mA/cm² and a co-extracted electron fraction of less than one have been achieved. The homogeneity of the beam – expressed by the beam divergence profile measured by Doppler-shift spectroscopy does not seem to correlate with the homogeneity of the plasma in front of the plasma grid. That can be explained by the fact that most of the negative hydrogen ions are created at the plasma grid by the conversion of neutrals; the neutral flux, however, onto the plasma grid is not influenced by the filter field and hence homogeneous in the IPP RF driven source. The experiments at the BATMAN test facility continued on studies of the effects of the magnetic field structure on the source performance, both in hydrogen and deuterium. Two clear correlations of the source performance with magnetic field parameters have been found (figure 2), which are consistent with the present understanding of the processes in the ion source. For ion extraction, the magnetic field strength in front of the plasma grid is the important parameter; a field of some mT in front of the plasma grid for sufficient negative ion extraction is needed, whereas the amount of co-extracted electrons is determined by the integral BdL from the driver to the plasma grid. First experiments in deuterium show similar trends as in hydrogen, the magnetic field at the plasma grid for optimum ion extraction yield and the required integral BdL for sufficient electron suppression, however, are larger than in hydrogen. In order to remove the necessity of an additional heating circuit at 1 MV potential of the ITER neutral beam system, experiments with a reduced source body temperature of 35 °C have been performed and showed no influence of the source performance and the speed of conditioning compared to operation at the standard value of 50 °C.

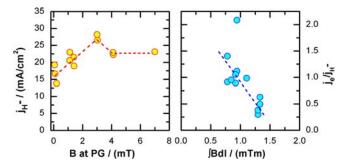


Figure 2: Left: Dependence of the extracted hydrogen current density on the magnetic filter field at the plasma grid; right: dependence of the amount of co-extracted electrons on the integral magnetic field.

The experiments at RADI, equipped with a large scale RF driven ion source, concentrated on stable RF operation of an ITER relevant RF circuit and tests of design choices (e.g. magnetic field configuration) of ELISE and SPIDER.

The experiments are strongly supported by modelling of the processes in the boundary layer near the plasma grid where the negative ions are generated as well as of the distribution of Cesium during and between the plasma pulses, also by basic experiments regarding Cs chemistry, Cs diagnostics and RF efficiency at the University of Augsburg (see chapter 13). The PIC code BACON was applied to investigate the transport of electrons through the magnetic field and the cooling of the electrons correlated to this transport. For the plasma parameters of the IPP ion sources and a small computational domain the electron cooling was reproduced.

ICRF Antenna Consortium and Design

The CYCLE consortium is progressing well with the design of the ICRF antenna for ITER. In May, a conceptual design review of the ICRF antenna was held in Cadarache. At the end of the year, CYCLE submitted a proposal to an extension of the scope: all tasks are now planned through to the completion of the relevant presentation to the preliminary design review. The duration of the task would be extended from 18 to 24 month. IPP is particularly involved in the mechanical design of the antenna. This design is being developed during four design cycles to provide a design by the Preliminary Design Review that best meets the requirements of the technical specifications. In particular, a CATIA model of the launcher for the integrated antenna showing the sum of all the subsystems and of the component parts will be provided, consistent with the preliminary calculations and computer models.

ECRH Upper Launcher

In recent years, IPP has coordinated the physics analysis of the ITER ECRH Upper Launcher. Hence, IPP is part of the recently formed consortium between KIT, ITER-NL, FOM, CNR and CRPP that aims at designing this system under an F4E Grant.

Fast Switches and Diplexers for High Power Microwave Beams

High power diplexers can strongly increase the performance and flexibility of large ECRH systems, and are therefore of potential interest for ITER. To this aim, the research on diplexers for combination of high-power microwave beams and/or switching ("FADIS") on a fast timescale with low loss and without mechanically moving parts, was conducted under the umbrella of the 'Virtual Institute' of the 'Helmholtz-Gemeinschaft deutscher Forschungszentren' (IPP Garching and Greifswald, IAP N.-Novgorod, IPF Stuttgart, KIT Karlsruhe, and IFP Milano) and terminated on schedule by end of 2010.

A major activity were the high-power tests of the compact long-pulse diplexer "Mk II" in the ECRH system of W7-X. It is based on a ring resonator consisting of four mirrors (figure 3). Coupling to the inputs and outputs is performed by grating beam splitters on two of the resonator mirrors, as well as via matching mirrors and TEM00-HE11 mode converters. This quasi-optical device is compatible with waveguide transmission systems. For the tests, the beams from one or two W7-X gyrotrons was coupled to the input(s), the transmitted power at the two outputs was measured by directional couplers, and finally was dumped into two cw calorimetric loads.

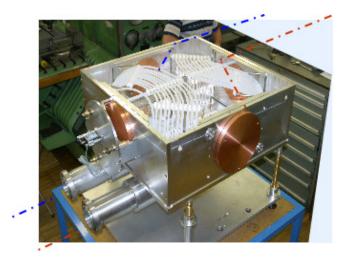


Figure 3: Photograph of the diplexer, which has been investigated using the high power ECRH system for W7-X. At the bottom, one can see the two HE11-waveguide outputs. The top plate with the two symmetrical inputs is removed to reveal the resonator geometry and the stray radiation absorbing hoses.

A fast drive for the resonator mirror (developed by TNO in Delft) controlled by the output power signals and an optional real-time frequency measurement allowed tracking of the slope or the peak of the diplexer resonance to the gyrotron frequency on a 20 ms time scale. Several diplexer applications were demonstrated with this arrangement: Slow switching (20 ms timescale) of the power between two output channels (without the need to turn off the gyrotron as is the case for conventional switches) was performed by controlled mirror movement. Fast switching (100 ms timescale) by frequency-shift keying of the gyrotron (using few kV voltage modulation of the body) was performed with optimum contrast.

For the application of resonant diplexers in in-line ECE experiments, where the high-power ECRH gyrotron and the low power ECE signal share a common launcher, tracking of the notch of the diplexer to the gyrotron was demonstrated. This is a necessary prerequisite to guarantee high suppression of possible stray radiation from the gyrotron into the delicate ECE receiver.

The combination of the power from two (or more) gyrotrons may be particularly interesting for large scale ECRH systems, because transmission lines and port space can be saved. When feeding two gyrotrons to the diplexer, stable power combination with an output contrast of 90 % could be achieved. Encouraged by the good high power performance of the diplexer under test, an HE11-resonator diplexer with a new mirror configuration for direct integration into corrugated waveguide was developed and investigated in detail.

The matching and the resonator mirrors are designed as phase-reversing elements for the fields radiated from the HE11 input waveguides; thus, a perfect image of the input field is obtained on the coupling gratings as well as at the output waveguide. The design is very compact without enhancing the power load on the mirrors, and therefore well suited for integration into large ECRH systems. Owing to the compact design and high mechanical precision, the measured transmission efficiencies were very close to the theoretical limit.

In the non-resonant channel, a transmission efficiency of >99.2 % was reached; the internal resonator round-trip efficiency was 99.1 %. Efficient mode filtering based on the difference in resonance frequencies of higher-order modes was demonstrated. The directivity was typically 60 dB, qualifying it as directional coupler for in-line ECE experiments, where the ECRH launcher is used simultaneously for electron cyclotron emission measurements. This 140-GHz diplexer was designed for integration into the ASDEX Upgrade ECRH system. However, it can be easily scaled to 170 GHz and a waveguide diameter of 63.5 mm. Based on this design, a preliminary proposal and cost estimate on the development of a water-cooled and evacuated version for ITER ECRH has been performed.

EFDA Tasks

The work on arc detection focussed on the development of an interface between the GUIDAR detector from POLITO and the ICRF transmission line and on the analysis of the frequencies emitted by an arc. The transient behaviour of an arc and its interaction with the ICRF system was analysed using a numerical model. A first draft of the architecture of an arc detection system for ITER was conceived, which took into account the particularities of the operations.

IPP participated in a multi-machine (TEXTOR, Tore Supra, AUG, JET) experiment on wall conditioning with ICRF. The work on AUG concentrated on the simulation of the ICWC scenario at ITER half-field and ICWC discharge optimisation. The results are presented in chapter 1.

Studies showed that local gas injection can substantially increase the ICRF antenna coupling without arcing in the antennas. The distance of the gas inlet valve relative to the ICRF antenna should be kept to minimum to increase the positive effect of gas injection.

Current ramp-up (\sim 1.4 MA/s) assisted by ICRF was achieved only with on-axis $\omega = \omega_{cH}@r/a = -0.1$ (f=36.5 MHz) and Voltsecond consumption similar to $2\omega_{ce}$ -assistance.

The use of (ECRF+ICRF)-assistance for plasma initiation reduced the volt-second consumption by $\sim\!10$ %. With off-axis ICRF, dI_p/dt degrades due to impurity rise ($P_{ECRF}\!=\!560\text{-}800~kW\text{+}P_{ICRF}\!=\!100\text{-}540~kW$).

The ECRH-sniffer-probes, which have been installed with EFDA-support were used to characterise the stray-radiation. With respect to their suitability for polarisation control it was found that five percent of the power in the wrong polarisation is the detection limit for X2 heating.

Diagnostics

ITER Bolometer Diagnostic

With many years of experience in the development of bolometer detectors IPP proposes to take the lead in a consortium with the Hungarian Association (RMKI) and the Karlsruhe Institute of Technology (KIT) for the full development of the ITER bolometer diagnostic. To this aim a consortium has been set up and the respective contract signed at the beginning of 2010 by all partners. However, the official call for tender by F4E on this topic is still pending. In order to continue the R&D activities started previously in the framework of tasks of the EFDA Technology Workprogramme IPP successfully applied for national funding. 5.7 M€ have been awarded for the period 10/2008 − 03/2012 for detector development, building and testing of prototypes and the development of the diagnostic integration in ITER.

In 2010, results have been achieved in several areas of investigation. The cooperation with IMM (Institut für Mikrotechnik Mainz GmbH) on the development of bolometer foils is being continued. A first batch of samples with a 4.5 µm thick absorber produced by galvanic deposition of Pt onto a thin SiN membrane with Pt meanders on the backside was characterised in the newly set up high-temperature vacuum test rig at IPP. All parameters relevant for operating the bolometers, resistance R of the meanders, cooling time constant τ and heat capacity κ of the absorber, show a very good linear dependence on the temperature up to values of above 200 °C (figure 4). However, from about 300 °C onwards a drift in R can be observed, which differs for each individual detector channel and is still under investigation. The laser trimming of the meanders achieved accuracies in the resistances within one detector channel of 0.8 %. Further optimisation of the trimming parameters will reduce this value. The cooling time constant $\boldsymbol{\tau}$ of the first samples was in the order of 420 ms. In order to enhance the response time and to achieve τ-values closer to the ones of the detectors currently in use, an additional heat conduction layer was deposited on the absorber side. The subsequent samples featured τ~220 ms. Finally, at the end of 2010 IMM managed to successfully produce a detector featuring a 12 µm thick Pt absorber. This is the minimum thickness deemed to be

required for the application in ITER. These samples now await their characterisation with respect to temperature dependence, mechanical and irradiation stability.

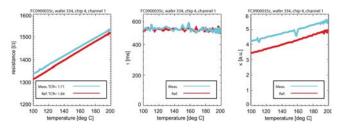


Figure 4: Meander resistance (left), cooling time constant τ (middle) and normalised heat capacity κ (right) for measurement (blue) and reference (red) absorber as functions of temperature for a prototype bolometer detector.

During the last year the design of the diagnostic components matured and several prototypes for collimator, mini-camera housing and electrical connectors have been manufactured and tested. For investigating the feasibility of manufacturing collimators with high-precision geometric constraints and to demonstrate a method for in-situ calibration of their geometric function, a light-weight robot has been brought into operation. It is used to illuminate the entrance slits of the collimator from many vertical and horizontal angles using a laser. By simultaneously measuring the response of the bolometer detector the transmission function of the collimator can be determined.

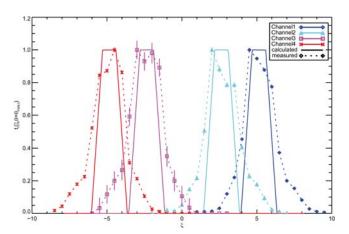


Figure 5: Measured (symbols with dashed lines) and calculated normalised transmission functions of the ITER prototype collimator in the poloidal plane given for each channel at perpendicular incidence.

First measurements (figure 5) proved the viability of this method and demonstrated that the current design of the collimator can be manufactured to the required accuracy of 0.1°, which is also the detection limit of the lab assembly. However, it was also demonstrated that the collimator prototypes suffer severely from stray light, as can be seen in figure 2 by the large deviation of the measured normalised

transmission from the theoretically expected one. Thus, the design of the collimators was changed and additionally, the next prototypes will feature viewing channels coated with Al₂O₃/TiO₂. This rough, dark gray ceramic can be deposited using plasma spraying. It was initially developed for W7-X and is an efficient absorber of microwaves. A cooperation with the IFKB at the University of Stuttgart has been started to provide the coating for the bolometer collimators.

In cooperation with IPF Stuttgart it could be demonstrated that the top plate designed for the collimators is able to reduce any incoming microwave radiation in the frequency range of 125-220 GHz by at least 70 dB. The complete assembly – collimators, mini-camera housing and connectors – will be tested with respect to their ability to screen the detector from microwaves in the test facility MISTRAL in Greifswald at the beginning of 2011.

Last but not least the finite element analysis of diagnostic components gave useful results. It could be shown that for the current design, if using TZM as main material, maximum temperatures of $\sim\!\!280~^\circ\text{C}$ can be expected at the top of the collimator and that the detectors will remain at $\sim\!\!200~^\circ\text{C}$ with temperature variations below 0.5 $^\circ\text{C}$ across the detector chip. The latter is important to prevent temperature drifts in the measurements. Also, the parameters in the simulations having the highest impact on the results have been identified. The simulations will continue by investigating design variants and the impact of electromagnetic forces during disruptions as well as by prototype tests to validate the simulations.

EFDA Tasks

Plasma diagnostics for present and next generation fusion devices are reviewed with respect to conventional and advanced data analysis and error evaluation techniques. Emphasis was put on forward modelling and synthetic diagnostics capabilities in a probabilistic framework necessary for an Integrated Data Analysis approach.

A development work-flow for synthetic diagnostics has been implemented aiming to support a physical design and optimisation of future instruments or to simulate measuring capabilities. The implementation of a pilot diagnostic (spectral MSE) focused on diagnostic forward models to simulate data. A concept for the validation of the synthetic diagnostic has been developed and tested with experimental data from AUG. The potential of GPUs (graphical processing unit) for real-time analysis and the analysis of large amounts of data was explored for the solution of partial differential equations. For large problem sizes the GPU based solutions showed a better performance. The installation of the necessary diagnostic and computing hardware for the real-time integration of the plasma position reflectometry has been completed. Diagnostic probe signals are collected in a fast FPGA and transferred to a host computer connected to the AUG control system. Separatrix position identification algorithms are being designed.

The visible video diagnostic was upgraded to a video realtime system for machine protection by implementing a fast algorithm for the recognition of hot spots and making use of fast frame grabber cards for video digitalisation and integrating both into the AUG discharge control system.

Additionally, EFDA supported diagnostic hardware upgrades at AUG for some diagnostics. Enhanced time and/or spatial resolution will be used to provide essential data for the analysis of various plasma scenarios in view of ITER to study e.g. fluctuations, disruptions and transport.

ITER Support

Contracts with F4E and ITER

IPP conducts several tasks, which are financially supported by contracts with either ITER or F4E. The results and activities of the most prominent among those have been presented in previous sections of this chapter (NNBI and ITER ICH antenna design). Additionally, the following activities were active in 2010.

In order to assess the tritium removal as currently suggested for ITER (wall baking at 240 °C for the main chamber, and 350 °C for the divertor), D retention and release behaviour of Be-containing materials were investigated in a contract with F4E. Pure Be, as well as Be/W/C intermixed and Be₁₂W and Be₂C compound layers were fabricated in collaboration with MEdC, Budapest. In pure Be, D is predominantly released around 150-200 °C within a relatively sharp desorption peak. The efficiency of tritium removal is reduced for compounds and intermixed Be-W/Be-C layers. At 350 °C Be-W mixtures release still around 80 % of the retained hydrogen. However, in the case of Be-C deposition with C concentrations above 50 % only 10 % of the retained D is released at 350 °C. In consequence, best performance of the wall baking can be expected for tritium removal from high purity Be layers deposited on the main chamber wall under the assumption that the temperature of main chamber wall surface remains below ~160 °C. Under these conditions out-gassing temperatures of 240 °C may be sufficient. Two Grants by F4E have been awarded in mid-2010. One aims at the determination of the three-dimensional distribution of power and particle fluxes during ELM control schemes using in-vessel coils. Another shall investigate the viability of a capacitive diaphragm monitor prototype for the quantitative measurement of dust inside a tokamak.

Physics Integration

Most of the experimental programme of ASDEX Upgrade is oriented towards the investigation of plasma scenarios required for the operation of ITER. These results are presented in chapter 1. In this section, the results of some specific investigations are presented, which are conducted within the framework of the EFDA Workprogramme.

Simulations of AUG VDEs and centred disruptions have been performed with the MHD-transport code DINA. This code relies on a 2D self-consistent model (from the electromagnetic point of view) of the plasma and surrounding conductors and can predict the evolution of the halo current if the halo region properties (width and temperature) are given.

For the measurement of electromagnetic forces an optical strain measurement system for internal components of ASDEX Upgrade has been installed by laser welding on the PSL. Its 38 sensors routinely collect data since the restart of the campaign.

The development of the edge kinetic profiles after an LH transition was studied and a dependence on the neutral gas inventory was found. In type-I ELMy H-modes the pedestal widths showed a weak correlation with poloidal beta when analysed in real space.

With the upgrade of the installed ECRH power (see chapter 1), the effect of the heating mix (NBI vs. ECRH) on transport will be analysed in the frame work of a PhD work in the 2011 campaign.

The optics of the core CXRS system were redesigned to increase the throughput of light and the number of lines of sight imaging the plasma. These upgrades significantly improve both the temporal and radial resolution of rotation measurements on AUG.

PWI Task Force

The prediction of erosion and co-deposition processes for ITER is necessary for the design and material choice for the first wall. In particular the formation of co-deposited layers determines the T retention during the nuclear phase. A novel global erosion/deposition model was developed, allowing to calculate the time and poloidal position resolved surface compositions and impurity influxes into the plasma in a self consistent way. From this information the growth rate of Be/C/W mixed layers can be calculated. Using the local plasma parameters to estimate particle energies and surface temperatures the scaling laws from PISCES, San Diego, are used to predict the fuel retention.

Trainee Programmes

The very successful ENTICE programme is winding down. Eight trainees were trained, out of the 8, 6 have initially found a position in the fusion programme at different fusion associations or at ITER, some of them permanent. One of those has moved to a position outside of fusion.

The ICRF group is also participating in the LITE programme, and numerous trainees from the LITE programme have spent part of their traineeship in the ICRF group. The NIPEE (Negative Ion Physics and Engineering Expertise) programme has started in the last year; it includes one trainee employed by IPP and another five employed by RFX Padua and KIT Karlsruhe.

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Plasma-wall-interactions and Materials

Plasma-facing Materials and Components

Head: Dr. Joachim Roth

Surface Processes on Plasma-Exposed Materials

Chemical Phase Formation of Beryllium with Tungsten and Oxygen

Interaction of the plasma with first wall materials will lead to formation of mixed materials due to erosion, transport and redeposition. In this study the chemistry of the beryllium-tungsten alloy

Be₂W is investigated under the influence of energetic oxygen ions by depth-resolved X-ray photoelectron spectroscopy (XPS) at the synchrotron radiation facility HZB-BESSY II. The sample is prepared in-situ in our preparation chamber 'LAICA', which is directly connected to the analysis chamber 'SurICat'. A layered system is prepared by physical vapour deposition of approx. 4 nm tungsten on a beryllium substrate. By heating to 900 K for 60 min the alloy Be₂W is formed. The oxygen implantation energies are chosen such that the implantation profile is within the accessible information depths of XPS at the selectable photon energies from the synchrotron. According to simulations with SDTrim.SP implantation energies of 500 and 1000 eV satisfy the experimental requirements for oxygen fluences of 5×10¹⁴ cm⁻². Between the individual implantation steps the sample is annealed to 600 K. Photoelectron spectra are taken at up to six different information depths for each involved element. This is achieved by varying the X-ray excitation energy, resulting in estimated information depths of 1.2, 1.8, 2.4, 2.9, 3.5 and 4.5 nm. In addition, survey scans are performed at two different photon energies for quantitative compositional analysis. After implantation of energetic O ions the formation of ternary compounds of Be, W and O is observed and investigated at room temperature (RT) and after annealing. Also the influence of different implantation energies on the depth distribution of involved chemical species is investigated.

The W 4f and Be 1s spectra reveal formation of beryllium tungstate BeWO₄ already at RT in significant amounts due to the energy deposition of implanted oxygen ions. For comparison, in thermal annealing experiments this is the case above 600 K. The spectra of the W 4f region show formation of BeWO₄ mainly near the surface. This depth distribution is in qualitative compliance with the simulated implantation depth profiles. No indication for oxygen diffusion at RT is observed. In previous experiments BeWO₄ has proven to be stable at temperatures up to 1100 K in a Be-poor environment. In contrast to these results, annealing of the implanted sample at 600 K leads to a decomposition of BeWO₄. This decrease of decomposition temperature is attributed to the excessive amount of Be. The implanted oxygen remains in the sample after annealing, bound in BeO.

Within the project "Plasma-facing Materials and Components" the areas of plasma-wall interaction studies, material modification under plasma exposure, development of new plasma-facing materials and their characterisation have been merged to form a field of competence at IPP. The work supports exploration and further development of the fusion devices of IPP and also generates basic expertise with regard to PFC-related questions in ITER and fusion reactors.

Properties of Nitrogen-implanted Beryllium and its Interaction with Energetic Deuterium

Recent successful experiments with nitrogen as seeding gas in fusion plasma devices, together with the decision to use beryllium as an armour material in the international fusion experiment ITER, have triggered interest in interactions of energetic N ions with Be and the influence of

possible compound formation on parameters relevant to reactor operation and safety. Laboratory experiments are performed to investigate the properties of the 'mixed material' formed upon bombardment of bulk Be with energetic (keV) nitrogen ions. The formation of beryllium nitride within the implantation zone of a few nanometres is observed by X-ray photoelectron spectroscopy and Rutherford backscattering spectrometry. Upon implantation of N at 1.5 keV per atom, saturation of the Be surface with N occurs at a fluence of 2×10¹⁸ Ncm⁻² and a retained areal density of approximately 4×10¹⁶ Ncm⁻². The nitride undergoes an ordering process upon annealing, but does not decompose at temperatures up to 1000 K. The influence of such nitride layers on the retention and release of D implanted with different fluences is investigated by nuclear reaction analysis and temperature-programmed desorption. The nitride layer does not act as diffusion barrier for out-diffusing hydrogen isotopes. A partial sputter yield of 0.013 N/D as a lower limit is measured upon bombardment of the nitride layer with D at 2 keV. These erosion measurements are influenced by the strong tendency of the nitride to oxidise.

Blistering due to Hydrogen Implantation into Tungsten

On hot-rolled, polished and stress-relieved polycrystalline tungsten (W) a large number of spherical blisters appeared after exposure to a deuterium plasma. The implantations were performed with an ion energy of 38 eV/D, a flux of 1×10^{20} D/m²s and fluences between 3×10^{23} and 6×10^{24} D/m². The sample temperature was stabilised at 300 K during plasma exposure. The diameter of the blisters was between 1 and 20 μm, their height reached up to 0.2 μm. At the larger fluences the blister areal density reached 3×10⁹ blister/m², which corresponds to a surface coverage of ~30 %. After removing all deuterium from the sample by thermal desorption spectroscopy (TDS) at temperatures up to 1200 K, ~75 % of the blisters had completely relaxed. Markers cut into the sample surface with the focussed ion beam (FIB) of a dual-beam scanning electron microscope (SEM) prior to the implantation allowed a direct comparison of identical surface areas before and after TDS.

To verify whether the relaxation of the blisters was due to the removal of high pressure gas inside the blisters or due to a thermal relaxation effect, the cap of several medium-sized blisters was punctured by FIB. During this procedure, the blister was periodically observed by SEM. After a milling depth of ~1 µm, complete elastic relaxation of the blister was reproducibly observed (see figure 1). This supports the assumption of a high pressure gas filling. Subsequent FIB cross-sectioning revealed a fine crack system running along grain boundaries in a depth of ~ 1 µm that intersected with the previously milled crater. Using typical values for blister diameter (10 µm), height (0.15 μm), and cap thickness (1 μm) together with the knowledge of a gas-driven and purely elastic deformation, a first rough estimate for the gas pressure was made using Kirchhoff's plate theory. Accordingly, the gas pressure necessary to cause the observed deformations is of the order of 0.7 GPa.

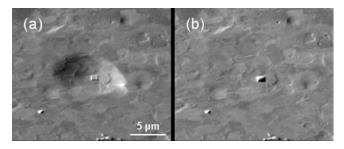


Figure 1: Fully elastic blister on stress-relieved tungsten implanted with deuterium with 38 eV/D at 300 K at the beginning of FIB milling (a) and after penetration of the blister cap (b).

For direct observation of the escaping D_2 gas puff due to the puncturing of the cap, a residual gas analyser was attached to the specimen chamber of the SEM/FIB. The amount of D_2 molecules inside such an elastic blister proved to be below the detection limit. However, much larger blisters (diameter up to several 100 μm) were found on a sample that had not been stress-relieved. This sample had been exposed to a deuterium fluence of $8\times 10^{24}~D/m^2$ with an energy of 200 eV/D and at a specimen temperature of 500 K. When the cap of one of these blisters was opened by FIB, a strong D_2 gas burst was detected by the residual gas analyser. A quantitative measurement of the gas pressure inside blisters is currently being prepared.

Migration of Materials in Fusion Devices

Additional contributions to material migration in ASDEX Upgrade (e.g., W melt experiment and dust classifiation) and JET (ITER-like Wall project and marker layers) are reported in the respective sections of this annual report.

Tungsten Erosion on Rough Surfaces in ASDEX Upgrade

Global erosion, re-deposition and transport of first-wall materials have been studied extensively in ASDEX Upgrade (AUG).

W-coated C tiles from the outer divertor of AUG were analysed post mortem after the 2007 campaign by ion beam analysis methods and scanning electron microscopy (SEM). The SEM images revealed a very inhomogeneous W erosion pattern. Areas on the µm rough surface that were inclined towards the magnetic field (='leading' surfaces) were fully eroded down to the C substrate. In contrast, the parts of the rough surface facing away from the magnetic field (='shadowed' surfaces) showed less erosion. In some cases even indications of W deposition in these shadowed areas were found. A very similar result was already observed in the AUG divertor after the 2004-2005 campaign and the same effect was observed with W marker stripes in the outer divertor of JET. The presence of these inhomogeneous erosion patterns puts constraints on the minimal W coating thickness required to avoid exposure of the C substrate to the boundary plasma during an experimental campaign in a fusion experiment. Therefore, an understanding of the underlying processes leading to these patterns is desirable. These patterns cannot be explained by the pure gyro motion of the impinging ions, since the gyro radius is much larger than the surface roughness, which should lead to a homogenous flux and consequently also erosion distribution. Therefore, a new model was developed that explains the erosion patterns by calculating the flux distribution of ions impinging on a rough surface by tracing the path of the ions from the gyro motion in the boundary plasma through the E×B drift in the sheath region until impact on the surface. The rough surface topography data used in the calculations were taken directly from an atomic force microscope (AFM) scan of a small sample cut from a W-coated carbon tile taken from the outer divertor of AUG. The calculated erosion patterns were compared to SEM images taken at the exactly same location as the AFM image and showed very good agreement both in shape and magnitude.

These model calculations show that the trajectories of particles arriving at the Debye sheath edge on gyro orbits from the boundary plasma are affected by the strong electric fields in the Debye sheath, leading to oblique impact angles, which in turn result in an inhomogeneous flux and erosion distribution. In contrast, promptly re-deposited W that is ionised within the magnetic pre-sheath after being sputtered from the surface has a very different impact angle distribution compared with ions arriving from the boundary plasma. Promptly re-deposited W impinges almost perpendicular to the surface, resulting in an essentially homogeneous flux distribution. This difference in the flux distribution between promptly re-deposited W and particles from the boundary plasma explains the erosion on leading surfaces and deposition of W on the shadowed surface areas: The local net effect depends on the balance between deposition and erosion. On leading

surfaces the homogeneous W redeposition is overcompen-

sated by W erosion mainly due to impurity ions arriving

from the boundary plasma. In shadowed areas sputtering is strongly reduced so that even net deposition can occur. Redeposited tungsten layers have a spongy, foam-like structure, the pore diameters range from a few to a few ten nm. These layers incorporate also impurities, especially B, C, and N.

Modelling the Beryllium Transport in JET

The new code WALLDYN was developed to simulate the global long-term re-distribution of wall materials in tokamak fusion experiments. It includes parameterised kinetic and thermodynamic wall processes such as physical sputtering, chemical erosion, chemical phase formation and sublimation. Based on these principal processes the code computes the time evolution of the first wall surface concentrations along a two-dimensional discrete representation of the tokamak first wall for an arbitrary number of chemical phases (e.g. Be, C, W, Be₂C, BeO, WC, Be₂W,...) under constant plasma contact. The local plasma thereby erodes wall material from the surface, which is transported as impurities to other surface areas along the first wall. The kinetic energy at the impact point of the impurity atoms can again lead to sputtering of wall material. Hence, also impurity- and selfsputtering are included, which is of particular importance for the correct description of W plasma-facing components. Transport through the plasma is assumed instantaneous on the time scale of wall evolution and represented in the code by redistribution matrices, which are pre-computed using, e.g., the DIVIMP code. Each column of such a matrix represents the spatial probability function for redeposition of an

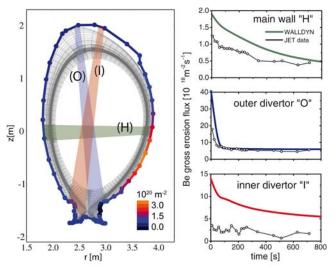


Figure 2: Measured and simulated Be gross erosion fluxes during 800 s L-mode discharges after heavy Be evaporation at JET (right hand side). The schematic view of the JET poloidal cross-section on the left hand side shows the respective spectroscopic viewing chords for main wall (H), inner (I) and outer divertor (O) respectively and the initial Be areal density. The WALLDYN simulations were performed with impurity transport computed by DIVIMP using a computational grid extending to the vessel wall.

eroded species from a particular wall element to the entire wall. The wall evolution processes in WALLDYN are described by a set of self-consistent coupled algebraic differential equations, which are solved numerically. The background plasma required for modelling of plasma impurity transport is provided by the OEDGE or SOLPS codes based on measured T_a and n_a profiles. Chemical surface reactions, such as carbide formation, oxidation or alloy formation, are implemented using parameterised XPS experimental data. The code was benchmarked with experiments performed at JET in 2009, where Be erosion was measured spectroscopically over 800 s total plasma time (identical L-mode discharges) after initial heavy Be evaporation (figure 2). Both the magnitude of the measured erosion flux and typical relaxation time constants towards steady state could be reproduced. Matching the experimental data required the use of a newly developed computational grid for DIVIMP, which extends right to the main chamber wall. Furthermore, the simulations suggest that cross-field diffusivity is a key parameter for the observed relaxation time constants.

Tritium Inventory – Understanding and Control

Many of the project activities devoted to the understanding and control of the tritium inventory are reported in section "Helmholtz-Russia Joint Research Group: Hydrogen Isotopes Retention in First-Wall Materials" at the end of this chapter.

Removal of Deuterium from Deposited Layers Containing Beryllium

In order to assess the tritium removal operation currently suggested for ITER (wall baking at 513 K (240 °C) for the main chamber, and 623 K (350 °C) for the divertor), deuterium retention and release behaviour of beryllium-containing materials were investigated. Be₁₂W and Be₂C compound layers were fabricated by thermally treating deposited C or W layers on Be substrates. Pure Beryllium depositions were done by means of Thermionic Vacuum Arc (TVA) deposition method in MEdC, Budapest. Intermixed layers were prepared by simultaneous Be-W or Be-C deposition by means of multiple Thermionic Vacuum Arc (TVA) deposition, resulting in fabrication of Be-W or Be-C layers with different Be/W or Be/C ratios.

In pure Be, D is predominantly released around 420-470 K within a relatively sharp desorption peak. Operation at elevated temperatures reduces the amount of retained D, but the remaining D is less efficiently outgassed at 623 K. Admixture of tungsten or carbon to Be changes the D release behaviour resulting in less efficient D removal by the baking procedure. Especially, the C concentration in Be affects D release behaviour significantly causing it to become difficult to remove by baking at 623 K.

Based on the results, the performance expected for the ITER wall baking scenario can be discussed as follows:

- Best performance of the wall baking would be expected for tritium removal from high purity Be layers deposited on the main chamber wall under the assumption that the temperature of main chamber wall surface remains below ~ 430 K.
- Tritium cannot be removed from plasma-facing surfaces where the temperature during implantation is higher than the planned baking temperature. Even for an implantation temperature of 423 K, only about 50 % is released at 623 K. Low operation temperatures are preferable and require the lowest outgassing temperatures. Under these conditions outgassing temperatures of 500 K may be sufficient. On the other hand, the amount of primarily retained tritium decreases with increasing implantation temperature.
- Mixed material deposition is expected to occur mainly in the divertor. The efficiency of tritium removal will be limited for compounds and Be-W/Be-C simultaneously deposited layers as summarised in figure 3. Be-W mixtures release at 623 K between 80 and 90 % of the retained hydrogen related to pure Be co-deposits. The formation of a stoichiometric Be₁₂W phase reduces D desorption even further.
- Mixing of C into Be results in a significant change of hydrogen desorption behaviour. In the case of C-rich Be-C deposition, hydrogen is difficult to remove by a baking at 623 K even if the deposit is formed under low temperature conditions. For such cases, one has to consider the application of other removal methods such as laser/flash heating or oxygen glow discharge cleaning. An exchange of the divertor cassettes as foreseen several times during ITER operation may alleviate this problem.

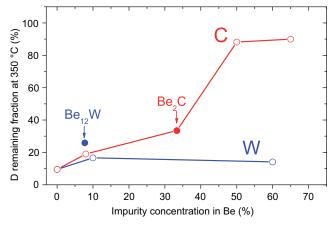


Figure 3: D remaining fraction after outgassing at 623 K for 20 min in Becontaining samples as a function of (W or C) concentration in Be. The data are normalised to the retention in pure Be.

Further measurements should extend the present investigations to thicker deposited layers (mm rather than nm), which requires a proper simulation of D co-deposition during film deposition. More temperature steps and longer temperature holding times (hours rather than mins) will make the extrapolation to ITER more reliable.

Influence of the Tungsten Microstructure on the Deuterium Retention

A very important factor determining the retention of hydrogen isotopes in tungsten is the microstructure of tungsten. Since the solubility in a perfect tungsten lattice is extremely low the deuterium inventory after plasma exposure is correlated with the density of defects that can serve as binding sites for the deuterium. In order to elucidate this correlation, hot-rolled tungsten samples (99.97 wt.% purity) from a single manufacturing batch were heat treated after highquality mechanical polishing in order to systematically modify the grain structure and dislocation density. The samples were then thoroughly characterised by scanning electron and scanning transmission electron microscopy (SEM/STEM). Samples that were degassed and stress relieved at 1200 K for 1 hour did not significantly change their microstructure compared to the initial material. They had small grains with a typical size of approximately 1 µm and a high density of dislocations. Samples annealed at 1700 and 2000 K for 30 minutes were fully recrystallised and also showed grain growth, whereas the typical grain size was smaller for 1700 K (5-20 µm compared to 10-50 µm for 2000 K). The dislocation density was extremely low in both cases.

Well-characterised samples were irradiated in a fully quantified plasma source at a sample temperature of 300 K. The ion energy was 38 eV/D at a flux of 10^{20} D/m²s. Rolled and stress-relieved samples were exposed to fluences between 3×10^{23} and 6×10^{24} D/m². Recrystallised samples were exposed to 6×10^{24} D/m² simultaneously with the corresponding stress-relieved samples.

Depth profiling by nuclear reaction analysis (NRA) revealed significant diffusion of D up to large depths of several µm below the implanted surface. In contrast, the implantation range of the ions is only a few nm. A high and narrow surface maximum was typically followed by a local concentration minimum and a secondary maximum. The shape of the depth profile was strongly affected by the microstructure of the sample. The total amount of deuterium in the accessible range of about 8 µm increased with fluence for the stressrelieved samples and showed a beginning saturation for the higher fluences. The samples recrystallised at 1700 K had approximately the same deuterium inventory as the stressrelieved sample exposed to the same fluence, whereas the inventory of the sample recrystallised at 2000 K was by a factor of 2 lower. Temperature programmed desorption (TPD) showed the same relative behaviour of the total inventory as the NRA analysis. The D2 release spectra (figure 4) were strongly affected by the microstructure.

The stress-relieved sample showed a clear two-peak structure, as opposed to a single broad peak for the samples recrystallised at 1700 K and a much smaller, narrow peak with broad shoulders for the samples recrystallised at 2000 K.

Under the irradiation conditions in these experiments a large number of spherical blisters with a diameter of up to 20 μm and a height of up to 200 nm appeared on the stress-relieved samples, whereas the recrystallised samples showed no signs of blistering.

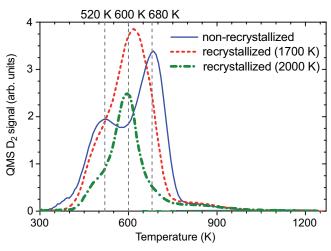


Figure 4: D_2 release spectra from rolled and recrystallised tungsten samples exposed at a fluence of 6×10^{24} D/m². The heating rate was 1.2 K/s for each sample.

Materials and Components

Tungsten Wire-reinforced Tungsten Composites for Toughness Enhancement

Inherent brittleness and further embrittlement by neutron irradiation are two of the most critical issues in the application of tungsten for plasma-facing components. Recently, we proposed an innovative novel toughening method for tungsten, which does not necessarily rely on physical ductility i.e. plasticity. To this end, we utilised tungsten wires as reinforcement with an engineered fibre/matrix interface. The idea is based on incremental dissipation of strain energy by controlled debonding and subsequent frictional sliding at the engineered interfaces. When a propagating matrix crack meets an array of fibres standing perpendicular to the crack front, it deflects along the interfaces, provided that a specific fracture mechanical condition is fulfilled. Then the strong fibres collectively bridge the primary crack, suppressing its dynamic extension and leading to stress redistribution over a finite volume. The total amount of the absorbed energy is a measure of apparent ductility or pseudo toughness. Here, fracture mechanical properties of the interface are the key factors. In order to achieve maximal toughness, the interfaces need to be optimised in terms of fracture behaviour. To this end, we coated the interfaces with thin films. As a preparatory study, we fabricated a number of single-filament composite specimens with various kinds of interface coatings using PVD and CVD processes. We evaluated their interfacial parameters such as shear strength or debonding energy by means of fibre push-out test together with theoretical models. The measured parameters satisfy the criterion for crack deflection. The mechanism of wire bridging was also demonstrated by miniaturised 3-point bending tests under in-situ SEM using a dedicated specimen design (figure 5). The present results confirm the basic feasibility of significant enhancement of tungsten toughness.

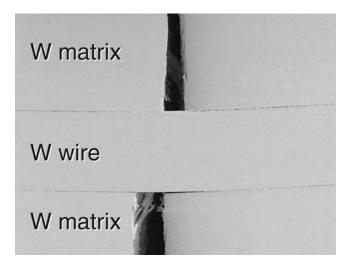


Figure 5: Crack bridging of the tungsten wire under bending load.

Microstructure-based Finite Element Analysis of Heterogeneous Materials

The image-based finite element analysis (FEA) is a numerical technique, which utilises the realistic micrographic images of a heterogeneous material. The image-based FEA allows one to take the characteristic features of the actual microstructure into account for simulating thermal and mechanical processes on a mesoscopic scale. We applied both of these techniques successfully to two sorts of heterogeneous materials considered for the plasma-facing components of next generation fusion reactors, namely, infiltrated particulate W/CuCrZr composites and plasma-sprayed porous tungsten coatings (PS-W). The aim of the study was to elucidate the effect of microstructure morphology on the local damage evolution and failure. To this end the representative volume elements (RVE) were used as a modelling domain.

For the W/CuCrZr composites with different chemical compositions plastic deformation and ductile rupture behaviour under tensile loads were simulated using plane RVE models created from scanning electron micrographs. A continuum damage evolution law was applied to the Cu matrix.

The predicted feature of meso-scale failure was the spontaneous formation of several plastic strain bands oriented to the loading direction at about 45° where ductile damage preferentially accumulated leading to fracture.

For validation the simulated tensile stress-strain curves were compared with the experimental data at RT, 300 and 550 °C considering the contribution of thermal stresses. They exhibited a remarkable agreement even for the final rupture stage. The findings of fractographical inspection also supported the predicted failure mechanism.

Stereographic mapping of the porous microstructure of the PS-W coating with a W/Fe interlayer was conducted using the synchrotron micro-tomography images with a detector resolution of 1.4 μ m/voxel. The reconstructed 3D microstructure image (figure 6) was implemented into a FEA model for further stress analysis. By comparing the computed stress fields of the 3D model with those of a planar model we could estimate the effect of dimensionality in meso-scale modelling. In addition the consequence of loss of geometric information about the defect fine structures was assessed.

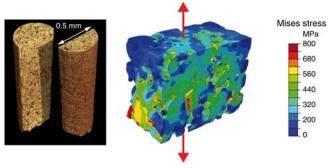


Figure 6: Micro-tomography image of porous tungsten coating (left) and 3D finite element analysis of local stress field (right).

Additional contributions to component behaviour are reported in the section JET cooperation of this annual report.

High Heat Flux Test Facility GLADIS

The high heat flux (HHF) test facility GLADIS offers testing of large water-cooled plasma-facing components (PFCs) as well as small samples with heat and particle loads similar to the expected operating conditions in current and future fusion experiments. The facility is equipped with two neutral beam sources, each up 1 MW power. The commissioning of the second source in 2010 considerably enhances the experimental capabilities to study the behaviour of plasma facing materials subjected to hydrogen or helium particles. The completely independent operation of the sources provides a unique capability for operation with H, He or mixed H/He neutral beams, as well as different thermal load profiles. The continuation of high heat flux testing of the actively water-

cooled divertor targets for W7-X was the main task in 2010.

Different types of tungsten as plasma facing material were investigated with power loads exceeding 20 MW/m² in hydrogen and helium beams. Further, W coatings on CFC for the JET ITER-like Wall Project (see section "JET cooperation"), powder metallurgy fabricated W components for the ASDEX Upgrade divertor (see section "ASDEX Upgrade, technical systems") and newly developed divertor materials in the frame of the EFDA topical group "W&W alloys" in collaboration with the Karlsruhe Institute of Technology were investigated.

Tests of pre-series IV targets for the W7-X divertor with power loads exceeding the design value by a factor of three were performed to study overload situations for the W7-X long pulse divertor. A sequence of 24 pulses with 30 s duration at 30 to 33 MW/m² did not cause significant failures in the CFC/Cu bonding and the integrity of the component was not affected. Only strong erosion of the CFC was observed due to the surface temperature of more than 2200 °C reached during high-heat-flux loading. After reduction of the cooling water velocity from 10 m/s to 8 m/s a partial melting of the CFC/Cu interface occurred. Nevertheless, a loss of the CFC tiles did not occur due to the strong graphite evaporation. This overloading test series demonstrates the maturity of the target component design for W7-X.

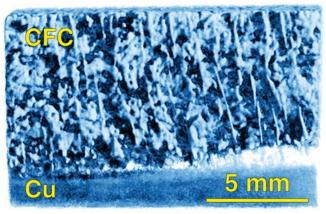


Figure 7: Example of a computed 3D tomogram of a 8 mm high CFC tile bonded onto a copper structure. The thickness of the sample (perpendicular to the plane of view) is 5 mm. More than 2000 individual images were reconstructed to generate the image. The sample was infiltrated with a contrast agent (gadolinium). Bright areas represent the open porosity of the CFC material, which is filled with the contrast agent thus revealing the structure of the CFC matrix. This sample was cut from a methodically overloaded component. The overloading caused delamination of the CFC from the copper substrate The delaminated region between CFC and Cu is visible on the lower right. It extends over the whole sample thickness of 5 mm and is therefore much brighter than the CFC porosity. Image: IPP and TUM.

For the investigation of the CFC/Cu interface crack mechanisms extensive metallographic and micro-chemical post-exposure examinations were conducted to analyse changes

of the CFC structure and of the CFC/Cu interface. All these analyses are based on two-dimensional investigations. An insight into the spatial distribution of structural material modifications and of interface failures is therefore limited. Neutron tomography opens up the possibility to analyse such structures on centimetre-sized samples non-destructively with a high spatial resolution. In the frame of the FEMaS project (see below) the ANTARES facility at FRM II was used to perform neutron radiography and tomography on samples of W7-X targets. The applicability of the method was successfully demonstrated and further improved by vacuum infiltration with a gadolinium agent as neutron absorption fluid. A spatial resolution of about 25 µm was achieved. The comparative analysis of an unloaded and a thermally cycled sample showed distinct differences at the CFC/Cu interface, but no changes of the CFC material. It is concluded that the slight surface temperature increase during loading up to 10,000 cycles at 10 MW/m² is based on a number of micro cracks in the CFC/Cu interface.

Integration of and Collaboration in EU Programmes

EU Task Force on Plasma-Wall Interaction

The contribution of the project to the EU PWI Task force has further intensified in 2010 with the TF leader, the new leader of the Gas Balance and Fuel Retention expert group and the leader of the Mixed Materials expert group from the PFMC project at IPP. In addition to leadership activities, PWI research within the PFMC programme is characterised by cooperation based on joint experiments (e.g. the ITERlike Wall experiment at JET, the joint impurity migration modelling efforts for ASDEX Upgrade, JET and ITER), which is the basis for several priority tasks assigned by EFDA. Consequently, strong contributions were made to all topics of the Task Force, amounting to 4.1 ppy Priority Support and 12.3 ppy Baseline Support. Within the EFDA Fusion Programme the Project provides two mid-size facilities: The High-Heat-Flux Test Facility GLADIS and the Integrated PWI Facility.

ExtreMat — New Materials for Extreme Environments (an EU Integrated Project in FP6)

The European research project ExtreMat is coordinated by IPP and brings together 37 European partners from industry, research centres and universities with the aim to develop new materials for very demanding applications. Application fields besides fusion are advanced fission, electronics and space applications, as well as gas turbine compounds, brake systems, X-ray generators etc. as spin-off applications. Common requirements are the basis for the development of self-passivating protection materials, new heat sinks, radiation-resistant materials and of compounds integrating these materials with their favourable properties. The project, started

end of 2004, was terminated successfully in September 2010. The final task was the termination of the neutron irradiation campaign, which for the first time enabled material scientists from many institutions to test their materials in a nuclear environment. Overall, the project was very successful, both in developing new materials concepts in the targeted applications fields, and in its integrative character. Several new lasting collaborations were initiated and a number of follow-up projects between ExtreMat partners are already running. ExtreMat was nominated as "FP6 Success Story" by the EU project officer.

FEMaS — Fusion Energy Materials Science (an EU Coordination Action in FP7)

The FP7 EU Coordination Action "Fusion Energy Materials Science (coordinated by IPP) aims to foster the integration of universities, research centres and in particular large-scale research facilities like synchrotrons and neutron sources into the fusion materials community. 27 participants from universities, research centres and large-scale facilities like ESRF, FRM II and HZB-BESSY II collaborate in training activities, summer schools and bilateral exchange of researchers. In 2010, the 2nd FEMaS Workshop was organised, presenting an overview of the fusion materials science activities in ~50 presentations.

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Helmholtz-Russia Joint Research Group "Hydrogen Isotopes Retention in First-Wall Materials"

Heads: Dr. Matej Mayer (IPP), Dr. Anna Golubeva (Kurchatov Institute)

This joint research group comprises scientists from the IPP, from the Moscow Engineering and Physics Institute (MEPhI), and from the Kurchatov Institute (both located in Moscow, RU). The research group is funded by the Helmholtz Association.

Deuterium Retention in Polycrystalline Tungsten and Tungsten Coatings

Deuterium retention in polycrystalline tungsten and tungsten coatings exposed to low-energy pure and helium-seeded deuterium plasmas was investigated. ITER-grade W and two W coatings with 200 μm and 10 μm thicknesses were used. Seeding of helium into D plasmas with a helium ion flux fraction of 10 % reduces the deuterium retention for all tungsten grades. A more significant reduction was observed for ITER-grade W, a less significant effect was found for W coatings. From thermal desorption spectroscopy measurements we conclude that the presence of He modifies the density of existing deuterium traps, but does not modify the nature of the traps. The maximum effect of deuterium retention reduction was observed at around 500 K.

Deuterium Retention in Damaged Tungsten

The effects of fast neutron damage on deuterium retention in W were simulated using fast charged particles. W samples were damaged by 5-20 MeV W ions and subsequently exposed to deuterium plasmas at different exposure temperatures. The D retention in damaged W correlates with the calculated damage level. Self-implantation of W results in D trapping in radiation damage (vacancies and vacancy clusters), thus increasing the D inventory. A diffusion model with dynamic trap formation during irradiation was validated by comparison with experiments. The model was applied for the calculation of hydrogen isotope retention in ITER in the presence of neutron irradiation. Calculations show that T retention does not reach the limit of 700 g until the end of the ITER lifetime.

Deuterium Retention in Co-deposited Mixed C-W-D Films

Co-deposition of tritium with eroded wall material in remote areas is considered as the main channel of tritium accumulation in fusion devices with a carbon wall. A divertor consisting of carbon and tungsten is planned for ITER, thus resulting in the formation of mixed C-W-D redeposited layers. Deuterium retention in C-W-D films co-deposited during a deuterium magnetron discharge with a mixed C-W cathode was investigated. Morphology and composition of deposited films were analysed by secondary electron microscopy, ion beam analysis, and thermal desorption spectroscopy. The films were carbon dominated with a maximal concentration of tungsten of 50 at.%. Deuterium retention in these films was comparable to C-D films and was still at a level of tens of percents at temperatures below 100 °C.

Deuterium Permeation through Carbon-coated Tungsten during Ion Bombardment

Ion-driven D permeation through tungsten membranes coated by amorphous carbon films was investigated and compared with the permeation through bare W at a temperature of 873 K. The initial thicknesses of the carbon films were 120-170 nm, detailed characterisations of these films were performed using AFM, NRA, RBS, FIB/SEM and XPS. The influence of the carbon films on permeation was strong ion energies, but different for each energy. In the case of 200 eV/D ions, the film was completely removed by the end of permeation due to intensive chemical sputtering, the lag time of permeation was much longer than for the bare membrane, and the permeation rate rose to a maximum value close to the bare membrane and then decreased to lower values. In the case of 1200 eV/D, the films were sputtered only very slowly, the lag time was much longer than in the case of the bare membrane but shorter than at 200 eV/D, and the permeation rate increased steadily up to several percents of the incident flux.

Simultaneous Depth Profiling of Hydrogen Isotopes and Helium

It is expected that helium implantation has a strong effect on the permeation of D through W. For the simultaneous detection of hydrogen isotopes and helium in tungsten after exposure to He seeded D plasmas the elastic recoil detection method using medium heavy ions (MI-ERDA) was further developed for 15 MeV oxygen ions. The recoil cross-sections for H, D and He were derived from backscattering cross-sections available from the IBANDL data base using kinematic transformations. A depth resolution of 25-30 nm at the surface is achieved.

Permeation of D Gas through Coated Carbon Materials

Hydrogen gas driven permeation through graphite coated with different types of tungsten coatings (magnetron-sputtered, VPS) with thicknesses up to 200 μ m has been investigated. The gasdriven permeation occurs through the carbon base-materials by hydrogen molecular gas flow through the internal porosity network rather than hydrogen atom diffusion through the graphite lattice. It was found that W coatings with thicknesses up to 3 μ m are transparent for hydrogen gas penetration and do not influence the permeability of coated fine-grain graphite, because the open porosity system of graphite remains open. Even a 200 μ m thick layer of VPS-W has an open system of connected pores, which connects the front and rear surfaces of the deposited layer.

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Plasma Theory

Theoretical Plasma Physics

Heads: Prof. Dr. Sibylle Günter, Prof. Dr. Per Helander

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Head: Prof. Dr. Sibylle Günter Tokamak Edge Physics Group

The neoclassical transport code NEOART by A. Peeters has been integrated as a module into the B2.5 code and tested on an ASDEX Upgrade discharge. Development of the SOLPS6-B2.6 project (which introduces a solution-adaptive finite volume

scheme to the B2 code) has continued. The main focus was on preparing the B2.6-structured branch of the code for production use and dissemination to users. A major milestone in this process was the implementation of a regression testing framework to ensure reproducibility of results between different versions of the B2 code. Further, development of the B2.6-unstructured code has progressed, and the associated grid generation tools were improved with the aim of enabling use of fully orthogonal grids close to the target plates. A test version of the kinetic module for the B2 fluid code has been completed. It combines a fast scheme for parallel electron propagation ("free-streaming"), a fully implicit scheme for the non-linear Coulomb collision operator for electron-electron collisions, an implicit scheme describing the parallel electric force on the plasma, and the Debye sheath. First tests revealed a good match with parallel electron transport coefficients in regimes of strong collisionality. The first SOLPS developers' meeting was held at IPP and included participants from IPP, Russia (State Polytechnical University of St Petersburg), France (CNRS-Paris), FZJ, and the Netherlands (FOM). Current developments of the code were presented and discussed.

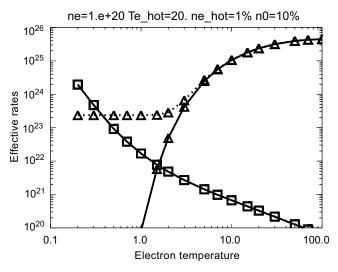


Figure 1: Rates for ionisation (triangles) and recombination (squares) without fast particles (solid lines) and with a 1 % 20 eV electron population (dotted line).

The project "Theoretical Plasma Physics" is devoted to first-principle based model developments and combines the corresponding efforts of the divisions Tokamak and Stellarator Theory, of two independent Junior Research Groups, and of the HLST Core Team of the EFDA HPC initiative. To exploit synergies between astrophysical and fusion plasmas, a collaboration between IPP and the Max-Planck-Institute for Solar System Research (MPS) has been started.

ITER has been designed to operate in the semi-detached regime on the basis of SOLPS calculations, but simulations of detachment on present machines are not always successful – with the main problem of the asymmetry in detachment between inner and outer target. A study was performed with SOLPS to identify physics mechanisms affecting the asymmetry. This asymmetry was large-

ly unaffected by: divertor geometry (vertical or horizontal target); fluid or kinetic neutrals; input heating power; varying the transport coefficients with upstream separatrix density; the presence or absence of impurities (C); or the presence of ELMs (the "standard" knobs used in the code). Including drift effects in SOLPS though had some impact on the asymmetry. A small (1 %) background of hot (20 eV) electrons in the divertor region had a significant effect on the ionisation rates at lower divertor temperatures, while leaving the recombination rate largely unaffected (see figure 1). This introduced a new loss mechanism into the simulations, which increased the small asymmetry between the inner and outer divertors substantially (see figure 2).

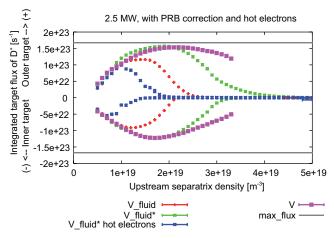


Figure 2: Integral particle fluxes to the outer (positive) and inner (negative) divertor plates as a function of the outer midplane separatrix density where the hot electron results are compared with the other vertical target results.

MHD Theory Group

Linear Stability Studies in the Presence of 3D Wall Structures

The three-dimensional, linear MHD codes CAS3DN and STARWALL in combination with the feedback optimisation code OPTIM have been used to perform stability studies investigating the stabilisation properties of various AUG wall designs with respect to ideal external kink modes. A model plasma based on AUG #20993 has been used to determine the ideal wall beta limit for several wall designs consisting of multiply-connected wall elements and ICRH antennas.

First results of this study show that Faraday screens connected to the wall increase the beta limit noticeably, while ICRH antennas (Faraday screen plus antenna box) that are not connected to the wall are less effective. However, the latter also contribute to the mode stabilisation.

However, damping mechanisms, such as plasma toroidal flow and drift kinetic resonances, play also an important role for the stabilisation of RWMs. Since these effects are not included in the above mentioned code package, the vacuum solution of the STARWALL code for given unit perturbations and 3D wall geometry has been coupled to the resistive, linear MHD code CASTOR_flow. This code already includes plasma rotation, resistivity, and viscosity. Furthermore, the CASTOR_flow code has been extended. The new code version, called CASTOR_3DW, includes eigenvalue splitting and toroidal mode coupling. Both effects are caused by the symmetry breaking 3D wall structures.

Kinetic MHD and Fast Particle Physics

Due to their importance with respect to energetic particle transport, the physics of BAE (beta induced Alfvén eigenmodes) modes has been further investigated. First, the frequency splitting of BAE modes with different poloidal mode numbers as predicted by an extended dispersion relation has been confirmed experimentally by dedicated ASDEX Upgrade discharges. Furthermore, the evolution of the mode frequencies during a sawtooth cycle has been explained by a detailed analysis: diamagnetic effects, finite k_{\parallel} corrections and trapped particle contributions all play a significant role and therefore stress the importance of a fully kinetic treatment of modes at and below the BAE resp. GAM (geodesic acoustic) frequency. The analysis for modes at even lower frequencies $\omega_{\text{REA}}/2$, as seen in many ASDEX Upgrade discharges has been started. Finally, fully kinetic electromagnetic BAE eigenfunctions were calculated for the first time with the LIGKA code. The modes exist in the BAE gap, but can also move into the continuum depending on the background temperature gradients. Steep thermal gradients also destabilise the mode. Therefore, despite increased ion Landau damping and coupling to sound waves, the modes can easily be destabilised by energetic particles, as seen experimentally.

Non-linear multi-mode runs were carried out to understand the complex interplay of Alfvén modes with different frequencies and radial localisations and their impact on the overall fast particle transport.

Linear MHD Stability Analysis

As part of the linear MHD stability chain workflow, the high resolution fixed boundary equilibrium module HELENA and the linear MHD stability module ILSA have been coupled to the free boundary equilibrium reconstruction module EQUAL. The workflow has been successfully applied in tests to JET and ASDEX Upgrade discharges and will now

enter the production stage. An effort to parallelise the eigenvalue solver of ILSA using cyclic reductions in a hybrid OpenMP/MPI algorithm has been started. The parallel version of ILSA will allow studying the effects of toroidal plasma rotation and edge resistivity on the linear MHD edge stability of tokamak discharges (j- α studies).

Stability Analysis of Vertical Displacement Events

The development of a non-linear resistive MHD code has been continued. The code is able to predict growth rates and non-linear behaviour of the generalised positional instability of a plasma in the presence of finite resistivity structures like the passive stabilizing loops (PSL) of ASDEX Upgrade. The implementation of projection boundary conditions eliminates the artificial stabilizing effect of the computational domain boundary. First comparisons of growth rates observed in experimental plasmas and obtained as result of the developed code (using CLISTE equilibria) show good agreement.

Non-linear MHD Studies

a) Three-dimensional non-linear reduced MHD Simulations Work on the three-dimensional non-linear reduced MHD simulation code JOREK (in collaboration with CEA/Cadarache) has continued comprising improved documentation, debugging and code cleanup, as well as handling on Linux-cluster and IBM-architectures. As additional functionality implemented in JOREK, an interface for ASDEX Upgrade data was realised that allows using specific experimental snapshots as initial data for simulation runs. Resistive wall boundary conditions that are necessary, e.g., for simulations of vertical disruption events or resistive wall modes are currently implemented by coupling JOREK with the STAR-WALL code. First simulations of edge localised modes in realistic ASDEX Upgrade geometry have been started. b) Linear and non-linear stability of drift-tearing modes The drift-tearing mode was investigated using two fluid equa-

tions in the large aspect ratio and cold ion approximation. For experimental data as input, the drift-tearing mode can be driven unstable by the electron temperature gradient if the classical perpendicular electron heat conductivity is taken into account, providing a possible explanation for the spontaneous growing tearing mode in experiments. In the non-linear phase, two saturation regimes are found: the small magnetic island regime and the neoclassical tearing mode (NTM) regime. For a low electron diamagnetic drift frequency and/or a high fraction of the bootstrap current density, the modes turn into large amplitude NTMs. In the opposite case, the saturated island width is small, being about the critical island width for flattening the local electron temperature profile, and the diamagnetic drift (ion polarisation current) dominates the non-linear saturation. A sufficiently large external trigger extends the NTM regime to the region with a lower bootstrap current fraction or a higher electron diamagnetic drift frequency.

c) Plasma response to externally applied resonant magnetic perturbations

The plasma response to resonant magnetic perturbations (RMPs), studied numerically by using non-linear two fluid equations, is affected by the plasma rotation direction and frequency, the RMP amplitude, and the particle, heat, and momentum transport coefficients: (1) In the case of a sufficiently high value of $S^2/(\mu \tau_p/a^2)$, the change of the plasma rotation frequency is more significant than that of the local electron pressure gradient (or electron diamagnetic drift frequency), where $S=\tau_R/\tau_A$, $\tau_R=a^2/\eta$ is the resistive time, $\tau_A=a/V_A$ the toroidal Alfvén time, µ the plasma viscosity, and a the plasma minor radius. The RMP can either speed up or slow down the plasma rotation or even change the rotation direction, depending on the original equilibrium plasma rotation frequency and direction. (2) In case of a sufficiently low value of $S^2/(\mu \tau_p/a^2)$, the change of the local electron density gradient can be significant, especially for plasmas with higher rotation speed or smaller perpendicular particle diffusivity at the resonant surface. The RMP can either increase or decrease the local electron density gradient, depending on the original equilibrium plasma rotation frequency and direction. The electron temperature changes in a similar way to the electron density, if the local parallel heat diffusivity and the island width are not too large. In the opposite limit the local electron temperature profile flattens, which enhances the change in the local electron density gradient.

MHD/Gyrofluid Ballooning Mode Analysis

A comparison between the gyrofluid fluxtube code GEM and the linear MHD solver ILSA for a ballooning unstable equilibrium yielded good agreement for the growth rates and the toroidal mode numbers during the initial linear phase of the instability. The circular equilibrium was based on an s- α model

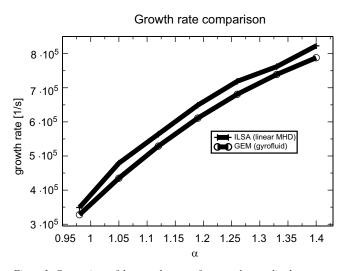


Figure 3: Comparison of the growth rates γ for several normalised pressure gradients $\alpha = -2\mu_{_0}Rq^{^2}/B^{^2}\frac{dp}{dr}$.

with analytical profiles where the edge current density was chosen artificially low to suppress peeling modes. The shape of the pressure profile was similar to an L-mode profile.

Transport Analysis Group

In the field of particle transport, theoretical research has been dedicated to electromagnetic effects in electron transport, by both analytical and numerical linear and non-linear gyrokinetic calculations. In ion temperature gradient turbulence, the loss of adiabaticity of passing electrons produced by the fluctuating perpendicular magnetic field provides an outward directed convective contribution to the particle flux, which decreases significantly the logarithmic density gradient at zero particle flux with increasing β . However, if the increase in pressure is mainly obtained by increased beam heating, the concurrent increase of beam fuelling can balance this effect, leading to the prediction of logarithmic density gradients, which can also moderately increase with increasing β . Gyrokinetic modelling of particle and impurity transport has been applied to explain the observation of increasing density peaking of both electrons and boron with increasing central ECH power, in low current NBI heated H-modes in AUG (see ASDEX Upgrade, section particle and impurity transport). The logarithmic electron density gradients have been determined by the condition of matching the experimental particle to heat flux ratio, evaluated by particle and power balance analyses, while the boron logarithmic density gradients have been determined by the condition of zero impurity flux. The quantitative agreement with the experimental results has confirmed the role of ion temperature gradient and trapped electron mode turbulence in governing the response of the electron density profile to central electron heating, and has indicated the non-negligible role of roto-diffusion in the modelling of impurity transport. Finally, research has been dedicated to the experimental characterisation and the theoretical modelling of plasmas during current ramps in AUG. The energy confinement time is observed to increase with increasing current during the ramp-up, while it remains rather constant during the ramp-down. Electron temperature and density profiles are more peaked at low currents, and the peaking of the density profile requires a turbulent pinch. Theory based transport modelling (GLF23) becomes unreliable at low currents, where a large portion of the minor radius is found to exhibit edge like parameters, at which usual core transport models become non-applicable. First gyrokinetic linear and non-linear calculations reveal that the dominant turbulence is usually TEM at low currents and moves to ITG when the current is increased.

Kinetic Theory and Wave Physics Group

The beam tracing method has been employed to investigate the possibility of a diagnostics based on the deformation of the beam cross section during its propagation in the plasma. Under cut-off conditions, a wave beam is found to be strongly distorted in the direction of the magnetic field at the reflection point, confirming previous ray tracing results, so that the return footprint can be used to measure the magnetic pitch. This measure is shown to be impossible in transmission, but a density measurement based on the rotation of the beam cross section after propagation in the plasma appears to be feasible. Algorithms for the evaluation of the orbit-averaged quasilinear operator describing the cyclotron ion heating in a general axisymmetric configuration have been developed and the corresponding numerical implementation has been performed. Particular attention has been devoted to the calculation of the resonant kernel of the wave-particle interaction, the algorithm being capable of dealing with all the possible positions of the resonance along the particle orbit.

The TORIC-SSFPQL package for the propagation and absorption of ICRF waves has been augmented with the beamlets code SINBAD in order to calculate the ionisation profile from neutral particle beams (NBI). This is used as an NBI source in the Fokker-Planck solver SSFPQL. With this addition, the package allows a self-contained simulation of simultaneous ICRF and NBI heating including possible synergies. Within an international benchmark activity of ICRF codes, TORIC has shown good agreement with the most developed codes in the field.

Neoclassical physics in a transport barrier like in the H-mode pedestal (with density and temperature gradient lengths of about a poloidal gyroradius and a stron electric field) has been studied with the delta-f code HAGIS. Due to the strong peaking of the electric field and the realistic aspect ratio, the effect of the orbit squeezing by the electric-field gradient on the plasma flow and on the bootstrap current is strongly reduced with respect to the usual large-aspect-ratio theory. The density of trapped ions decreases due to a shift of the trapping region in velocity space caused by the electric field. This leads to a reduction of the ion heat flux. The bootstrap current, however, depending on the fraction of trapped electrons, is close to the usual value without orbit squeezing. The flux-tube gyrokinetic spectral code GKW has been employed to compute the electrostatic potential connected with the rotation of a magnetic island, allowing for finite-Larmorradius effects and plasma toroidicity. In the limit of small islands, which cannot be treated with existing analytic techniques, the ion response becomes more and more adiabatic. The corresponding density perturbation is shown to lead to a flattening for the case of island rotation in the ion diamagnetic direction and to a steepening in the opposite case. This confirms previous drift-kinetic results obtained without a self-consistent calculation of the electrostatic potential. Gyrokinetic turbulence simulations including the island geometry in both ion and electron response show the formation

of a time-dependent potential vortex with the wavelength of

the island. The associated E×B velocity is found to impact

the transport across the rational surface where the island is located and its shearing reduces drastically the transport across the island separatrix. Self-consistent electromagnetic gyrofluid simulations demonstrate that the non-linear coupling between turbulence and island scales contributes to the island stability under realistic tokamak conditions.

Turbulence Theory Group

Progress was made on a wide front in both analytical and computational efforts. A solution was given for the momentum conservation controversy in global gyrokinetic theory. Global gyrokinetic electromagnetic turbulence simulations with a particle in cell (PIC) model were carried to the high performance tokamak regime. A self consistent bootstrap current was captured by total-f gyrokinetic computations. Full flux-surface edge turbulence computations explored the connection to a self consistently generated MHD component. Other elements including non-linear collisionless magnetic reconnection are also reported.

Fundamental Theory

A major controversy involving gyrokinetic theory was addressed. It was asserted that the theory as currently known was inadequate to determine the radial electric field of a magnetised plasma because the part of the theory governing the establishment of self consistent fields was not developed to high enough order in the ion gyroradius or fluctuation amplitude. In general however the theory as we know it today is a Hamiltonian field theory supported by general theorems governing the conservation laws. Since circa 1983 gyrokinetic theory is no longer a gyrokinetic equation governing particle motion but a self consistent system of equations governing the collective responses of both particles and fields. And since circa 2000 it is known as a field theory supported by the Noether theorem. We addressed the question of momentum conservation and transport in detail for general systems subject to any ordering scheme. The problem was addressed in terms of functional form by transforming the gyrokinetic Lagrangian for the particles into a form, in which the dynamical fields enter only in the Hamiltonian. Conservation laws then result from the symmetries in the coordinate-space components of the Lagrangian (for gyrokinetic motion these components are the gyrocenter positions in 3D plus the two variables governing parallel and perpendicular dimensions of velocity space). Energy conservation is well known and was used as an example. Momentum conservation is more involved because the Noether theorem gives the canonical momentum as the globally conserved quantity. To show the actual plasma motion is conserved it is necessary to use the (ambipolar/quasineutral) charge conservation equation, which then obtains the parallel and E-cross-B components of the toroidal plasma momentum. We then examined the local form of momentum conservation, that is,

the equation of momentum transport. Conversion of canonical to plasma momentum is done by using the radial component of the charge conservation, which is one and the same with the statement that the flux surface average of the radial current is zero. We therefore proved that not only canonical but also plasma momentum is conserved both locally and globally by modern gyrokinetic field theory. The sole necessity is to start from an energetically consistent form, which is guaranteed by the use of the canonical version of the Lagrangian. Currently used global codes such as FEFI, ORB/NEMORB, Gysela, and GTC were shown to satisfy these conditions at least at the level of the coded equations.

Gyrokinetic Study of Core Turbulence

Work was done to understand the high performance tokamak regime, similar to expectations for the ITER core, in which electron drift-Alfvén transients control saturation and therefore transport scaling. The particle pushing algorithm was rebuilt around equations with explicit Hamiltonian support following the above-mentioned work on energetic consistency.

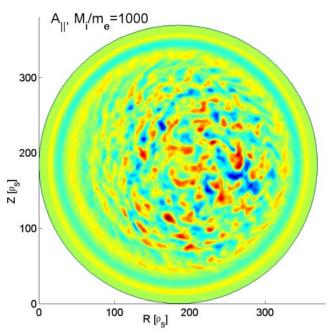


Figure 4: Morphology of the parallel component of the magnetic vector potential in the poloidal plane. The toroidal symmetry axis is to the left near R=-350 in the units of the plot.

Gyrokinetic/Fluid Edge Studies

A series of edge turbulence parameter scalings run with the fluxtube delta-f gyrokinetic model delta-FEFI uncovered a long-wavelength electromagnetic component, which controls saturation and therefore scaling. A scaling campaign in computational domains commensurate with the entire flux surface in terms of perpendicular scale, about 1500 ion gyroradii in the electron drift direction while still following the narrow

edge channel was carried out. The spectrum was found to peak in the long-wavelength MHD regime, while companion linear scaling runs showed instabilities only at wavelengths of 10 to 20 gyroradii. The scalings were also very different, underpinning the need for a non-linear perspective in the central role and not as an afterthought for instability studies. The total-f gyrokinetic model FEFI was employed in a 4D axisymmetric form (2-space 2-velocity) to study the neoclassical equilibrium. Collisions were incorporated in the isotropic field particles model of Brizard, a non-linear treatment with exact conservation properties. FEFI was demonstrated to conserve momentum as well as energy with and without collisions. The basic neoclassical control case of no transport and no bootstrap current was found for the collisionless case, while

The introduction of global conformal coordinates allows closed field line computations to go arbitrarily close to the X-point of a diverted tokamak geometry. The FEFI code is being re-written to use this representation.

a bootstrap current emerged self consistently in the collisional

cases. In all cases radial force balance and Pfirsch-Schlüter

balances in currents, flows, and heat fluxes were found.

In collaboration with IPFN (Lisbon, Portugal) the GEMR model is used together with the full-wave reflectometry simulation model REFMUL as a synthetic diagnostic for detailed comparisons to experimental signals. A time trace is constructed using 2000 temporal realisations of the GEMR turbulence. The effects of various flux surface shapings are being explored.

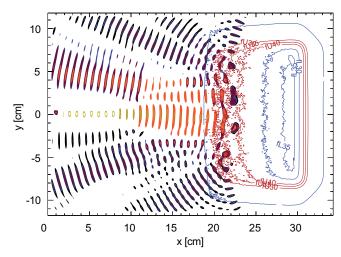


Figure 5: Snapshot of the EM field contour of an LFS X-mode reflectometry simulation (REFMULX code) in a poloidal plane of the electron density given by GEMR.

Other Topics

Our study of collisionless magnetic reconnection under the IPP/MPS astro/spaceplasmas project focused on non-linear acceleration in 3D Harris-pinch cases. A complicated non-linear evolution is found en route to saturation.

Unlike 2D cases, which simply grow a coherent magnetic island structure and then saturate, 3D cases generate their own set of both subsidiary islands as well as self generated turbulence. Both effects produce acceleration of the original linear growth rate by a factor of a bit less than one order of magnitude. A full battery of convergence tests against detailed energetic diagnostics was undertaken before the result could be verified.

An analytical study of drift wave turbulence produced a model, which could correctly predict the non adiabatic density spectrum in the simplified 2D Hasegawa-Wakatani model. An attempt to calculate rotation effects of edge/SOL coupling through turbulence, which exists mostly on the outboard side of the torus was started. A PhD project studying the mathematical underpinning of the gyrokinetic Lagrangian in terms of differential forms was started. A possible aim is to find whether coordinate-free discrete systems satisfying an approximate Lagrangian but with exactly symplectic properties can be a possible basis for improved numerical models.

EFDA Task Forces, Topical Groups, and Other Activities Integrated Tokamak Modelling (ITM)

IPP continues to play an important role within the ITM (http://www.efda-itm.eu/), providing two Integrated Modelling Project Leaders (IMP3 and IMP4), two deputy leaders (IMP12 and IMP3), and, from September 2010, a deputy task force leader. In addition, the following physics contributions have been made: The neoclassical transport code NEOART has been converted from a standalone code into a transport module complying with the ITM standards for data structures. Based on previous work by J. Storrs at CCFE a new web publishing system based on XML was developed and applied for the ITM Task Force. The first production workflows for the linear MHD stability analysis chain have been developed using the EQUAL, HELENA, and ILSA actors. To support the use of the ITM general grid description, a multi-language library is being developed, which allows generic grid manipulation and plotting. Based on these tools, integration of the SOLPS package into the ITM structure has started.

Transport Topical Group (TTG)

IPP has contributed to research activities within the EFDA Transport Topical Group. An IPP scientist has been directly involved as Topical Group Vice Chair, and is at present Chair of this Topical Group. Scientific contributions are provided in the fields of the L-H transition, with investigations on the role of fluctuating and mean fields in the H-mode trigger, and on the physics governing the pedestal width, on electron heat transport, with particular focus on measurements and simulations of high wave number fluctuations, on core impurity transport, as well as on edge and SOL turbulence.

EFDA Goal Oriented Training in Theory (GOTiT)

IPP continued as coordinator of GOTiT (http://solps-mdsplus.aug.ipp.mpg.de/GOTiT/), as well as leader of WP2 (High Level Courses). Three high level courses ("Anomalous Transport in Fusion Plasmas" at ULB Bruxelles, "Transport in Tokamaks" at CCFE Culham, and "Modern Programming and Visualization Techniques" at IPP Garching) have been organised by IPP. The web pages for the GOTiT project have been extended.

ITPA Group on Energetic Particles

A world-wide benchmark of codes concerning the damping rates of low-n TAE modes (n=3) was carried out. In general, good agreement among the codes and reasonable agreement with experimental measurements were found. The results of the LIGKA code allowed to relate the different damping mechanisms to radial locations and therefore facilitated a detailed distinction between local and non-local damping mechanisms.

EUFORIA and MAPPER

IPP continued to contribute to the EU FP7 project EUFORIA (http://www.euforia-project.eu/), providing leadership (deputy coordinator) as well as input in the area of workflows. The EUFORIA project came to an end at the end of 2010.

IPP is also taking part in the FP7 project MAPPER (http://www.mapper-project.eu/) on "Multiscale Applications on European e-Infrastructures", which started in October, 2010.

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Stellarator Theory Division

Head: Prof. Dr. Per Helander Stellarator Optimisation

Looking beyond W7-X and towards a reactor, it is important to establish whether suitable quasi-isodynamic configurations exist. Such configurations with four periods, very good alpha-particle confinement, low neoclassical transport, and negligible bootstrap current have been investigated in collaboration with the Kurchatov Institute in Moscow.

In theory, it should be possible to construct magnetic configurations that are exactly quasisymmetric on one flux surface. A quasihelical configuration has been found through computational optimisation that satisfies this requirement to a high degree of accuracy and has benign neoclassical properties throughout the plasma volume.

In collaboration with the University of Nancy, a low aspect ratio, low-beta, quasi-axisymmetric stellarator has been designed. The aim is to produce a device that can confine a plasma with beta up to 0.5 % having very good neoclassical transport properties, which is achieved in a configuration with two periods and an aspect ratio of 5. The magnetic field is produced by 20 modular coils of five different types. Because of the modest beta requirement, the rotational transform is limited to about ¼ and can be produced with relatively simple magnetic field coils.

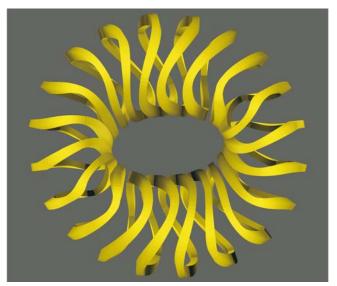


Figure 6: Top view of the coil system of the quasi-axisymmetric stellarator.

Gyrokinetic Simulations Zonal Flows

Zonal flows are believed to be important for regulating the level of turbulence driven by ion-temperature-gradient modes, both in tokamaks and stellarators. To understand these flows better, the linear response of a collisionless stellarator plasma to an applied radial electric field has been calculated, both analytically and numerically. Unlike in a tokamak, the electric

field and associated zonal flow develop oscillations before settling down to a stationary state, the so-called Rosenbluth-Hinton flow residual. These oscillations are caused by locally trapped particles with radially drifting bounce orbits and were first predicted in 2008. The prediction has now been confirmed by gyrokinetic simulations, both in local (flux-tube) and global geometry, using two independent gyrokinetic codes, GENE and EUTERPE. It has also been established that the oscillations are subject to a kind of Landau damping that depends sensitively on the magnetic configuration. The relative importance of geodesic acoustic modes and zonal flow oscillations therefore varies among different stellarators and it is expected that both could be instrumental in regulating the turbulence level.

Benchmarking of Gyrokinetic Codes

In collaboration with PPPL, a thorough linear benchmark of the codes GS2 vs. GENE was accomplished in several stellarator configurations. The code GIST was used for both codes, which predicted similar linear ion-temperature-gradient (ITG) instability growth rates and frequencies within a few percent. In collaboration with NIFS, the Japanese code GKV has also been benchmarked with GENE, producing a non-linear ITG comparison for LHD geometry, demonstrating an excellent statistical agreement. In both cases, the electrons were taken to be adiabatic, since the computational cost (especially for the non-linear comparison) of the full gyrokinetic system is very high.

Turbulence Optimisation for Stellarators

The GIST code, which is able to produce geometrical elements relevant to gyrokinetic simulations, was included in the stellarator optimisation code STELLOPT, together with the introduction of a new target function peculiar to the ITG instability, stemming from a linear response analysis. Initial studies concerned the NCSX configuration, where it was shown that a new configuration can be created with significantly reduced ITG transport levels. This new configuration is characterised by surfaces shifted outwards, similar to a Shafranov shift, thus creating an improved magnetic well.

Statistical Analysis of Drift-Wave Turbulence

A first attempt for a theoretical interpretation of numerically generated probability density functions of intermittent plasma transport events was carried out. In particular, GENE simulations of ITG turbulence with adiabatic electrons for a simple circular large-aspect-ratio tokamak were performed, and the resulting radial heat flux was treated as a time series allowing for statistical analysis. It was demonstrated that, after the removal of autocorrelations via a specific numerical technique (Box-Jenkins modeling), the probability distribution function of the heat flux can be matched with predictions from a fluid theoretical setup, based on the instanton method. This result points to a universality in the modeling of intermittent stochastic processes, offering predictive capability.

Collisions

The global three-dimensional gyrokinetic PIC code EUTERPE includes a pitch angle scattering operator. As an application, the stabilising influence of collisions on ITG instabilities in various geometries (cylinder, tokamak, LHD) has been investigated. The strongest reduction of the growth was found for the cylinder and the weakest for a tokamak, while the stellarator case was intermediate. To further benchmark the neoclassical capabilities of the code, the particle transport for an LHD configuration was simulated and compared with DKES calculations. Including collisions in a δf Monte Carlo algorithm requires a two-weight scheme. Unfortunately, this scheme leads to so-called weight spreading. Using the Ornstein-Uhlenbeck diffusion as a model problem, it has been demonstrated that the statistical error resulting from this scheme increases linearly with time, so that the error for a δf simulation can exceed that of a full-f simulation. However, by exploiting an enhanced control variate, where a free parameter is used to minimise the variance of the solution, an improved algorithm has been developed and applied to the Ornstein-Uhlenbeck diffusion. The error of the new scheme behaves much better: it no longer increases but is bounded by the error of the full-f scheme. The enhanced control variate can also be used to ensure the conservation of certain moments of the distribution function. Using the TORB code this has been demonstrated for the particle number, which, with the new scheme, stays constant instead of increasing as for the standard δf scheme.

International Collaboration on Neoclassical Transport

Over the past ten years, the International Collaboration on Neoclassical Transport in Stellarators has undertaken an extensive benchmarking activity of various computer codes used within the stellarator community to determine the three monoenergetic transport coefficients required for a complete neoclassical description of stellarator plasmas. This activity was concluded during 2010 and the results obtained for twelve different magnetic configurations have been thoroughly documented in a report, which has been submitted for publication.

DKES Analysis of W7-X Configurations

The Drift-Kinetic Equation Solver (DKES) has been used to analyse the neoclassical transport and the bootstrap current in various W7-X configurations. In particular, the bootstrap current has been found to be rather large in all low- ι configurations and smaller (even negative) at high ι and high mirror ratio. For nearly all configurations under investigation, higher β increases the bootstrap current. Minimum bootstrap current is only found in configurations with relatively large neoclassical transport.

Collision Operators with Momentum Source Correction

Several linearised collision operator models with parallel momentum conservation enforced by source functions are benchmarked against the correct collision operator based on Rosenbluth potentials. The benchmarking is performed both for the parallel conductivity with the ions assumed at rest and for the bootstrap current, where ion and electron flows are collisionally coupled. The accuracy of the results obtained with the operators varies from rather poor in the case of the simplest mono-energetic model to quite satisfactory for the models employing an energy-weighted parallel momentum source function.

Predictive Transport Modelling

Minimisation of neoclassical transport is a key element in the design of economic fusion reactors based on the stellarator concept. In the long mean free path regime, the neoclassical transport has a very unfavourable temperature dependence, in particular in the 1/v-regime where the neoclassical heat diffusivity for electrons scales as $T^{7/2}$. To study the impact of the neoclassical optimisation on the confinement, predictive energy transport calculations have been carried out for the optimised magnetic configuration of LHD and for the "standard" configurations of TJ-II, W7-AS and W7-X. These stellarators exhibit very different magnetic field structures, and their transport coefficients in the 1/v-regime differ by more than one order of magnitude. The energy confinement times $\tau_{\scriptscriptstyle E}$ from these simulations are compared with the ISS04 scaling based on experimental results of quite different stellarators. Good agreement is found, supporting the conclusion that high-performance stellarator discharges with sufficiently high temperatures are governed by neoclassical transport in the bulk of the plasma and that anomalous transport is only dominant at outer radii. A direct comparison of the impact of neoclassical confinement optimisation on the achievable $<\beta>$ and τ_E has been performed with the LHD and the TJ-II configurations scaled in plasma volume to the W7-X "standard" configuration while holding the aspect ratio fixed. The neoclassical transport coefficients for scaled configurations are derived from the database for the original device. For the same density and magnetic field strength, the volume averaged $<\beta>$ as well as τ_E normalised to the ISS04 scaling are calculated in a heating power scan. It is found that the impact of the quite different neoclassical optimisations on the confinement is not as strong as would be expected from the ratio of their transport coefficients in the 1/v-regime, which scale as $\varepsilon_{\rm eff}^{3/2}$ / R^2 . The reason is that the high non-linearity of the thermal transport coefficients with respect to temperature and electric field diminishes the large difference in transport implied by a "pure" 1/v-regime. For fixed heating power, $<\beta>$ is highest for the W7-X configuration, reduced by a factor of two for the LHD case, and further reduced by the same factor for the TJ-II configuration. The required power to achieve a given $<\beta>$ reflects directly the degree of neoclassical confinement optimisation. Whereas for the W7-X configuration $<\beta>=2.6\%$ is obtained at 5 MW, the required power to reach this $<\beta>$ in the optimised LHD is 15 MW, and even $<\beta>=2$ % cannot be achieved in TJ-II. It should be borne in mind that these results are "best-case" scenarios obtained by assuming that turbulence is only important at the plasma edge. Finally, the impact of the device size on the neoclassical confinement is studied; the results are consistent with the ISS04 scaling where $\tau_{\rm E}$ roughly scales with the plasma volume. It is found that while the electron heat transport is significantly decreased in the $1/\nu$ -regime when the device is made larger, the ion heat transport is amplified. Increasing the magnetic field strength to reduce the neoclassical transport leads to much greater forces on the coils and correspondingly greater demand on the support structure. Increasing only the size of a device does not help without increasing significantly the heating power. Therefore, neoclassical optimisation is essential to allow for a reasonable reactor perspective of stellarators.

Steady-State Scenarios for W7-X

The prospects for W7-X to create high-performance plasmas under steady-state conditions have been investigated with respect to the properties of equilibrium, transport and fastparticle confinement. Equilibria of different configurations with varying toroidal mirror ratio and 1-values have been calculated and were investigated with a 1-D transport code under optimistic confinement assumptions (anomalous transport only relevant at the plasma boundary). Most critical for reaching steady-state discharge conditions is the combination of good confinement and minimised bootstrap current. Since the bootstrap current evolves on an L/R-time (some tens of seconds), the net plasma current needs to be minimised to keep the boundary-value of t constant for proper island divertor operation. In some configurations electron cyclotron current drive offers the possibility to counteract the bootstrap current, usually at the expense of a deformed ι-profile. A conservative approach to steady-state is offered by the high-mirror configuration, which has a very small bootstrap current, but somewhat greater neoclassical transport than the optimum. To extend the reliability of the transport modelling, turbulent transport is investigated using gyro-kinetic turbulence codes. First results investigating ITG-modes using the GENE-code for an NBI-scenario maximizing the ion temperature gradient show instability of these modes over the outer 40 % of the minor radius where the gradients are steep. However, the strong radial electric field shear, which is expected in this scenario from neoclassical considerations and which has not been considered in the simulations should reduce the linear growth rates as well as the turbulent transport level.

Benchmarking of 3D-equilibrium MHD Codes

The 3D equilibrium codes HINT2 and PIES have been benchmarked in collaboration with NIFS and PPPL. A new version of HINT2 using a rectangular cylindrical grid has replaced the previous version using a helically rotating one.

The new grid is advantageous with respect to the simplicity of the metric and therefore for the accuracy of splines and differentials. Beta-sequences for the selected reference configurations of W7-X and LHD have been generated with both codes up to $<\beta>$ -values of 5 % for W7-X and of 2 % for LHD.

Ideal MHD

The CAS3D code has been used to assess the impact of error fields on stellarator equilibria. To this end, the code was further developed along its perturbed equilibrium line and, as a first step, proved to reliably determine the effect of a periodicity preserving perturbation causing an inward shift of the W7-X plasma.

Fast Equilibrium Recovery by Function Parametrisation

Function parametrisation (FP) has been implemented in Java for recovering the flux surface geometry and the magnetic field strength from pressure and toroidal current profiles. The implementation allows the use of FP as an XML/SOAP web-service with response times on the order of milliseconds.

Monte Carlo Simulations of Fast Particles

The ANTS (plasmA simulation with drift and collisionS) code has been used to investigate NBI particle losses in all standard configurations of the magnetic field for both injection systems on W7-X, at different plasma densities. Several regions requiring power flux mitigation were identified. The ANTS code was also used to investigate the ability of W7-X to confine fast particles. Recent calculations had shown that small design changes have degraded fast-particle confinement at finite beta. Various optimisation strategies have yielded configurations of coil currents resulting in a significant improvement of pressure-induced fast-particle confinement.

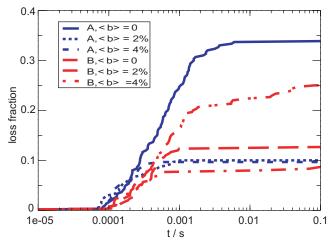


Figure 7: Fast Particle loss fraction over time for collisionless 60 keV protons initiated isotropically at r/a= 1/4 for two different optimised W7-X configurations of the coil currents and for different values of beta.

Global Particle-in-cell Simulations of Electromagnetic Modes

The effect of plasma pressure on Alfvénic modes has been studied. Global electromagnetic gyrokinetic simulations in realistic tokamak geometry have been performed using the particle-in-cell codes GYGLES and EUTERPE. The simulations have demonstrated that the fast-particle pressure can considerably affect the shear Alfvén wave continuum structure and hence the toroidicity induced gap in the continuum. It has further been found that energetic ions can substantially reduce the growth rate of ballooning modes. It has also been shown that the diamagnetic effects associated with the bulk-plasma temperature and density gradients can modify the Toroidal Alfvén Eigenmodes (TAE) in a large-aspect ratio tokamak, even at moderate mode numbers, since it is relatively easy to match the TAE frequency to the diamagnetic one, if the aspect ratio is large enough. The BSPLINES package developed at CRPP Lausanne has been integrated into the GYGLES code, making computations with non-equidistant grids possible. This can be very useful when studying global modes, such as the kink or tearing modes, which can develop extremely fine scales at resonant surfaces. In collaboration with CIEMAT, calculations for energetic particle driven Alfvén modes using CAS3D, CONTI and a local model for growth rates have been made for a recent campaign of TJ-II.

Kinetic MHD

The three-dimensional particle-in-cell code EUTERPE has been successfully coupled with a linear reduced MHD model implemented in the CKA code to investigate the influence of fast particles on Alfvén modes. In the present status, EUTERPE calculates the linear growth rates from

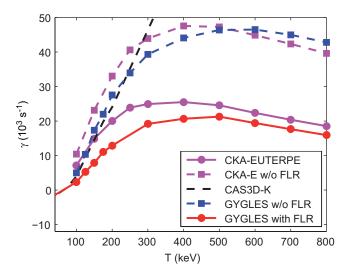


Figure 8: The figure compares results for the growth rate of an n=-6 TAE mode in a circular tokamak driven by energetic ions. The radial extend of the orbits, which is not included in CAS3D-K, causes deviations from GYGLES und EUTERPE for higher energies. The fully kinetic GYGLES model and the CKA/EUTERPE model agree quite well.

the energy transfer between the waves and the particle population using the MHD eigenfunctions and particle orbits, which are not influenced by the wave. The resulting CKA/EUTERPE MHD/gyro-kinetic hybrid model has been benchmarked against several other codes for tokamaks where good agreement has been found. As an example, the comparison with GYGLES and CAS3D-K is shown in figure 8. The new hybrid code includes effects of the full particle orbits and finite Larmor radius (FLR), and can therefore replace the older CAS3D-K, which does not account for these effects. Consequently, the benchmark results (see figure) agree with those of the fully kinetic code GYGLES and deviate from those of CAS3D-K for higher fast particle energies where the size of the orbits or the FLR effects are important. The extension to three-dimensional stellarator geometry is in progress.

ECCD Calculations with Parallel Momentum Conservation and Finite Collisionality Effects

Various computational codes and the approximations that are used in them have been compared and developed to describe various scenarios of electron cyclotron resonance heating and current drive (ECRH/ECCD). It was found that in high temperature (relativistic) plasmas where the low-collisionality limit is valid, it is important to account for parallel momentum conservation in electron-electron collisions. In ITER scenarios it was found that the usual high-speed limit model underestimates the current drive efficiency by 10 %-30 %. In addition, effects of finite collisionality are investigated in collaboration with TU Graz. The solution of the generalised Spitzer problem from the NEO-2 code was applied for calculation of the local ECCD efficiency, and for dense plasmas with moderate temperatures finite-collisionality effects were found to be significant.

Edge/Divertor Physics

Comparison between Stellarator and Tokamak Divertor Transport

The essential divertor transport features of the non-axisymmetric divertors currently investigated on helical devices have been compared with those of the typical poloidal tokamak divertor, surveying the fundamental similarities and differences in divertor concept and geometry and their consequences for the divertor functionality. In particular, the importance of the various physics terms governing axisymmetric and helical scrape-off-layers (SOLs) was examined, with special attention being paid to energy, momentum, and impurity transport. Several of the main features of tokamak and stellarator SOLs can be understood from a few geometric parameters governing the relative importance of various physical effects, which makes it possible to assess these by simple models and estimates. More quantitative assessments must nevertheless rely on numerical modeling. The theoretical results correlated closely with experimental observations.

EMC3-EIRENE Optimisation for Large Tokamak Application

Several numerical improvements have been made in the EMC3-EIRENE code to enhance its computational efficiency for large tokamaks. A flexible mesh structure is now possible, where the computational domain can be resolved into arbitrary sub-domains to better match the local field geometry and the local physics requirements. A particle splitting technique is developed and implemented for improving the overall Monte Carlo statistics of the calculated plasma parameters, which, with increasing size of the device and the computational domain, can vary by several orders of magnitude. The new code version has been implemented at ASDEX-Upgrade and ITER.

Kinetic Transport Modelling

Hydrodynamics is widely used to model transport phenomena at the edge of fusion devices. However, it is well known that under typical conditions the mean free path is not short enough to justify local transport coefficients. Over the years, several attempts have been made to improve the situation within the framework of hydrodynamics. The opposite strategy has been followed here, trying a kinetic model with simplified collision operator that however obeys the correct conservation laws exactly. The penalty is an error of up to 25 % in the resulting transport coefficients. The 1D kinetic and corresponding "reference" fluid models have been implemented numerically; their benchmarking shows that the error lies within the theoretically predicted range. Significant efforts have also been made to parallelise the kinetic code. Currently, the algorithm requires computers with shared memory, which limits its capacity.

Runaway Energy Amplification in Vertical Disruptions

In a tokamak disruption, a substantial fraction of the plasma current can be converted into runaway electrons. Although these are usually highly relativistic, their total energy is initially much smaller than that of the pre-disruption plasma. However, through numerical simulation, it has been shown that as the post-disruption plasma drifts toward the first wall, a large part of the energy contained in the poloidal magnetic field can be converted into kinetic energy of the runaway electrons. In ITER, an energy of order 100 MJ can be channelled into runaway electrons by this mechanism. The model was implemented and solved using the finite-volume transport code BoRiS.

Effect of Toroidal Currents on lota in W7-X

The effect of positive and negative toroidal currents (of the order of several [kA]) on the beta-profile has been investigated by using the VMEC/MFBE code package. Results for beta=4 % are shown in the figure 9: fn corresponds to -15 [kA], fp corresponds to +15 [kA].

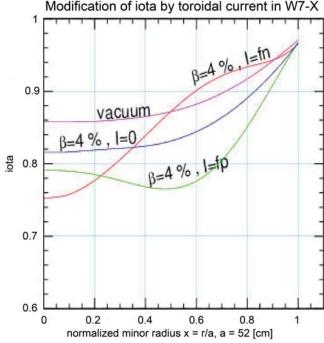


Figure 9: Effect of toroidal currents on iota in W7-X for beta= 4 %.

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Helmholtz University Research Group

"Theory and Ab Initio Simulation of Plasma Turbulence"

Head: Prof. Dr. Frank Jenko

The main goal of our research is to better understand the important unsolved problem of plasma turbulence. Spanning a wide range of approaches, from simple analytical models to simulations on massively parallel computers, we address both fundamental issues as well as applications to specific experiments. Beyond this, we hope that our research helps to improve the general dialogue and cross fertilisation between plasma physics and neighbouring fields of science. Below, three examples of current projects are described briefly.

Global GENE Simulations: Finite Size Effects

One of the important open questions concerning turbulent transport in magnetised fusion plasmas is its scaling with the system size. This issue has been addressed recently by means of numerical simulations with the gyrokinetic GENE code (see gene.rzg.mpg.de). GENE is physically comprehensive (including e.g. multiple particle species, electromagnetic effects, and collisions), well benchmarked, and scalable up to more than 100,000 cores. It can be run either as a radially local (flux-tube) or global (full-torus) code. Moreover, it can be interfaced with MHD equilibrium codes for both tokamak and stellarator geometry. By means of global GENE simulations of ion temperature gradient (ITG) driven turbulence for values of the ratio ρ^* of the thermal ion gyroradius and the minor radius between 1/140 and 1/1000 (corresponding to ITER), it was shown that radial heat flux avalanches, which are often considered as candidates for breaking the standard ("gyro-Bohm") scaling of turbulent transport are meso-scale phenomena (extending typically for 20-40 ion gyroradii radially), but are linked to the ion gyroradius, not to the system size. Moreover, avalanches with the same properties can also be observed in local simulations, in which the average gradients are held fixed, but the (radially) local gradients may vary. In this context, it could also be shown that increasing the physics realism and adding effects due to turbulence drive by trapped electron modes, the influence of avalanches is further reduced. In summary, the present studies demonstrate that avalanches are unlikely to contribute to the breaking of the gyro-Bohm transport scaling, which is sometimes observed experimentally.

Global GENE Simulations: Transport Barriers

By means of both the local and global versions of GENE, we addressed important aspects of the nature of electron internal transport barriers in the TCV tokamak. Using the experimentally determined temperature and density profiles as well as realistic MHD equilibria, it could first be shown by local runs that the low levels of cross-field particle transport are likely due to a competition between ITG and trapped electron modes, as also suggested by simple quasilinear models.

Preliminary global GENE simulations (see the figure below), on the other hand, were able to confirm that the heat transport tends to be strongly dominated by the electron channel, and that small-scale electron temperature gradient (ETG) driven turbulence seems to play a role in the steep gradient (barrier) region. Further investigations along these lines are underway.

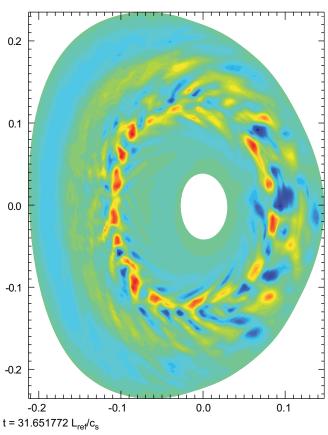


Figure 10: Snapshot of a global gyrokinetic turbulence simulation for an electron internal transport barrier in the TCV tokamak using GENE.

Turbulent Transport of Cosmic Rays

Recently, a newly developed scaling theory describing the turbulent transport of energetic particles in tokamaks could be extended to astrophysical problems like the propagation of cosmic rays in magnetic turbulence. Based on the well-known Taylor theorem, expressing an exact analytical relation between the Lagrangian velocity autocorrelation function of the test particles and the running (time-dependent) diffusion coefficient, the energy dependence of the crossfield diffusivity could be worked out both non-relativistically and relativistically.

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EURYI Research Group "Zonal Flows"

Head: Priv.-Doz. Dr. Klaus Hallatschek

The group focuses on the properties and interaction of large scale flows, a critical agent determining the level and deleteriousness of turbulence. In toroidal systems, the curvature induced coupling of the flows perpendicular to the magnetic field to pressure fluctuations and parallel flows results in two branches, the oscillating geodesic acoustic modes (GAMs), and the stationary zonal flows (ZF) with a dominant parallel flow component.

Geodesic Acoustic Mode Studies: Radial Propagation and Geometry Effects

To search for global eigenmodes of the GAMs and their potential non-local excitation, it is necessary to study how and when they can propagate radially. Following the successful discovery of a useful and physically meaningful way to express the linear propagation terms in terms of fluctuation Poynting fluxes, which leads itself to straightforward estimation even for asymmetric flux surface shapes, we have begun studying the non-linear, i.e., turbulence induced propagation of GAMs. Since for that purpose the turbulence naturally must not be influenced, the numerical investigation of the non-linear transfer involves full turbulence computations. Clear evidence for the effect has been obtained in Non-Boussinesq (i.e. global) NLET code runs of high-gradient ITG turbulence pertaining to the tokamak edge region. Using a frequency filter, the turbulence modified radial eigenmode structure can be extracted from the flow oscillations. The associated radial propagation velocities depend on the turbulence parameters. The non-linear, turbulent contribution typically dominates the linear one by an order of magnitude.

Even discounting the dispersive effects associated with the radial propagation, the turbulence must be included in the description of GAMs for shaped flux-surfaces, since there are several linear flow modes with different frequencies, and the one(s) actually realised are selected by the turbulence. To test our understanding of the geometry dependence of GAM frequencies against observations in present tokamak experiments (specifically ASDEX Upgrade and NSTX), we have developed a method to reinterpolate the flux functions delivered by the respective tools for the flux surface geometry to the needs of the turbulence codes, including, in particular, well converging second derivatives of the interpolating function, which enter in the magnetic curvature terms. The ensuing turbulence runs have resulted in GAMs with frequencies consistent (NSTX) or rather well agreeing (ASDEX Upgrade) with the observations.

Zonal Flow Studies: Revnolds Stress Functional

The Reynolds stress response to ZFs determines the evolution and flow structures in tokamak core turbulence. Its functional form is restricted by symmetry, the flow saturation level, and the observed existence of a preferred wavelength. Having traced back an acceptable approximation of the perpendicular stress to the form

$$R_{\alpha\theta} = Q(\alpha u(1 - \beta u^2) - \gamma \partial_{\alpha}^2 u - \delta \partial_{\alpha}^4 u),$$

with $u = \partial_{\rho} v_{\theta}$ dependent on the heat flux Q and the poloidal flow velocity v_{θ} , the actual numerical coefficients, in particular, the existence and positive signs of γ , β have been reliably determined from extensive computer studies of ITG turbulence with varying flow profiles using a novel optimal filter algorithm. A qualitatively identical functional has been found for the parallel stress.

Scientific Staff

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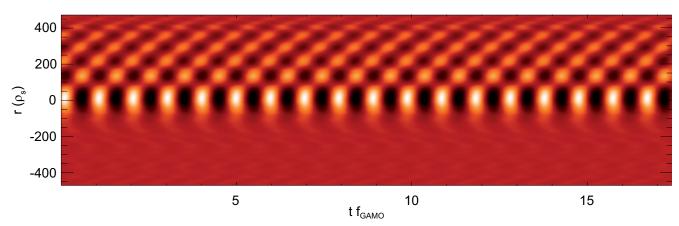


Figure 11: Global GAM Eigenmode caused by non-linear dispersion due to background turbulence in an NLET code computation. The plot shows the flux surface averaged poloidal flow velocity versus minor radius and time.

High Performance Computer for Fusion Applications — High Level Support Core Team

Head: Dr. Roman Hatzky

Tasks of the High Level Support Team

The High Level Support Team (HLST) provides support to scientists from all Associates of the European Fusion Development Agreement (EFDA) for the development and optimisation of codes to be used on the dedicated High Performance Computer for Fusion (HPC-FF) supercomputer located in the Forschungszentrum Jülich Supercomputing Centre (JSC). The HLST consists of a core team based at IPP Garching and of high level support staff provided by the Associates. At present the core team has five members and the high level support staff contributes additional seven scientists. This year the HLST core team was involved in nine different projects submitted by scientists from all over Europe. Exemplarily, we present here the work being done for three projects with IPP participation.

GYNVIZ Project

The aim of the GYNVIZ project is to unify and to provide support for the whole hardware and software chain concerned with the visualization process of large datasets being produced by major European gyrokinetic codes.

Three main components can be identified. The first one consists of a uniform data format, namely XDMF. It has been decided to use this format as standard because a wide spectrum of data types can be expressed and its design is very flexible implying rather low effort on the code developer side. A collaboration with the XDMF team in the U.S. has been set up to improve parts of the implementation for our needs.

The second component consists of a set of post-processing software. The main part is intended to turn 3D time-varying datasets in 4D compressed ones to explore them with 4D visualization. The 4D compression and visualization are technologies transferred from a former EUFORIA (EU Fusion fOR Iter Applications) project while the post-processing tool is a genuine development within the GYNVIZ project. Finally, network and computing infrastructures hosted by the computer centres, Rechenzentrum Garching (RZG) and JSC are the third component. In close collaboration with RZG, a DEISA (Distributed European Infrastructure for Supercomputing Applications) project involving JSC has been established. As a result, data generated by HPC-FF can be easily and efficiently transferred from JSC to RZG via the DEISA file system. Subsequently, a remote visualization session can be started on the newly built visualization cluster at RZG to explore the transferred data.

EUTERPE Project

The EUTERPE code is a global gyrokinetic particle-in-cell code aimed at simulating turbulence in fully 3D stellarator

geometry. It was created at the Centre de Recherches en Physique des Plasmas (CRPP) and afterwards developed further at IPP. Beside these institutions it is currently used at the Centro de Investigaciones Energéticas, Medioambientales y Tecnológicas (CIEMAT) in Madrid as well.

The focus lay on the performance improvement of the EUTERPE code by making use of the Single Instruction, Multiple Data (SIMD) capabilities of the Intel Nehalem processor also known under the term of vectorization. Such SIMD capabilities will be further extended in future CPU design and are in line with the Single Instruction, Multiple Thread (SIMT) concept of Graphics Processing Units (GPUs). The two main particle loops of EUTERPE had to be restructured for vectorization. In addition, it was necessary to get detailed information of the performance of the vector registers. Corresponding results were achieved with a self programmed test bed of common intrinsic functions on both, Intel's Nehalem and IBM's POWER6. Detailed results of these tests are published in the HLST report "Performance Tuning Using Vectorization" as a contribution for training young scientists to the use of upcoming new computer architectures. Unfortunately, in the special case of the EUTERPE code, the performance improvement due to vectorization was cancelled by its own overhead so that the overall performance did not change significantly. However, the new code structure made a more detailed performance analysis possible, which revealed further potential for performance improvement.

MGEDGE Project

Work was done on the efficient implementation of the multigrid method in the GEMZ (Gyrofluid ElectroMagnetic) code of B. Scott, which solves non-linear gyrofluid equations for electrons and one or more ion species in tokamak geometry. Starting from an already existing implementation of the multigrid method we amended the intergrid transfer operators and the linear solver. We further continued with detailed adaptation and testing of the implemented multigrid algorithm on the HPC-FF machine at JSC and the VIP machine at RZG. Overall, we proved that our implementation of the multigrid method using the conjugated gradient method as a "lowest level" solver and first-order intergrid transfer operators has very good strong and weak scaling properties up to 2048 cores. Thus, it is suitable for usage on massively parallel machines like HPC-FF. For details please see the HLST report "Parallelization of the Multigrid Method on High Performance Computers", which has been published as IPP report 5/123.

Scientific Staff

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Supercomputing and other Research Fields

Computer Center Garching

Head: Dipl.-Inf. Stefan Heinzel

Introduction

The Rechenzentrum Garching (RZG) traditionally provides supercomputing and archival services for the IPP and other Max Planck Institutes throughout Germany. Besides operation of the systems, application support is given to Max Planck Institutes with high-end computing

needs in fusion research, materials science, astrophysics, and other fields. Large amounts of experimental data from the fusion devices of the IPP, satellite data of the MPI for Extraterrestrial Physics (MPE), also data from institutes outside Garching, and supercomputer simulation data are administered and stored with high lifetimes. In addition, the RZG provides network and standard services for the IPP and part of the other MPIs at the Garching site. The experimental data acquisition software development group XDV for both the W7-X fusion experiment and the current ASDEX Upgrade fusion experiment operates as part of the RZG. Furthermore, the RZG is engaged in several large MPG, national and international projects in collaboration with other scientific institutions.

Major Hardware Changes

The RZG operates a supercomputer complex with two system parts, an IBM Power6 system with 6624 processors and a fast 8-plane-InfiniBand communication network yielding a peak performance of 120 TFlop/s; and an IBM Blue Gene/P system with 16 384 PowerPC@850MHz-based cores corresponding to a peak performance of 55 TFlop/s. Furthermore, an IBM p575-based cluster of 8-way nodes and a series of Linux clusters with Intel Xeon and AMD Opteron processors are operated. Dedicated compute servers are operated and maintained for an ever increasing number of MPIs. They mostly consist of modern Intel-processor based nodes in blade technology with Infiniband interconnect. The largest system has around 4500 processor cores, 54 TF peak performance and 18 TB of main memory.

In December 2010, the RZG has upgraded an existing system for developing and testing GPGPU (General purpose Graphics Processing Unit) computing applications. The system now comprises an additional NVidia S2050 unit with four GPUs of the latest "Fermi" generation, which feature significantly enhanced performance for double-precision arithmetic and are equipped with error-correcting (ECC) memory.

In order to provide interactive remote-visualization services to scientists of the Max Planck Society a Linux cluster with powerful graphics hardware was installed in the computing centre. The production phase started in October, 2010.

A major task has been the optimisation of complex applications from plasma physics, materials science and other disciplines. Based on the tests on WEGA all major components of the control and data acquisition system for W7-X were reviewed for adjustments. The RZG has continued its engagement in several large MPG, national and international projects in collaboration with other scientific institutions.

The new cluster (delivered by Hewlett Packard) comprises a login node and 6 visualization nodes. Each of the latter nodes contains two NVidia FX5800 GPUs. Five of these nodes are equipped with 2 Intel "Nehalem" quad-core CPUs and 144 GB RAM. For especially demanding tasks, a large node with 4 Intel hexa-core CPUs and 256 GB

RAM is available. The nodes are connected with a fast InfiniBand network. A 30 TB scratch file system is dedicated to the cluster. In addition, the scratch file system of the Power6 supercomputer and the DEISA file system are accessible from the visualization nodes. Thereby, HPC users can investigate their simulation results directly without having to transfer raw data to their sites.

Developments for High-End Computing

The application group of the RZG gives support in the field of high-performance computing. This includes supervising the start-up of new parallel codes, giving advice in case of software and performance problems as well as providing development software for the different platforms. One of the major tasks, however, is the optimisation of complex codes from plasma physics, materials sciences and other disciplines on the respective, in general parallel high-performance target architecture. This requires a deep understanding and algorithmic knowledge and is usually done in close collaboration with the authors from the respective disciplines. In what follows selected optimization projects are presented in more detail.

ASDEX Upgrade Real-time Solver

To control the plasma discharge of the fusion experiment ASDEX Upgrade, the discretised Grad-Shavranov differential equation has to be solved numerically within the control cycle of the experiment, which is 1.5 ms. In order to achieve the necessary computational performance a new algorithm based on Fourier analysis has been implemented, which is significantly faster than the previously employed cyclic reduction method and allows straightforward parallelization. At RZG the program has been parallelised and optimised for multi-core x86 (Intel or AMD) servers. On an up-to-date Intel platform with 8 cores running at 2.5 GHz the latest version of the program requires less than 0.3 ms for a complete equilibrium cycle when using a numerical resolution of 128×64 zones.

In parallel, the suitability of this algorithm for GPGPU computing was assessed in the context of a master thesis, which was jointly supervised by IPP, RZG and LRZ/TUM.

For standard resolution sizes (128×64 zones) it turned out that it was not possible to outperform the latest CPU version, which is mostly due to relatively large overheads for data transfer between the GPU and its host server. At the same time it was shown that GPUs could in principle serve as an attractive alternative hardware platform for this type of application, when significantly larger numerical resolution and/or next-generation GPU hardware is employed.

GENE Code

An important tool for the simulation of gyro-kinetic turbulence in fusion plasmas is the GENE code, which is used for many years now on various architectures and is under continuous development both under physical and under computational aspects. The latest version of the GENE code was optimised to the effect that large runs within the framework of PRACE became possible (50 million CPU hours on the Blue Gene/P at the FZ Jülich). Especially by switching from full matrices to sparse ones and by skilful exploitation of the shared memory on the node for large data structures needed by all MPI tasks running on the node, the memory consumption of the code could be reduced and the scalability increased. Scalability benchmarks on the Blue Gene/P in Jülich proved a good scaling up to 256 000 cores for larger problems.

FHI-aims Code

The FHI-aims code is a new quantum-chemical code developed at the FHI on basis of the density-functional theory. The RZG continued to support the developers in optimizing the code for three different architectures with corresponding software environments: for IBM Blue Gene/P, IBM Power6 and Intel Xeon (Nehalem) based compute nodes with Infiniband interconnect. The work was concentrated on the performance of the direct eigenvalue solver for symmetric matrices. In the framework of the BMBF project ELPA, which is carried out together with the FHI and the MPI for Mathematics in the Sciences as well as with the University of Wuppertal and the TU Munich, a new, two-stage algorithm was developed, which has meanwhile reached production state. Compared to the former one-stage algorithm this new two-stage method is superior in scalability, especially for the case that a large fraction of all eigenvectors is needed. The efficiency of the new solver was successfully tested on up to 65 536 processor cores on the Blue Gene/P and on up to 4096 Intel Xeon cores, the results have been submitted for publication.

Scientific Visualization

In 2010, a Linux cluster was installed at the RZG which is dedicated to quantitative analysis and visualization of simulation data from scientists of the IPP and the Max Planck Society. It is comprised of a dedicated file system and 6 visualization nodes which are equipped with large main memory and two powerful graphics processing units (GPUs) each. The cluster enables scientists to efficiently perform remote visualization of large data sets, in particular without the need to transfer the data to their local workstations. On the cluster, state-of-the-art visualization applications for various purposes are available.

In addition to providing a hardware and software platform, the RZG offers support in the selection and usage of visualization and data analysis tools and in the instrumentation of simulation codes. A close cooperation with the High Level Support Team (HLST) takes place, in particular in the framework of the GYNVIZ project. Moreover, the visualization staff at the RZG has recently supported a number of particularly challenging visualization projects directly. In these cases, either the complexity or size of the simulation data, or specific visualization goals required expert knowledge of existing visualization methods or even the development of tailored software solutions. Examples include projects from plasma physics (IPP), materials research (FHI) and astrophysics (MPA, MPE).

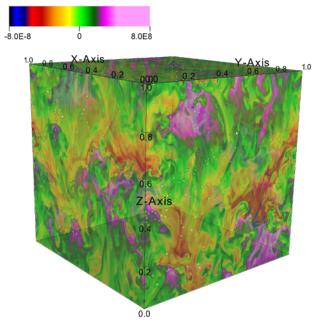


Figure 1: Visualization of temperature fluctuations and Lagrangian tracer particles in a direct numerical simulation of turbulent magneto-hydrodynamic Boussinesq convection. Simulation: J. Pratt, W.-C. Müller (IPP), Visualization: J. Pratt, K. Reuter (RZG).

As a recent example for a successful collaboration between visualization experts and computational plasma physicists we cite visualizations of fluctuations and Lagrangian tracer particles in simulations of turbulent magneto-hydrodynamic (MHD) Boussinesq convection. The simulations are

performed by J. Pratt and W.-C. Müller (IPP) to study magnetic field generation (dynamo action) in the solar convection zone. An amplitude-dependent colour coding of the fluctuations allows the identification of structures in the turbulent fields that extend over large spatial scales. Simultaneously, massless Lagrangian test particles are shown which are advected by the turbulent flow. Following such particles individually or in pairs provides insight into the statistics of turbulent transport mechanisms, field-line stretching, and large-scale magnetic structure formation. Figure 1 shows a snapshot of the temporal evolution of temperature fluctuations and tracer particles from an MHD convection simulation.

Projects in Collaboration

The Munich-ATLAS-Tier2 Project

As part of an active research program the MPI for Physics (MPP) participates in the ATLAS experiment, which is located at the Large Hadron Collider (LCH) in CERN Geneva. To overcome the computing challenges associated with enabling thousands of users to access and analyse the petabytes of data which will be produced by ATLAS the collaboration has turned to grid computing. A multi-tiered computing grid has been formed and extensively tested during the last decade as the LHC experiments have prepared for their long-awaited data taking phase. In Munich a Tier2 centre is supported by collaboration from RZG/MPP and the LRZ/LMU. One half of this federated centre is hosted at the RZG with the other half being hosted at the LRZ. During the past 12 months the Tier-2 centre has been continuously used for the production of simulated data and, more importantly, the analysis of real data from the ATLAS experiment. In addition to the role of a standard Tier2 the Munich Tier2 acts as one of three centres which will perform a special role as a Muon Calibration centre. This activity requires an extremely quick cycle of data import from CERN, analysis of the data and the subsequent return of important calibration data to CERN. New hardware purchased in 2010 more than doubles the compute and storage capacity of the Tier-2 centre. During 2011 the Tier-2 system will be re-optimised to incorporate the new hardware and fit to the changing needs of the ATLAS community. Additionally, upgrades of several core services are expected to follow the evolution of the gLite middleware.

The DEISA2 Project

The DEISA Consortium has continued to support and further develop the *Distributed European Infrastructure for Supercomputing Applications* as an EU FP7 project from 2008 to 2011, coordinated by RZG/IPP. Activities and services relevant for Applications Enabling, Operation, and Technologies have been continued and further enhanced.

The very successful DEISA Extreme Computing Initiative (DECI) with annual calls for Europe's most challenging computational science projects has also been continued. In meantime, scientists from more than 180 universities or research institutes from 25 European countries with collaborators from four other continents have already benefitted from DECI. In addition, DEISA has started support for science communities as a whole, among them from fusion energy research, climate research, astro sciences, and life sciences. DEISA services will be continued at European level by PRACE after the end of the DEISA2 project in 2011.

HLST Project

The High-Level Support Team (HLST) was set up with support of the EU to ensure support for HPC applications in the European fusion community. With the help of the RZG the core team has been established at the IPP, with the other partners residing at different other EFDA sites. The team consists of HPC experts with experiences in scientific computing, having especially a deep knowledge in the fields of numerical algorithms and visualization. The scope of tasks reaches from technical advice, training, all sorts of optimization and visualization of large data sets to the challenging task of increasing the scalability of existing parallel applications.

Bioinformatics/Computational Biology

Initiated several years ago in the context of the MIGenAS project, the RZG maintains a dedicated hardware and software infrastructure for computational biology applications and offers high-level application support for all kinds of bioinformatics projects of the Max Planck Society. Among others, a number of prominent genome projects were completed with the help of this infrastructure in the course of 2010. Specifically, RZG staff participated in the bioinformatics analysis of two economically and biologically particularly relevant microbial genomes, namely Halomonas elongata and Haloferax volcanii.

MPGAAI — An MPG-wide Authentication-and-authorization Infrastructure

MPGAAI is a joint project of MPDL, GWDG and RZG to establish an MPG-wide corporate and federal infrastructure for authentication ("who am I") and authorization ("what am I entitled to") on the Web. Via this authentication-and-authorization infrastructure (AAI), based on the Shibboleth Framework (http://shibboleth.internet2.edu/about.html) and SAML protocol (http://saml.xml.org/about-saml), scientists and staff of the MPG can login directly with their local user accounts at their home institute (Identity Provider), and in doing so obtain access (Single Sign On) to online resources of all Service Providers within the so-called AAI Federation.

Thus, users can have easy and secure access to participating publisher's protected online contents like articles, publications, databases and other services, also and especially from outside the home institute's intranet, when at home or away on business. Pilot service with several MPIs has started.

Videoconferencing (VC)

The VC infrastructure based on the Open Source GnuGK gatekeeper with integrated phonebook application worked reliable without downtime (99.99 % availability) in 2010. The gatekeeper was migrated to new hardware with higher performance to manage the increasing load of HD videoconferencing connections. To meet future requirements H460 and URI support were enabled. Currently 466 VC systems are registered at the gatekeeper. After an update, the Codian MCUs of the DFN service manage connections with Full-HD resolution (1080p). The booking system supported by the VC group worked also with highest availability. Until today 44 000+ bookings were executed. Solutions for a protocolindependent, but commercial videoconferencing infrastructure were successfully evaluated.

Data Network

The data network is based on the concept of a "collapsed backbone" consisting of high-level switches at a few central locations which directly connect to all endpoints via links based on copper or fibre – eliminating the need of aggregating and limiting switches at workgroup or story level. This structure greatly enhances overall network performance, for most of the connections between the backbone routers/switches are at a speed of 1 Gigabit/s (Gigabit Ethernet technology) and a few have even been raised to 10 Gigabit/s on demand, numbers increasing. With this structure security and integrity of data have also been improved because eavesdropping is almost impossible.

Due to various reasons within the compute and data centre the concept of fat trees with high flexibility and performance, but very expensive routers/switches will probably be ruled out by small standard-based switches which are clustered by specific software to form a "virtual chassis". To adopt this rather innovative technique, all new network devices have to be checked against this functionality.

For logical security based on the functionality of the internet protocol suite TCP/IP a packet filter firewall combined with stateful inspection at the access point to the internet (a Cisco 6509 router with hardware-based firewall module) is implemented, where all the incoming/outgoing packets are checked against a set of blocking or granting rules. Additionally, all incoming electronic mail is scanned for viruses and only clean and unobjectionable data (based on known problems) will be passed to the internal network, the rest gets quarantined.

To relocate part of this procedure, a security appliance (from Ironport) was successfully tested and will be adopted in the future. Spam mail marking is also active. Based on a level of probability users can define and set filter threshold values at their PC's email client. In addition, the individual activation of "greylisting" drastically reduces the incoming of unwanted emails.

In the beginning of the year Internet connectivity via DFN was upgraded to a capacity of 4 Gbps to keep pace with the ever growing bandwidth demand. The RZG participates in the eduroam initiative via DFNRoaming. This allows users to make use of the wireless networks of other institutions also participating in eduroam. A controller-based Wireless LAN solution from Trapeze consisting of 23 access points (802.11n-devices) has been installed in the buildings D2/D2A/D2B. Various profiles for employees, guests and eduroam users implement specific security rules.

Data Acquisition and Data Bases for Plasma Fusion Experiments

The XDV group at the RZG is responsible for the development of the data acquisition and data storage system of the W7-X experiment in Greifswald. These components, together with the control components developed by the control group of W7-X were successfully tested as a complete integrated system on the smaller machine WEGA. Following these tests the opportunity was taken to review all major components of the system internally. The review based on the results of the tests showed where minor corrections of the component structures are necessary and where some improvements must be developed. The next step will be the installation of the components needed for the operation of W7-X in the near future.

Scientific Staff

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Energy and System Studies

Head: Dr. Pascal Mühlich (Prof. Dr. Thomas Hamacher till March 2010)

Fusion Power Plant Models

System Code Studies

At the beginning of this year we started to develop a systems code for 0D tokamak power plant system analysis. The objective is to assess the impact of physics and technology improvements on fusion power plants in a multi-parametric space. The systems code

is composed of different modules, which operate on a central data structure. Most of the work was done in the physics module, which consists of balances for particles, power and current in the plasma.

Dual Use in Fusion and Industry

On the way to solutions for the complex requirements of a fusion reactor, researchers are developing new manufacturing processes, constructions, materials, theories etc., to overcome this challenge. At the same time this know-how may refine products and technologies in other applications and thus deliver the industry already today a significant benefit for the high-tech sector and qualify the industrial partners for future tasks. The outline of these multiple-use scenarios and the promotion of cooperations between industry and research is the scope of a project with the TU München and the Siemens AG.

Sustainability Analysis of Fusion

Sustainability requires a new look on any kind of material use. Either materials are abundant relative to their current use or the material cycles need to be closed by recycling technologies. This rule should be followed right from the beginning for fusion. A first analysis of this kind was performed for lithium, which is a key material for the construction of fusion blankets and which plays a central role in the fuel cycle. Problems are also expected for a number of other materials like beryllium and helium.

Fusion Economics

Assessments on the economic prospects of nuclear fusion are usually performed on the basis of cost competitiveness; It is common to compare the expected cost of fusion power electricity to the projected cost of other technologies and conclude on the profitability of a fusion investment. While the merits of this method, especially its low complexity, are evident, there are several shortcomings: The differences of investor's decision fields are neglected; also, in absence of support schemes, intermittency penalties can negatively impact the relative profitability of alternative energy sources, and slight variations of technological and economic parameters can produce very different results. Our review of several prominent cost and technology scenarios shows that it is not possible to draw reliable conclusions from cost comparisons alone. Especially when expressed

The financial crisis has once more demonstrated the strong correlation between economic growth and energy, especially electricity demand. The restless search for new energy and material resources leads on the one hand to new opportunities like shale gas in the US, but also to catastrophes like the oil spill in the Mexican sea. New, sustainable energy sources need to be brought online as fast as possible, fusion being one of them.

in single values instead of ranges, cost projections must be treated with caution. Therefore we develop an improved framework for the valuation of fusion power that takes into account the important parameters and limitations of a potential investor's decision as well as the effect of fusion investments on the power system.

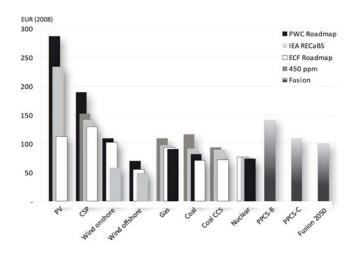


Figure 1: Levelised unit cost of electricity projections. References: ECF Roadmap 2050, PWC Roadmap 2050, IEA, RECaBS (2025), PPCS, Ward, IEA World Energy Outlook 2009.

Global Energy Models

EFDA-TIMES Model

The IPP participates in the development of the global energy system model EFDA-TIMES, concentrating on the evaluation of future pathways for the integration of fusion power in the electricity market of the 21st century. Recent scenario results ascertain that substantial market shares can be expected for fusion power, premising serious political efforts on climate change mitigation. Furthermore, a strong interdependence to the nuclear fission sector was figured out. Consequently, the current work focuses on an enhanced model of the nuclear fuel cycle and extended climate equations to advance the model's scope and significance.

European Supergrid

The integration of variable renewable energies (VRE), such as wind and solar PV energy challenges the energy system. We analyse the medium and long term implications of VRE integration in Europe, with a regionally resolved energy system model based on linear optimisation. Special focus lies on the role of transmission grid extensions – i.e. building a "supergrid" in Europe. We find that VRE strongly influence the price dynamics at the electricity spot markets. While today, electricity prices

are demand driven, they may in near future be driven by the VRE supply, as due to increased investments in wind and solar power, the VRE contribution may reach total demand in several hours. This oversupply drives electricity prices. These stochastic price dynamics imposed by VRE contribution can partially be alleviated through extensions of the interregional transmission grid capacities. In the long term, major structural changes of the European power supply system are needed to integrate high shares of VRE. Grid extensions facilitate VRE integration: they lower the impacts of VRE to the power system and the total system costs. We quantify necessary grid extensions for varying VRE shares and mixes between wind and solar energy. The costs for grid extensions remain below 20 % of the investments in the VRE capacities themselves.

Energy and Cities

PACT and Timebudget-microsimulation

The PACT (Pathways for Carbon Transition) project is now already in the second half of its duration. The project is under the leadership of ENERDATA. The aim of the project is to show pathways of society in the long run (2050 and beyond) and its implications especially for the energy demand. The mid-term reports are meanwhile available. One of the key factors is how time is spent in daily life. To improve the understanding of this aspect and the resulting demand of energy, a micro simulation linked with a geographic information system is currently built up at city level.

Greifswald

In cooperation with three partners the working group developed an integrated climate protection concept for the city of Greifswald, funded by a program of the Federal Ministry for Environment. The concept consists of five parts: a CO₂-inventory, CO₂-saving measures for the transport sector and for energy supply and demand, civic participation in transport sector and

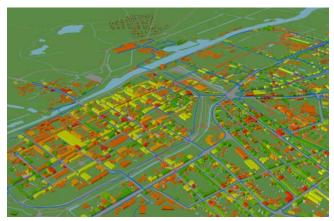


Figure 2: GIS based building database for the city of Greifswald and power supply networks for Gas and district heating-buildings are coloured in green for less energy demand to red for high energy demand.

energy usage. The main results are two scenarios for saving CO₂. A first scenario shows how to reach a self-imposed goal reducing the CO₂ emissions of 2005 by at least 14 % until 2020. A second scenario in the climate protection concept even shows the opportunity to achieve a 24 % reduction. The working group was responsible for the CO₂-inventory, analysed the energy system and developed a CO₂-saving action plan in the energy sector. A linear optimisation model of the energy system and a GIS-based building database were the main working instruments. On 27th September 2010, the city council of Greifswald passed the concept. A first measure of the concept, a local district heating act, was established only a few weeks later.

Salzburg

The project was finished in October 2010 and provided reliable results for the energy infrastructure in Salzburg. The first challenge was to set up a good physical description of the building stock. Working on single objects, the energy models can be set up in a high geographical resolution. The localisation of the heat demand dependent on refurbishment and energy prices was therefore possible. On that base, optimal supply structures were analysed. Furthermore, the influence of specific climate on the city's energy system structure is considered.

Oldenburg

The project "energy efficient city of Oldenburg", concerning all energy demand sectors was finished and the suggested decrease of CO₂-emissions of 40 % until 2020 based on 1990 was decided by the city council. In a second project, a geo-referenced building database containing the whole city area and characteristic information like construction date, size, usage and inhabitants of every building was completed. With this database heat demand and cost-effectiveness of refurbishment measurements could be calculated depending on expected heat price development.

St. Roman

The subject of this project is to develop methods which enable an understanding of drivers, quantities and qualities of transport in rural areas. Spatial methods of data processing and visualization using geographic information systems (GIS) are the centre stage of the project. Mobility images and indicators are developed and contribute to a better understanding of the transport system. Furthermore, first approaches for the integration of mobility into the energy system modelling are aimed for. The project was financially supported by the Friedrich Schiedel Foundation for Energy Technology.

Scientific Staff

M. Bartelt, P. Böhme, F. Botzenhart, S. Braun, M. Busch, T. Eder, T. Hamacher, T. Hartmann, N. Heitmann, P. Hennemann, J. Herrmann, D. Köther, P. Kurz, C. Linder, P. Mühlich, G. Pitl, K. Schaber, I. Schardinger, M. Sommerer.

Electron Spectroscopy

Head: Dr. Uwe Hergenhahn

Electron Spectroscopy Using Synchrotron Radiation

Arguably electron spectroscopy is the most powerful method for studying the electronic structure of materials. In order to carry out such studies with a defined, intense and tuneable excitation source the group uses synchrotron radiation from the storage

ring BESSY (Berlin), and, for experiments on ultra-dilute targets, the Free Electron Laser FLASH (Hamburg). Topics covered in 2010 were the investigation of excited state dynamics by electron spectroscopy and experiments on ionization of a free, fast moving ion beam. For the former project, a major upgrade of our experimental apparatus was undertaken in 2009, which has led to a series of interesting results in the last twelve months. Some of these are described below.

Electronically excited states in weakly bonded aggregates, e.g. water, can decay in a number of fundamentally different ways: Fluorescence and dissociation are well known, and more involved phenomena such as transitions to other electronic states via conical intersections have been intensively studied in the last two decades. In 2003, the electron spectroscopy group first demonstrated experimentally the importance of another decay mechanism, namely, a low energy autoionization process, which involves a concerted transition at two, or even three adjacent sites in the aggregate. The existence of this process had been predicted several years before the experiment by the theory group of L. S. Cederbaum (Heidelberg), who termed it Intermolecular Coulombic Decay (ICD).

Autoionization: Charge Transfer vs. Energy Transfer

Intermolecular Coulombic Decay has since been found in a number of systems, both by the IPP group and by several other teams. Examples are clusters of Ne and, more recently, water clusters (see Annual Report 2008). In our ICD experiments, a vacancy in the valence charge cloud of a free cluster is produced by photoionization, and the filling of this vacancy is monitored by detection of a low kinetic energy electron, which is liberated by the excess energy. The effect is thought to occur generally in weakly bonded systems, and for any excitation source with sufficiently high energy transfer. An apparatus dedicated to the flexible production of cluster beams of various materials, and to the efficient detection of their photoelectron spectra, was commissioned by the electron spectroscopy group in 2009. For studies of ICD, the coincident detection of the primary photoelectron, and of the low kinetic energy electron produced by autoionization, is crucial in order to reliably show the signature of the process. Towards this end, we now use electron spectrometers additionally equipped with magnetic guiding fields ('magnetic bottle' spectrometer).

The electron spectroscopy group at IPP is internationally known for its studies of excited state relaxation in free nanoparticles. Further, the group plays a leading role in the development of electron co-incidence spectroscopy, which is of possible future technological relevance. Highlight of its research in 2010 was the spectroscopic proof of ultra-fast charge transfer processes in mixed rare gas clusters.

As the spectrometer detects electrons in a large interval of kinetic energies with almost 4π sR solid angle, the electron pairs can be easily distinguished from any background processes, e.g. from inelastic electron scattering. Examples of ICD spectra recorded by a magnetic bottle spectrometer have been shown in the Annual Reports 2008 and 2009.

In Intermolecular Coulombic Decay, a vacancy in the valence shell at a site "A" is filled by an even less strongly bound electron, and the energy released in this transition is transferred to a neighbouring site "B". There, a low kinetic energy electron is ejected by the excess energy. Electron correlation is responsible for this process, which can take place in some tens of femtoseconds. In principle, a similar process can occur involving electron transfer instead of energy transfer between the two participating sites A and B, i.e. a vacancy is created at site A, then filled by electron transfer from site B, and another electron is ejected by the excess energy also at site B, or a third site B'. Indeed, the theoretical prediction of these processes is almost as old as that for ICD, and such transitions were termed 'Electron Transfer Mediated Decay' (ETMD).

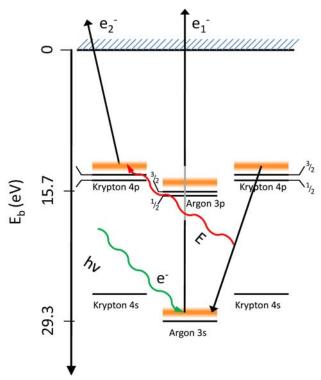


Figure 1: Scheme of a non-local autoionization process mediated by charge transfer, ETMD (3), in a Kr-Ar-Kr cluster. The first experimental demonstration of these processes was made this year by the IPP electron spectroscopy group (see text for details).

As we are considering autoionization processes in weakly bonded clusters, the dependence of the decay rates on bond length R is critical. For ICD, an algebraic dependence by an R^{-6} power law was shown. In ETMD, however, an electron has to be transferred between the two participating sites. An exponential dependence on R would therefore be expected. As a consequence, ETMD has never been observed in competition with ICD. In mixed systems however, cases exist were the energy levels are arranged such that only ETMD, but not ICD is energetically viable. Mixed clusters of Ar and Kr represent one such system. Here, a vacancy in the Ar 3s shell created by photoionization can relax by autoionization, but only into a state were two outer valence vacancies are located at two different Kr atoms (figure 1). The decay to any state involving Ar vacancies is ruled out, as these states would be too high in energy.

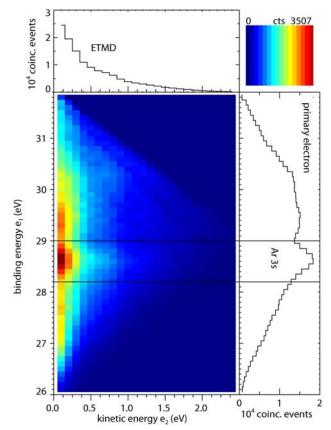


Figure 2: Color-coded map showing the intensity of electron pairs vs. binding energy of the primary electron e_1 and vs. kinetic energy of the secondary electron e_2 (central panel). The region between the two bars corresponds to primary photoelectrons from the Ar 3s shell. The energy spectrum of the primary electrons can be obtained by summation of the intensity along the e_2 axis. It is plotted in the right hand panel, where the 3s photoline from Ar clusters is observed. An increased yield of electron pairs with a 3s primary electron, and a secondary electron of very low kinetic energy, can be seen in the central panel. The energy spectrum of the secondary electron in the region marked by the two horizontal bars can be obtained by summation of the intensity along the e_1 axis, and is plotted in the right hand panel.

We have performed an experiment, in which the ETMD process sketched in figure 1 has been shown in larger, mixed Ar-Kr systems. Generally, noble gas clusters can be produced by expansion of the gas through a small, conical nozzle under a high pressure into vacuum. Clusters form by three-body collisions and subsequent aggregation in the nozzle. Under suitable conditions, expansion of a gas mixture, so-called co-expansion, leads to formation of mixed clusters. For Ar-Kr mixtures, these consist of a Kr core, which is covered by one or a few outer layers of Ar. The electron-electron coincidence spectrum from Ar-Kr mixed clusters after photoionization with a photon energy of 32 eV is shown in figure 2. At this photon energy, the majority of photoionization events lead to emission of only one outer valence electron, from the Kr 4p or Ar 3p shell. In figure 2 this part of the spectrum does not show up, as we consider only the detected electron pairs. Electron Transfer Mediated Decay is one of the processes, which contribute to electron pair emission. The Figure shows a clear increase in the number of secondary electrons recorded when the energy of the primary electron corresponds to that of Ar 3s photoemission. We attribute this to ETMD (Förstel et al, Phys. Rev. Lett. 106, 033402 (2011), which so far has only been predicted theoretically. In a control experiment on pure Ar clusters, no emission of secondary electrons related to 3s photoionization has been observed. Charge transfer processes in chemistry conventionally are thought to arise when fluctuations in the nuclear coordinates make Franck-Condon like transitions between two different configurations possible, or when tunneling, called 'hopping' in this context, occurs.

Other Studies

Several other projects have been carried out successfully, but cannot be covered in detail here. Briefly, for water clusters we have investigated the dependence of the ICD energy spectrum on cluster size. First information on the interplay of ICD with the nuclear dynamics in larger clusters was gathered by a comparison of water to deuterated water clusters. Non-local autoionization (ICD and ETMD) was also shown in two other types of mixed noble gas clusters, ArXe and NeKr. Photoionization of hydrogen still continues to be a benchmark for theory. Surprisingly, this photoelectron spectrum has never been recorded with vibrational resolution over an extended range of energies. We have measured the pertaining spectra using our magnetic bottle set-up. Finally, as a test for our FEL experiments we have qualified our spectrometer by recording photoelectrons from a negatively charged ion beam using an optical laser for excitation.

ETMD is a charge transfer process produced solely by electron correlation, and its discovery may lead to a change in paradigm.

Scientific Staff

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Astrophysics and Laboratory Plasma Studies (ALPS)

Heads: Prof. Dr. Günther Hasinger, Dr. Mara Salvato

Laboratory Experiments

During experiments at the WEGA stellarator in Greifswald, high energy emission was originally detected outside the torus by X-Ray dosimeters. The quantity of this emission was significant during a) OXB-mode conversion experiments with the 28 GHz ECRH and b) lower hybrid heating sce-

narios with an additional non-resonant 2.45 GHz heating system. Using the Silicon Drift Diode (SDD) sensors, which we originally had tested on ASDEX Upgrade (provided by the HLL and the PNSensor and PNDetector companies), we have been able to study and quantify this emission in detail. Two detectors were used: first a 450 µm thick SDD with Al-coated entrance window behind an 11 µm beryllium filter suitable for the detection of soft X-Rays (0.8 keV to 30 keV) placed inside the WEGA vacuum chamber. The spectrum obtained with this detector while applying OXB-mode ECRH (see figure 1, top) showed a continuum together with line emission from Ar, Cr, Fe, Cl and S.

kT_{e,Sup} = 5 keV

Fe K_α

Ar K_α

Cr K_α

Data + Model
(Bremsstrahlung)

102

Energy (keV)

Energy (keV)

Figure 1: Confirmation of the super-thermal electrons during the LH heating (#35609) at WEGA, Greifswald, observed with new X-ray SDD PHA system developed at ASDEX Upgrade. The emission lines produces by the impurities are also indicated (top). Hard X-ray spectrum obtained at WEGA with the new SDD detector (bottom).

The "Astrophysics and Laboratory Plasma Studies" (ALPS) was established in November 2009. Half of the group is currently testing X-ray detectors conventionally used in X-ray space astronomy while the other half is occupied in studying the properties of galaxies hosting an Active Galactic Nuclei (AGN), one of the most powerful sources of X-ray emission in the Universe. Our work is done in close collaboration with the HLL and MPE.

Assuming a thermal Bremsstrahlung continuum, an electron temperature of 10.8 keV could be derived. However, a simple power law is an even better description of the spectrum. Since the bulk temperature of the electrons in the WEGA is only of the order of a few 10 eV, it is immediately clear that this high-energy emission has to originate from a supra-

thermal population of electrons. The emission lines are produced by impurities originated from the steel parts inside the vessel (Cr, Fe), from rest gas of other discharges (Ar) and possibly the cleansing of the vessel (Cl, S). For the detection of Hard X-Rays (20 keV to few 100 keV) a second sensor consisting of a cylindrical CsI(Tl) scintillator crystal (5 mm height, 5 mm diameter) coupled to a Silicon Drift Diode was used outside the WEGA vacuum vessel. During lower hybrid heating scenarios in helium plasma discharges an emission of up to several 100 keV was detected (see figure 1, bottom). The spectral shape of this emission could not be determined in more detail due to the large soft X-ray absorption of the setup. However, more tests with an advanced imaging hard X-ray detector inside the vessel are planned for the future. In addition, we are currently planning a set of experiments using the new detector for particle induced X-ray (PIXE) and gamma-ray (PIGE) analysis at the 3MeV tandem accelerator in Garching.

Astrophysics

In the recent years it has become obvious that AGN are a key, possibly recursive, phase of the evolution of almost every galaxy. AGN trace the growth of supermassive black holes in the nuclei and provide important energetic feedback to their hosts and the intergalactic medium. Thus, the complete census of AGN and the detailed characterisation of their properties is of paramount importance to improve our understanding of the evolution of the Universe. In particular, the actual distance (redshift) of the AGN is extremely important and at the same time very time consuming to be directly obtained at the telescope via spectroscopy, as the majority of the galaxies hosting an AGN is very distant and thus faint. Our group is involved in improving the determination of the distance using a secondary method called "Photometric Redshift" fitting precise multiband photometry to the spectral energy distribution (SED) of known sources hosting AGN. We successfully managed to obtain photometric redshifts with a precision competitive with very low resolution spectroscopy (see figure 2). This was obtained also by taking into account the AGN variability and carefully selecting the templates used for the comparison.

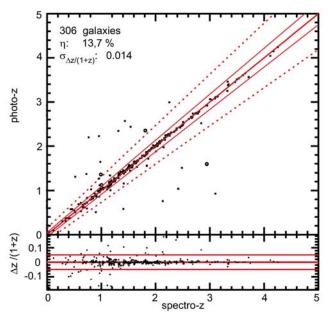


Figure 2: Comparison between photometric redshift and actual (spectroscopic) redshift for a sample of AGN. The number of sources, the fraction of outliers (η) and the accuracy (σ) are indicated. From Salvato et al. (2011), submitted.

The method is at the moment applied to the CHANDRA-COSMOS and Lockman Hole surveys, which are among the best-studied sky fields at any wavelength. When an accurate redshift is known, it is possible to use the spatial clustering of AGN to put constraints on how the AGN are triggered and fuelled and to understand how galaxies and AGN co-evolve.

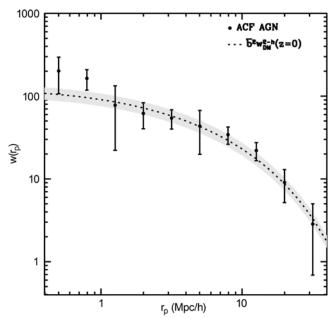


Figure 3: Projected AGN correlation function $w_p(r_p)$ (black circles) compared to the projected 2-halo term $b_{AGN}^{\ \ 2} w_{DM}^{\ \ 2-h}(r_p)$ (grey region), where b_{AGN} is the AGN bias respect to the DM distribution and is the DM 2-halo term evaluated at z=0. From Allevato et al. (2011), submitted.

The statistics commonly used to measure the clustering properties of AGN is the two-point projected correlation function (see figure 3), which relates clustering properties of AGN to typical mass of dark matter (DM) halos, in which they reside and allow various types of AGN to be placed in a cosmological context. Modeling the AGN correlation function with the 2-halo term, we studied the redshift evolution of the projected correlation function of 593 X-ray selected AGN extracted from the 0.5-2 keV X-ray mosaic of the XMM-COSMOS survey. We found evidence of a redshift evolution of the bias factor for X-ray selected AGN up to z<2 with an average mass of the DM hosting halos that remains constant over time. Another line of investigation is aimed at global, statistically significant characterisations of the physical properties of AGN hosts in the COSMOS field.

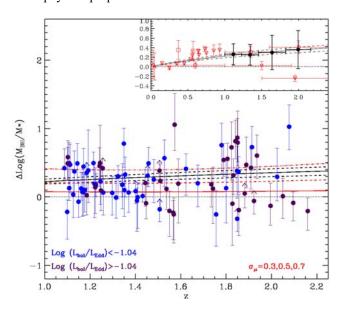


Figure 4: Redshift evolution of the offset measured for zCOSMOS type 1 AGN from the local MBH-M* relation. Black lines show the best fit obtained assuming an evolution of the form $\Delta Log(MBH/M^*)(z)=(0.68\pm0.12)Log(1+z)$. Red lines show the bias due to the intrinsic scatter in the scaling relations to be expected even if they are universal. In the inset, we show a comparison of our data (black circles) with data from the literature. From Merloni et al. (2010).

For the sub-sample of broad-line AGN, for which black hole masses can be estimated through the measure of the broad lines width, we show that the local scaling relation between BH and host stellar masses must have evolved at 1<z<2, either in normalisation or in intrinsic scatter. At the observed growth rates, the requirement that high redshift QSOs will evolve onto the locally observed scaling relations put additional constraints on the lifetimes and duty cycles of quasar activity.

Scientific Staff

V. Allevato, J. Belapure, S. Fotopoulou, G. Hasinger, B. Huber, A. Merloni, M. Salvato.

University Contributions to IPP Programme

Cooperation with Universities

Author: Dr. Udo v. Toussaint

Teaching and Mentoring

Teaching plasma physics at various universities has a long tradition at IPP. Since fusion-relevant physics and engineering are not the most prevalent subjects in Germany's academic landscape, IPP is interested in sparking students' interest in high-energy plasma physics and other fusion-relevant fields. In

2010, 22 members of IPP taught at 9 universities or universities of applied sciences: Many members of the IPP staff are Honorary Professors, Adjunct Professors or Guest Lecturers at various universities and give lectures on theoretical and experimental plasma physics, fusion research, data analysis and materials science. The table gives an overview.

University Members of IPP staff University of Greifswald Dr. Hans-Stephan Bosch Dr. Andreas Dinklage Prof. Olaf Grulke Prof. Per Helander Prof. Thomas Klinger Dr. Heinrich Laqua Technical University of Munich Prof. Sibylle Günter Dr. Klaus Hallatschek Prof. Thomas Hamacher Prof. Günther Hasinger University of Munich Dr. Jörg Stober Prof. Hartmut Zohm Dr. Ralph Dux University of Augsburg Prof. Ursel Fantz University of Ulm Dr. Emanuele Poli Dr. Frank Jenko Dr. Jeong-Ha You Dr. Udo v. Toussaint Technical University of Graz Dr. Rudolf Neu University of Tübingen Dr. Wolf-Christian Müller-University of Bayreuth Nutzinger Dr. Wolfgang Suttrop University of Gent Prof. Jean-Marie Noterdaeme

Table: IPP staff who taught courses at universities in 2010.

The teaching programme has been highly successful over the years and many students who first came into contact with plasma physics through lectures given by IPP staff have later done thesis work and even taken up a career in the fusion research. Lecturing at and cooperation with universities are supplemented by IPP's Summer University in Plasma Physics: one week of

Many important goals in plasma physics, technology and materials science have to be attained on the way to a fusion power plant. Since this process will last another generation, IPP attaches great importance to training young scientists. Close interaction with universities in teaching and research is therefore an important part of IPP's mission. Moreover, joint projects with several universities form an integral part of IPP's research programme.

lectures given by IPP staff and lecturers from partner institutes providing detailed tuition in nuclear fusion – in 2010 for the 25th time at Garching. Most of the participants were from Europe but the number of participants from abroad is steadily increasing. Some of them are taking part in the "European Doctorate in Fusion" programme. A "European Doctorate" title is awarded to

PhD students in parallel to a conventional one. This requires spending a significant part of the work on their subject at another European university or research centre. The European Doctorate in Fusion was initiated three years ago. At present institutions in Germany, Italy (EURATOM Association Consorzio RFX Padova and the University of Padua), and Portugal (EURATOM Association IST) are supporting this programme.

The international character of fusion research is also reflected in the countries of origin of graduate students at IPP: onefifth of the postgraduates and approximately two-thirds of the postdocs are from abroad In the year 2010 a total of 60 postgraduates were supervised, 12 of them successfully completing their theses.

Joint Appointments, Grown and Growing Cooperation

IPP cooperates closely with some universities in the form of joint appointments. In 2010 there was a joint appointment with the Technical University of Berlin of Prof. Wolf in the field of plasma physics/stellarator optimisation.

A second W2-appointment in the field of plasma astrophysics is expected to take place in 2011.

In December 2009, IPP and the Technical University of Munich contracted to intensify cooperation: Three joint professorships were agreed on fusion-relevant research fields of plasma edge and divertor physics, plasma-wall interactions, and numerical methods in plasma physics. The appointment process is actively pursued.

Annother example of very close cooperation with universities is that with Stuttgart University by virtue of its essential contributions to the development of heating systems for W7-X as well as for ITER within the Helmholtz Virtual Institute, Advanced ECRH for ITER. The development of a negative-ion source for the neutral-beam injection – selected as reference source for ITER – is being continued with Augsburg University. The collaboration, even in lecturing and practical courses, has a sound tradition.

Networking

In addition, IPP uses specific instruments developed by the Max Planck Society, the Helmholtz Association, Deutsche Forschungsgemeinschaft (DFG), Leibniz-Gemeinschaft or the German government for more intensive networking with universities on a constitutional basis – partly in conjunction with non-university research partners and industrial partners.

Organisation of or participation in graduate schools:

- the International Max Planck Research School on Bounded Plasmas at Greifswald in cooperation with Greifswald University,
- the International Leibniz Graduate School for Gravity Waves and Turbulence in the Atmosphere and Ocean started 2008 in cooperation with Leibniz Institute of Atmospheric Physics, Kühlungsborn, Leibniz Institute for Baltic Sea Research, Warnemünde, and Rostock University.

Young investigators groups:

- Helmholtz Young Investigators Group, Theory and Ab Initio Simulation of Plasma Turbulence, headed by Dr. Frank Jenko, in cooperation with Münster University,
- European Young Investigator Award Group, Zonal Flows, headed by Dr. Klaus Hallatschek,
- Helmholtz Russia Joint Research Group, Hydrogen Behaviour in Advanced and radiation damaged materials for fusion applications, headed by Dr. Matej Mayer as Helmholtz Principle Investigator and Dr. Alexander V. Spitsyn, RSC Kurtschatov Institute.

Research partnerships:

- participation in the DFG Collaborative Research Centre Transregio 24, Fundamentals of Complex Plasmas, together with Greifswald University, Kiel University and Leibniz Institute for Plasma Science and Technology, Greifswald,
- Helmholtz Virtual Institute, Advanced ECRH for ITER, together with the University of Stuttgart and Karlsruhe Institute of Technology (merging of the former and Karlsruhe Research Centre and University of Karlsruhe).

Participation in Clusters of Excellence in the context of the German government's Excellence Initiative in cooperation with Ludwig Maximilian's University and Technical University Munich:

- Munich Centre for Advanced Photonics, together with Universität der Bundeswehr München, Max Planck Institute of Quantum Optics, Max Planck Institute for Extraterrestrial Physics, Semiconductor Laboratory and Max Planck Institute of Biochemistry as scientific partners and Siemens AG/Healthcare as industrial partner,
- Origin and Structure of the Universe, together with Max Planck Institute for Astrophysics, Max Planck Institute for

Extraterrestrial Physics, Semiconductor Laboratory and Max Planck Institute for Physics and the European Southern Observatory.

A few years after its formation IPP joined the European Fusion Development Agreement as a EURATOM Association. When the decision was made to build ITER, it became clear that training of young scientists and engineers had to be intensified. A European Fusion Education Network (FUSENET) was therefore formed in FP7. FUSENET consists of 14 EURATOM associations – one of them IPP – and 22 universities from 18 European countries. FUSENET provides education material and training opportunities in fusion science and technology covering all education levels, from secondary school through Bachelor and Master level to PhD.

University of Augsburg Lehrstuhl für Experimentelle Plasmaphysik

Head: Prof. Dr.-Ing. Ursel Fantz (acting)

Low Temperature Plasmas

Helicon-like discharges (rf frequency 13.56 MHz, Helmholtz coils with an axial magnetic field up to 150 mT) in hydrogen and deuterium have been established to explore their feasibility as plasma driver in ion sources for negative hydrogen ions. They could replace the inductive rf-coupling used in the IPP prototype ion

source for the ITER neutral beam systems promising higher rf-power efficiency as well as higher atomic hydrogen and positive hydrogen ion densities. In contrast to classical helicon discharges, which operate in rare gases using long and thin vessels, the helicon mode must be achieved in hydrogen and deuterium using an aspect ratio close to one. Figure 1 compares the axial averaged density ratio of atoms to molecules in H₂ and D₂ plasmas (vessel: 10 cm diameter, 40 cm length) obtained by emission spectroscopy. Obviously, a higher dissociation is achieved in deuterium than in hydrogen and a peak at low magnetic field is obtained followed by an almost linear increase. The peak in D₂ becomes even more pronounced with increasing power and is also observed in the vibrational and gas temperature as well as in the total plasma emission. In comparison to the standard ICP configuration the density ratio is typically increased by a factor of five, which demonstrates the high potential for the usage of this kind of discharge as driver in ion sources. Further investigations will follow subsequent to this diploma thesis in the framework of a PhD thesis.

A planar coupled ICP experiment at a frequency of 27.12 MHz and up to 600 W power is used for systematic investigations on hydrogen and deuterium plasmas in a pressure range of 0.5 to 20 Pa. Helium is routinely added to actively change the plasma parameters. Profiles of electron density and temperature are

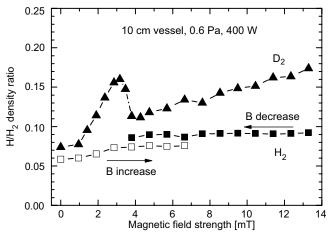


Figure 1: Atomic to molecular hydrogen density ratio in hydrogen and deuterium plasmas using a Helicon-like discharge (ICP with magnetic field).

The research at the University of Augsburg is concentrated on diagnostics of molecular low temperature plasmas, on investigations of plasma chemistry and on plasma surface interaction studies. For that purpose several different low pressure plasma experiments are available. Focus is laid on the development and application of diagnostic methods for negative hydrogen ion sources, which is carried out in close collaboration with the Technology Division of IPP.

obtained with a Langmuir probe system. Atomic and molecular hydrogen densities as well as rotational and vibrational temperatures are obtained from atomic and molecular hydrogen lines; the CR models for H and H₂ are continuously updated. The plasma characterisation is being completed by an energy resolved mass spectrometer for measuring densities of neutrals and ions as well

as ion energies. The densities of hydrogen ion species in a hydrogen/helium mixture are compared to results from a 0-dim dissociation and ionisation model using the flexible solver Yacora. In some cases a good agreement is observed, however in other cases not. Based on such measurements, the model will be further improved and benchmarked in order to receive reliable predictions of the positive ion distribution in hydrogen ion sources. The CR model for molecular nitrogen (see Annual Report 2009) has been improved. To reflect the measured emission from the 1st positive system of nitrogen (B³ $\Pi_a \rightarrow A^3 \Sigma_u^+$) in argon low-pressure arc discharges a collision induced transition from the A- to the B-state had to be considered, where the inducing collision-partner can either be a nitrogen molecule or an argon atom: $N_2(A)+M \leftrightarrow N_2(B)+M$ (M=N₂, Ar). Using this modified CR model and experimental determined plasma parameters the intensity of the molecular nitrogen emission can now be simulated for a wide parameter space of gas mixture $(0.1 \% \text{ N}_2 \text{ in Ar to } 100 \% \text{ N}_2)$, absolute pressure $(10^{-1}-10^2 \text{ mbar})$ and discharge current (100-500 mA).

Diagnostics for Negative Hydrogen Ion Sources

Experimental campaigns at the IPP test facilities for negative hydrogen ions (see ITER contributions) showed a high relevance of the caesium dynamics for the ion source performance. Key issues are the routine achievement of high, uniform and stable negative ion current densities accompanied by a low co-extracted electron current. Caesium is used for an effective conversion of atoms and positive hydrogen ions into negative ions at surfaces close to the extraction system. The control and monitoring of caesium dynamics is strongly supported by basic investigations in the lab.

As reported last year, a diode laser absorption system on the cesium D_2 transition (852 nm) for monitoring Cs densities has been validated at EPP. The benefit of such a system is – besides its perfect suitable dynamic range – the fact that it is applicable during both plasma and vacuum operation. This system has been transferred to the BATMAN test facility and implemented as a routine on-line diagnostic method. First very interesting results have been obtained already giving an insight into the Cs dynamics.

Figure 2 shows a typical time trace of the neutral Cs density in a line-of-sight parallel to the convertor surface at a distance of 2 cm. The signal of the Cs line emission is shown for comparison (plasma only). Three phases are to be seen: (i) the vacuum phase before the plasma pulse reflects a stable neutral Cs density, (ii) the plasma phase, in which the neutral Cs density stays at the same level although more than 90 % of the Cs is singly ionised, which means that a huge amount of Cs is released from the surfaces by the plasma and (iii) the vacuum phase after the plasma pulse, which implies the recombination of the ions and the time constant for transport and sticking of Cs at the surfaces. During Cs conditioning of the source a steady increase of the Cs density is measured until a saturation level is achieved. The saturation seems to be correlated with a high source performance. In-detail studies of the Cs dynamics by laser absorption are one of the high priorities for the next experimental campaign at BATMAN.

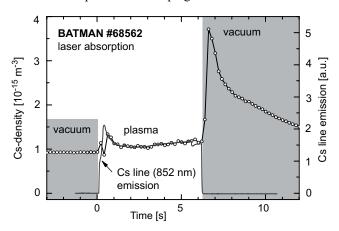


Figure 2: Temporal evolution of the neutral caesium density before, during and after a hydrogen discharge in the IPP prototype ion source (BATMAN test facility) as measured by the laser absorption spectroscopy technique.

To monitor the evaporation rate of the currently used liquid caesium ovens, a surface ionisation detector (SID) mounted directly in front of the oven nozzle (therefore called oven SID) was investigated. Showing good agreement with absorption spectroscopy and an established local SID, this oven SID gives the opportunity for a feed-back-controlled evaporation. In order to overcome the prevailing issues arising from the high reactivity of the pure caesium with impurities of the background gas in the liquid Cs ovens at IPP, Cs compound dispensers were investigated. Besides the well-known chromate dispensers new alloy dispensers have been tested showing a better stability and a reproducible evaporation.

Subsequent to the successful realisation of the laser photodetachment diagnostic in an ECR plasma experiment, the volume process of negative ion production has been systematically investigated. In order to reduce the destruction of negative ions the hot plasma region is separated by a meshed grid from the cold part, in which the measurements take place.

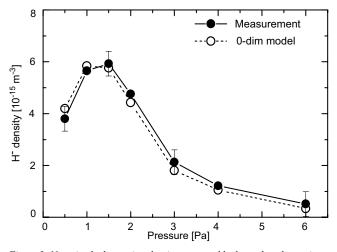


Figure 3: Negative hydrogen ion density measured by laser detachment in an ECR discharge compared to results from a 0-dim particle balance model.

As shown in figure 3 a strong pressure dependency of the H-density is obtained; the maximum at about 1.5 Pa represents a ratio of negative ions to electrons of about 16 %. Using the general plasma parameters measured by means of a Langmuir probe and OES, a particle balance for ion production and destruction has been established. The excellent agreement with the measurements allows for an analysis of potential improvements of the volume generation process in this experiment. Further steps will be the quantitative investigation of the enhancement of negative ion production by different surfaces at relevant ion source parameters to investigate alternatives to caesium.

Diploma and PhD Theses

R. Gutser: Experiments and Simulations for the Dynamics of Cesium in Negative Hydrogen Ion Sources for ITER N-NBI. (PhD Thesis)

S. Dietrich: Verifikation von optischen Diagnostikmethoden an H₂/D₂-Plasmen. (PhD Thesis)

P. Schmidt: Verdampfung von Cäsium und dessen Einflüsse auf Austrittsarbeiten von Oberflächen und Wasserstoffplasmen zur Optimierung von negativen Ionenquellen. (Diploma Thesis)

C. Wimmer: Laserabsorptionsspektroskopie zur Quantifizierung von Cäsium. (Diploma Thesis)

D. Ertle: Teilchendichten in HF-angeregten Wasserstoff- und Deuteriumplasmen. (Diploma Thesis)

B. Ruf: Cäsium- und Plasmahomogenität in großflächigen Quellen zur Erzeugung von negativen Wasserstoffionen. (Diploma Thesis)

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University of Bayreuth Lehrstuhl für Theoretische Physik V

Head: Prof. Dr. Arthur G. Peeters

In the frame of the collaboration between IPP

Cooperation

In June 2010 the University of Bayreuth opened a new Chair researching the physics of high temperature plasmas. The Chair is financially supported by the University, the 'Volkswagen-Stiftung', through a Lichtenberg Professorship for Prof. A. G. Peeters, and the IPP. Through

and the University of Bayreuth, research projects on nonlinear dynamics and computational physics are carried out. They include the study of turbulent dynamics around a magnetic island, of the influence of the centrifugal force on plasma turbulence, of electromagnetic effects within the global plasma description and of toroidal momentum transport.

and, consequently, lead to radial transport of particles and energy. The potential structure inside the island leads to an enhanced radial transport across the island, which can compete with the transport along the perturbed magnetic field. The potential structures show a complex behaviour, being non stationary in time.

this Chair the University and the IPP continue and strengthen their long term collaboration, in particular in the areas of nonlinear dynamics and computational physics. Both these areas are central in the research at the IPP and the close collaboration will also give input to the research conducted in Bayreuth. The dedication to the collaboration is clearly expressed through the involvement of two IPP employees, PD Dr. W. Suttrop and PD Dr. W.-C. Müller, in the teaching at the University. It is also evident from the multiple collaborative projects between the University and the IPP. In 2010 these projects resulted in six publications with shared co-authorship. Two examples, the turbulent dynamics around a magnetic island and the influence of the centrifugal force on plasma turbulence, are discussed in some detail below. Other, equally successful projects exist, like the study of electro-magnetic effects within the global plasma description, and the study of toroidal momentum transport, but are not reviewed here.

Island Dynamics

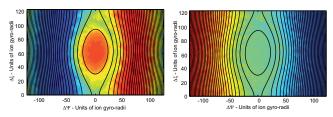


Figure 1: Electro-static potential (left) and total density (right) in the radialbinormal plane. The dashed line gives the (stationary) island.

Magnetic island formation plays an important role in fusion plasmas. One of the long outstanding questions is the interaction between small scale turbulence and meso-scale magnetic islands. Turbulence around a static magnetic island has been computed including, for the first time, the effect of kinetic electrons. The consistent physics description of the electrons allows electrostatic perturbations to develop that are constant on the perturbed magnetic flux surfaces. Indeed, as shown in figure 1, large scale potential structures develop that coincide with the island structure. These structures are similar to the zonal flows found in plasmas without islands. However, the potential structures in the case with an island have a finite toroidal wave number

High Mach Number

At high Mach number the centrifugal force must be retained in the description of instabilities and turbulence. The force enhances the mirror force, modifies the trapping condition as shown in figure 2, and redistributes the density over the flux surface. At intermediate scales the enhanced trapping can result in the promotion of the trapped electron mode over the ion temperature gradient (ITG) mode. The increased fraction of slow trapped electrons enhances the convective particle pinch, leading to an increase in the steady state density gradient. Linear ITG mode results show an increased pinch of heavy trace impurities due to their strong centrifugal trapping.

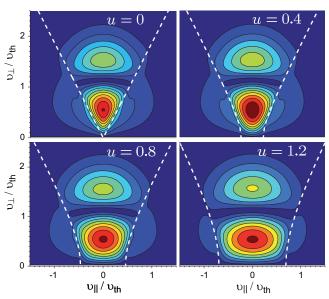


Figure 2: The perturbed electron distribution in velocity space for a trapped electron mode at the outboard midplane with increasing toroidal Mach number. The trapped-passing boundary is shown as a dashed line.

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Ernst-Moritz-Arndt University of Greifswald

IMPRS "Bounded Plasmas"

Head: Prof. Dr. Thomas Klinger

The International Max-Planck-Research School "Bounded Plasmas", jointly run since 2001 by IPP, the Institute for Physics of the Ernst-Moritz-Arndt University (IfP) and since 2003 also the Institute for Low-Temperature Plasma Physics (INP), provides

an international framework for education and research of highly qualified PhD students in the field of plasma physics. Currently, 24 PhD students are member of the IMPRS. As shown in figure 1 the members are generally equally distributed over IPP and the other two institutions with a total fraction of non-German students of 44 %. Research results are communicated in a weekly graduate colloquium, which also fosters collaborations across the individual PhD projects. In addition to the university curriculum advanced education in specialised plasma physics fields is provided by guest lecturers. In total 47 guest lectures have been realised, two in 2010. The excellent research conditions are also expressed in the average duration of the PhD projects of 3.2 years, which is well below the German university average.

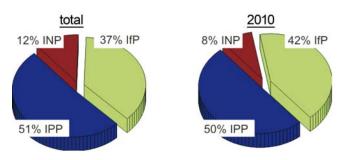


Figure 1: Distribution of PhD students over institution for the total period (left) and for the year (right).

Particle Modelling of Plasma Thrusters

Head: Prof. Dr. Ralf Schneider

Within the DLR project 50RS0804 particle-in-cell models, originally developed for fusion applications, are applied to ion propulsion systems in collaboration with Prof. Dr. Ralf Schneider at the Ernst-Moritz-Arndt University in Greifswald. Ion propulsion gets more and more attractive for satellites due to the larger exit velocity compared with chemical propulsion allowing weight reductions of some 100 kg. Developments of ion propulsion systems are dominated by empirical testing of prototypes. Advances in the physics models for plasmas in contact with walls and in computing create new chances for numerical optimisation and cost reduction by a smaller number of prototypes. The interaction of the plasma with the walls and

The key element of the cooperation with the Ernst-Moritz-Arndt University Greifswald is the education within the framwork of the "International Max-Planck Research School", successfully operated since 2001. Another scientific collaboration is performed in the field of plasma propulsion, where dedicated particle-incell simulations are performed. This is considered as an important plasma science spin-off.

its influence on the performance as well as fluctuation-induced transport processes are key elements for a better physics understanding, as also in fusion plasmas. The DLR project is realised in close collaboration with Thales Electron Devices GmbH Ulm to develop and validate a modular Particle-in-Cell (PIC) code for the simulation of so-

called HEMP-Ts (high efficiency multistage plasma thrusters). The 2d3v RZ PIC code was used to study and compare two different thruster concepts – Hall effect thruster (HET) and HEMP-T. The simulations demonstrated that in the HEMP thruster the plasma contact to the wall is limited only to small areas of the magnetic field cusps, which results in much smaller ion energy flux to the thruster channel surface as compared to HET.

The erosion yields for dielectric discharge channel walls of HET and HEMP thrusters were calculated with the binary collision code SDTrimSP. For the HET the erosion rate on level of 1 mm of sputtered material per 1000 hours was observed. For HEMP thruster the simulations have shown that there is no erosion inside the dielectric discharge channel.

The electron current in the thrusters with a strong magnetic field is defined by fluctuations driven anomalous transport. The electron transport model based on Bohm-like diffusion was developed and tested in collaboration with PPPL. The model results have shown a good agreement with measurements for PPPL 100 W cylindrical hall thruster (CHT).

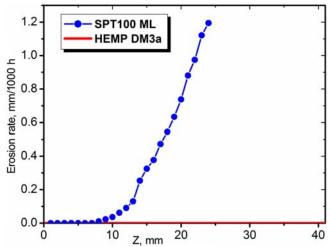


Figure 2: The erosion rate for the dielectric discharge channel wall of the HEMP DM3a thruster and for the inner wall of HET (SPT100 ML) as calculated with SDTrimSP.

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Technical University of Munich Lehrstuhl für Messsystem- und Sensortechnik Head: Prof. Dr.-Ing. Dr. h.c. Alexander W. Koch

Introduction

Speckle interferometry (SI) is a powerful tool that can be used for fast, robust and noncontact measurement of deformation, vibration, roughness or shape and derivable quantities. In each case the accuracy of measurement is depending on the measurement setup and its components, the environmental conditions while

There has been a continuous cooperation of IPP and Technische Universität München in the past. Next to thermography measurement techniques and thin film interferometry, speckle interferometry has always been a shared field of research. Speckle measurement techniques can be used to detect arc traces, deformation, erosion, surface roughness, surface structure and surface contour of the inner wall and the divertor region of experimental fusion devices.

it is only valid as long as both wavelength λ_1 and λ_2 are nearly equal. Figure 1 shows four different phase images, each produced by a speckle simulation tool [3] modeling a Mach-Zehnder speckle interferometer with a plane measurement surface (with a given roughness σ) tilted with respect to a reference mirror.

performing the measurement and the device under test itself. Most applications in the field of SI aim at measurements of a single quantity (e.g. shape): influences on the measurement result due to vibrations or material property of the surface under test are reduced or compensated by vibration-cushioned design, algorithms or a specific choice of measurement setup and components. Our approach is not to eliminate these influences but to acquire as much information about the surface under test as possible and to increase the measurement performance by applying data fusion algorithms. Hereby, both shape and surface roughness may be measured at the same time.

Surface Shape Measurement

Both measurement of shape and surface roughness using SI depend on the used wavelengths. In case of shape measurement at least two interferograms are recorded at different wavelengths (or different angles of observation, respectively). When two wavelengths λ_1 and λ_2 are used, the obtained sensitivity is determined by the synthetic (or effective) wavelength Λ :

$$\Lambda = \frac{\lambda_1 \lambda_2}{2 \left| \lambda_1 - \lambda_2 \right|}$$

On the one hand, Λ is equal to the sensitivity of the measurement system due to separation between two adjacent fringes in the resulting phase image. On the other hand, Λ is linked to the height resolution in relation to the surface roughness σ : an increasing roughness leads to a decrease of fringe visibility. Here, a limit is given by [1]:

$$8\sigma < \Lambda$$

If Λ is chosen too small, a second effect appears: high frequency fringes appear in the phase image resulting in a misleading wrong interpretation of the phase map [2]. The origin of these additional fringes is the term of the synthetic wavelength:

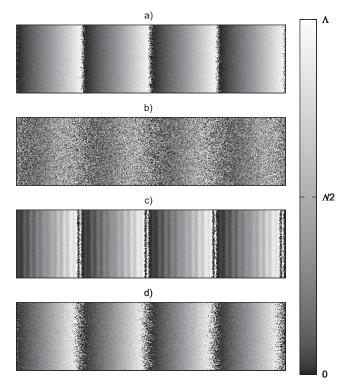


Figure 1: Results of four simulations with the following parameters: a) Λ =100 μm, σ =1 μm, b) Λ =100 μm, σ =10 μm, c) Λ =2.4 μm, σ =0.01 μm, d) Λ = 2.4 μ m, σ = 0.05 μ m. Each phase image is illustrating a plane tilted surface with respect to a reference plane. The tilt angle is chosen to show the same four fringes in each image. Due to different synthetic wavelengths and roughnesses the images have different qualities.

The simulation results are in good agreement with theory showing fringe visibility where $8\sigma << \Lambda$ (figures 1a and 1c) and almost no visibility where $8\sigma \approx \Lambda$ (figure 1b). Figure 1c shows the mentioned high frequency fringes that would lead to assume a rippled instead of a flat surface under test in this case. These additional fringes are only visible, if the surface under test is smooth. If the roughness exceeds a certain limit, fringes cannot be observed. Nevertheless, the quality of the result is still worse compared to a measurement where a small difference in wavelength was used.

Surface Roughness Measurement

There are several techniques for roughness measurement using SI: in case of surface roughness $\sigma < \lambda/4$ speckle contrast can be used to determine the roughness. If σ is above this limit the speckle contrast method cannot be applied due to fully developed speckles. A second method is angular speckle correlation (ASC). Two images of the surface under test are acquired while the angles of observation and illumination, respectively, are changed.

As mentioned above, roughness measurement using SI is also depending on the used wavelengths. A well known technique for roughness measurement using SI is the spectral speckle correlation (SSC). A camera is used to acquire at least two speckle interferograms, each using a different illumination wavelength. The correlation coefficient ρ of two acquired speckle images is an indicator for the surface roughness. A simple equation describing the relation between the correlation coefficient ρ and the surface roughness σ can be found if a certain measurement setup is used [4]:

$$\rho = e^{-(2\pi\cos(\alpha)\sigma\frac{1}{\Lambda})}$$

The following figure includes three plots for three different sets of wavelengths.

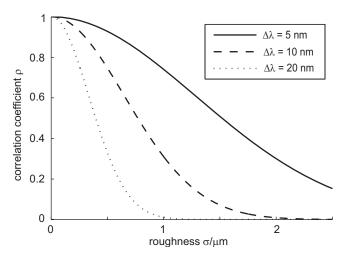


Figure 2: Relation between the correlation coefficient ρ of two acquired speckle interferograms and the surface roughness σ . The slope of this relation differs depending on the used set of wavelengths.

It is obvious that certain sets of wavelengths are more appropriate for specific regions of roughness: large differences in wavelength lead to a small region of sensitivity. In this case, the sensitivity itself is higher compared to a region with small differences in wavelength, where the slope of the function $\rho(\sigma)$ is much lower.

Data Fusion

Both measurement techniques feature a high dependency of roughness and wavelength. To our knowledge there is no system that is able to measure shape as well as surface roughness at the same time using the SI method. The performance of such a system can be increased by applying data fusion. By adding a third wavelength to the procedure, the roughness measurement can be divided into three single measurements with the wavelength sets (λ_1, λ_2) , (λ_1, λ_3) and (λ_2, λ_3) . The obtained correlation coefficients ρ_{12} , ρ_{13} and ρ_{23} can be merged with the following equation

$$\rho = c_{12}\rho_{12} + c_{13}\rho_{13} + c_{23}\rho_{23}$$

where the coefficients cii are calculated by scaling the derivation of ρ_{ij} with respect to $\sigma_{ij}.$ Using this method enables an enhanced region of sensitivity, and more reliable results. Further improvement can be achieved by taking into account the speckle interferograms and phase images from the shape measurement: the fringe contrast in SI shape measurement is an indicator for surface roughness. If the object under test features a very smooth surface ($\sigma << \lambda$) it is also possible to take into account the speckle contrast of each interferogram. The principle of data fusion is not only applicable to improve the results of roughness measurement but also the ones of shape measurement. Without any knowledge of the surface finish of the object under test, it is often not possible to discriminate measurement errors from a decline of quality in the phase image due to roughness effects. Sources for such errors can be decalibration of the setup or vibrations during measurement. Since the presented proposal improves both shape and roughness measurement using SI according simulations and measurements will be presented in near future.

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ECRH in Over-dense Plasmas

In 2010, the microwave heating system of TJ-K was upgraded. The old magnetron operating at 2.45 GHz was replaced with a magnetron, whose power can be modulated with frequencies of $50 \text{ Hz} \le f_{\text{mod}} \le 25 \text{ kHz}$. In power modulation experiments, magnetic diagnostics revealed an energy content of 20 mJ and a plasma- β

of 1.4-7.2·10⁻⁵ in low-field discharges (B₀=72 mT). Furthermore, a parametric decay instability was found in the low-field discharges, where the injected wave decays into upper hybrid oscillations and ion-acoustic and lower-hybrid waves. Figure 1a shows the spectrum in the vicinity of the heating frequency f_0 . A sideband with a continuous decay down to $f_1 \approx 2.4$ GHz can be recognised. The corresponding low-frequency component $f_2 = f_0 - f_1$ is found in the spectrum shown in figure 1b.

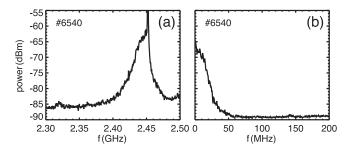


Figure 1: (a) Frequency spectrum in the vicinity of injected microwave, (b) frequency spectrum showing the corresponding low-frequency component.

The old microwave system operating at 7.9-8.4 GHz has a maximum power of 1 kW. It turned out that the achieved plasma density is too low to allow for efficient O-X-B mode conversion. Therefore, a new microwave system was bought with an increased power of 3 kW. A crucial parameter for mode conversion is the injection angle of the microwave beam with respect to the background magnetic field. In first experiment, indications for successful mode conversion at the optimum injection angle were found.

TJ-K was furthermore equipped with a new microwave heating system operating in the frequency range of 13.75-14.5 GHz. It consists of three klystrons, each capable of a maximum power output of 2.5 kW. The design process of the transmission line was completed in 2010 and its components are currently manufactured in the mechanical workshop of IPF. An optimisation and feasibility study of the O-X-B mode conversion heating scenario has been started in 2010 for the Pegasus Toroidal Experiment with the full-wave code IPF-FDMC. This study is performed in preparation of heating experiments and will be continued in 2011.

The joint program between IPF and IPP on ECRH systems for AUG, W7-X, and ITER as well as contributions to the experimental program of AUG can be found on the respective pages of this report. Here is summarised the part of the program carried out at IPF: the development of new mm-wave components, investigations of plasma waves and turbulent transport. Experiments are carried out on the torsatron TJ-K, which is operated with a magnetically confined low-temperature plasma.

Global Turbulence and Confinement Studies

Studies from 2009 on drift-wave (DW)/zonal-flow (ZF) interactions were continued. Further analyses of data from the poloidal 128-pin Reynolds stress probe array showed an increase in the drive of kinetic ZF energy, when background flows are imposed externally by plasma biasing.

This suggests that sheared background seed flows could serve as a trigger mechanism of turbulence generated ZFs. The temporal behaviour of DW and ZF enstrophy showed that the interplay between small-scale DW turbulence and large-scale ZFs follows a predator-prey mechanism. First indications for spontaneously driven ZFs in TJ-K were observed in limited discharges.

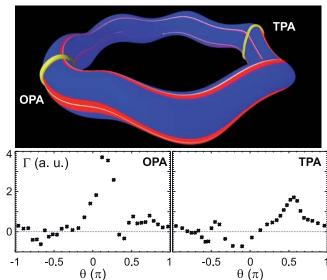


Figure 2: Top: 3D turbulent structure mapped onto a flux surface. Bottom: Turbulent transport measured with poloidal outer (OPA) and top port array (TPA).

The 3D structure of DW turbulence was studied with a pair of poloidal probe arrays set up at variable toroidal positions. Correlation analyses between these positions revealed that the structure is aligned with the field lines with a length of $L_{\parallel}\approx 3$ m and a speed $v_{\parallel}\approx 500$ km/s between ion-sound and Alfvén velocity. Poloidally it forms an m=4 mode corresponding to $\iota\approx 1/4$. The perpendicular dynamics was found to agree with first results from fast imaging. Local maxima in the turbulent transport were found in unstable regions of negative normal curvature, which in TJ-K is wound helically (figure 2, bottom). They agree with locations of maximum linear growth rates calculated in TJ-K geometry using the new magnetic configuration code.

Ion temperatures of up to 1 eV were measured by LIF and passive spectroscopy. An ion-power balance was set up. Evidence for turbulent heat transfer from electrons to the ions was found. To measure the emitted radiative power, an 8-channel bolometer was put into operation. The numerical reconstruction of radial emission profiles from the line-integrated signals is in progress.

Simulations of a Plasma-filled Horn Antenna

The investigation of metamaterials in physics, electromagnetics and optics in the last years resulted in many improvements of different devices. In the field of microwave antennas, the phenomenon of gain increase of a shortened horn antenna by embedding a wire-medium-based slab was reported in several papers. The simulation of the wire-media with a homogenised model (ENZ slab, described with Drude dispersion) showed that it is feasible to replace the wire media with a cold plasma inside the horn. Whereas the plasma frequency of the wire media is determined with the diameter of the wires and their distances, the resonant frequency of the plasma can be controlled with the plasma density. This opens new possibilities for optimisation of the horn properties for different frequencies, due to the simultaneous tuning of the plasma density. The numerical investigation of electromagnetic wave propagation in plasma filled horn and the influence of the plasma properties on the radiated field distribution is shown in figure 3. Without plasma (top), the beam divergence is large and the phase fronts are strongly curved. With a homogenous plasma (bottom) at 95 % cut-off density, the phase fronts are nearly planar and the beam is much more narrow.

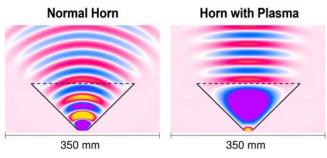


Figure 3: Electric field E_x of the horn antenna in vacuum (top) and filled with a plasma near the cut-off density of the wave (bottom).

Reflectometry Simulations with IPF-FD3D

The finite-difference code IPF-FD3D is a fullwave code that solves Maxwell's equations and the electron equations of motion in a cold plasma. It is used for a variety of applications, including the plasma-filled horn antenna, Doppler reflectometry, and remote steering optimisation. It is continually enhanced and upgraded. In a diploma thesis, a set of new solvers for the plasma currents in the presence of a magnetic background field was implemented and tested.

The most useful algorithm was determined to be the Crank-Nicolson solver. Its advantages over the previously used symplectic solver are improved stability in the transition region from vacuum to plasma, and in the presence of strong fluctuation gradients. It is also more accurate than the symplectic, in that it does not introduce a small anisotropy in the current components. Furthermore, the computational requirements are only moderately increased over the symplectic solver. There are ongoing benchmarking efforts within the European Reflectometry Code Consortiums (ERCC) to prove the correctness of the codes that are in use within the ERCC. Figure 4 shows the result for O mode of ERCC benchmark scenario "Case 1", where a microwave beam hits a plasma with an embedded sinusoidal density fluctuation whose phase is varied from 0 to 2π . Comparisons between the codes used by ERCC members show some agreement and some disagreement, and it is currently being discussed how the different simulation methods used within the various codes effect these differences. Activities within the Integrated Tokamak Modeling (ITM) task force under ID WP10-ITM-EDRG-ACT6 have been continued. The European 3D reflectometer code for use on ITER is to be ported to the ITM computers. Work has commenced on integrating the CPO interface (consistent physical objects), which ensure compatibility between the diverse ITM codes

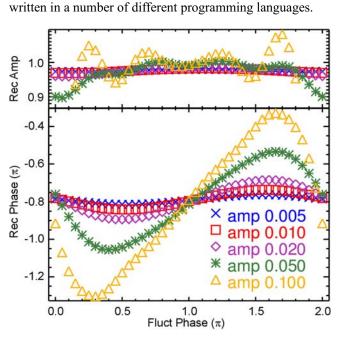


Figure 4: Amplitude and phase of the received signal as a function of the position of the fluctuation ("Case 1" ERCC benchmark scenario using IPF-FD3D).

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Teams

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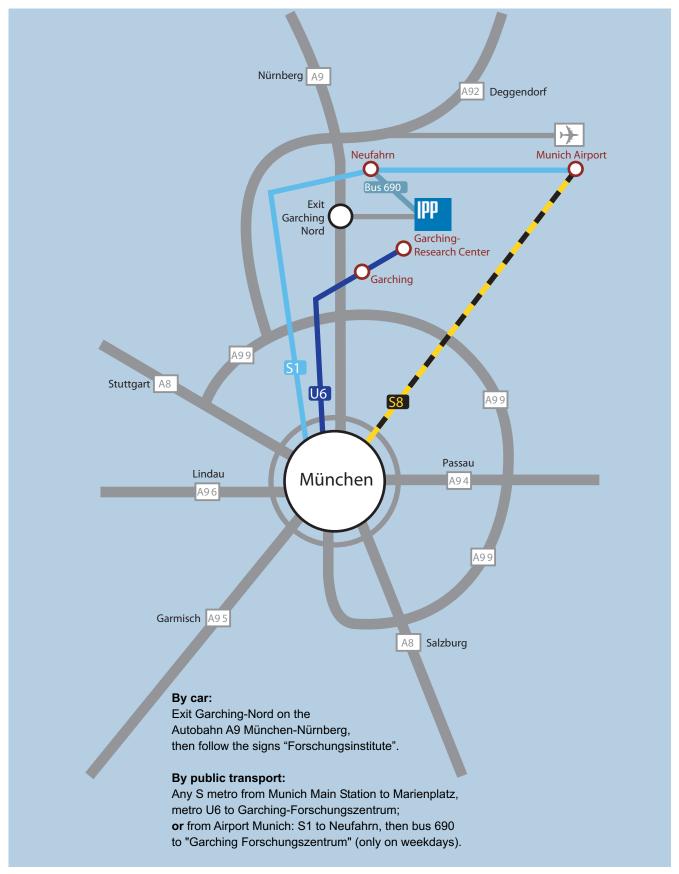
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⁺ LITE-Trainee

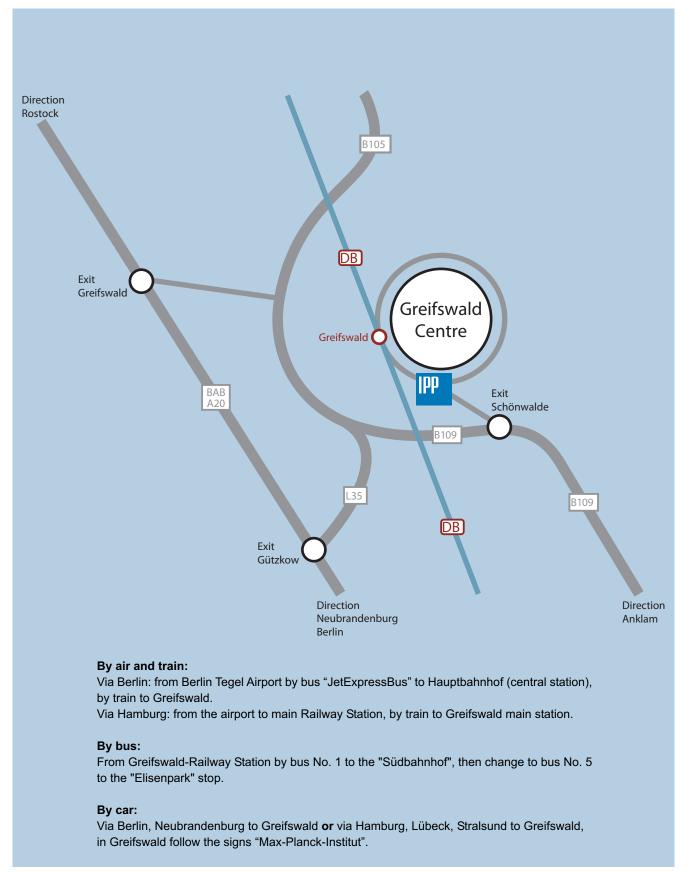
⁺⁺ EnTicE-Trainees

Appendix

How to reach IPP in Garching



How to reach Greifswald Branch Institute of IPP



IPP in Figures

Funding

IPP received approx. 16 % of its total funding from EURATOM. The Federal Government funded 90 % of the national expenditure for fusion research, the states of Bavaria and Mecklenburg-West Pomerania were providing the remaining 10 %. This came to total funding of approx. 113 million euros for the year 2010.

Garching

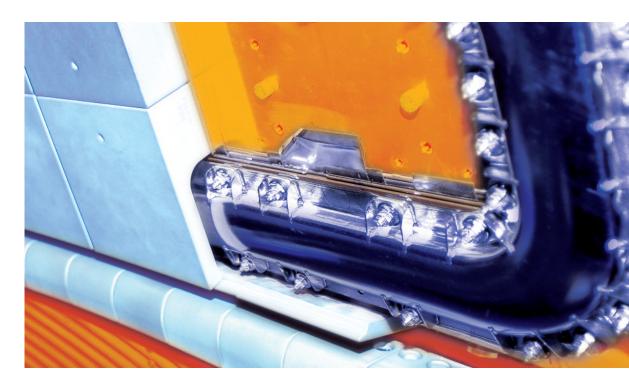
Greifswald

Scientific Staff

At the end of the year IPP had a total of 1171 members of staff, 446 of them worked at IPP's Greifswald site. The workforce comprised 296 researchers and scientists, 54 postgraduates and 38 postdocs. In addition, 12 guest researchers used the research infrastructure.

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