#### **Mixed-material studies in PISCES-B**

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Work performed as part of US-EU Collaboration on Mixed-Material PMI Effects for ITER

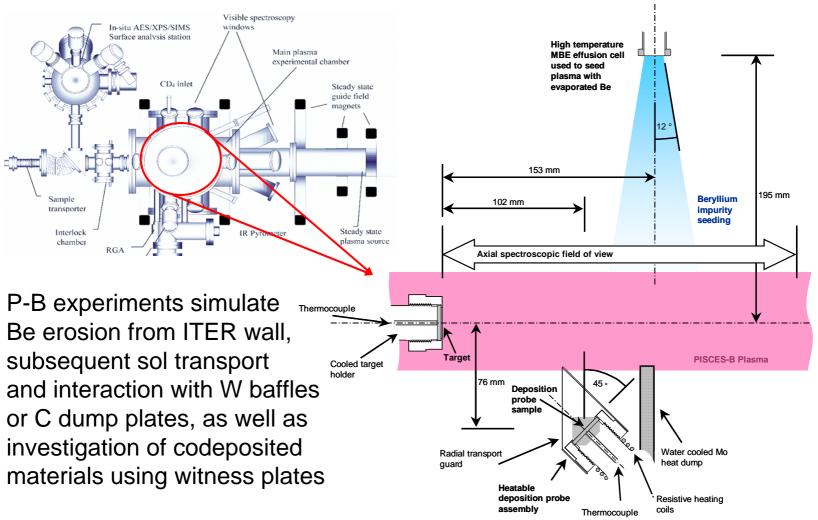
### Outline

- Introduction
- Technical results
  - Temporal behavior of chemical erosion suppression
  - D retention in, and release from, Be- rich codeposits
  - Response of Be/C to thermal transients
  - Be/W formation conditions
- Summary of possible mixed-material implications for ITER



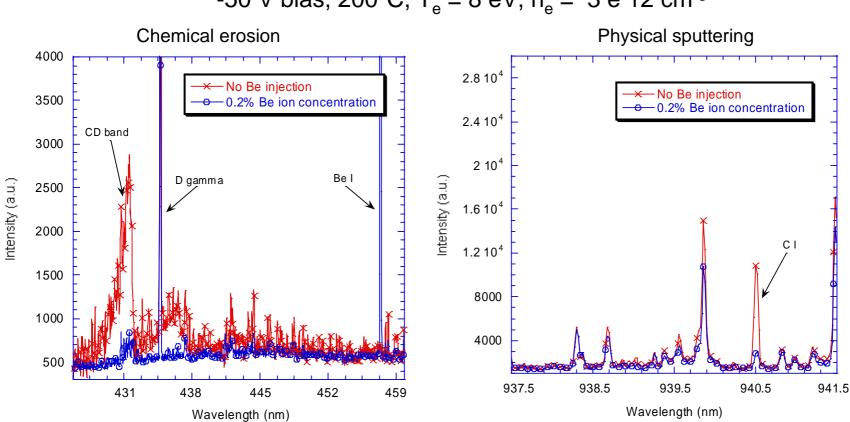


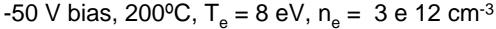
#### PISCES-B has been modified to allow exposure of samples to Be seeded plasma





#### A small beryllium impurity concentration in the plasma drastically suppresses carbon erosion



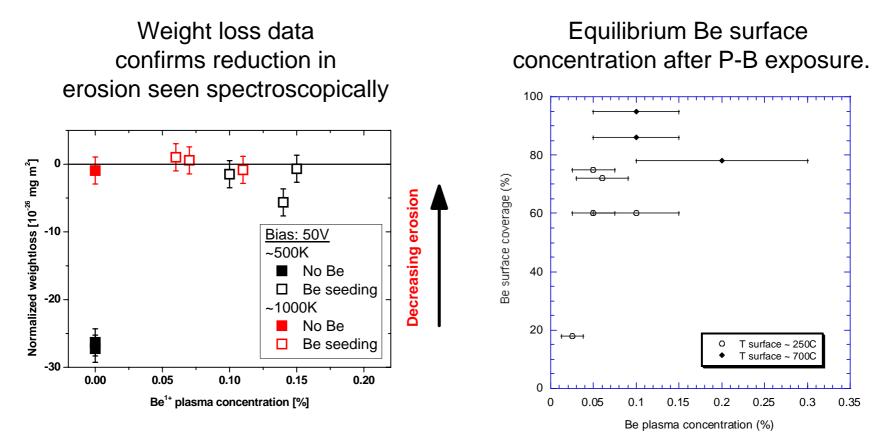




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# Be-rich surface layers form during exposure and shield underlying carbon from erosion

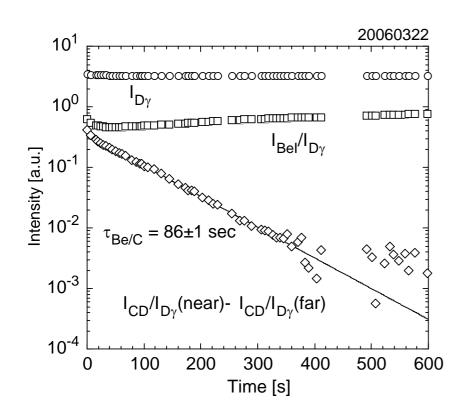


 ITER is expected to have 1-10% Be impurity concentration in the divertor plasma





# Erosion suppression exhibits a temporal evolution ( $\tau_{Be/C}$ )



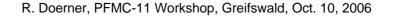
- Understanding the temporal behavior is critical to determining the fundamental mechanisms responsible for erosion mitigation
- PMI modeling codes should be able to reproduce temporal behavior to provide confidence (D. Borodin will describe this)





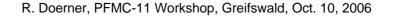
- Incident Be ions react with C target atoms forming  $Be_2C$
- The presence of Be in the surface of the carbon target reduces chemical erosion of the surface
- Once all surface carbon is bound as Be<sub>2</sub>C, the Be<sub>2</sub>C layer thickness saturates
- Subsequent Be ion bombardment enriches the surface with Be that is easier to erode (compared to the Be in  $Be_2C$ )
- Primary species eroding from the target and being codeposited with deuterium is Be





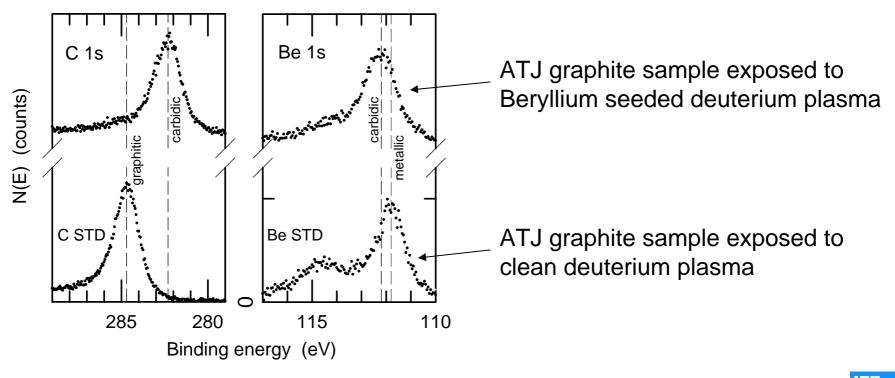
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### In-situ XPS analysis shows carbidic bonding

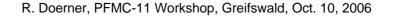
• Virtually all C in the surface is bound in carbidic bonds after mitigation of chemical erosion



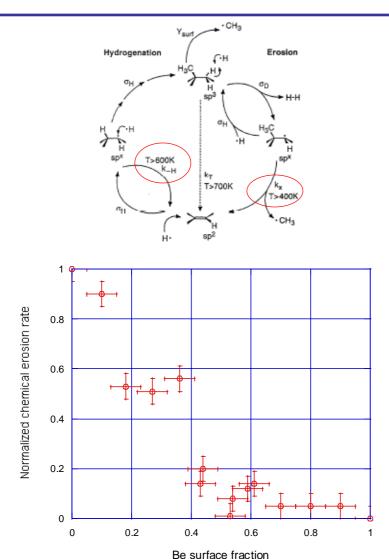


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#### Be doping seems to act like B doping, inhibiting chemical erosion



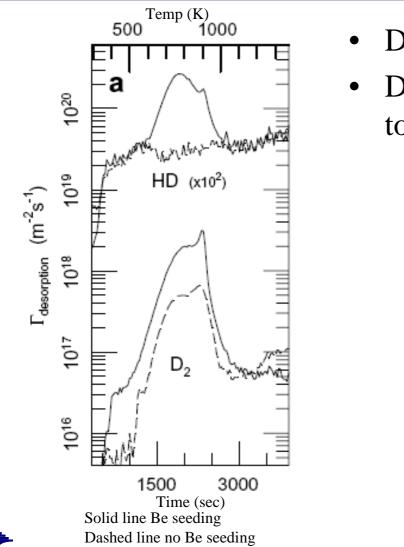
 Graphite dopants can alter the balance between hydrogenation steps that lead to thermal chemical erosion [Roth JNM 266-269(1999)51.]

• In-situ Be seeding (Be<sub>2</sub>C surface formation) may also affect chemical sputtering term

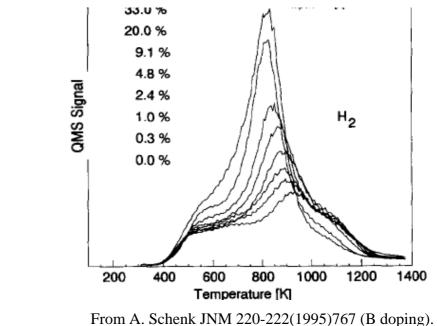




## In-situ Be doping of graphite exhibits similar behavior to boron doping of graphite



- Dopant increases retention
- Dopant shifts hydrogenic release to lower temperature





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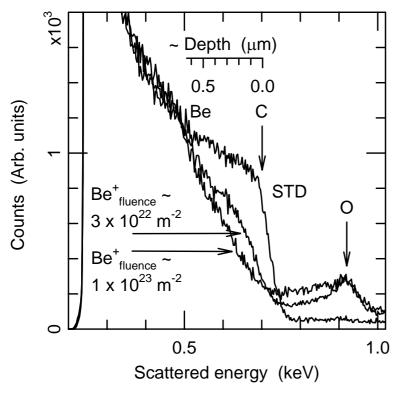
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### Be<sub>2</sub>C layer thickness saturates

UW-Madison RBS spectra of P-B samples exposed to unseeded and Beseeded plasma



From M. Baldwin et al., in press JNM

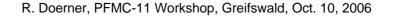
- Be layer observed after ~3E22 Be<sup>+</sup>/m<sup>2</sup> (i.e 1600 s) accounts for virtually all incident Be
- Be layer after 1E23 Be<sup>+</sup>/m<sup>2</sup> (i.e 4800 s) accounts for only ~30% of incident Be
- $\tau_{Be/C}$  under these plasma exposure conditions would be ~ 2000 sec



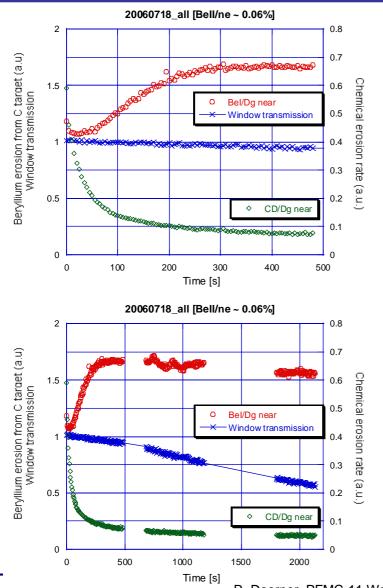


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### Be first shuts down C chemical erosion, then subsequent Be re-erodes from surface



- Be oven opens at t = 0 sec.
- Be ions arriving at t < 50s shut down chemical erosion by forming Be<sub>2</sub>C surface layer [Baldwin JNM 2006 available on-line]
- Be<sub>2</sub>C surface thickness saturates after carbide forms 50s in this exposure [Baldwin JNM 2006]
- Once Be<sub>2</sub>C is formed, subsequent Be arriving (T > 50 s) is more easily eroded and begins coating windows



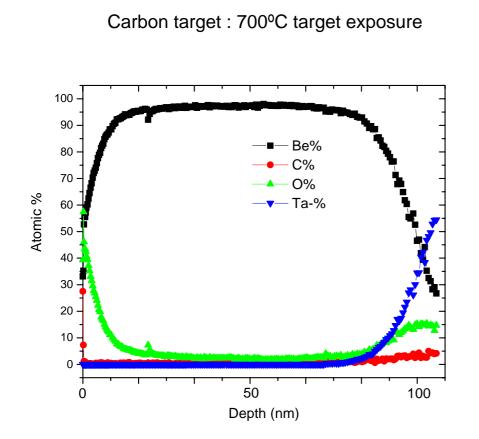
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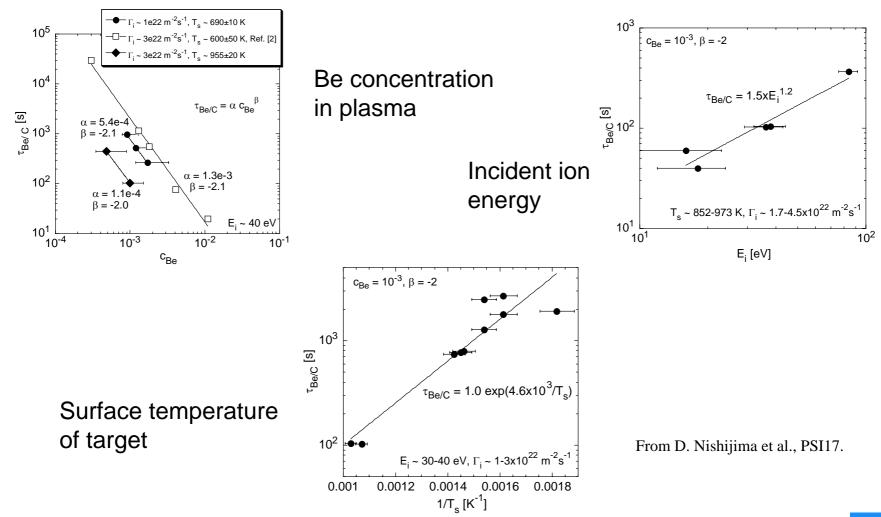
## WPM samples show collection of beryllium-rich codeposits during Be seeding runs



- t = 0 sec codeposited layer begins to form on Ta witness plate (100 nm in depth scale)
- Only a small amount of C is initially collected (90 – 100 nm depth scale)
- Almost pure Be (little O) continues to be deposited until discharge terminates (0 nm depth scale, surface of codeposited film)



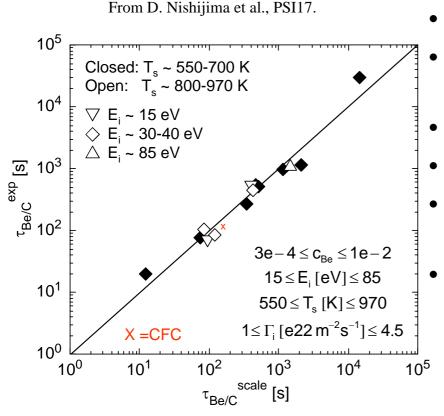
### Chemical erosion suppression time $(\tau_{Be/C})$ depends on several variables that can be varied almost independently





## PISCES chemical erosion mitigation time scaling predicts suppression between ELMs in ITER

 $\tau_{\rm Be/C}^{\rm scale} \,[\rm s] = 1.0 x 10^{-7} \; c_{\rm Be}^{-1.9 \pm 0.1} \; E_{\rm i}^{0.9 \pm 0.3} \; \Gamma_{\rm i}^{-0.6 \pm 0.3} \; \exp((4.8 \pm 0.5) x 10^3 / T_{\rm s})$ 



- Surface temperature effects reaction rate
  - Be plasma concentration effects arrival rate at surface
  - Ion energy effects erosion rate
  - Ion flux impacts through redeposition
  - Type of graphite does not seem to play a significant role (ATJ vs. CFC) (R. Pugno poster)
- Scaling law using these variables has been developed to allow extrapolation to ITER

conditions ( $\tau_{\text{Be/C}}^{\text{ITER}} \sim 6 \text{ msec}$ ) [ $c_{\text{Be}} = 0.05, E_i = 20 \text{ eV}, T_s = 1200 \text{ K} \text{ and } \Gamma_i = 10^{23} \text{ m}^{-2} \text{s}^{-1}$ ]

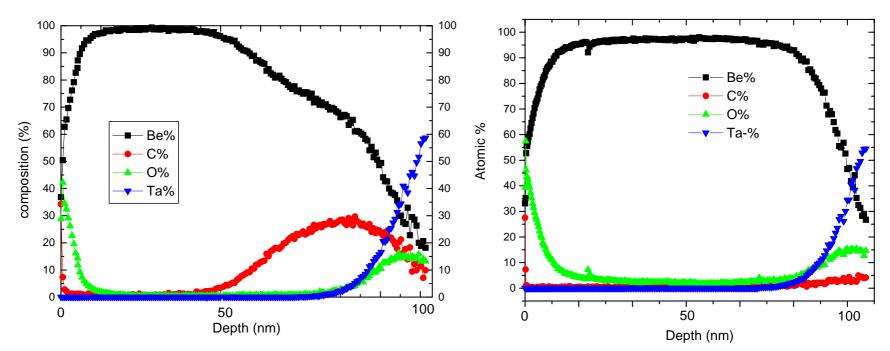




## Faster mitigation time results in less C content in witness plate codeposits

Carbon target : 300°C target exposure

Carbon target : 700°C target exposure

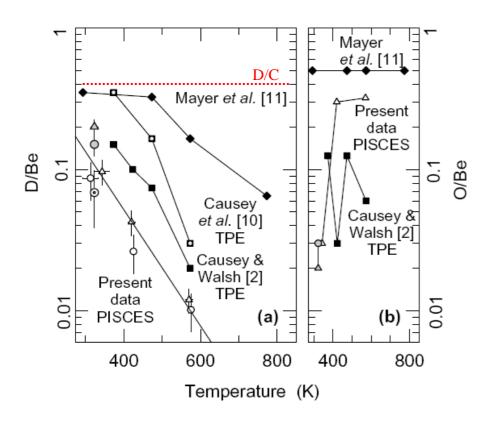


More C is detected in codeposits during lower C target temperature exposure (possibly due to a combination of lower chemical erosion yield and/or quicker beryllium carbide layer formation at higher temperature)





## T accumulation in ITER is dominated by codeposited material

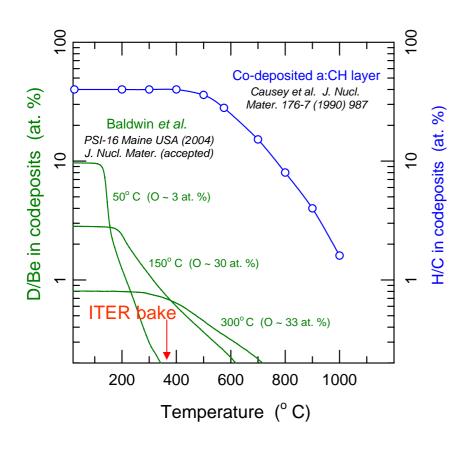


From Baldwin et al. JNM 337-339(2005)590. Refs. 2, 10 & 11 therein

- Impurity content in Be codeposits impacts D retention level
- Surface temperature during codeposition has a more pronounced effect on retention
- Be codeposits will be in line-ofsight of erosion location
- Role of oxygen (i.e. BeO) in codeposits still needs to be determined

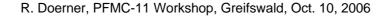


#### T retained in Be rich codeposits can be more easily removed during divertor bakeout



- Although more hydrogen isotopes are retained during lower surface temperature Be codeposition, they are more easily desorbed (role of oxygen needs to be determined)
- ITER can bake divertor to 375°C (after coolant drain)
- Oxygen bake may not be needed to remove fuel atoms from codeposits

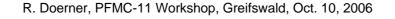




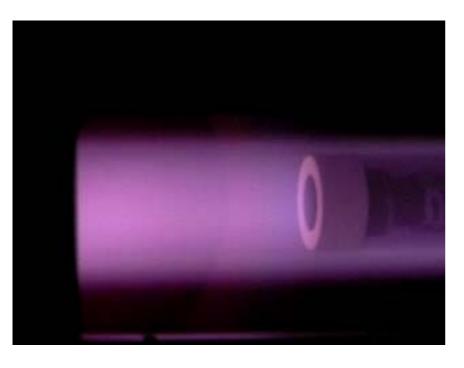
Thermal transient experiments: Motivation for positive pulse biasing

- PISCES has shown that Be plasma impurities suppress carbon target erosion at temperatures up to 1000°C
- ITER will experience large temperature excursions (up to 3800°C) at the carbon dump plates during periodic ELMs
- Will the thin, surface Be, Be/C layers survive such dramatic temperature excursions?
- It is possible to simulate the large temperature excursions associated with ITER ELMs in PISCES-B using positive sample biasing during plasma discharges.





## Large power loads can be drawn to P-B sample during positive biasing

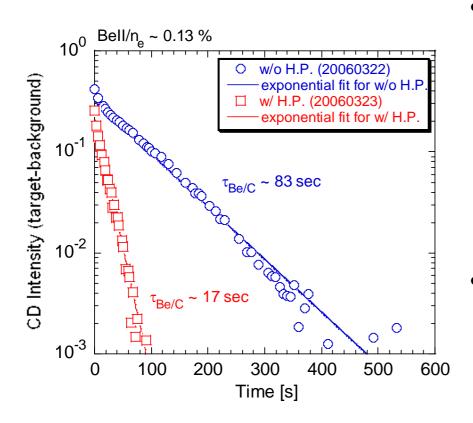


- During 1.5 MW/m<sup>2</sup> power pulse graphite surface temperature rises to ~2000°C (by pyrometers)
- Bulk graphite temperature rise at back of sample
  ~20°C during 0.1 s. pulse (thermocouple)
- Surface temperature rise is limited by power supplies (IPP has supplied a new power supply as part of US-EU collaboration)





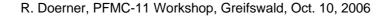
## Transient surface heating promotes $Be_2C$ formation leading to shorter mitigation times



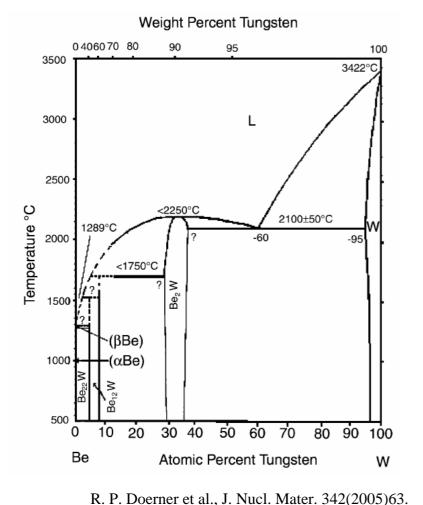
Surface temperature during heat pulse ~ 1200°C [from R. Pungo et al., PSI17]

- Pulsing surface temperature to the 1200°C range results in faster chemical erosion suppression
  - Be<sub>2</sub>C disassociates at ~2200°C at 1 atm
  - Beryllium boiling point = 2471°C at 1 atm
- D retention during transient surface heating also increases by ~50% both with and without Be plasma seeding





## Tungsten beryllides (Be/W) have very recently become a big mixed-material concern



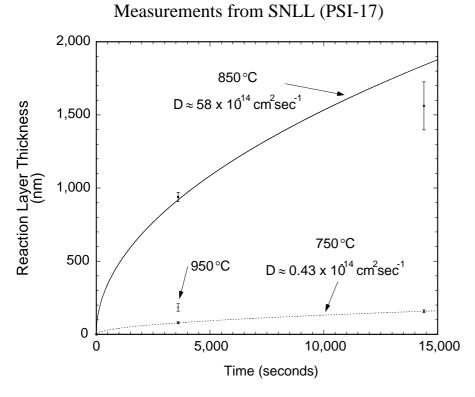
- Be<sub>2</sub>W, Be<sub>12</sub>W and Be<sub>22</sub>W are all stable beryllides with significantly lower melting temperature than W
- Possibility for a major malfunction was realized (fortuitously?) during PISCES Be seeding experiments, where the W crucible holding molten Be experienced melting during operation at only ~1200°C



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## Tungsten beryllide (Be<sub>x</sub>W) formation may plague hot W plasma facing components

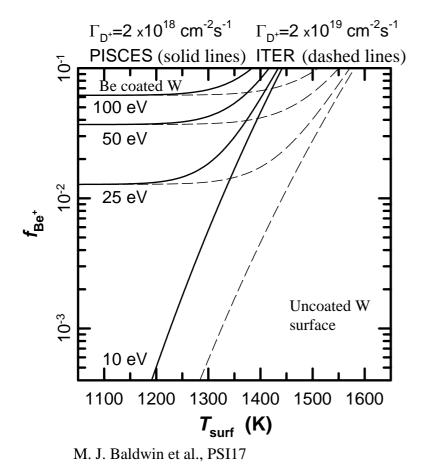


- Be<sub>2</sub>W and Be<sub>12</sub>W appear preferred (Be<sub>22</sub>W not seen)
- Beryllides only form in high temperature W surfaces (> 600°C)
- Be diffusion rate into W becomes significant above ~800°C
- At high temperature, Be availability (high vapor pressure of Be) on the surface can limit growth rate



### Plasma conditions play a dominant role in determining the Be availability on the surface

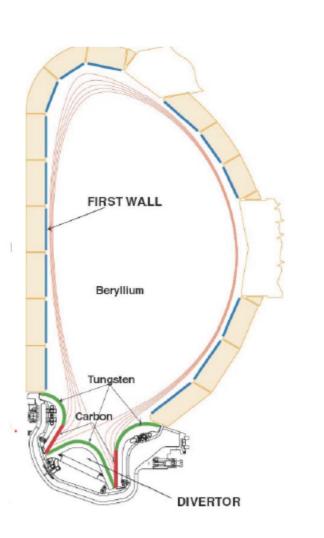
 $f_{\text{Be}} \Gamma_{\text{plasma}}(1-R_{\text{f}}) = Y_{\text{D-Be}} \Gamma_{\text{plasma}}(1-R_{\text{d}}) + f_{\text{Be}} Y_{\text{Be-Be}} \Gamma_{\text{plasma}}(1-R_{\text{d}}) + \Gamma_{\text{evap}}(1-R_{\text{e}}) + D_{\text{bulk}}$ 



- At high surface temperature, Be sublimation may prevent significant beryllide formation
- Sputtering at higher incident ion energies also tends to prevent significant beryllide formation
- Higher incident plasma flux tends to push energy, and temperature, necessary to limit beryllium availability to larger values



### How might mixed materials impact ITER?



- Due to elevated temperature of C dump plates, carbides will likely form and limit C erosion
- Be deposition on W baffles will likely not result in significant beryllide formation  $(T_W \sim 400^{\circ}C)$
- If a full C divertor were employed, carbide formation on regions of the baffles, where the temperature is lower, would take longer, resulting in more C erosion and thereby more hard-to-remove tritium
- If a full W divertor were used, beryllide formation near the strike points could be a concern (perhaps an issue for the JET ITER-like wall experiments)
- Beryllide formation in ITER may be a concern on the W cassette liner 'louvers' (that are designed to be hot surfaces)

