# International Atomic Energy Agency intercomparison of Ion Beam Analysis software

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#### **Abstract**

Ion Beam Analysis (IBA) includes a group of techniques for the determination of elemental concentration depth profiles of thin film materials. Often the final results rely on simulations, fits, and calculations, made by dedicated codes written for specific techniques. Here we evaluate numerical codes dedicated to the analysis of Rutherford Backscattering Spectrometry (RBS), non-Rutherford Elastic Backscattering Spectrometry, Elastic Recoil Detection Analysis, and non-resonant Nuclear Reaction Analysis data. Several software packages have been presented and made available to the community. New codes regularly appear, and old codes continue to be used and occasionally updated and expanded. However, those codes have to date not been validated, or even compared to each other. Consequently, IBA practitioners use codes whose validity, correctness and accuracy have never been validated beyond the authors' efforts. In this work, we present the results of an IBA software intercomparison exercise, where seven different packages participated. These were DEPTH, GISA, DataFurnace (NDF), RBX, RUMP, SIMNRA (all analytical codes) and MCERD (a Monte Carlo code). In a first step, a series of simulations were defined, testing different capabilities of the codes, for fixed conditions. In a second step, a set of real experimental data were analysed. The main conclusion is that the codes perform well within the limits of their design, and that the largest differences in the results obtained are due to differences in the

fundamental databases used (stopping power and scattering cross section). In particular,

spectra can be calculated including Rutherford cross-sections with screening, energy

resolution convolutions including energy straggling, and pileup effects, with agreement

between the codes available at the 0.1% level. This same agreement is also available for the

non-RBS techniques. This agreement is not limited to calculation of spectra from particular

structures with predetermined parameters, but also extends to extracting information from real

data. In particular, we have shown data from an Sb implanted sample where the Sb fluence

was certified with an uncertainty of 0.6%. For this sample, and using SRIM03 stopping

powers for 1.5 MeV 4He in Si, the codes were able to extract the Sb fluence with an average

0.18% deviation from the certified value and a 0.11% agreement between the codes. Thus

IBA is a suitable technique for accurate analysis where traceability is critical. These results

confirm that available IBA software packages are, within their design limitations, consistent

and reliable. The protocol established may be readily applied to validate future IBA software

as well.

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#### 1. Introduction

Low-energy particle accelerators have contributed a major part of our current knowledge of nuclear physics. The scientific outputs and technology developed in the pursuit of a better understanding of the atomic nucleus have evolved into mature accelerator applications supporting amongst other things, materials modification and materials analysis. Ion Beam Analysis (IBA), with its historical roots in ion beam interactions with atoms and nuclei, is the mainstay of the utilization of many low-energy ion beam accelerators. A recent survey conducted by the International Atomic Energy Agency (IAEA) <sup>1</sup> showed that there are more than 200 particle accelerators in 40 countries that utilise IBA techniques to various extents. The primary IBA techniques used are PIXE (Particle Induced X-Ray Emission), PIGE (Particle Induced Gamma-ray Emission), RBS (Rutherford Backscattering Spectrometry), Elastic (non-Rutherford) backscattering spectrometry (EBS), NRA (Nuclear Reaction Analysis) and ERDA (Elastic Recoil Detection Analysis).

Practitioners of IBA and researchers who utilise IBA techniques as part of their work are dependent on the availability of suitable analytical software and the accuracy of the outputs. Many software packages have been developed over time to address ongoing endusers needs and expectations. Understandably, they are of little commercial interest since they demand high amounts of intellectual input, and have limited profit potential. Computer programs to analyse data from the particle-particle IBA techniques of RBS, NRA, and ERDA date back to the 1970s. The needs of ion beam production, modification, and characterisation techniques from outside the ion beam community began to arise with the growing semiconductor technology. These IBA techniques for quantitative depth profiling in the micron range and determination of low-concentration elemental impurities were quickly recognized and widely applied. As these analytical tools became more versatile, also the

samples, spectra and data analysis problems became more complicated. By the end of the 1990s, the codes had developed in various directions; codes exist which can handle very general data analysis problems and various IBA techniques, some are highly automatic, others treat specified problems with great exactness.

The simulation modelling used in all IBA software assumes that the underlying physics, mathematics and nuclear and atomic data are valid, and adequately describe the physical processes involved. Starting from a known sample structure, the corresponding experimental energy spectrum, be it either particle or electromagnetic, created from ion beam interactions can be theoretically simulated from a few basic data, and the known formalism of the reaction spectrometry. Comparing the experimental and theoretical spectra, after a few user-conducted iterations where the assumed composition of the sample is iteratively modified, a close similarity of the spectra is accomplished. The sample structure leading to the theoretical spectrum is then taken to correspond to the material's sample structure. Erroneous results or misinterpretations of the material's structure can result from incorrect science, ambiguous data, or inadequate documentation and guidance for people to extract the correct information. The analytical software in wide-spread use today has underlying physics and computational strategies that in most applications have been demonstrated to be reliable and robust. This conclusion arises from the long track record of good agreement with other results obtained from independent and complementary techniques. With evolving technologies, IBA is being called upon to analyse increasingly complex materials, creating new challenges for IBA software. Of emerging importance is the necessity for IBA users to have sufficient confidence and evidence of the ability of the software codes to produce reliable and correct results, if used properly.

The IAEA organised in 2002 a technical meeting on the "Status of Software for Ion Beam Analysis in Materials Development" <sup>2</sup>, where 12 different particle-particle analysis

software packages were identified, each using various nuclear models, nuclear data, physics and mathematical algorithms. A description of these particle-particle software packages, a history of their development, and a review of their current status has been published<sup>3</sup>. The present paper describes the results of an IAEA exercise undertaken with the objectives to compare and ascertain the reliability and correctness of the outputs of seven different particle-particle analytical software codes. The usability (ease of use) and documentation of these codes were not assessed.

Although falling in the general IBA rubric, PIXE and PIGE will not be discussed in this paper. The IAEA has previously reviewed the status of gamma ray analysis software packages<sup>4,5</sup> and PIXE analysis software packages <sup>6,7,8</sup>.

#### 2. Methodology

All authors of software codes that calculate energy spectra known to us were invited to participate. The participating codes are DEPTH <sup>9,10</sup>, GISA <sup>11,12</sup>, MCERD <sup>13,14</sup>, DataFurnace (NDF) <sup>15,16,17</sup>, RBX <sup>18,19</sup>, RUMP <sup>20,21</sup>, and SIMNRA <sup>22,23,24</sup>. More details are given in Table 1. Note that codes that analyse data using different methods, such as directly converting the yield to concentration values <sup>25</sup> or other alternative methods such as artificial neural networks <sup>26</sup> were not considered.

While it was understood that many codes can only perform a subset of the simulations and analyses defined, the objective was to test and validate only those relevant aspects for which the code was specifically designed. Further details about the codes can be found in ref.

3. All codes were used by the authors, in some cases working together with close collaborators. MCERD is a Monte Carlo code in binary collision approximation that takes multiple collisions between incident ions and target atoms into account, while all other codes

utilise versions of the standard simulation procedure first described by Ziegler et al. <sup>27</sup>, where ion trajectories are approximated by straight lines. Multiple collisions can be approximated by some codes as an additional energy broadening contribution, and some codes also calculate the yield due to double scattering. We note that DEPTH is geared towards the calculation of energy spread, and not towards simulation of energy spectra.

From the multitude of physical effects and processes that can be investigated, we decided to test the ability to correctly:

- (1) Extract film thicknesses and compositions of multilayered structures with abrupt interfaces, but which have complex, overlapping spectra.
- (2) Extract hydrogen and deuterium concentrations and depth profiles.
- (3) Model Rutherford cross-section screening corrections.
- (4) Model sharp nuclear reaction resonances.
- (5) Model multilayered structures with interdiffused interfaces.
- (6) Model multiple and plural scattering effects.
- (7) Model surface and interfacial roughness.
- (8) Model resolution broadening as a function of depth.

The intercomparison exercise was divided into two main tasks: the first task included pure simulations only, done by each code for well-defined sample structures, well-defined experimental conditions, and well-defined physics. A set of five sample structures was defined, shown in Table 2, for which a total of 28 different simulations were selected, shown in Table 3. The objective was to use common grounds to unambiguously quantify differences between the different simulations of the underlying physics and physical processes. All software should input exactly the same experimental parameters, material properties, stopping

power database and use the same differential cross-sections. All inputs were fixed. Simulated spectra were then produced by each code and compared. The calculations reported by each code are listed in Table 4. Note that absence of any given calculation does not mean that the code in question is not able to do it, but simply that it was not reported.

The second task considered the analysis of experimental data. The objective was to determine the full potential of the codes using their entire programmed science, algorithms and models. The authors had no constraints, and might freely choose any stopping power database and differential cross-sections, and were free to vary any scaleable parameters to obtain a best fit between the simulated and measured spectra. A simulated spectrum was then produced for the relevant measurement. All final parameters, databases, differential cross-sections, physics used, ad-hoc procedures, etc must be specified to enable a proper evaluation of the science that contributed to successes. The experiments are briefly described in Table 5. Table 6 lists the analyses reported by each code. Note that absence of any given analysis does not mean that the code in question is not able to do it, but simply that it was not reported.

The IAEA organised a meeting between the participants in October 2005, where the first results were reported and compared with each other. During that meeting, the participants had the opportunity to correct mistakes or to present improved calculations. Some participants still corrected or improved their calculations later on. It is the final results that are presented here, since the purpose of this work is to report on the current state of the codes, including all their best capabilities.

Finally, while it was agreed that the stopping powers to be used would be SRIM <sup>28</sup> version 2003.26, GISA could not implement this on time for the exercise, and therefore used SRIM 1991 <sup>29</sup>.

## 3. Results - calculation of theoretical spectra

We will not report on all the calculations done, since some of those defined in Table 3 do not include extra physics or algorithms. They test, for instance, the capability to include different experimental configurations, or electron screening.

#### 3.1 Simulations of simple RBS spectra

The spectra calculated for Structure 1, Calculation 1, are shown in Fig. 1. This will be referred to here as the "baseline" calculation: the structure considered is Si / 200 nm SiO2 / 50 nm Au, measured with a 1.5 MeV <sup>4</sup>He<sup>+</sup> beam detected with a 16 keV FWHM resolution detector located at a 150° scattering angle, for entrance and exit angles 60° and 30° (angles are always given respective to the sample normal, except where explicitly stated otherwise), respectively. The codes considered Bohr straggling <sup>30</sup> (with propagation of straggling in thick layers, the so-called Tschalär effect <sup>31,32,33</sup> in those codes that include it, which are DEPTH, NDF, and SIMNRA), unscreened Rutherford cross sections, and SRIM03 stopping except for GISA, which used SRIM91. All codes calculate nuclear stopping in this and all other simulations. All codes did this calculation. In general terms, the results are similar for all codes. The single largest difference is the cut-off energy at which the codes stop the calculation. This is highest for MCERD, since the Monte Carlo calculations become very inefficient for low beam energies. In any case, the low energy region is often disregarded in data analysis, and was not the point of this calculation.

However, some important differences do exist. The Au signal is shown in Figure 2, where it is clear that RBX calculates a smaller straggling than the other codes. 1.5 MeV <sup>4</sup>He in Au is close to the stopping power maximum, so that propagation of straggling in thick

layers (Tschalär effect) is negligible in this case and straggling can be approximated by the simple Bohr straggling formula <sup>30</sup> for the Au layer in the given geometry. It can be shown that RBX is calculating too little straggling in this case. Also, the Si and O signals are shown in Figure 3, and GISA produces a different calculation, as expected since it uses different stopping powers. A simulation made with NDF using the same stopping reproduced the GISA simulation.

It is clear that in this baseline case, the largest differences, besides the low energy cutoff and the calculated straggling, are due to the stopping power data base used, with smaller differences being due to some differences that exist in the actual physics considered (the only stated difference is to consider or not the Tschalär effect) or in their implementation in the codes <sup>3</sup>. A quantitative comparison of the results is discussed in detail in Section 5.

Calculation 4 tests the capability of simulating very sharp edges, using the baseline but with 3 keV FWHM resolution and no straggling. As the energy width of each channel in the calculation is also 3 keV, careful convolution with the resolution is required. The results for the back edge of the Au signal are shown in Figure 4. All the codes make a more or less smooth transition, albeit with differences in the details. NDF, RUMP, and SIMNRA are very close to each other.

#### 3.2 RBS: continuous profile

Calculation 27 tests the ability to simulate a continuous profile, in this case a Gaussian distribution of Ge in Si. The results shown in Figure 5 suggest that all codes are equivalent, but a close up of the Ge peak in Figure 6 reveals that RBX differs from the other codes in the tails of the distribution, possibly due to round-off errors.

## 3.3 RBS/Channelling

Calculation 28 tested the capability of simulating channelling. The calculations are for sample 5, which is a  $1\times10^{16}$  at/cm<sup>2</sup> Ge implant into bulk (100)Si. The Ge was taken as 100% substitutional, and a point defect distribution in the Si was assumed, following the Ge distribution but with a 2% maximum concentration.

Only RBX submitted results, as it is the only participating code that implements calculations of channelled spectra based on theory <sup>19</sup>. The dechannelling is calculated following the theory in ref. 34. The ratio between the channelled to random stopping power was taken to be 0.88.

Some of the other codes can, to some extent, implement ad-hoc corrections to the yield and to the stopping power of random materials in order to approximate channelled spectra, but these corrections are not related to actual physical properties of a given crystalline structure or of a given defect distribution.

The calculations are shown in Figure 7. For comparison, both the random spectrum, and the channelled spectrum from pure Si, as calculated by RBX, are shown. The minimum yield calculated for the Si surface (1500-1550 keV) and at the Ge peak are 2.1% and 4.3%, respectively.

A Monte Carlo simulation of the same system was made with the code BISIC <sup>35</sup>. This is not a code designed for IBA data analysis in general, but specifically for analysis of RBS/Channelling spectra in the Si, SiC, and Si<sub>x</sub>Ge<sub>1-x</sub> crystalline systems. The results are also shown in Figure 7. The agreement is surprisingly good, even considering the differences in the width of the Ge signal and of the defect distribution in the Si, and in the height of the Si surface peak. Both codes assumed a perfect (unreconstructed) surface with the Si bulk lattice constants.

## 3.4 EBS and sharp resonances

The next four examples test the capability of modelling non-Rutherford cross sections in general and resonances in particular. The first two test the Si(p,p)Si cross section, which has a fairly broad resonance at 1672 keV, with 1.4 MeV and 1.8 MeV proton beams in Calculations 13 and 14, respectively. The second two test the much sharper  $^{16}O(\alpha,\alpha)^{16}O$  resonance at 3.031 MeV with a 3.15 MeV  $^4$ He beam, with and without straggling in Calculations 15 and 16, respectively. In this sense, these examples are limited, since they do not include the calculation of a buried sharp resonance, which is the really difficult test case  $^{36}$ . In what follows we shall show only the resonance signal, except for calculation 13 (1.4 MeV protons), where there is no resonance. In all cases the cross sections were calculated with the code SigmaCalc  $^{37,38,39}$  developed by Dr. Alexander Gurbich.

Calculation 13, for 1.4 MeV protons, is shown in Figure 8. Good agreement is obtained. For 1.8 MeV protons, the Si 1672 keV resonance (calculation 14), is detected at about 1350 keV and is shown in Figure 9. The NDF and SIMNRA curves are virtually undistinguishable, with GISA being very close to them. RUMP leads to a slightly broader resonance, and DEPTH and RBX even more so. DEPTH and RBX put the oxygen signal (1400 keV) at slightly higher energies than the other codes.

Calculations for 3.15 MeV <sup>4</sup>He without and with straggling are shown in Figure 10 and Figure 11, respectively. The codes have a different treatment of the cross section, which is input as an energy/cross section table. RUMP uses the integral cross section with a spline interpolation. NDF treats the values in the table as steps of a histogram, each one representing the energy interval given by half the difference to the neighbouring table points. The cross section is considered constant in each interval, and integrated over the internal layer being

considered. DEPTH, RBX and SIMNRA use integrated cross sections with linear interpolation between the tabulated values. Each method has advantages and disadvantages, particularly considering that experimental cross sections, ad-hoc fitting functions based on experimental data, and semi-empirical calculation models, are in fact not completely equivalent. This discussion is quite involved, and is beyond the scope of this paper.

Without straggling (Figure 10), NDF and RUMP lead to very similar results, while SIMNRA is broader, and DEPTH and RBX seems to be shifted to higher energies. DEPTH calculates an area higher than the other codes.

When straggling is taken into account, NDF becomes broader than RUMP and SIMNRA. The reason is that NDF takes into account the effect of the energy spread of the beam before scattering <sup>36,40</sup>, by calculating correctly both the cross section for scattering at each depth (which is an average of the energy-dependent cross section over the beam energy distribution), and the average beam energy after scattering (which depends on the beam energy distribution before scattering in relation to the shape of the resonance), both of which effects require the calculation of two integrals for each depth of scattering. The first effect makes the resonances broader, while the second makes them sharper. The net effect is still a broadening of the resonance, which becomes important at any particular depth when the beam energy spread at that depth is comparable to the resonance width.

DEPTH and RBX calculate the correct cross section for scattering at each depth taking the energy spread before scattering into account, but not the correct average energy after scattering, and thus produce a resonance broader than the other codes. RUMP and SIMNRA did not consider the effect of energy spread before interaction.

# 3.5 <sup>4</sup>He ERDA

ERDA spectra using a 1.8 MeV <sup>4</sup>He beam corresponding to Calculation 18 and Calculation 19 are shown in Figure 12 and Figure 13, respectively, for Sample 6 (Si bulk / CD<sub>2</sub> 150 nm / C<sup>1</sup>H<sub>2</sub> 150 nm / CD<sub>2</sub> 150 nm, considering the polymer density 1×10<sup>23</sup> at/cm<sup>3</sup>). They differ only in the fact that the first used Rutherford cross sections, and the second uses scattering cross sections for the H isotopes determined by V. Quillet <sup>41</sup>. In both cases, all calculations are very similar. RBX and RUMP seemingly did not calculate the signal due to the forward scattered beam. DEPTH calculated a slightly different energy loss for the backscattered signal. Finally, the signal edges are sharper in the RBX and RUMP calculations than in the other codes, for both Calculations 18 and 19, while being different from each other. A quantitative comparison of the results for Calculation 18 is discussed in detail in Section 5.

## 3.6 Heavy ion RBS and ERDA, including multiple scattering

All codes simulated Calculation 9, which is for 3.5 MeV <sup>7</sup>Li<sup>+</sup>, all other parameters equal to the baseline. The results are shown in Figure 14. The difference seen for GISA is due to the stopping power data base used, SRIM91, while the other codes used SRIM03. The large difference is due to the large evolution in knowledge about the stopping of <sup>7</sup>Li<sup>+</sup> and other heavy ions that occurred in the last two decades. The differences within the group that used SRIM03 are small, which shows that the basic algorithms used are correct. RBX calculates slightly less straggling than the other codes using SRIM03 stopping. A quantitative comparison of the results is discussed in detail in Section 5.

The results for Calculation 10 are shown in Figure 15. This is 50 MeV <sup>127</sup>I<sup>10+</sup> on Structure 1, forward scattering with detection of recoils. Bohr straggling and a constant 200 keV energy resolution were considered. MCERD, NDF and SIMNRA all give almost

identical results, except on the back edges of the Au related signal (both Au recoils at 23 MeV and <sup>127</sup>I backscattered from Au at 30 MeV). RUMP and RBX calculate different straggling, most visible at the oxide/substrate interface. DEPTH and RBX also leads to some differences in spectral height and width, which could to be due to differences in the handling of the stopping power.

Calculation 11 is the same as 10, but a realistic time-of-flight resolution of 300 ps for 50 cm flight path was considered. Only MCERD and SIMNRA implement this, and the results are shown in Figure 16.

Calculation 12 is the same as 10, but including multiple scattering. This is a very hard case due to the incident heavy ion, heavy substrate, and low energy: Multiple scattering plays an important role, including changes in total yield <sup>3,42</sup>. The results are shown in Figure 17. First of all, it is clear that when the full ion-target interaction is taken into account, as in the Monte Carlo code MCERD, the results are substantially different. This is probably one case where the traditional spectrum generation methods, which assume straight ion trajectories and include multiple scattering only as an additional broadening contribution, become inadequate. However, the main difference is due to the <sup>127</sup>I ions backscattered from the Au layer, while the recoil signals are similar in MCERD code and in the other codes. One should note that these kind of spectra are usually detected with mass sensitive detectors where direct comparison of full energy spectra is not made.

Second, to calculate the energy spread of the detected ions several analytical codes (DEPTH, RBS, SIMNRA) implement the same theory of multiple scattering <sup>9</sup>. NDF uses DEPTH automatically in run-time. RBX and SIMNRA contain independent implementations of this theory. However, DEPTH and RBX produce a spectral shape closer to that of MCERD than NDF or SIMNRA do, because they included a better description of the shape of the energy distribution, which is non-Gaussian <sup>9</sup>. SIMNRA and NDF can produce spectra which

are closer to the MCERD result, if they additionally include plural scattering (approximated by dual scattering).

#### **3.7 NRA**

Calculation 20 is shown in Figure 18. It is NRA with a 1 MeV <sup>3</sup>He beam and with the reactions d(<sup>3</sup>He, <sup>4</sup>He)p and d(<sup>3</sup>He,p)<sup>4</sup>He, on the same sample as in Calculations 18 and 19, and also with the same stopper foil, but measured at a 170° scattering angle and normal incidence. The cross section was taken from ref. 43. Only NDF and SIMNRA did this calculation. The low energy signal corresponds to <sup>4</sup>He being detected, while the high energy signal is for detected protons. The difference in the alpha and proton yields calculated is 0.2% and 0.6%, respectively. There are differences in the straggling calculated for the <sup>4</sup>He; nevertheless, agreement is considered good, taking into account that the <sup>4</sup>He loses almost all its energy in the foil before being detected. Details of the straggling calculations at very low energies could be responsible for the differences found.

Calculation 21 is shown in Figure 19. It is NRA with a 1 MeV deuterium beam with the reaction <sup>14</sup>N(d, <sup>4</sup>He)<sup>12</sup>C, for a bulk Fe<sub>4</sub>N sample, measured at a 170° scattering angle and normal incidence. Only NDF and SIMNRA did this calculation. The interesting point is the kinematics of this reaction, which requires careful programming (see e.g. ref. 44). At energies above 550 keV the kinematics is normal, i.e. the energy of the reaction product decreases with decreasing projectile energy. At energies below 550 keV the kinematics is inverted, and the energy of the ejected ion increases with decreasing projectile energy. Agreement is excellent, except at the low energy tail where NDF calculates yield down to slightly lower energies.

#### 3.8 Geometric straggling, multiple scattering, plural scattering

Calculations 22 to 24 were intended to test the separated effects on energy spread of geometric straggling and multiple scattering. Unfortunately, for the particular conditions chosen, in the region of the Au and SiO2 films, Bohr straggling is the largest contribution to energy spread. Geometric straggling is very small, and multiple scattering only leads to an energy spread deeper in the Si substrate. Thus Calculations 22 to 24 all lead to fairly similar results.

Calculation 24 is shown in Figure 20. It is for the baseline experimental conditions, but considering all effects that lead to energy spread, including the Chu correction <sup>45,46</sup> to Bohr straggling, geometric straggling and multiple scattering. NDF and SIMNRA produce a slightly sharper Au back edge than DEPTH, possibly because they use a Gaussian shape for the energy spread, while DEPTH uses more realistic distribution shapes. The actual contribution of multiple scattering to energy spread as calculated by DEPTH and SIMNRA (and also MCERD) is actually very similar <sup>47</sup>. As mentioned previously, NDF uses a version of DEPTH at run time to calculate all these energy spread contributions.

Only NDF <sup>48,49</sup> and SIMNRA <sup>50</sup> can calculate double scattering, which is the main contribution to plural scattering. The results for Calculation 26 are shown in Figure 21. Given that the calculations required are complex and involve a definition, to some degree arbitrary, of which events effectively constitute double scattering, agreement is surprisingly good. Calculation 25 involves double scattering at grazing angle, which leads to further difficulties <sup>48</sup>

One should note that the codes that can calculate geometric straggling and multiple scattering for RBS also do it for the other techniques. This is not the case for double scattering, that is implemented only for RBS in both NDF and SIMNRA.

## 3.10 Pulse pileup calculation

Only NDF, RUMP and SIMNRA submitted results for Calculation 7, which is the baseline with pulse pileup taken into account, considering a detector with 5 µs shaping time T<sub>w</sub> and no pileup rejection circuit. The results are in Figure 22. NDF and SIMNRA codes use implementations of the same basic algorithm <sup>51-53</sup>, and considered that the time required for the pulse to reach a maximum value T<sub>p</sub> is related to the shaping time of the amplifier via T<sub>pulse</sub> = 1.9 T<sub>w</sub>. While NDF and SIMNRA approximate the pulse shape as parabolic, RUMP approximates it as triangular. The agreement between the simulations can be considered excellent, particularly when compared with the simulation without pileup, also shown (SIMNRA Calculation 1). The difference between RUMP and the other two codes is assigned to the different shape of the pulses considered. As for NDF and SIMNRA, the differences could be due to different implementations of the basic algorithm, but the most likely cause is that the pile-up calculation is based on the calculated spectrum without pile-up, and NDF extends the calculation to lower energy values than SIMNRA. As the yield at those energies is high, this should lead to a higher pile-up, as seen in Figure 22.

Only NDF and SIMNRA submitted results for Calculation 8, which is the baseline with pulse pileup taken into account, considering a detector with 5 µs shaping time and a pileup rejection circuit with 0.5 µs rejection time. The results, shown in Figure 23, are very close.

Pulse pileup affects all the techniques, not only RBS, and the algorithms to calculate it are the same. Differences arise depending on the detection and electronics system.

#### 4. Results - analysis of experimental data

MCERD did not participate in this part of the intercomparison exercise. DEPTH is not designed primarily for analysis of experimental data, and only did the simulation of the amorphous silicon sample.

## 4.1 Amorphous silicon

Every code should be able to reproduce a 2 MeV <sup>4</sup>He RBS spectrum from amorphised Si. The sample was produced and measured at the CNR-IMM-Sezione di Bologna, as described in detail in ref. 54, and the details of the RBS experiment are given in ref. 55. Of all the data analysed in this intercomparison exercise, this is the set-up described in most careful detail and with best accuracy of the experimental parameters.

The beam was 2 mm wide and 1 mm high, with a 0.03° divergence. The beam current and fluence were 28 nA and 46.0(5) μC, respectively. The collection and live time were 1642 and 1625 s, respectively. The amplifier had a gain of 3.840(8) keV/ch, determined without taking the pulse height defect (PHD) into account, and a 0.5 μs shaping time. A 16 keV at FWHM circular detector with 5.01(2) mm diameter was located at a 150.0(2) scattering angle, at a distance of 100.5(3) mm from the sample, for a 1.95(2) msr solid angle. The angle of incidence was 0.0(1)°. No pile-up rejection was used. The measurement of the stopping power depends at first order on the electronic gain, and this was measured very precisely using a 7 point correlation. The effect of the PHD correction can be calculated *ex post hoc* using the formalism of Lennard *et al.* <sup>56</sup>; using a dead layer equivalent thickness of 25×10<sup>16</sup> Si/cm² we find the gain changing by 0.22%. This will be a (small) systematic error on the determination of the stopping power.

All the simulations are shown in Figure 24. They are almost undistinguishable at the Si surface edge and in the yield in the near-surface region. These are the regions that are

normally considered in analysis of real data, as the low energy yield is notoriously difficult to calculate correctly. Differences between the different calculations start to appear at energies below around 600 keV, which are mostly due to the different stopping powers used (GISA used SRIM91 <sup>29</sup> scaled by a factor of 0.97, DEPTH used SRIM95, RUMP and SIMNRA used SRIM03 <sup>28</sup>, and NDF used Barradas <sup>57</sup> which is equivalent to KKKNS\*1.02 <sup>58</sup>). All codes calculate nuclear stopping in this and all other analyses of real data. Different implementations of straggling, and eventually pile-up and other algorithmic issues can also lead to differences. Table 7 shows details of the different calculations. Some of us did different simulations using different stopping power data bases, and altering very slightly the beam fluence and the detector resolution. No large differences are noted. In general, we consider that the results are excellent, validating the correctness of the codes.

We calculated the function  $\chi^2 = \frac{1}{n} \sum_i \left( \text{data}_i - \text{simulation}_i \right)^2 / \text{data}_i$ , where n is the number of points over which the sum is made, for different energy windows. The first window is from 250 to 1150 keV, encompassing almost all the Si signal, and the second window is from 800 to 1100 keV, corresponding to the Si signal at energies above the oxygen signal. In both cases the Si surface edge signal was excluded, because small differences in defining what the energy of a channel is, can lead to large changes in  $\chi^2$ . The third window, 1250-1900 keV, includes the signal above the Si surface barrier, where only pile-up is expected to be observed. For Gaussian distributed data, the expectation value of the  $\chi^2$  for a perfect simulation is 1.

In the case of GISA, the factor used to multiply the SRIM91 stopping power was adjusted to obtain a ratio between the simulated and experimental yield in the 800-1100 keV energy window equal to 1. In this case, the  $\chi^2$  statistic is not meaningful for GISA.

The results are shown in Table 8. The overall best  $\chi^2$  is obtained by DEPTH, due to choosing the best energy dependence of stopping power for silicon. At the same time, DEPTH has the worst  $\chi^2$  in the near surface region. On the contrary, SIMNRA has the best  $\chi^2$  at high energies, with NDF a close second, but the worst overall one, with NDF being almost as bad. GISA and RUMP obtain fairly good  $\chi^2$  values in both energy windows. Given that the low energy signal is often disregarded in data analysis, we consider that all the codes obtain excellent agreement in the important high energy region of the Si signal. Finally, while DEPTH and GISA did not calculate pile-up, the calculations made by NDF, RUMP and SIMNRA are approximately equivalent.

## 4.2 Certified Sb implant

The sample is a 15 mm square piece of the certified reference material IRMM0001/BAML003, provided by the European Institute for Reference materials and Measurements. It is was made by implanting Sb into a (100) Si wafer with a 90 nm surface oxide layer. The material has a certified retained Sb content (uncertainties given at one standard deviation) of  $48.1(3)\times10^{15}$  /cm<sup>2</sup> (which is a 0.6% uncertainty) <sup>59</sup>. The oxide thickness and interface quality are not certified. The sample was amorphised to a depth of about 630nm with a 500 keV  $5\times10^{15}$  Si/cm<sup>2</sup> implant on a stage cooled by liquid nitrogen.

The sample was measured at the University of Surrey Ion Beam Centre with a 1.557(2) MeV <sup>4</sup>He beam, detected simultaneously by two detectors, located at 172.8(2)° and 149.2(2)° scattering angles with electronic gains of 3.388(10) and 3.545(10) keV/ch and energy resolutions of 21 and 14 keV respectively. The amplifiers had 0.5 µs shaping time and pileup rejection with a time resolution of about 500ns was used. Further details can be found in ref. 60.

The parameter to be derived was the Sb retained fluence. The amorphised silicon substrate was used to determine the charge - solid angle products of the detectors. Some participants also reported the Sb peak depth  $R_{max}$  and width  $\Gamma$  (FWHM), and also the thickness  $t_{SiO2}$  of the oxide layer. The experimental uncertainty of the Sb from counting statistics is 0.2%, with a maximum uncertainty of the experiment is 0.8%  $^{60}$ , including all other factors except for the effect of stopping power.

The data can be analysed by fitting an arbitrary continuous distribution of Sb throughout the sample (including in the oxide), where the area of the fitted Sb signal matches the area of the data. This creates a continuous profile that is reported as concentration versus areal depth. Alternatively (and equivalently), the data can be replotted (with pileup subtracted) on a concentration vs. areal depth scale, using the energy loss function (and energy dependence as a function of depth) determined from the fit. The area of this signal can be directly interpreted as the Sb fluence. This procedure is independent of the Sb peak depth Rp and width values, and leads to very high accuracy in the Sb fluence determined. The different codes used variations of this procedure.

The results are given in Table 9. SIMNRA and RUMP analysed the two spectra independently, obtaining two different values for the Sb. We show the average value. NDF did both independent and joint analyses. The other codes derived one single value. All the codes obtain values close to the certified value. The uncertainty shown for NDF, 0.06%, was obtained from a Bayesian inference analysis <sup>16</sup>, and reflects only the total expected counting statistics uncertainty for the Sb signal (0.05%). Note also that the Sb fluence determined is directly affected by the Si stopping power used. Some codes also did complementary analyses using different sets of stopping powers. Various Sb fluence values were reported, with differences up to 2% consistent with the differences in the stopping power databases.

The standard deviation of the reported values using SRIM03 stopping is  $0.055 \times 10^{15}$  Sb/cm<sup>2</sup>, which is 0.11% in relative terms. The average value is  $48.015 \times 10^{15}$  Sb/cm<sup>2</sup>, which is -0.18(11)% away from the certified value. This is an extraordinary agreement not only amongst the codes, but between the codes and the known Sb amount, which means that RBS can be used to obtain accuracies in the region of 0.2% in the determination of fluences, if best practice is used both in performing the experiment and in analysing the data.

It also means that the Si stopping power in SRIM03 is consistent with the certified standard to the accuracy of the certified standard (0.6%,  $1\sigma$ ). We point out here that this represents a significant improvement in the accuracy with which the Si stopping powers are known, since the current uncertainty on these values is no better than 1% <sup>54,56</sup>, and there is no independent confirmation of that accuracy. At present we have to cite an uncertainty of 2% <sup>58</sup> in critical work. SRIM2003 itself has no critical traceability for particular stopping power values.

Table 9 also shows the ratio of the results obtained independently for the two detectors, which should be unity, and which has an uncertainty from counting statistics of 0.12%.

The pile-up calculated in the region of the Si substrate used for absolute normalisation is around -0.3% and -0.8% of the calculated yield for the 172.8° and 149.2° detectors, respectively. NDF, RUMP, and SIMNRA all included pile-up in the analysis. Double scattering in the same region, as calculated with NDF, is +0.25% and +0.28% of the single scattering. Inclusion of double scattering in the other codes would have led to a slightly lower charge - solid angle product required to fit the bulk Si yield, by about 0.2 to 0.3%, and consequently to an Sb fluence higher by the same amount. The electronic screening correction for Sb is 1.3% of yield, and must be included. The difference between the L'Écuyer <sup>61</sup> and Andersen <sup>62</sup> formulations is however only 0.04% in this case. It is thus clear that inclusion or

not of these effects, and their different treatment in the various codes, could justify the differences found between the codes. Note that the Sb content in this sample is certified only at 0.6% ( $1\sigma$ ), so that even without the double scattering correction the Si stopping power for this beam energy is validated at this accuracy.

Values for the range Rp and width of the Sb distribution, together with the oxide thickness, are also given in Table 9. These parameters are only reported for information: the determination of the Sb fluence does not depend on them. Rp in some cases was simply taken as the centre of the layer with maximum Sb concentration. In other cases a semi-Gaussian was fitted to the distribution. The standard deviation of the Sb Rp values is  $0.2 \times 10^{17}$  at./cm<sup>2</sup> which is 2.2% in relative terms, much larger than that for the Sb fluence, which is not surprising given that the depth resolution is  $1.5 \times 10^{17}$  at./cm<sup>2</sup>. Note that the position of the peak of a distribution in an RBS spectrum can be determined with a precision better than the nominal depth resolution <sup>63</sup>.

## 4.3 Hafnium oxide on silicon

The sample is a thin hafnium oxide layer of unknown composition and with unknown impurities, on silicon. It was measured at the Accelerator Laboratory of the University of Helsinki with a 2.5 MeV <sup>4</sup>He beam with 15° angle of incidence, detected at a 165° scattering angle. Not much more was known about the sample, which makes this a good test case since that is how routine RBS analysis is often done. The data and the simulations made by the different codes are shown in Figure 25.

GISA, NDF and SIMNRA used for the O cross section SigmaCalc <sup>37</sup> results. RUMP used an analytical representation of the resonance from a model by Cameron <sup>64</sup>. SIMNRA used for the C cross section the data of Feng et al. <sup>65</sup>. GISA used SRIM1991 <sup>29</sup> stopping for all

elements. NDF used Barradas et al. <sup>57</sup> for the Si stopping, and SRIM03 <sup>28</sup> for the other elements. RUMP and SIMNRA used SRIM03. NDF, RUMP and SIMNRA calculated the effect of Andersen electron screening in the cross section.

Pile-up leads to a maximum change in the Hf yield of -0.22%. Only GISA did not take this into account. NDF calculated the contribution of double scattering. However, this was not enough to reproduce the background seen at energies below the Hf peak. This background could be due to plural scattering, slit scattering, some heavy impurity in the Si substrate, or other unknown causes <sup>66</sup>. NDF, RUMP, and SIMNRA introduced an ad-hoc contribution to the yield to obtain a good fit to this background (and to the Si bulk signal). In the case of SIMNRA, this was done by introducing 0.078 at.% Hf in the Si. NDF and RUMP created an artificial background manually, which is then added to the simulated total scattering. GISA did not introduce this ad-hoc background in the region of the Zr signal, and thus determined the Zr content by simulating the height of the Zr signal relative to the background, which is as valid and accurate a method. GISA did introduce an ad-hoc background in the region of the O signal, to reproduce the Si signal in that region. Note that ad-hoc backgrounds and corrections are just a convenient way to extract the information required. They do not have a physical basis in themselves and any information the spectrum may have relating to the affected part of the signal is effectively disregarded.

The most relevant parameters are given in Table 10. The shape of the O signal (Figure 25b) is due to a resonance in the scattering cross-section at 2484keV. First of all, while all codes introduced one hafnium oxide film with a Zr contamination, NDF also considered a natural oxide layer on top of the Si substrate, and SIMNRA introduced a contamination layer on the surface of the sample. There seems to be a rather large variation on the values found for the thickness of the hafnium oxide layer, which is 870(28) ×10<sup>15</sup> at./cm<sup>2</sup>, i.e. the variation amongst codes is 3.2%. However, the layer thickness is mostly determined from the total Hf

and O content. The total Hf content is 296(4) ×10<sup>15</sup> Hf/cm<sup>2</sup>, which is a 1.4% variation. The variation expected from counting statistics only is 0.2%. For the O, one should consider the total amount derived, including the oxygen in the surface and interfacial layers for SIMNRA and NDF, respectively. This leads to an average and standard deviation of 584(31) ×10<sup>15</sup> O/cm<sup>2</sup>, which is a 5.3% scatter amongst codes. However, if we consider only those codes (GISA, NDF, SIMNRA) that used the same cross section (SigmaCalc), then we obtain 599(5) ×10<sup>15</sup> O/cm<sup>2</sup>, which is a 0.8% scatter. This is unexpectedly small since the counting statistics uncertainty is 4.5% for the O signal. All of the analysts have correlated the Hf and O signals thus trading a larger than expected uncertainty for the Hf signal for a smaller than expected uncertainty for the O signal. However, it is clear that the use of a different data base leads to the largest differences in the results produced by each code.

Finally, for the Zr impurity the results are  $2.96(8) \times 10^{15}$  Zr/cm<sup>2</sup>, which is a 2.7% scatter, comparable to the 5.6% expected from the counting statistics.

## 4.5 Cobalt/rhenium multilayer

Multilayers with nominal structure Si bulk / Re 5nm/(Co 2nm/Re 0.5 nm)<sub>15</sub> were produced by magnetron sputtering, and analysed at ITN, Sacavém <sup>67,68</sup>. The layers are not atomically flat, with roughness values in the order of a fraction of nm. The RBS analysis was done using a 1.0 MeV <sup>4</sup>He beam, detected at 160° in the Cornell geometry. A set of six spectra were collected, from near-normal incidence to grazing incidence, with angles with respect to the sample surface down to 6°.

The objective of this analysis is to test the capability to retrieve very complex layer structures, as well as roughness parameters. This information cannot be obtained by analysing each spectrum on its own. Only NDF and SIMNRA reported on this case. The two sets of

simulations are shown in Figure 26, and the layer structure derived is given in Table 11. Note that for the layer thicknesses for layers 20-32 cannot be derived from the spectra, and the numbers are just assumptions. SIMNRA analysed the six spectra with the same layer structure except for the thickness of the surface C layer, which is a valid assumption given that at least part of the C is deposited during the measurement (made at pressure around 10<sup>-7</sup> mbar). NDF made one single fit of the six spectra, and thus it used the same surface C thickness. Considering that these layers are ultra-thin (in particular, the Re layers correspond to 2 to 3 monolayers each), the agreement between the layer structures found is excellent.

The analysis made by both codes showed that some form of roughness must be present. However, it is difficult, and sometimes impossible, to determine from RBS alone the type of roughness present. NDF <sup>69,70</sup> and SIMNRA <sup>71</sup> implement different roughness models. NDF used a model where it is considered that the substrate is rough, with the presence of steps, and the subsequent layers are deposited conformally on top of these steps. Of all the models implemented in NDF, this is the one that best matches the other results known about this system <sup>67,68</sup>. The standard deviation of the height of the substrate features was determined as 0.61 nm, with an average lateral width of 40 nm. A fit assuming a wavy sample was also achieved, but it was not as good as that obtained with the rough substrate. SIMNRA, on the other hand, assumed also that the substrate is rough, not with steps but with a Lorentz distribution of the substrate surface angle with a FWHM of 0.3°.

#### 5. Validation of codes

Here we shall give quantitative results on the differences between the calculations made by the different codes, that can be assigned to the codes themselves. This means that only those codes that use the same stopping, i.e. SRIM03, will be compared. We selected three case for comparison: the baseline, i.e. an RBS spectrum; Calculation 9, i.e. heavy ion RBS; and Calculation 18, i.e. ERDA.

For each one of these cases, we selected relevant features that can be compared quantitatively, such as total yield of separated signals, height of given plateaux, position and width of edges. To determine the position and width of edges, we used commercial software to differentiate the calculated spectra, and to fit Gaussians to each peak that corresponds to a given edge. This procedure leads to some error, particularly for the edge width, which is difficult to quantify and may be responsible for some of the differences found.

## 5.1 <sup>4</sup>He RBS

The features selected for Calculation 1 were the Au total yield, the height of the plateaux for Au (in region 1240-1260 keV), Si in the SiO<sub>2</sub> layer (720-740 keV), Si in the substrate (580-600 keV), and O (450-470 keV), and the position and width of all the relevant edges: right and left Au, Si surface edge and Si/SiO<sub>2</sub> interface, and right and left O.

The results are given in Table 12. For the yield and heights, the average and standard deviation values were calculated from the DEPTH, NDF, RBX, RUMP, and SIMNRA values. The MCERD results were not considered because the statistical nature of the MC calculations leads to an extra error. For the edge position and widths, the RBX results were also excluded from the calculation of the average and standard deviation values, due to the problems with straggling in this calculation seen in Figure 1.

For the yield and height calculations, the standard deviation amongst the different calculations is between 0.12 and 0.26%. This is close to what can be achieved experimentally, and much better than the accuracy of the data bases used, particularly stopping power. Here, we must stress that the average is not the "correct" value. Finally, the results obtained with

MCERD are extraordinarily close to the results obtained with the standard codes, which validates the Monte Carlo approach.

For the edge positions, agreement is obtained within 0.1 and 0.7 keV. Amongst the subset of codes NDF, RUMP, and SIMNRA, a 0.1 keV standard deviation is obtained. MCERD leads to values consistently below the average, which could however be due to a different definition of what an energy bin actually is. Please note that the PHD non-linearity <sup>56</sup> can lead to a change in the edge positions. However, none of the codes considered this effect in these calculations, and thus the results are directly comparable, that is, the PHD non-linearity is not responsible for the small deviations between the codes.

For the edge widths, the agreement is better for the higher energy edges. The 2 keV standard deviation found for the lower energy edges is still smaller than the energy width of one channel, which is 3 keV in this case, and could also be due to the analysis procedure. However, it can also be due to differences in the handling of the straggling.

# 5.2 <sup>7</sup>Li RBS

The same features as for <sup>4</sup>He RBS were selected. For the yield and heights, the average and standard deviation values were calculated from the DEPTH, NDF, RBX, RUMP, and SIMNRA values. The MCERD results were not considered because the statistical nature of the MC calculations leads to an extra error. For the edge position and widths, the RBX results were also excluded from the calculation of the average and standard deviation values, due to differences in the straggling calculated. The results are given in Table 13.

For the yield and height calculation, the standard deviations are higher than for <sup>4</sup>He RBS, between 0.2 and 0.7%. This is between 0.1 and 0.3% when calculated for the NDF, RUMP and SIMNRA subset of codes. MCERD shows the scatter of values expected for a

Monte Carlo code, with deviations up to 2.6% in the low energy region where statistics are poorer. Nevertheless, these results validate the Monte Carlo approach.

For the edge position and width, again close agreement is reached amongst the codes. Note that here the energy width of a channel was 7 keV, so the errors in the determination of the edge widths are still less than half a channel, and again, could be due to the analysis procedure. The PHD correction is expected to be larger than for <sup>4</sup>He RBS, but as discussed in the previous section, none of the codes considered this effect in these calculations, and thus the results are directly comparable.

## 5.3 <sup>4</sup>He ERDA

The features selected were the edge and width of the <sup>1</sup>H and <sup>2</sup>H signals, the total yield of the two <sup>2</sup>H signals (surface layer - high energy, and bottom layer - low energy) and of the <sup>1</sup>H signal. The bottom <sup>2</sup>H signal is not entirely separated from the <sup>1</sup>H signal, but the distinction is however clear enough. The limit between them was taken to be the channel where the yield is minimum.

For the yields, the average and standard deviation values were calculated from the DEPTH, NDF, RBX, RUMP, and SIMNRA values. For the edge positions and widths, RUMP and RBX were excluded because they show some marked differences, possibly due to straggling, as seen in Figure 12. The MCERD results were not considered because the statistical nature of the MC calculations leads to an extra error.

The results are given in Table 14. Agreement between 0.5 and 1.3% is obtained for the yield calculation. This is not good agreement, given that such differences are within what an accurate experiment can reach. For NDF, RUMP, and SIMNRA, agreement between 0.03 and 0.21% is obtained.

For the edge positions agreement between 0.9 and 2.1 keV is obtained (between 0.1 and 0.4 keV for the NDF, RUMP, SIMNRA subset), while for the edge widths, agreement is slightly worse.

#### 6. Conclusions

In this paper some of the particle-particle nuclear data analysis software codes available to the ion beam analysis community for thin film depth profiling have been compared and evaluated for the first time. In the first step of this exercise, a series of simulations were defined, testing different capabilities of the codes, for fixed conditions. In the second step, a set of real experimental data were analysed; the objective being to determine the full potential of the codes with no constraints.

Within the limits of their design the codes perform well, and the largest differences in the results arise from differences in the fundamental data bases used. All codes gave useful results in the case of simulations, and for experimental data evaluation all the software gave reliable results with acceptable errors. Some complex structures could be analysed by only a limited number of codes.

There are a number of subsidiary conclusions that should be stated. We did not compare extensively the physics or its implementation into the codes or any computational details. All the codes are very extensive, with the concomitant probability of algorithmic errors, which are recognised as notoriously difficult to correct. These errors can be in the implementation of the physics (for instance mismatched units; interchanging FWHM and standard variation; and many more, some only occurring when some specific features are used simultaneously), or in numerical algorithms (poor integration methods; faulty convolutions in the tails of the distribution or for very small FWHM values; adding millions of small numbers in single

precision; and many more, some only occurring when some specific features are used simultaneously)

That completely different implementations of the physics (using different programming languages, different algorithms, and different general philosophy and structure of the codes) result in only small differences, and often give indistinguishable results, is very strong evidence for the reliability of the codes as a whole. The fact that there is excellent agreement between the single scattering codes and the Monte Carlo code is particularly encouraging.

Because IBA has well known physics, it is an ideal technique for use in standards or quality assurance work where traceable accuracy is critical. The present work has validated IBA codes for this purpose. In most important cases the demonstrable calculation accuracy of the codes can reach the 0.1% level. The exception is for non-Rutherford resonances, where significant differences between the codes exist.

The validity of the codes has been demonstrated not only for Rutherford backscattering with light ions but also for heavy ion RBS, non-Rutherford elastic backscattering and nuclear reaction analysis. HI-RBS is valuable for ultra-high sensitivity, and EBS for much thicker samples or for light element sensitivity. NRA is particularly useful for some light elements. A range of real effects such as pulse pileup, energy straggling and sample roughness can be shown to be treated correctly by the codes. Thus, we have shown that IBA spectra can be interpreted accurately for a very wide variety of samples, including samples of considerable complexity.

There is one case where the physics is not yet sufficiently well understood to be able to interpret scattering data quantitatively with single scattering codes. This is calculation 12 (Figure 17), which is heavy ion ERDA with multiple scattering, where the single scattering codes gave results inconsistent with the Monte Carlo code (which is known to agree reasonably well with experiment) for the backscattered ions.

The channelling technique has been so far overlooked by most codes. The comparison of RBX results, which is the only traditional code for IBA data analysis that implements channelling calculations, with a dedicated channelling Monte Carlo code, BISIC, shows that excellent results can be obtained by traditional codes.

A standard sample with an Sb content certified to a 0.6% error was measured with a 0.2% experimental uncertainty, determining the charge - solid angle product from the a-Si yield using SRIM 2003 stopping powers for  $^4$ He on Si for a beam energy around 1.5 MeV. The average of the Sb content values as determined with each code was -0.18% away from the certified value, with a standard deviation of 0.11%. Inclusion of extended physics, such as calculation of double scattering, can lead to still better agreement. It should be emphasised that the experimental uncertainty in the measurement of  $^4$ He stopping in Si is currently 2%  $^{57,58,72,73,74}$ . This analysis has now established that the SRIM03 tables correctly predict the backscattered yield for this beam in Si at this beam energy with an uncertainty of 0.6% ( $1\sigma$ ), which is the certified value of the Sb content of this sample.

The objective of this work was not to rank the relative strengths and weaknesses of the different programs and no such ranking has been produced. Other aspects, such as how easy each code is to use, the ability for semi or fully automatic data analysis, and data bases for stopping powers and cross-section data included, have not been evaluated. Nevertheless we believe we have provided the end user all the necessary elements to choose the most appropriate software for their specific needs.

This exercise was the first opportunity for code authors to compare and check their calculations in a systematic way. Many changes, corrections and improvements were made, often related to subtle details of the calculations. Better physical models and better implementations of the existing models were developed. The result has been improved codes

available to the IBA practitioners. Finally, the calculations presented here are made available to the community  $^{75}$ .

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Table 1 General information about the participating analysis programs.

Analysis Program	Technical Contact	Operating Systems	Distribution Mode	Status of source code
DEPTH	Edit Szilágyi	DOS (or emulators),	No charge. Downloadable from the	Restricted to author -
	KFKI Research Institute for Particle and Nuclear Physics	Windows	WEB.	not available.
	Budapest, Hungary			
	<u>szilagyi@rmki.kfki.hu</u> ; www.kfki.hu/~ionhp/			
GISA	Eero Rauhala	DOS (or emulators)	No charge. Write to author for copy.	Restricted to author -
	University of Helsinki, Helsinki, Finland			not available.
	and Jaakko Saarilahti, Technical Research Center of Finland			
	Eero.rauhala@helsinki.fi; Jaakko.Saarilahti@vtt.fi			
MCERD	Kai Arstila	Linux, UNIX	No charge. Write to author for copy.	Source code
	University of Helsinki, Helsinki, Finland and IMEC, Leuven, Belgium			available.
	Kai.Arstila@iki.fi			
NDF:	Nuno Barradas	Windows, UNIX	Commercial through Univ. of Surrey	Restricted to author -
DataFurnace	Technological and Nuclear Institute		Evaluation copies available by	not available.
	Sacavem, Portugal		request.	
DDV	nunoni@itn.pt; www.ee.surrey.ac.uk/ibc/ndf/	**** 1	N. 1. W	D ( ) ( )
RBX	Author: Endre Kótai; User in this exercise: Gabor Battistig	Windows	No charge. Write to author for copy.	Restricted to author -
	KFKI Research Institute for Particle and Nuclear Physics			not available.
	Budapest, Hungary			
DIIMD	kotai@rmki.kfki.hu	Windows Linus	Commonoial through Commuter	Carrana
RUMP	Mike Thompson  Port of Motorials Science Cornell University	Windows, Linux,	Commercial through Computer	Source code
	Dept. of Materials Science, Cornell University	UNIX, OS2	Graphics Service	available.
	Ithaca, NY USA		Evaluation copies available on WEB.	
CD D D A	mot1@cornell.edu; www.genplot.com	TT 1	C '14 INDIC DI	The second second
SIMNRA	Matej Mayer	Windows	Commercial through MPI for Plasma	Restricted to author -
	MPI for Plasma Physics		Physics	not available.
	Garching, Germany		Evaluation copies available on WEB.	
	Matej.Mayer@ipp.mpg.de; www.rzg.mpg.de/~mam/			

Table 2. Sample structures defined. The following densities were used:  $\rho(Si) = 4.978 \times 10^{22}$  at/cm³,  $\rho(SiO_2) = 6.6 \times 10^{22}$  at/cm³,  $\rho(Au) = 5.9 \times 10^{22}$  at/cm³,  $\rho(CD_2) = \rho(CH_2) = 1 \times 10^{23}$  at/cm³, where D is deuterium. Natural isotopic distribution except where otherwise specified.

Sample	Structure
S1	Si bulk / SiO <sub>2</sub> 200 nm / Au 50 nm
S2	Si bulk / CD <sub>2</sub> 150 nm / C <sup>1</sup> H <sub>2</sub> 150 nm / CD <sub>2</sub> 150 nm
S3	Fe <sub>4</sub> N bulk
S4	Si bulk / SiO <sub>2</sub> 200 nm / Au 20 nm
S5	1×10 <sup>16</sup> at/cm <sup>2</sup> Ge implant into bulk Si: maximum at 500 nm, 100 nm FWHM
	(Gaussian shape)

Table 3. Theoretical calculations defined. \* denotes a detailed quantitative comparison (see Section 5 and Tables 13, 14, 15). FWHM is the detector resolution;  $\Omega$  is the detector solid angle; bes is the initial beam energy spread in keV; bas is the initial beam angular spread in degrees;  $\varnothing$  is the detector diameter in mm. All angles are given in degrees. Entrance and exit angles are given in relation to the normal to the sample, except for ERDA where they are given in respect to the sample surface. The three numbers under the column "pileup" are the beam current in nA, the shaping time ( $\mu$ s) of the amplifier, and the resolution time ( $\mu$ s) of the pileup rejection system (0 if no pileup rejection system was used). Calculation 1 is the baseline. The stopper foil considered is 6  $\mu$ m Mylar ( $C_{10}H_8O_4$ ) with density 9.6×10<sup>22</sup> at/cm³ (1.3915g/cm³). MS is multiple scattering. PS is plural scattering.

Calculation	Structure	technique	ion	Е	FWHM	straggling,	Ω	charge	pileup	cross section	screening	stopper	scattering	entrance	exit	geometry	bes/bas/Ø
				(MeV)	(keV)	MS, PS	(msr)	(µC)				foil	angle	angle	angle		
1 *	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr 1	1	10	-	Rutherford	none	no	150	60	30	IBM	ideal
2	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr	1	10	-	Rutherford	Andersen <sup>2</sup>	no	150	60	30	IBM	ideal
3	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr	1	10	-	Rutherford	L'Ecuyer 3	no	150	60	30	IBM	ideal
4	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	3	none	1	10	-	Rutherford	none	no	150	60	30	IBM	ideal
5	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr	1	10	-	Rutherford	none	no	170	0	10	Cornell	ideal
6	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr	1	10	-	Rutherford	none	no	170	60	60.501	Cornell	ideal
7	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr	1	10	50/5/no	Rutherford	none	no	150	60	30	IBM	ideal
8	S1	RBS	<sup>4</sup> He <sup>+</sup>	1.5	16	Bohr	1	10	50/5/0.5	Rutherford	none	no	150	60	30	IBM	ideal
9 *	S1	RBS	$^{7}\text{Li}^{+}$	3.5	16	Bohr	1	10	-	Rutherford	none	no	150	60	30	IBM	ideal
10	S1	heavy ion ERDA	$^{127}I^{10+}$	50	200	Bohr	0.1	1000	-	Rutherford	none	no	40	10	30	IBM	ideal
11	S1	heavy ion ERDA	$^{127}I^{10+}$	50	300ps 50cm	Bohr	0.1	1000	-	Rutherford	none	no	40	10	30	IBM	ideal
12	S1	heavy ion ERDA	$^{127}I^{10+}$	50	200	Bohr, MS	0.1	1000	-	Rutherford	none	no	40	10	30	IBM	ideal
13	S1	EBS	$^{1}\text{H}^{+}$	1.4	16	Bohr	1	10	-	SigmaCalc 4	-	no	150	60	30	IBM	ideal
14	S1	EBS	$^{1}\text{H}^{^{+}}$	1.8	16	Bohr	1	10	-	SigmaCalc 4	-	no	150	60	30	IBM	ideal
15	S1	EBS	<sup>4</sup> He <sup>+</sup>	3.15	16	none	1	10	-	SigmaCalc 4	-	no	150	60	30	IBM	ideal
16	S1	EBS	<sup>4</sup> He <sup>+</sup>	3.15	16	Bohr	1	10	-	SigmaCalc 4	-	no	150	60	30	IBM	ideal
17	S1	EBS	<sup>4</sup> He <sup>+</sup>	3.15	16	Bohr	1	10	-	SigmaCalc 4	-	no	150	60	30	IBM	1/0.05/1
18 *	S2	ERDA	<sup>4</sup> He <sup>+</sup>	1.8	16	Bohr	1	10	-	Rutherford	none	yes	30	15	15	IBM	ideal
19	S2	ERDA	<sup>4</sup> He <sup>+</sup>	1.8	16	Bohr	1	10	-	Quillet 5	-	yes	30	15	15	IBM	ideal
20	S2	NRA	$^{3}\text{He}^{+}$	1	16	Bohr	1	10	-	Möller 6	-	yes	170	0	10	Cornell	ideal
21	S3	NRA	$^{2}\text{H}^{+}$	1	16	Bohr	1	10	-	1 mb/sr	-	no	170	0	10	Cornell	ideal
22	S4	RBS	<sup>4</sup> He <sup>+</sup>	1	16	Bohr	1	10	-	Rutherford	none	no	150	60	30	IBM	1/0.05/1
23	S4	RBS	<sup>4</sup> He <sup>+</sup>	1	16	Bohr, MS	1	10	-	Rutherford	none	no	150	60	30	IBM	ideal
24	S4	RBS	<sup>4</sup> He <sup>+</sup>	1	16	Chu <sup>7</sup> , MS	1	10	-	Rutherford	none	no	150	60	30	IBM	1/0.05/1
25	S4	RBS	<sup>4</sup> He <sup>+</sup>	1	16	Chu, MS, PS	1	10	-	Rutherford	none	no	170	80	80.153	Cornell	1/0.05/1
26	S1	RBS	<sup>4</sup> He <sup>+</sup>	1	16	Chu, MS, PS	1	10	-	Rutherford	none	no	150	60	30	IBM	1/0.05/1
27	S5	RBS	$^{4}\text{He}^{^{+}}$	2.7	16	Bohr	1	10	-	Rutherford	none	no	150	60	30	IBM	ideal
28	S5	Channelling	$^{4}\text{He}^{+}$	2.7	16	Bohr	1	10	-	Rutherford	none	no	150	0	60	IBM	ideal

<sup>&</sup>lt;sup>1</sup> Bohr [30]. <sup>2</sup> Andersen et al. [Fehler! Textmarke nicht definiert.]. <sup>3</sup> L'Ecuyer et al. [Fehler! Textmarke nicht definiert.]. <sup>4</sup> Gurbich [37]. <sup>5</sup> Quillet et al. [41]. <sup>6</sup> Möller et al. [43]. <sup>7</sup> Chu [45], Yang et al. [46].

Table 4. Calculations reported by each code. Absence of report does not mean that the given code is not capable of doing the given calculation.

Calculation	DEPTH	GISA	MCERD	NDF	RBX	RUMP	SIMNRA
1	yes	yes	yes	yes	yes	yes	yes
2 3				yes		yes	yes
3	yes			yes			yes
4	yes	yes	yes	yes	yes	yes	yes
5	yes			yes			yes
6	yes			yes			yes
7				yes		yes	yes
8				yes			yes
9	yes	yes	yes	yes	yes	yes	yes
10	yes		yes	yes	yes	yes	yes
11			yes				yes
12	yes		yes	yes	yes		yes
13	yes	yes		yes	yes	yes	yes
14	yes	yes		yes	yes	yes	yes
15	yes			yes	yes	yes	yes
16	yes			yes	yes	yes	yes
17	yes			yes			yes
18	yes		yes	yes	yes	yes	yes
19	yes			yes	yes	yes	yes
20				yes			yes
21				yes			yes
22	yes			yes			yes
23	yes			yes			yes
24	yes			yes			yes
25				yes			yes
26				yes			yes
27			yes	yes	yes	yes	yes
28					yes		

Table 5. Experiments defined.

Experiment	nominal structure	analysing ion	purpose
E1	a-Si / SiO <sub>2</sub> $13 \times 10^{15}$ at./cm <sup>2</sup> / C $4 \times 10^{15}$ at./cm <sup>2</sup>	2 MeV <sup>4</sup> He <sup>+</sup>	Sanity check - reproduction of a Si
	16. 0		spectrum
E2	4.81(3)×10 <sup>16</sup> /cm <sup>2</sup> 80 keV Sb implant in	1.557 MeV	Retrieval of Sb fluence
	Si bulk/SiO <sub>2</sub> 90nm	<sup>4</sup> He <sup>+</sup>	
E3	Si bulk / Hafnium oxide with impurities	$2.5~{\rm MeV}^4{\rm He}^+$	Determination of structure
E4	Si bulk / Re 5nm/(Co 2nm/Re 0.5 nm) <sub>16</sub>	1 MeV <sup>4</sup> He <sup>+</sup>	Determination of complex structure
	, , , , , ,		and roughness at grazing angle

Table 6. Analyses of experimental data reported by each code. Absence of report does not mean that the given code is not capable of doing the given calculation. DEPTH is not a code designed for analysis of experimental data. MCERD did not participate in this phase of the intercomparison exercise.

Experiment	DEPTH	GISA	MCERD	NDF	RBX	RUMP	SIMNRA
E1	yes	yes		yes		yes	yes
E2		yes		yes	yes	yes	yes
E3		yes		yes		yes	yes
E4				yes			yes

Table 7. Parameters used for the analysis of experiment E1 (amorphous Si).

Code	Si Stopping	pile-up	beam fluence	beam energy and	energy FWHM	geometry	layer structure
			$(\mu C)$ (nominal 46)	calibration	(keV)		
DEPTH	SRIM95	no	47.0	nominal	nominal	nominal	nominal
GISA	0.97 × SRIM91	no	nominal	nominal	nominal	nominal	nominal
NDF	Barradas <sup>1</sup>	yes	nominal	nominal	nominal	nominal	nominal
RUMP	SRIM03	yes	46.74	nominal	nominal	nominal	nominal
SIMNRA	SRIM03	yes	nominal	nominal	nominal	nominal	nominal

<sup>&</sup>lt;sup>1</sup> Barradas et al. [57].

Table 8. Normalised  $\chi^2$  values obtained for different energy windows of experiment E1 (amorphous Si).

Code	Si high energy 800-1100 keV	Si signal 250-1150 keV	pile-up 1250-1900 keV
DEPTH	1.303	1.384	5.953
GISA	1.034	1.583	5.953
NDF	1.018	5.695	1.374
RUMP	1.064	2.043	1.816
SIMNRA	1.000	6.254	1.389

Table 9. Results obtained for experiment E2 (certified Sb implant). Only the Sb fluence was required to be derived in the analysis. The certified value is  $48.1(3)\times10^{15}$  Sb/cm<sup>2</sup>. The mean value of all codes is  $47.99(7)\times10^{15}$  Sb/cm<sup>2</sup>. The last three columns are for information only: these parameters are not involved in the fluence determination. The depth resolution at Rp is  $1.5\times10^{17}$  at./cm<sup>2</sup>.

Code	Stopping	Sb fluence	Sb deviation	Ratio A/B of Sb	Sb peak	Sb peak	Oxide thickness
		$(10^{15} \text{ at./cm}^2)$	from certified	content for two	depth R <sub>p</sub>	width $\Gamma$	$t_{\mathrm{SiO2}}$
			value (%)	detectors	$(10^{17} \text{ at./cm}^2)$	$(10^{17} \text{ at./cm}^2)$	$(10^{17} \text{ at./cm}^2)$
GISA	0.96 × SRIM91	47.9	-0.41		9.8	6.7	6.0
NDF	SRIM03	48.03(3)	-0.15	1.00125	9.6	6.4	5.7
RBX	SRIM03	48.0	-0.21		9.3	6.2	5.8
RUMP	SRIM03	48.08	-0.04	1.00417	9.6	6.0	6.1
SIMNRA	SRIM03	47.95	-0.31	1.00476	-	-	6.0

Table 10. Results obtained for experiment E3 (hafnium oxide on silicon). Layer thickness t and elemental total amounts are in  $10^{15}$  /cm<sup>2</sup> units, elemental concentrations in at.%.

	GISA	NDF	RUMP	SIMNRA
surface layer	-	-	-	t=80; H 1 O 1 C 1
main layer	t=898; Hf 33.5 O 66.2 Zr 0.34	t=882; Hf 33.5 O 66.1 Zr 0.34	t=831; Hf 35.0 O 64.7 Zr 0.35	t=870; Hf 34.0 O 65.7 Zr 0.33 roughness FWHM 93×10 <sup>15</sup> /cm <sup>2</sup>
interfacial layer	-	t=32; Si 1 O 2	-	-
substrate	Si	Si	Si	Si 99.92 Hf 0.078
Hf total amount	300.8	295.5	290.7	295.8
O total amount	594.5	604.3	537.4	598.3
Zr total amount	3.05	3.00	2.91	2.87
stopping power	SRIM91	Barradas, SRIM03 <sup>1</sup>	SRIM03	SRIM03
scattering cross sections	O: SigmaCalc	O: SigmaCalc	O: Cameron <sup>2</sup>	O: SigmaCalc
C	no screening	Andersen screening	Andersen screening	C: Feng et. al <sup>3</sup>
		•	-	Andersen screening
plural scattering	ad-hoc contribution required to	double scattering calculated; ad-hoc	ad-hoc contribution required to	Hf in substrate to simulate plural
	simulate the background below	contribution required to simulate the	simulate the background below the	scattering
	the O signal	background below the Hf signal	Hf signal	-
pile-up	no	yes	yes	yes

<sup>&</sup>lt;sup>1</sup> The stopping of Si was that in Barradas et al. [57], all other were SRIM03.

<sup>2</sup> Cameron <sup>64</sup>.

<sup>3</sup> Feng et al. <sup>65</sup>.

Table 11. Layer structure obtained for experiment E4 (Co/Re multilayer).

1	<u> </u>	
layer	$t_{\text{SIMNRA}}$	$t_{NDF} (10^{15} \text{ at./cm}^2)$
1 0 ( 0 )	$(10^{15} \text{ at./cm}^2)$	
1 - C (surface)	41.2	50.7
2 - Re	4.2	4.0
3 - Co	24	22.2
4 - Re	3.75	3.7
5 - Co	23.5	22.7
6 - Re	3.6	3.4
7 - Co	24	20.9
8 - Re	3.65	3.3
9 <b>-</b> Co	22	19.1
10 - Re	4	3.6
11 <b>-</b> Co	21	17.6
12 - Re	3.3	3.1
13 - Co	21	19.9
14 - Re	3.8	3.8
15 - Co	24	22.5
16 - Re	3.2	3.8
17 - Co	21.5	21.3
18 - Re	3.6	3.3
19 - Co	23	19.8
20 - Re	3.3	3.4
21 - Co	19	19.8
22 - Re	3.3	3.2
23 - Co	19	19.6
24 - Re	3	4.0
25 - Co	19	23.5
26 - Re	2.5	2.0
27 - Co	18	18.2
28 - Re	2.5	2.4
29 - Co	18	18.1
30 - Re	2.5	2.7
31 - Co	18	19.6
32 - Re	26.5	24.0
33 - Si substrate	infinite	infinite

T Average of independent values obtained for each spectrum

Table 12. Quantitative analysis of differences amongst simulations in Calculation 1 (standard RBS). Only codes that used SRIM03 stopping are included. The columns for each code give the deviation, in % or in keV, relative to the average value. The average and standard deviation values were calculated, for the yield and height values, from the DEPTH, NDF, RBX, RUMP, and SIMNRA values. MCERD was excluded because the statistical variation of yield leads to fluctuations that can disturb the average. For the edge position and width, the RBX value was also excluded from the calculation of the average and standard deviation, due to differences in the straggling calculation.

signal	DEPTH	MCERD	NDF	RBX	RUMP	SIMNRA	average
Au yield (%)	-0.11	-0.01	-0.01	-0.19	+0.25	+0.06	$637885 \text{ counts} \pm 0.17\%$
Au height (%)	-0.17	-0.18	-0.01	+0.18	+0.07	-0.07	$5901.4 \text{ counts/keV} \pm 0.13\%$
1340-1360 keV							
Si in SiO2 height (%)	+0.09	-0.36	-0.09	+0.16	-0.05	-0.12	$222.54 \text{ counts/keV} \pm 0.12\%$
720-740 keV							
Si substrate height (%)	+0.16	+0.10	-0.16	+0.06	+0.15	-0.21	$624.2 \text{ counts/keV} \pm 0.17\%$
580-600 keV							
O in SiO2 height (%)	+0.29	+0.70	-0.19	+0.28	-0.22	-0.16	906.8 counts/keV $\pm$ 0.26%
450-470 keV							-
Au right edge position (keV)	-0.1	-0.2	-0.0	-0.1	+0.1	+0.1	$1392.1 \pm 0.1 \text{ keV}$
Au left edge position (keV)	+0.1	-0.3	+0.1	+0.4	-0.0	-0.1	$1284.9 \pm 0.1 \text{ keV}$
Si surface edge position (keV)	+1.0	-0.7	-0.3	+0.3	-0.3	-0.4	$795.0 \pm 0.7 \text{ keV}$
SiO2/Si edge position (keV)	+0.8	-0.1	-0.2	+1.1	-0.2	-0.3	$648.0 \pm 0.5 \text{ keV}$
O right edge position (keV)	+1.0	-0.7	-0.3	+0.3	-0.3	-0.3	$512.7 \pm 0.7 \text{ keV}$
O left edge position (keV)	+0.6	-2.8	-0.3	-0.2	-0.2	-0.2	$393.5 \pm 0.4 \text{ keV}$
Au right edge width (keV)	-0.1	+2.2	+0.4	+0.1	-0.2	-0.1	$14.4 \pm 0.3 \text{ keV}$
Au left edge width (keV)	-0.2	-0.2	+0.0	-5.1	+0.2	-0.1	$21.8 \pm 0.2 \text{ keV}$
Si surface edge width (keV)	-0.2	+0.2	-0.2	-3.7	+0.8	-0.5	$18.9 \pm 0.6 \text{ keV}$
SiO2/Si edge width (keV)	+0.4	+1.9	-0.5	-4.7	+1.0	-0.8	$23.2 \pm 0.8 \text{ keV}$
O right edge width (keV)	-1.9	-1.5	+0.3	-3.6	+1.7	-0.2	$20.1 \pm 1.5 \text{ keV}$
O left edge width (keV)	+2.5	+3.5	-1.2	-3.7	-0.1	-1.2	$18.3 \pm 1.7 \text{ keV}$

Table 13. Quantitative analysis of differences amongst simulations in Calculation 9 (heavy ion RBS). Only codes that used SRIM03 stopping are included. The columns for each code give the deviation, in % or in keV, relative to the average value. The average and standard deviation values were calculated, for the yield and height values, from the DEPTH, NDF, RBX, RUMP, and SIMNRA values. MCERD was excluded because the statistical variation of yield leads to fluctuations that can disturb the average. For the edge position and width, the RBX value was also excluded from the calculation of the average and standard deviation, due to differences in the straggling calculation.

signal	DEPTH	MCERD	NDF	RBX	RUMP	SIMNRA	average
Au yield (%)	+0.4	-0.1	+0.1	-1.3	+0.5	+0.2	$260191 \text{ counts} \pm 0.7\%$
Au height (%)	+0.2	-0.2	+0.2	-1.1	+0.5	+0.2	1360.7 counts/keV $\pm$ 0.6%
2950-3000 keV							
Si in SiO2 height (%)	+0.6	-2.6	-0.1	+0.1	+0.1	-0.2	$61.45 \text{ counts/keV} \pm 0.4\%$
1120-1170 keV							
Si substrate height (%)	+0.3	-0.3	-0.2	-0.0	+0.1	-0.2	$173.45 \text{ counts/keV} \pm 0.18\%$
900-950 keV							
O in SiO2 height (%)	+0.3	+1.7	-0.4	+0.1	+0.2	-0.3	$346.70 \text{ counts/keV} \pm 0.32\%$
450-500 keV							
Au right edge position (keV)	+0.1	-0.3	-0.0	-0.0	-0.0	-0.0	$3068.0 \pm 0.1 \text{ keV}$
Au left edge position (keV)	+0.6	-0.4	-0.1	+0.7	-0.1	-0.2	$2877.1 \pm 0.4 \text{ keV}$
Si surface edge position (keV)	+2.8	+0.7	-1.1	+2.3	-0.9	-1.0	$1233.6 \pm 1.9 \text{ keV}$
SiO2/Si edge position (keV)	+2.6	+0.9	-1.2	-9.5	-0.7	-0.8	$1036.4 \pm 1.8 \text{ keV}$
O right edge position (keV)	+3.3	+0.0	-1.3	+1.4	-1.1	-0.9	$537.9 \pm 2.2 \text{ keV}$
O left edge position (keV)	+2.0	+0.2	-1.1	-6.4	-0.4	-0.4	$416.1 \pm 1.4 \text{ keV}$
Au right edge width (keV)	-0.1	-0.2	+0.8	-0.7	-0.0	-0.6	$17.2 \pm 0.6 \text{ keV}$
Au left edge width (keV)	-0.0	-1.8	+0.0	-5.9	+0.5	-0.5	$29.6 \pm 0.4 \text{ keV}$
Si surface edge width (keV)	-0.8	-1.4	-0.2	-3.5	+4.1	-0.4	$20.8 \pm 3.1 \text{ keV}$
SiO2/Si edge width (keV)	-1.8	-1.1	-1.0	-4.5	+4.4	-1.5	$26.9 \pm 3.0 \text{ keV}$
O right edge width (keV)	-1.8	+10.0	+1.4	-5.4	+1.1	-0.6	$23.6 \pm 1.5 \text{ keV}$
O left edge width (keV)	-0.8	+3.7	-0.2	-9.6	+1.2	-0.1	$29.7 \pm 0.9 \text{ keV}$

Table 14. Quantitative analysis of differences amongst simulations in Calculation 18 (ERDA). Only codes that used SRIM03 stopping are included. The columns for each code give the deviation, in % or in keV, relative to the average value. The average and standard deviation values were calculated, for the yield and values, from the DEPTH, NDF, RBX, RUMP, and SIMNRA values. MCERD was excluded because the statistical variation of yield leads to fluctuations that can disturb the average. For the edge position and width, the RBX and RUMP values were also excluded from the calculation of the average and standard deviation, due to differences in the straggling calculation.

signal	DEPTH	MCERD	NDF	RBX	RUMP	SIMNRA	average
<sup>2</sup> H high yield (%)	+0.8	+1.3	-0.4	+0.3	-0.3	-0.4	22391 counts $\pm 0.5\%$
<sup>2</sup> H low yield (%)	+1.2	+0.8	-0.6	+0.2	-0.2	-0.6	$27884 \text{ counts/keV} \pm 0.7\%$
<sup>1</sup> H yield (%)	+2.2	-0.5	-0.7	+0.0	-0.7	-0.8	69339 counts/keV ± 1.3%
<sup>2</sup> H high right edge position (keV)	-2.1	+0.8	+1.2	+1.3	+0.2	+0.8	904.5 ± 1.8 keV
<sup>2</sup> H high left edge position (keV)	-1.5	+0.9	+0.8	+2.0	+1.4	+0.7	$809.9 \pm 1.2 \text{ keV}$
<sup>2</sup> H low edge position (keV)	-1.0	+1.1	+0.4	+2.8	-0.4	+0.6	$708.5 \pm 0.9 \text{ keV}$
<sup>2</sup> H low edge position (keV)	-1.0	+0.4	+0.6	+3.9	-2.7	+0.4	$597.7 \pm 0.9 \text{ keV}$
<sup>1</sup> H yield edge position (keV)	-2.4	+1.3	+1.1	+0.4	+4.5	+1.3	$556.6 \pm 2.1 \text{ keV}$
<sup>1</sup> H yield edge position (keV)	-2.2	+1.4	+1.1	+1.0	+4.4	+1.1	$478.8 \pm 1.9 \text{ keV}$
<sup>2</sup> H high right edge width (keV)	+1.1	-1.0	-0.5	-2.1	-9.2	-0.7	$23.9 \pm 1.0 \text{ keV}$
<sup>2</sup> H high left edge width (keV)	+1.3	-1.1	-0.6	-2.6	-7.6	-0.6	$25.2 \pm 1.1 \text{ keV}$
<sup>2</sup> H low edge width (keV)	+1.3	-2.3	-0.2	-3.4	-7.3	-1.0	$27.8 \pm 1.1 \text{ keV}$
<sup>2</sup> H low edge width (keV)	+2.1	-0.8	-1.1	-4.8	-7.4	-1.0	$30.4 \pm 1.8 \text{ keV}$
<sup>1</sup> H yield edge width (keV)	+1.5	-1.5	-0.6	-3.0	-8.5	-0.9	$25.8 \pm 1.3 \text{ keV}$
<sup>1</sup> H yield edge width (keV)	+2.2	-1.4	+0.2	-3.0	-6.8	-2.3	$26.6 \pm 2.3 \text{ keV}$

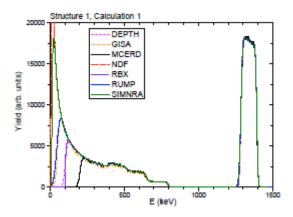


Figure 1. Calculation 1 - simple RBS spectrum from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.5 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

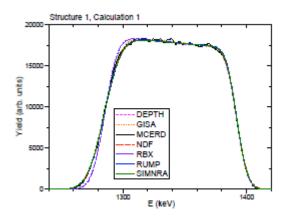


Figure 2. High energy region of Calculation 1 - simple RBS spectrum.

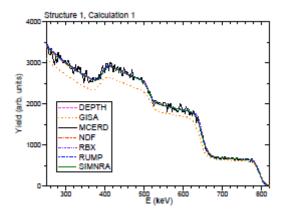


Figure 3. Low energy region of Calculation 1 - simple RBS spectrum.

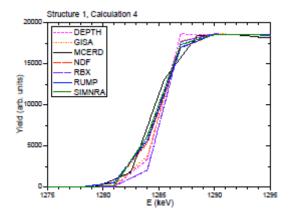


Figure 4. Calculation 4 - simple RBS spectrum from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.5 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 3 keV FWHM, no straggling, ideal beam and detector. No screening.

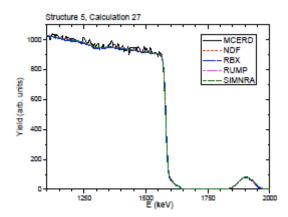


Figure 5. Calculation 27 - continuous profile RBS spectrum from  $1\times10^{16}$  at/cm<sup>2</sup> Ge implant into bulk Si. 2.7 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

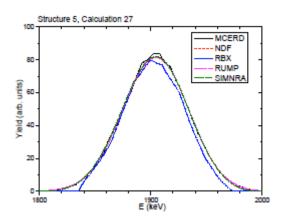


Figure 6. Calculation 27 - Ge peak.

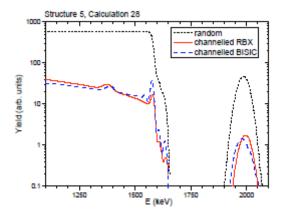


Figure 7. Calculation 28 - RBS/Channelling spectrum from  $1\times10^{16}$  at/cm<sup>2</sup> Ge implant into bulk (100)Si. The Ge is 100% substitional, the Si has a point defect distribution that follows the Ge but with a 2% maximum concentration. 2.7 MeV  $^4$ He<sup>+</sup>,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

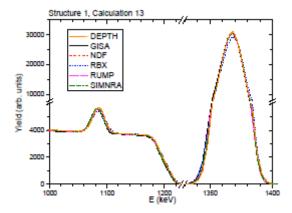


Figure 8. Calculation 13 - Elastic backscattering without resonances, from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.4 MeV  $^{1}$ H $^{+}$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

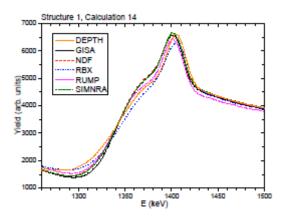


Figure 9. Calculation 14 - Elastic backscattering with resonances, from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.8 MeV  $^{1}$ H $^{+}$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

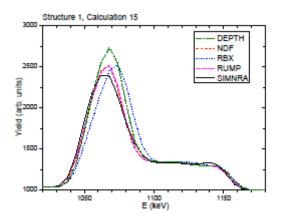


Figure 10. Calculation 15 - Elastic backscattering with sharp resonances and without straggling, from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 3.15 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, no straggling, ideal beam and detector. No screening.

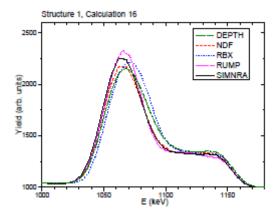


Figure 11. Calculation 16 - Elastic backscattering with sharp resonances and with straggling, from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 3.15 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

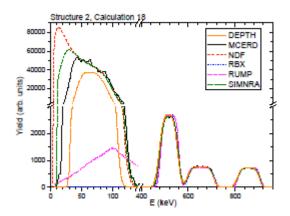


Figure 12. Calculation 18 -  $^4$ He ERDA with Rutherford cross sections, from Si bulk / CD<sub>2</sub> 150 nm / CH<sub>2</sub> 150 nm / CD<sub>2</sub> 150 nm. 1.8 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =30°,  $\alpha_{inc}$ =15°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening. Rutherford cross sections are used.

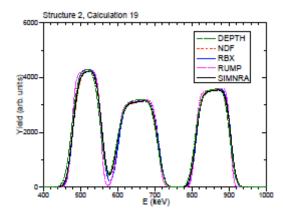


Figure 13. Calculation 19 - same as Calculation 18, but with given non-Rutherford cross sections.

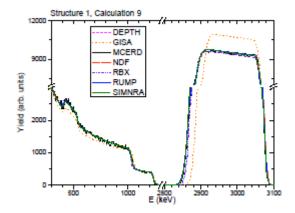


Figure 14. Calculation 9 - heavy ion RBS spectrum from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 3.5 MeV  $^7$ Li $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

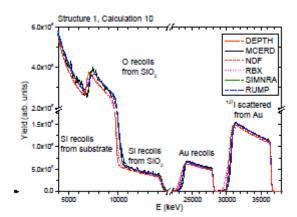


Figure 15. Calculation 10 - heavy ion ERDA spectrum from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 50 MeV  $^{127}I^{10+}$ ,  $\theta_{scatt}$ =40°,  $\alpha_{inc}$ =10°, IBM geometry, 200 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

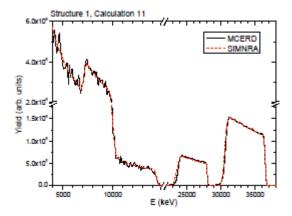


Figure 16. Calculation 11 - heavy ion ERDA, same as Calculation 10, but with a 300 ps time resolution for 50 cm time of flight, as opposed to a 200 keV resolution.

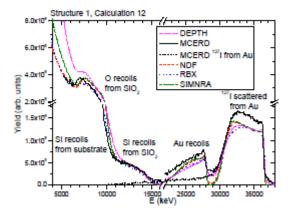


Figure 17. Calculation 12 - heavy ion ERDA, same as Calculation 10, but including mutliple scattering.

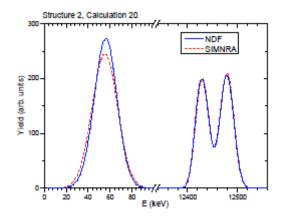


Figure 18. Calculation 20 - NRA spectrum from Si bulk /  $CD_2$  150 nm /  $CH_2$  150 nm /  $CD_2$  150 nm. 1 MeV  $^3$ He $^+$ ,  $\theta_{scatt}$ =170°,  $\alpha_{inc}$ =0°, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

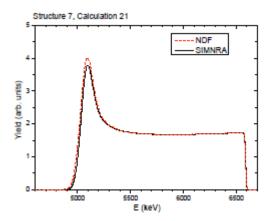


Figure 19. Calculation 21 - NRA spectrum from  $N_1Fe_4$  bulk. 1 MeV  $^2H^+$ ,  $\theta_{scatt}$ =170°,  $\alpha_{inc}$ =0°, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

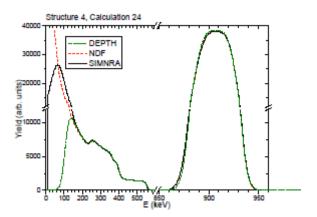


Figure 20. Calculation 24 - RBS spectrum with all broadening options, from Si bulk / SiO<sub>2</sub> 200 nm / Au 20 nm. 1.5 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling with Chu correction, multiple scattering, realistic beam and detector. No screening.

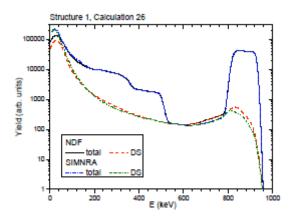


Figure 21. Calculation 26 - RBS spectrum, including the double scattering contribution (DS) from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.5 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening.

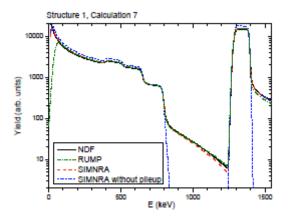


Figure 22. Calculation 7 - pulse pile-up calculation from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.5 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening. Pile-up included, 50 nA,  $T_W$ =5  $\mu$ s, no pile-up rejection system.

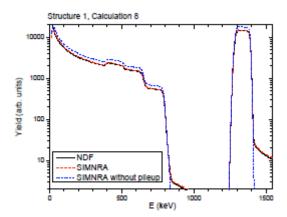


Figure 23. Calculation 8 - pulse pile-up calculation from Si bulk / SiO<sub>2</sub> 200 nm / Au 50 nm. 1.5 MeV  $^4$ He $^+$ ,  $\theta_{scatt}$ =150°,  $\alpha_{inc}$ =60°, IBM geometry, 16 keV FWHM, Bohr straggling, ideal beam and detector. No screening. Pile-up included, 50 nA,  $T_W$ =0.5  $\mu$ s, pile-up rejection system with 0.5  $\mu$ s resolution.

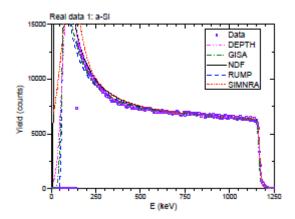


Figure 24. Experiment a-Si - 2 MeV <sup>4</sup>He RBS spectrum from amorphised Si.

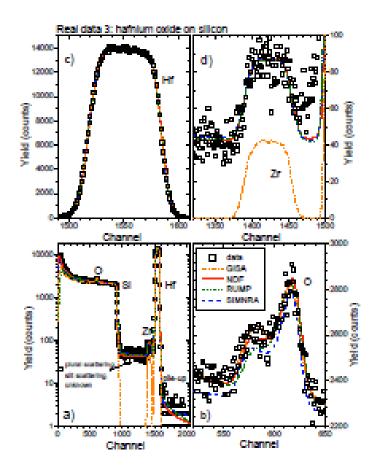


Figure 25. Experiment HfO - 2.5 MeV <sup>4</sup>He RBS spectrum from a hafnium oxide film on silicon. a) The entire spectrum; b) O signal; c) Hf signal; d) Zr signal.

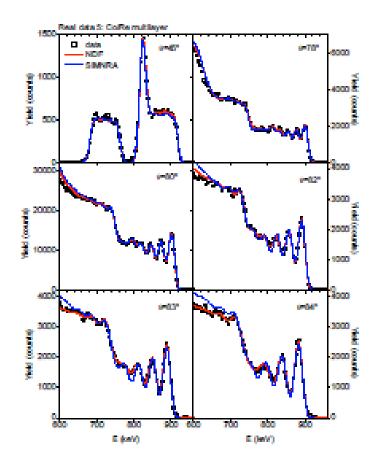


Figure 26. Experiment Co/Re - 1 MeV  $^4$ He RBS spectra from a Si bulk / Re 5nm/(Co 2nm/Re 0.5 nm) $_{16}$  multilayer, taken at different angles of incidence in the Cornell geometry.