

# ***Characterization and erosion of metal-containing carbon layers***

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## ➤ Introduction

- *Importance of mixed layers*
- *Why are we interested in metal-containing amorphous carbon layers (a-C:Me)?*

## ➤ Characterization

- *Which material systems are investigated?*
- *How are specimens produced?*
- *Which characterization techniques are applied to obtain which material property?*

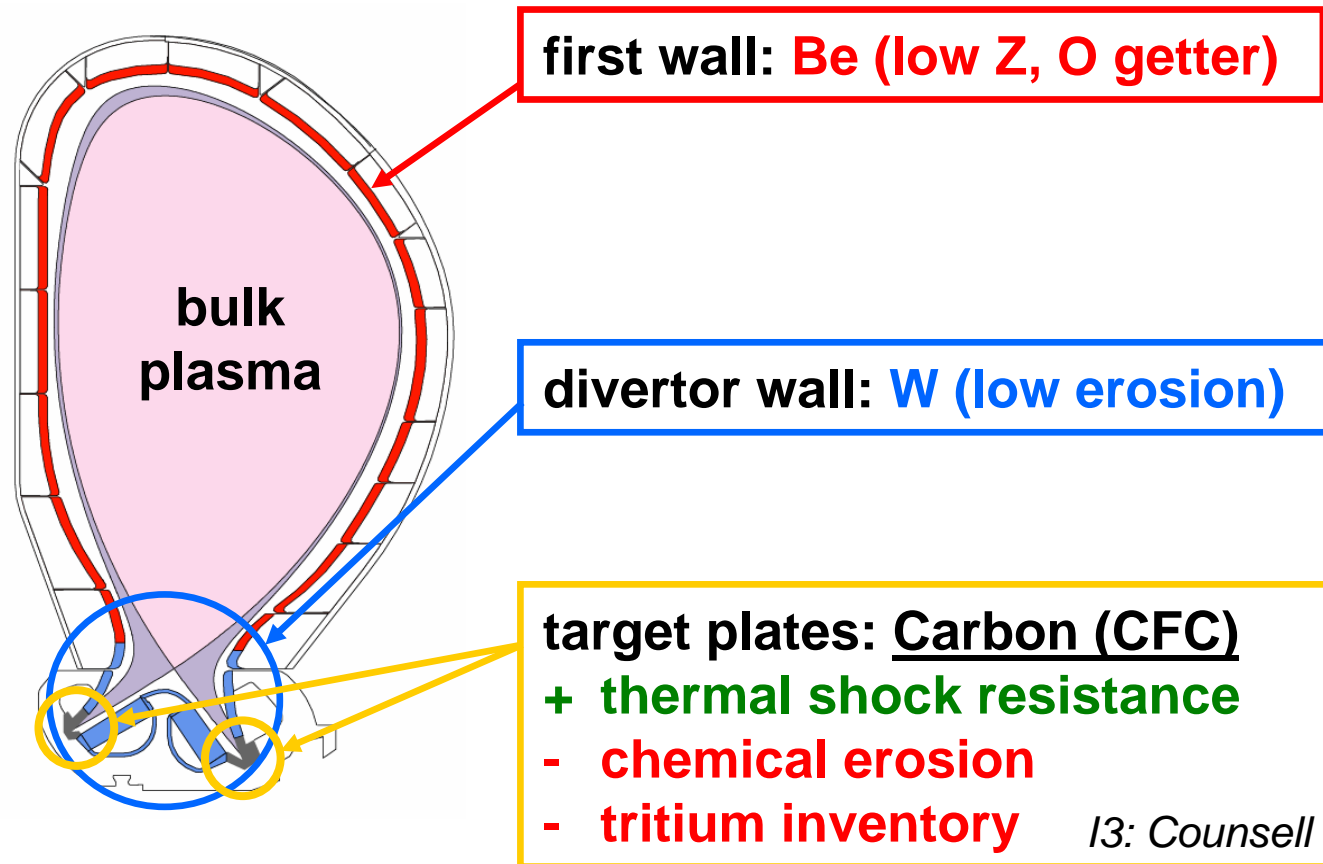
## ➤ Chemical erosion by hydrogen impact

- *Total erosion yield of carbon: IBA*
- *Chemical erosion yield (CD<sub>4</sub>): QMS*

## ➤ Conclusion

## Plasma-facing materials: ITER design (Mix)

SEM



## JET: ITER-like wall project

*110-13: Matthews, Hirai, Neu, Lungu, P06, P50-52*

## Chemical erosion of **carbon** by hydrogen

↳ source term: re-deposited C layers containing **tritium**

↳ material mix (Be, W, C, steels, ...) ⇔ erosion / deposition

↳ **mixed layers:** properties

- erosion *(18: Doerner)*
- H-retention
- composition
- thermal stability
- ...

↳ microstructure

C rich

**Reduction of chemical erosion by doping**

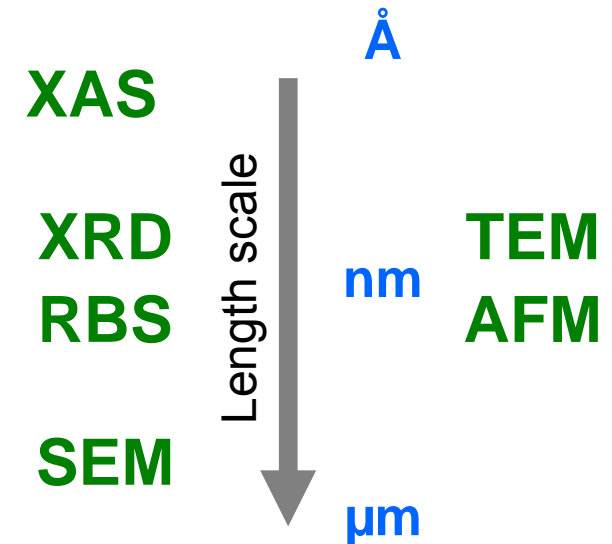
**mechanism**

- to simulate mixed layers
  - ↳ magnetron sputtered metal-containing carbon films
- **well characterized model materials**
  - ↳ **laboratory erosion studies on a-C:Me films**
    - ↳ **focused on W + C** (additional: Ti, V, Zr)

## Investigation of mixed layers

*composition, distribution in depth, lateral homogeneity, impurities, crystallinity, chemical state, film morphology*

- ↪ characterization on
- atomic level
  - nanometer scale
  - micrometer scale



## ↪ chemical erosion

↪ energy & mass-separated hydrogen ion beam:

- + **total erosion yield**: MeV ion beam analysis (weight loss; in-situ)
- + **chemical erosion yield**: mass spectrometry

# Production and Characterization

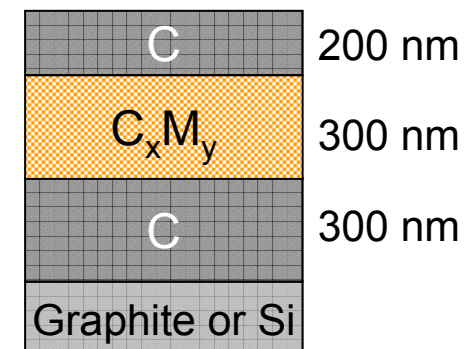
# Production of a-C:Me layers

- metal-doped amorphous carbon layers:
  - **magnetron sputter deposition** dual source, 300 K

- **single** and **triple** layers on graphite or Si

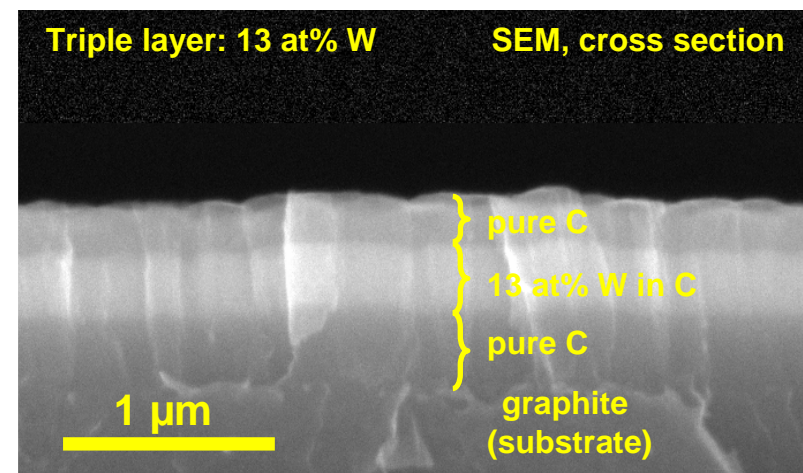
↙ erosion  
0.2-2 μm

↙ thermal treatment, diffusion  
↙ no surface-substrate influence



- **dopant** (**W**, Ti, V, Zr)
- **concentrations** (0 - 20 %)

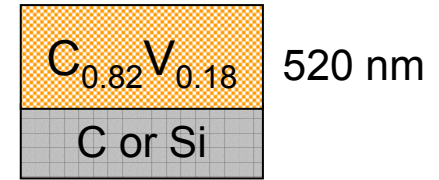
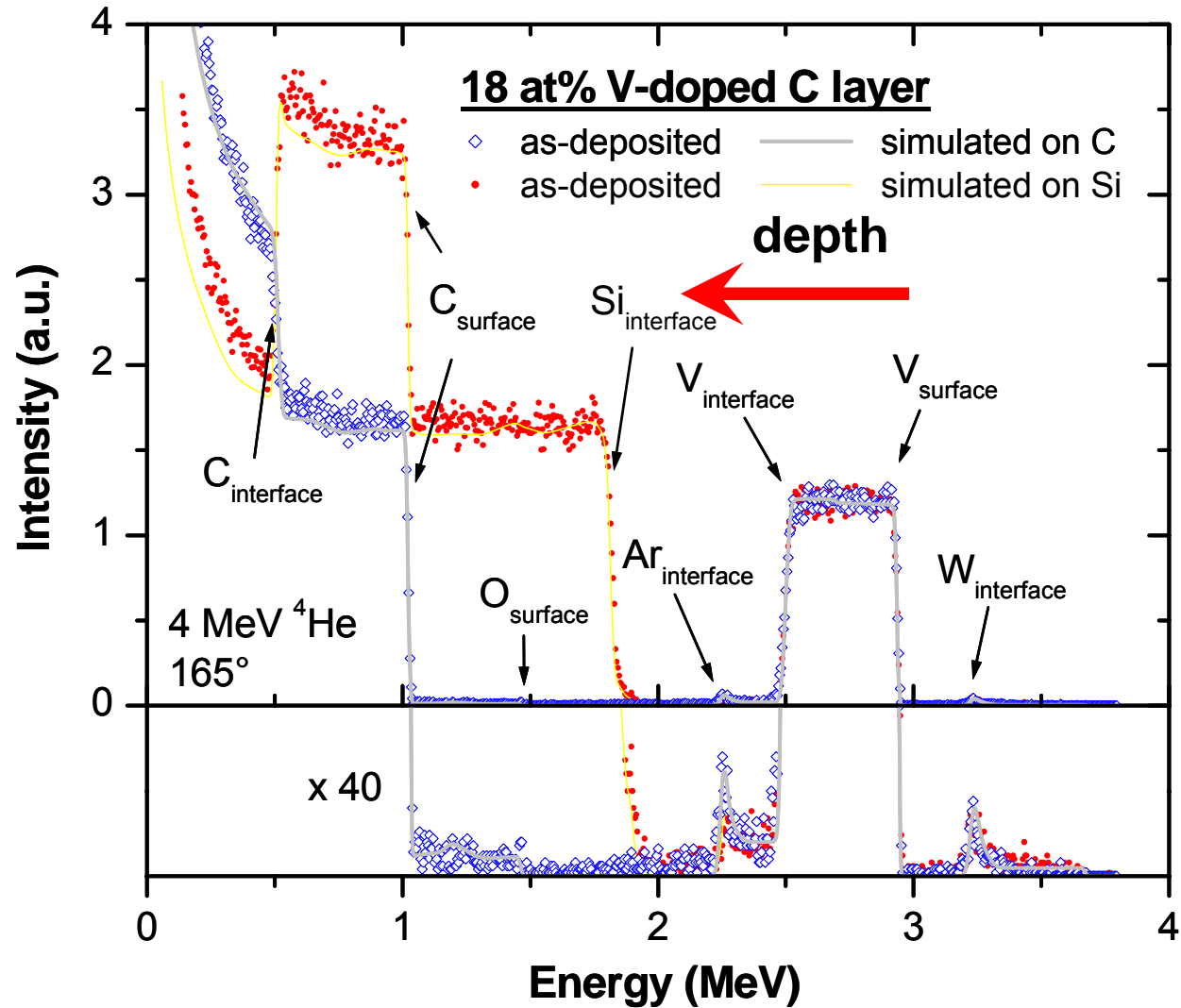
- **annealing:** 500-1300 K (0.25 & 2 h)  
(e.g. carbide formation, diffusion)



*composition, homogeneity, morphology*



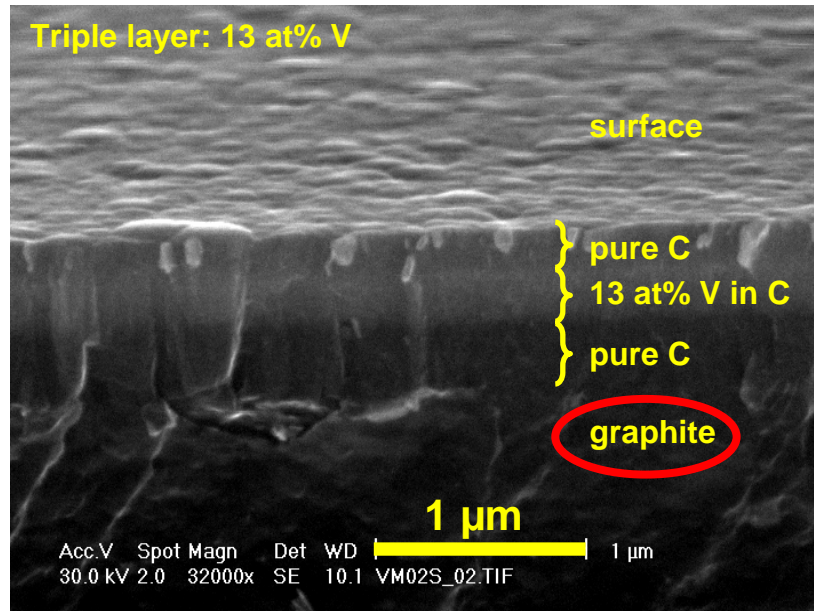
# Composition, distribution & impurities (RBS)



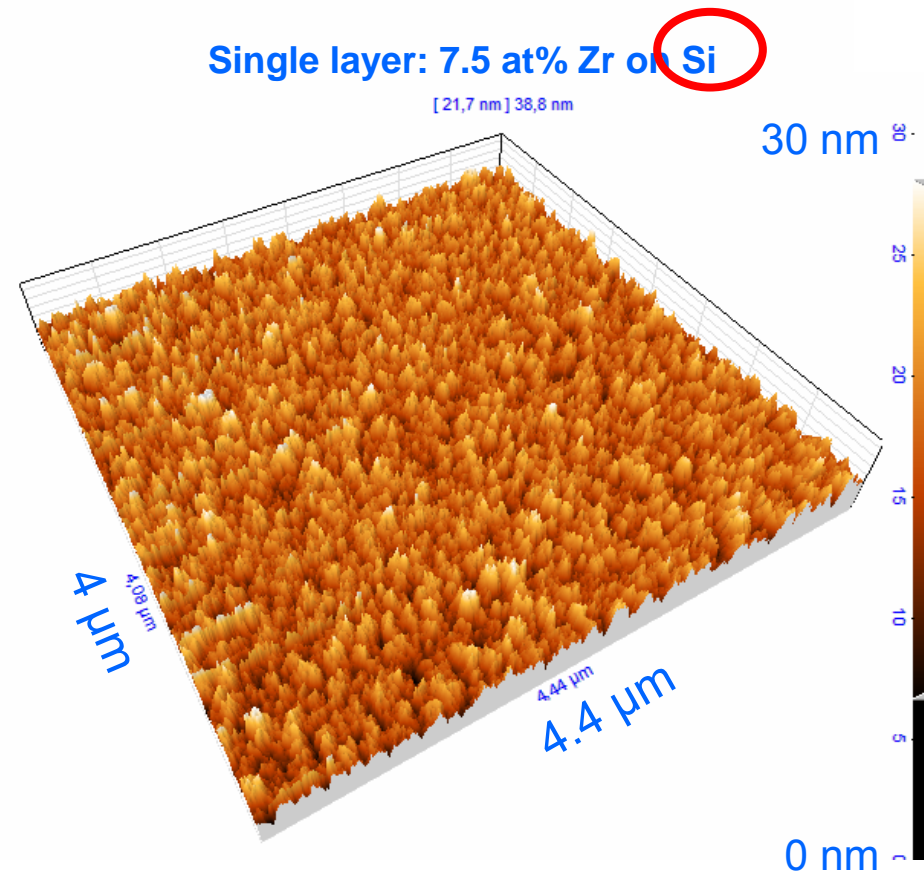
- dopant homogeneity
- O < 1 at%
- Ar ~ 1 at%  
released by annealing
- W < 0.01 at%  
unusual

H-RBS

# Layer morphology (SEM, AFM)



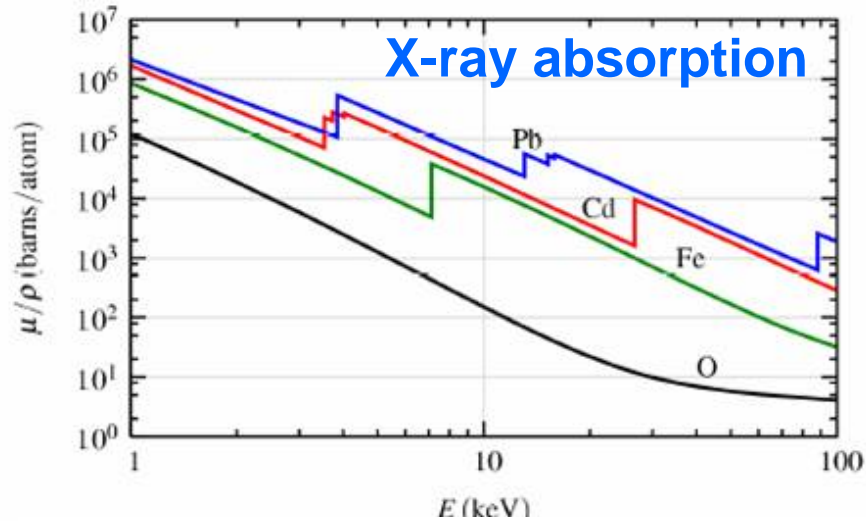
- no significant changes by annealing



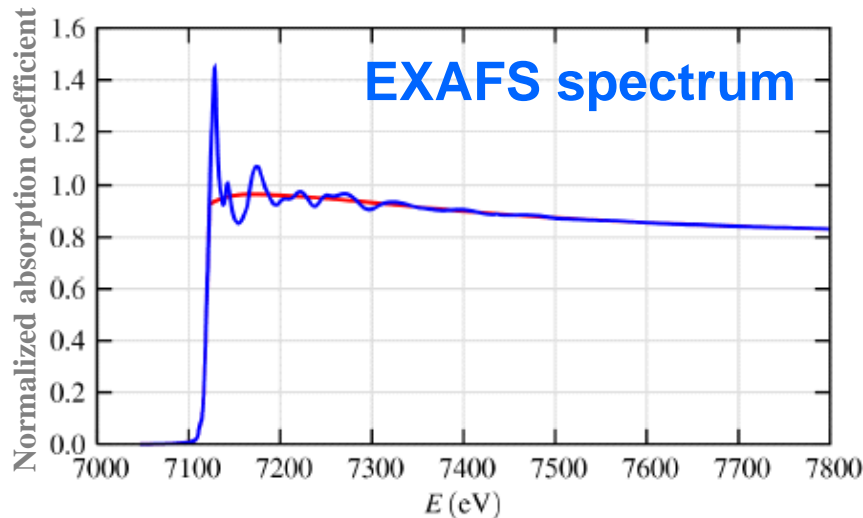
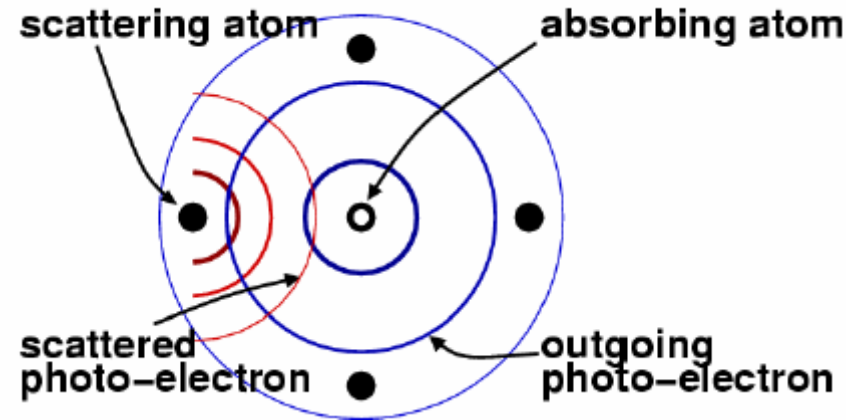
- homogeneous, columnar growth
- structures size triggered by substrate roughness
- no change in columnar growth by dopant

# Chemical bonding of metals and crystallinity

## EXAFS: Extended X-ray absorption fine structure



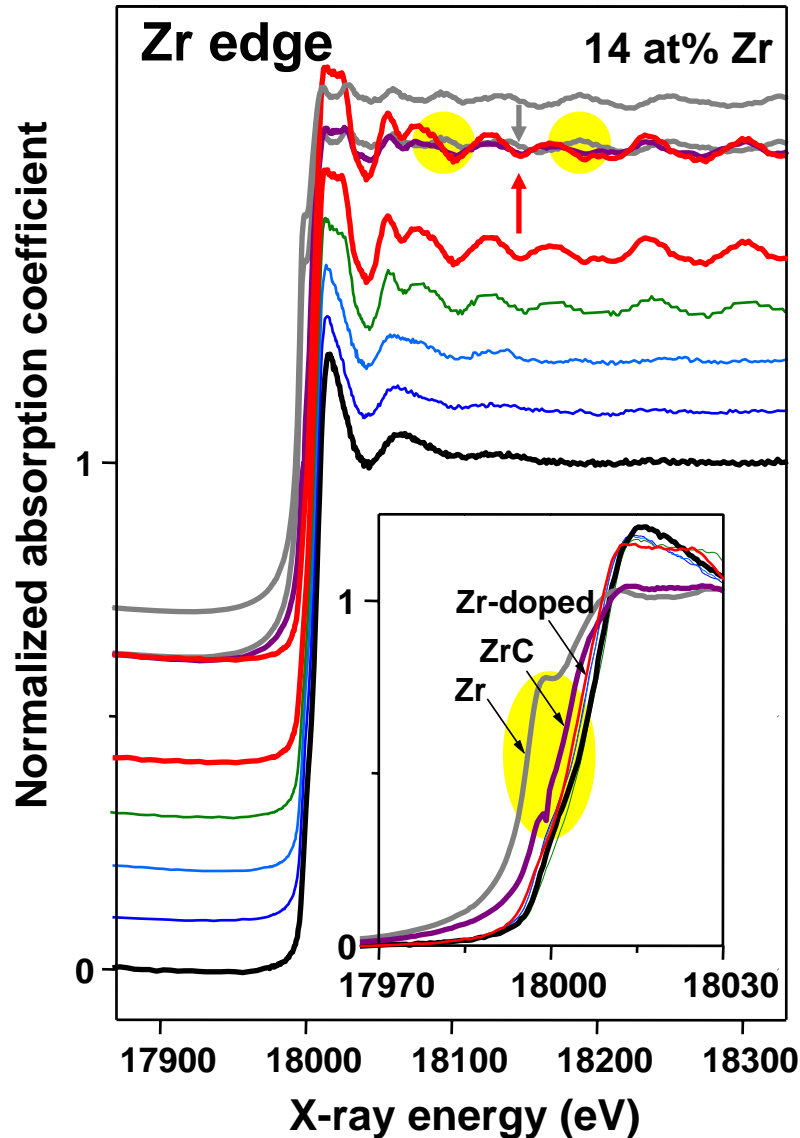
### Photo electrons



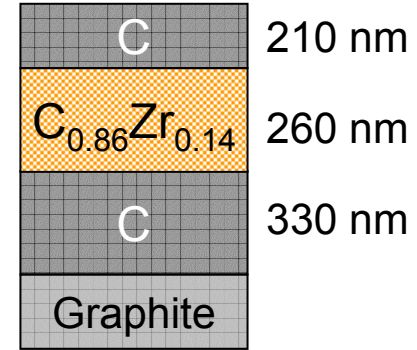
### Interference / Oscillations $\Rightarrow$ EXAFS

Information about the local atomic environment of the absorbing atom (Neighboring atoms  $N$ , distance  $R$ , disorder  $\sigma$ )

# Local atomic environment (XAS: EXAFS)



Zr } references  
 ZrC }  
 1300 K, 1/4 h  
 1100 K, 2 h  
 900 K, 1/4 h  
 700 K, 2 h  
 as-deposited (300 K)



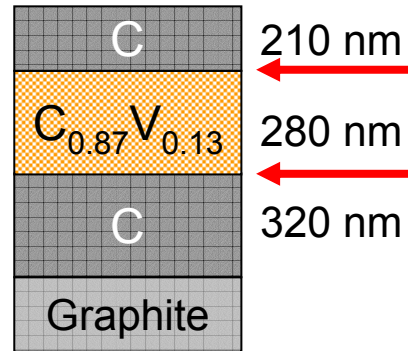
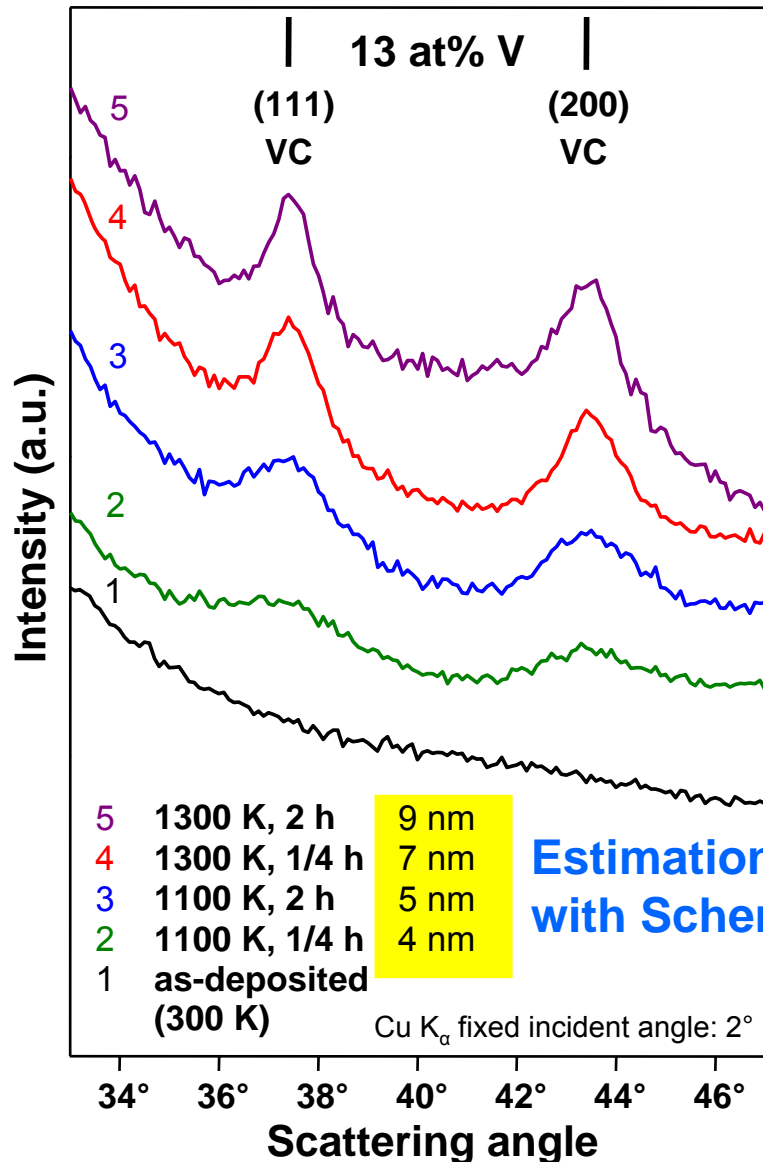
## Doping with Ti, V & Zr

- “as-deposited”: - **amorphous** / disorder  
- **non-metallic** state
- **carbide** structure already at 1100 K  
(qualitative  $\Rightarrow$  quantitative)

## Exception W-doping:

- “as-deposited”: higher **order**
- **annealed**: only slight changes

# Crystallinity of layers (XRD): annealing



**Diffusion:**  
**<20 nm (RBS)**

## Doping with Ti, V & Zr

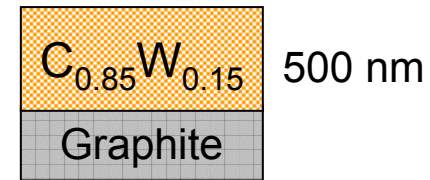
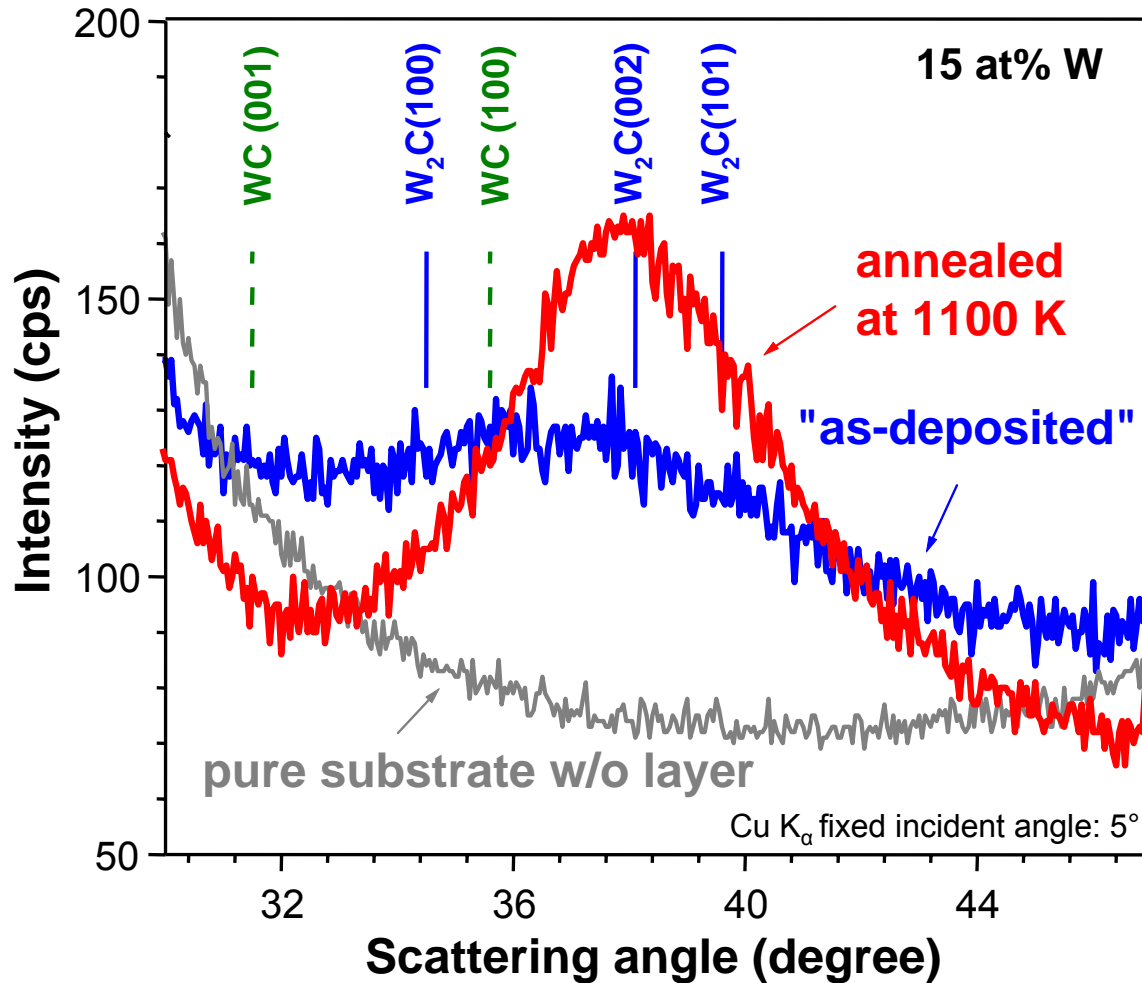
atomically deposition → crystallite growth

- **carbide formation** after annealing (carbon-poor TiC, VC, ZrC)
- crystallite size increasing with T and t

**Estimation of crystallite size with Scherrer's formula**

↳ **exception W-doping**

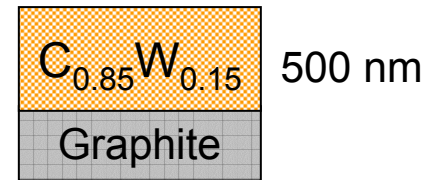
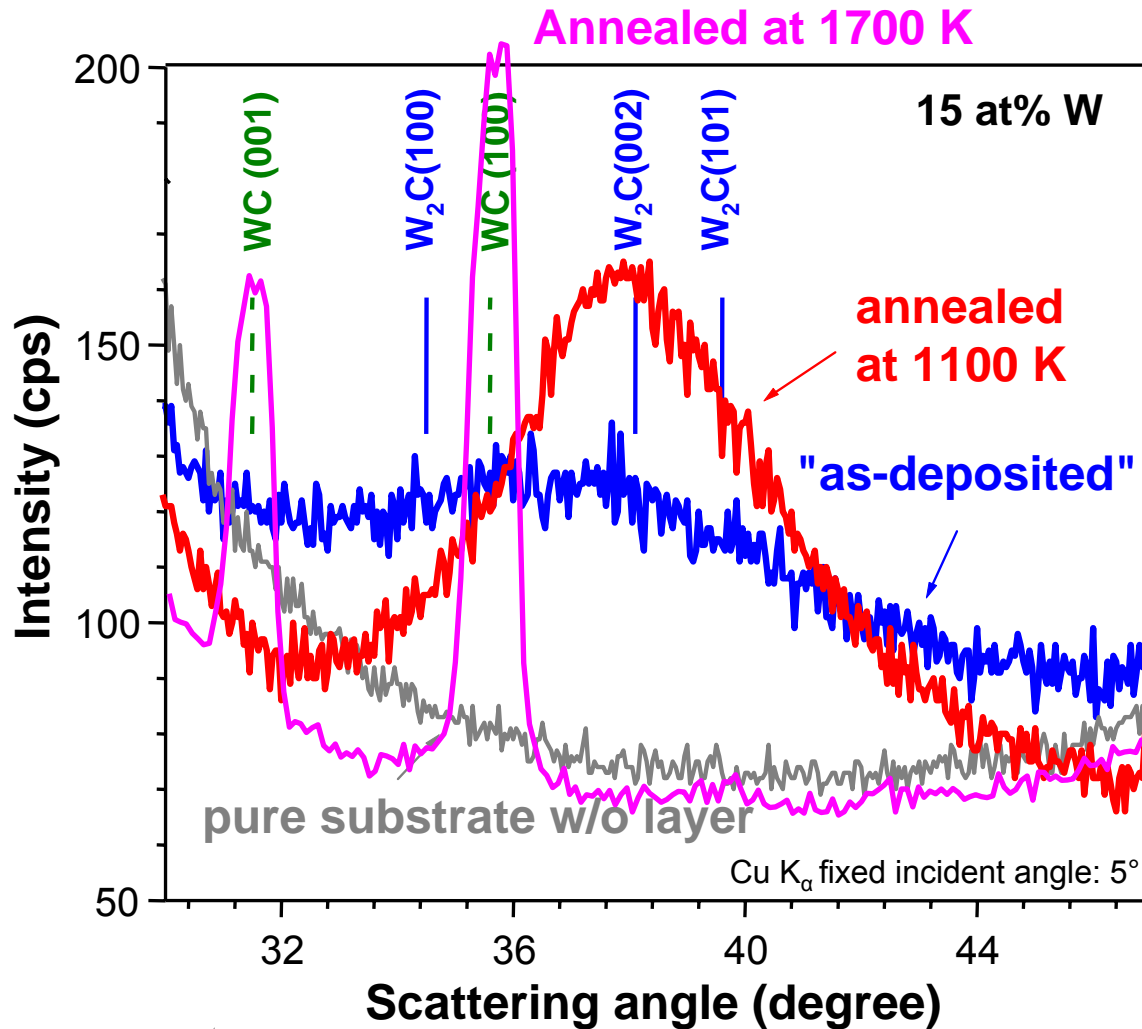
# Crystallinity of W-doped layers (XRD)



- already “as-deposited” show peak
- sub-carbide ( $W_2C$ ) instead of carbide ( $WC$ ) more pronounced after annealing
- grain size: ~ 2 nm (always) (estimation with Scherrer’s formula)



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## Annealing at 1700 K

↪ **WC** → larger grains  
>20 nm

TEM



# Chemical erosion

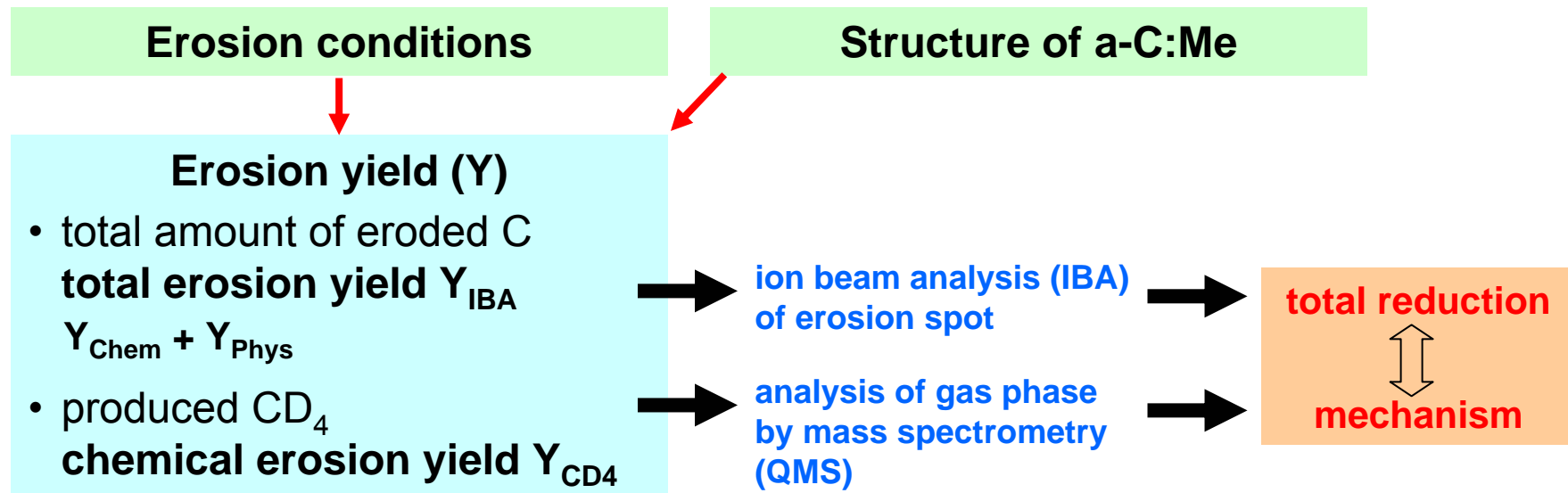
## Experimental setup

- mono-energetic mass-separated ion beam:  
30 eV, 200 eV, 1 keV D ( $D_3^+$ )
- flux:  $\sim 10^{19}$  D/m<sup>2</sup>s
- temperature controlled (RT-1450 K)

## Experimental procedure

- annealing to 1100 K  $\Rightarrow$  carbide grains: W 2 nm, other 4-8 nm
- D bombardment of a-C:Me
  - D energy: **30 eV / 200 eV**
  - temperature: **fixed RT / ~750 K**  $3 - 7 \times 10^{23}$  D/m<sup>2</sup> } **two types of measurements**  
**stepwise increased: RT - 1000 K** }  
 $4 - 7 \times 10^{21}$  D/m<sup>2</sup> per step, total  $< 10^{23}$  D/m<sup>2</sup>

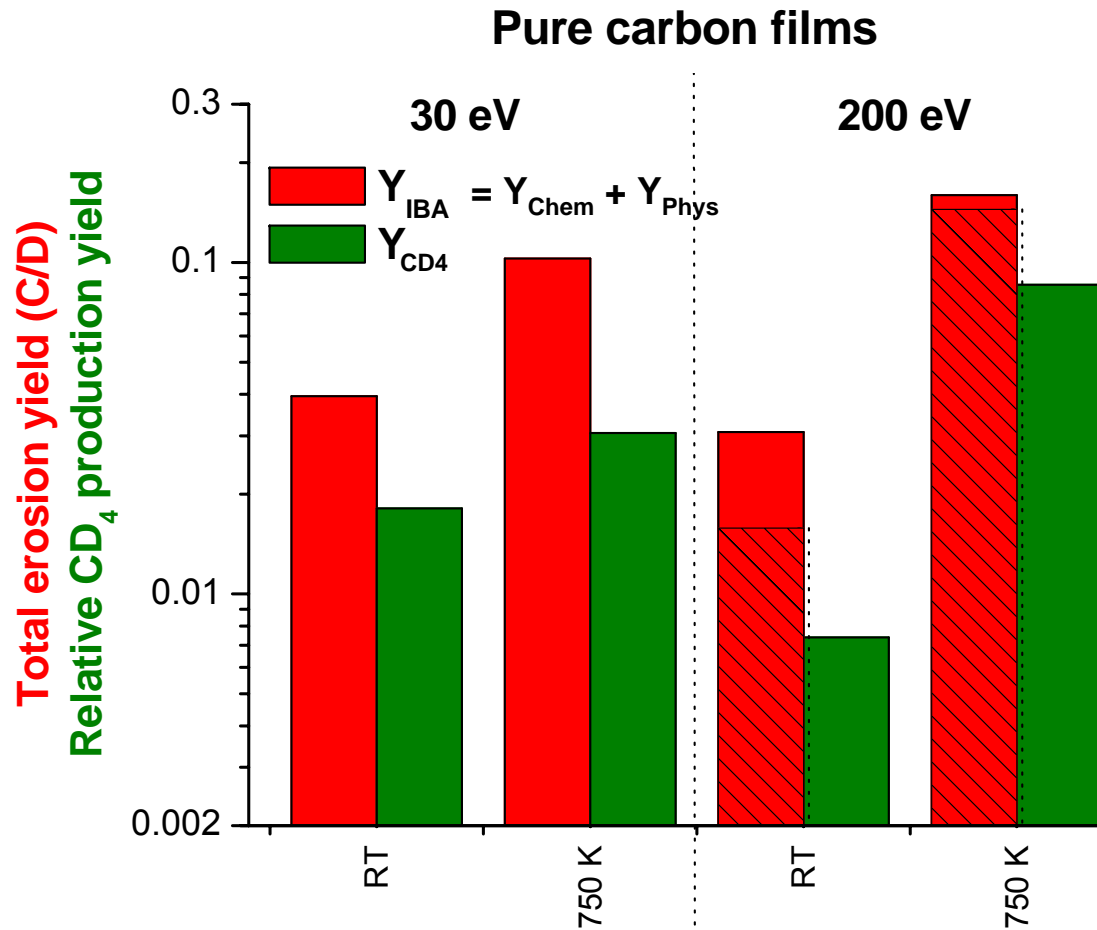
## Metal-containing amorphous carbon films (a-C:Me)

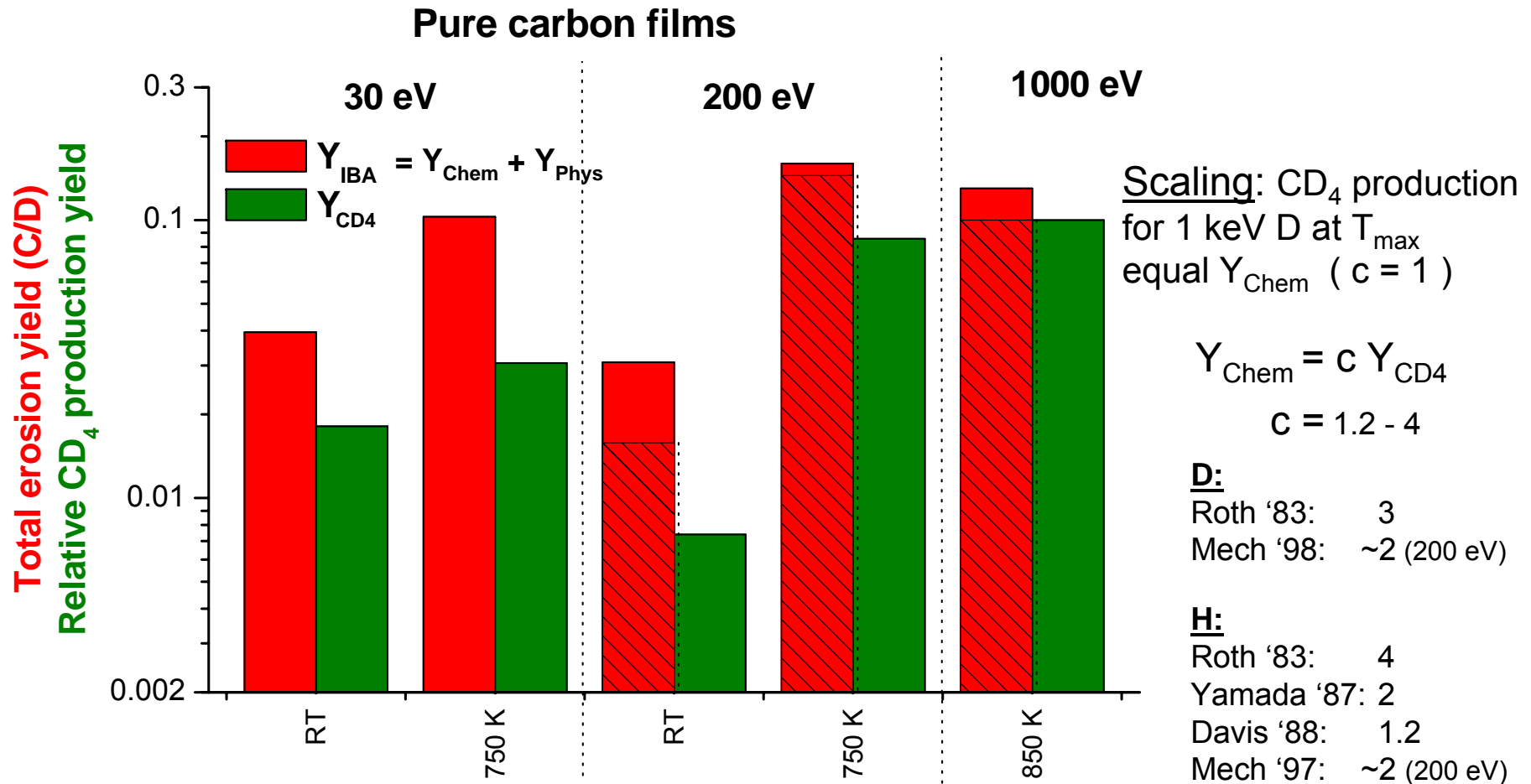


$$Y = \frac{\sum C_{removed}}{\sum D_{incident}}$$

Influence of doping on produced hydrocarbons expected  
⇒ reflected in amount of produced  $CD_4$

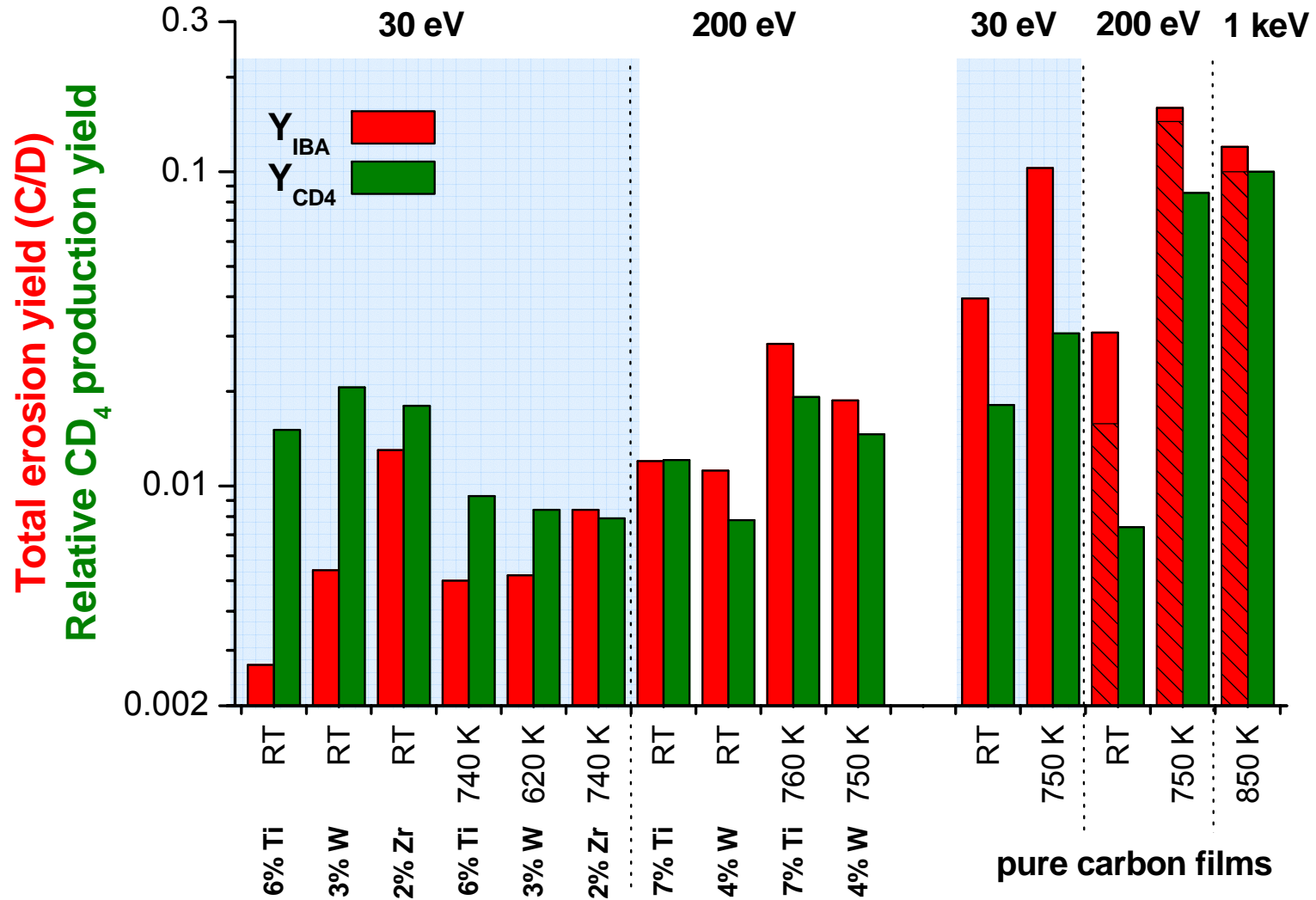
# Results: Erosion Yield IBA / QMS





- $Y_{hot} > Y_{RT}$  (well known)
- $Y_{CD4}$  always smaller than  $Y_{IBA} \Rightarrow$  less  $CD_4$  produced compared to 1 keV at  $T_{max}$

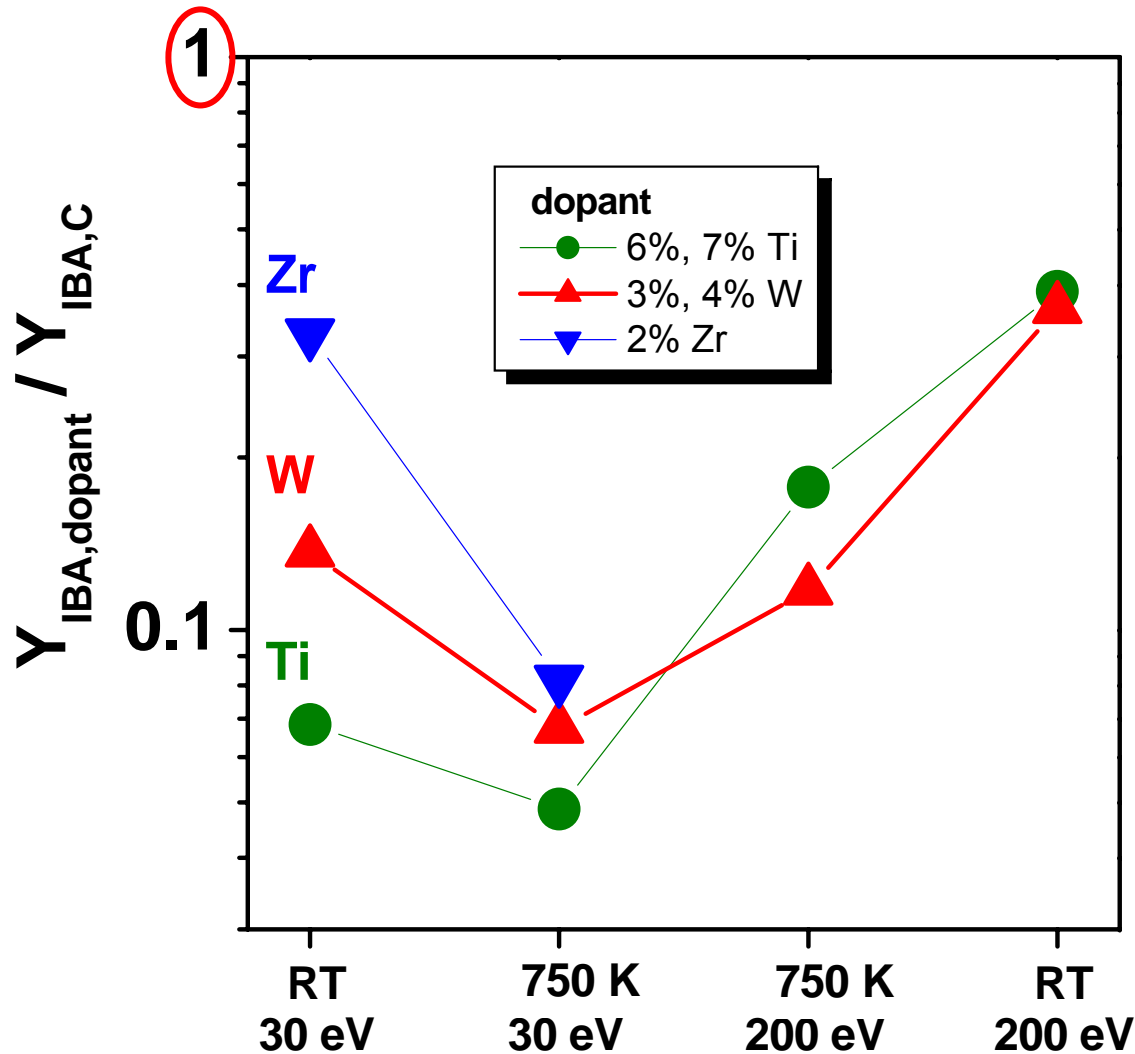
# Comparison Erosion Yield IBA / QMS



# Total erosion yield $Y_{IBA}$ : Effect of doping



## Carbon erosion yield

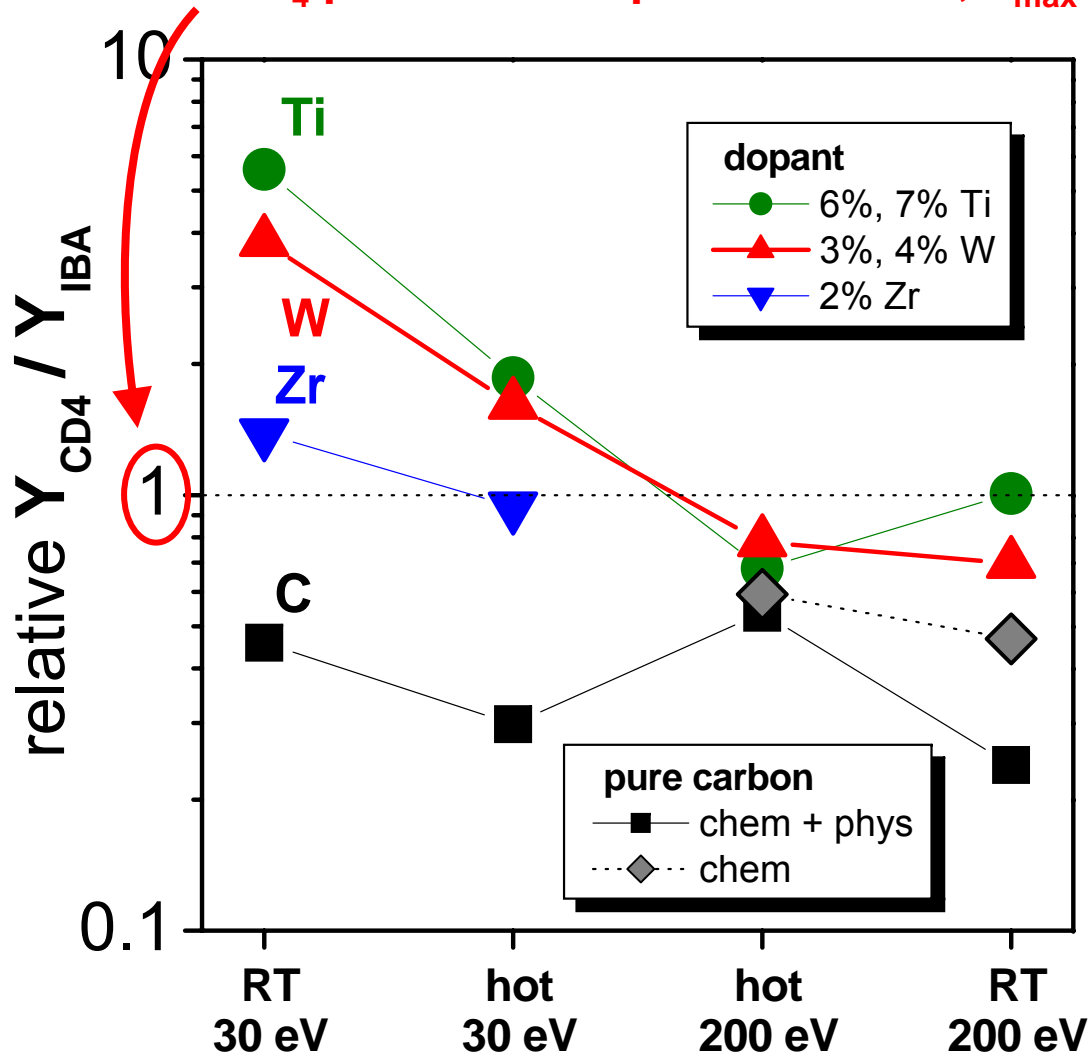


- reduced total erosion for all doped samples
- reduction most prominent at high temperatures and 30 eV (for Ti only 5 %)
- reduction changes with metal content / type
- metal erosion observed for 200 eV
- ↳ comparable to yields for carbides

# Comparison Erosion Yield QMS / IBA



CD<sub>4</sub> production equal to 1 keV D, T<sub>max</sub> ( $Y_{\text{Chem}} = 1.2 - 4 Y_{\text{CD}_4}$ )



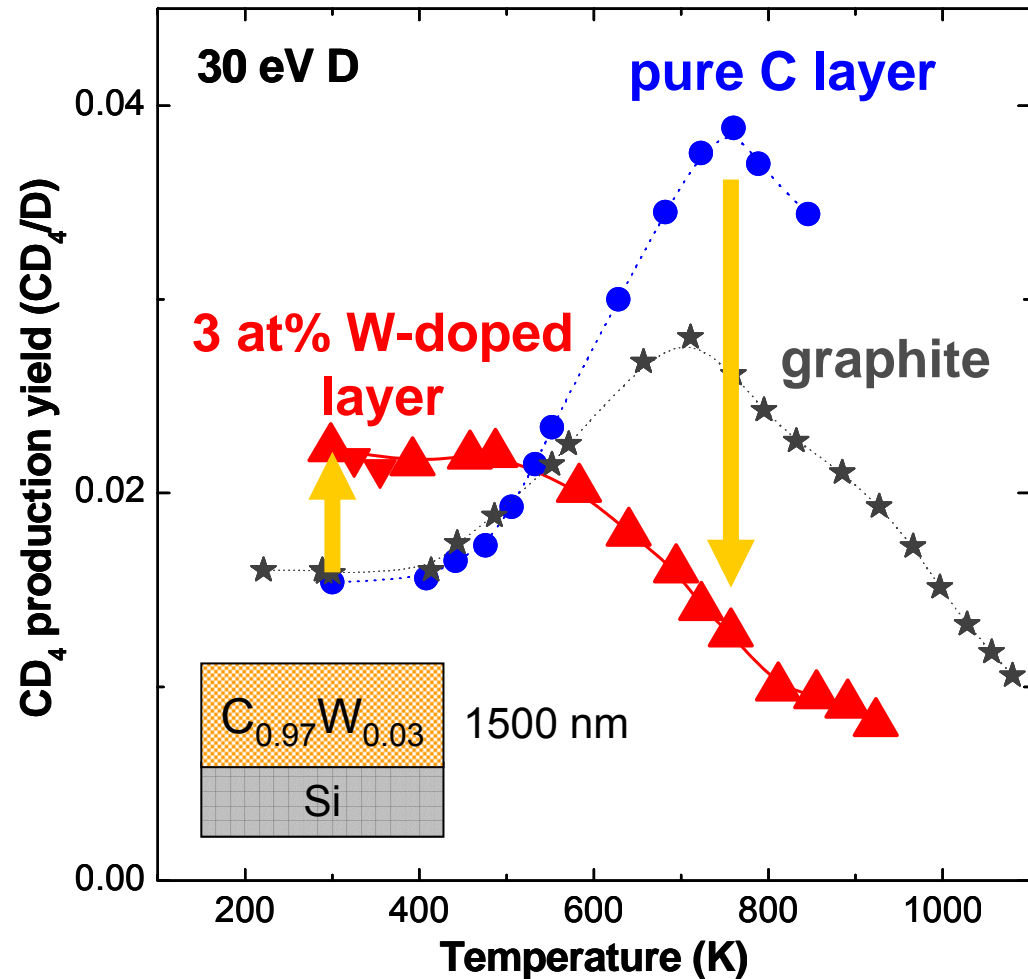
- $Y_{\text{CD}_4} / Y_{\text{IBA}} < 1$  for pure C  
 ↳ more C<sub>x</sub>D<sub>y</sub> / radicals
  - ratio always higher for a-C:Me compared to C
  - 200 eV:  $Y_{\text{CD}_4} / Y_{\text{IBA}} \leq 1$   
 ↳ more C<sub>x</sub>D<sub>y</sub> / radicals
  - 30 eV:  $Y_{\text{CD}_4} / Y_{\text{IBA}} \geq 1$   
 ↳ more CD<sub>4</sub> production
- compare to published factors (1.2 - 4)
- ↳ mainly CD<sub>4</sub>



## Doping with W (V, Ti, Zr)

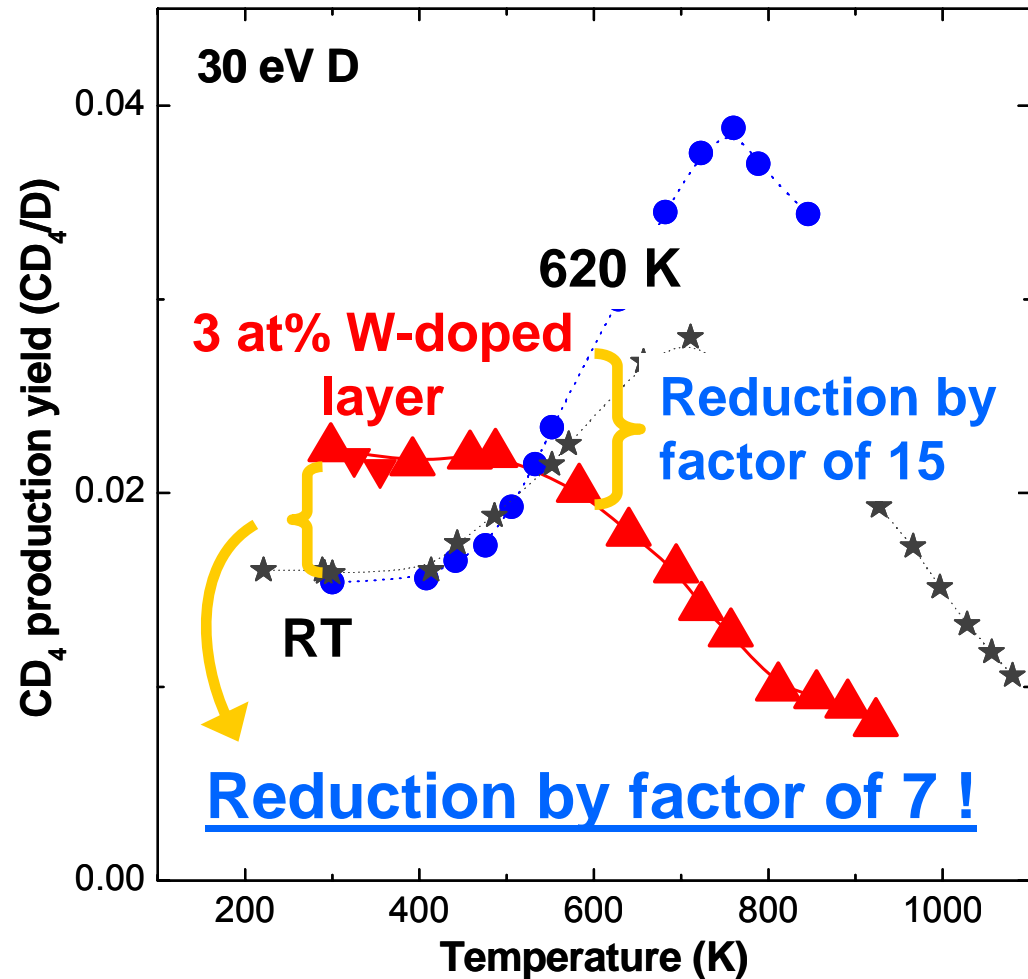
- mass- & energy-separated ion beam (30 & 200 eV/D)
- detection of volatile erosion species ( $\text{CD}_4$ )
- $\text{CD}_4$  production yield
  - strong reduction at elevated temperatures
  - enhancement at RT

↳ **total yield reduced**



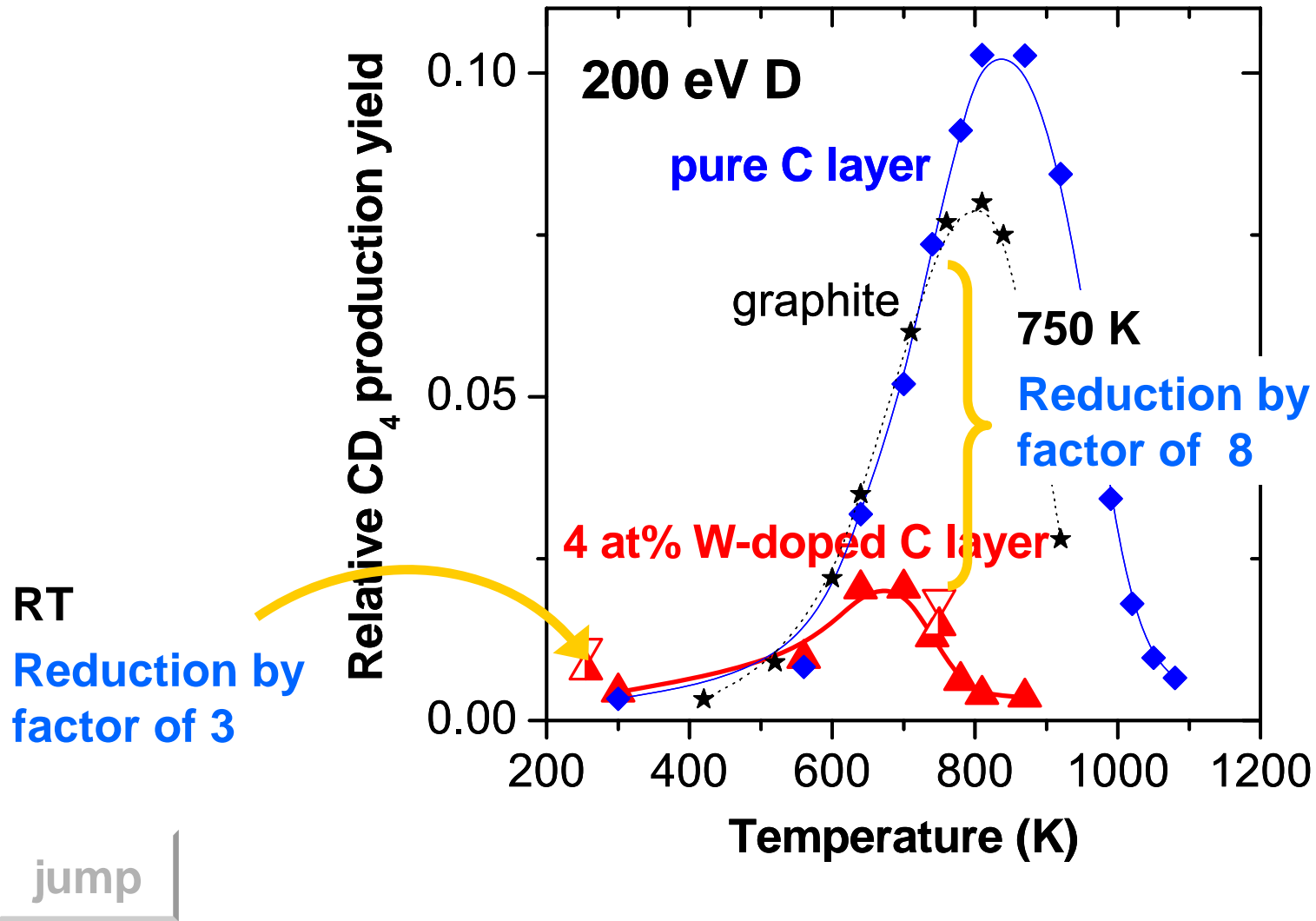
## Doping with W (V, Ti, Zr)

- mass- & energy-separated ion beam (30 & 200 eV/D)
- detection of volatile erosion species ( $CD_4$ )
- $CD_4$  production yield
  - strong reduction at elevated temperatures
  - enhancement at RT
  - ↳ **total yield reduced**
  - ↳ **distribution of erosion products changed**

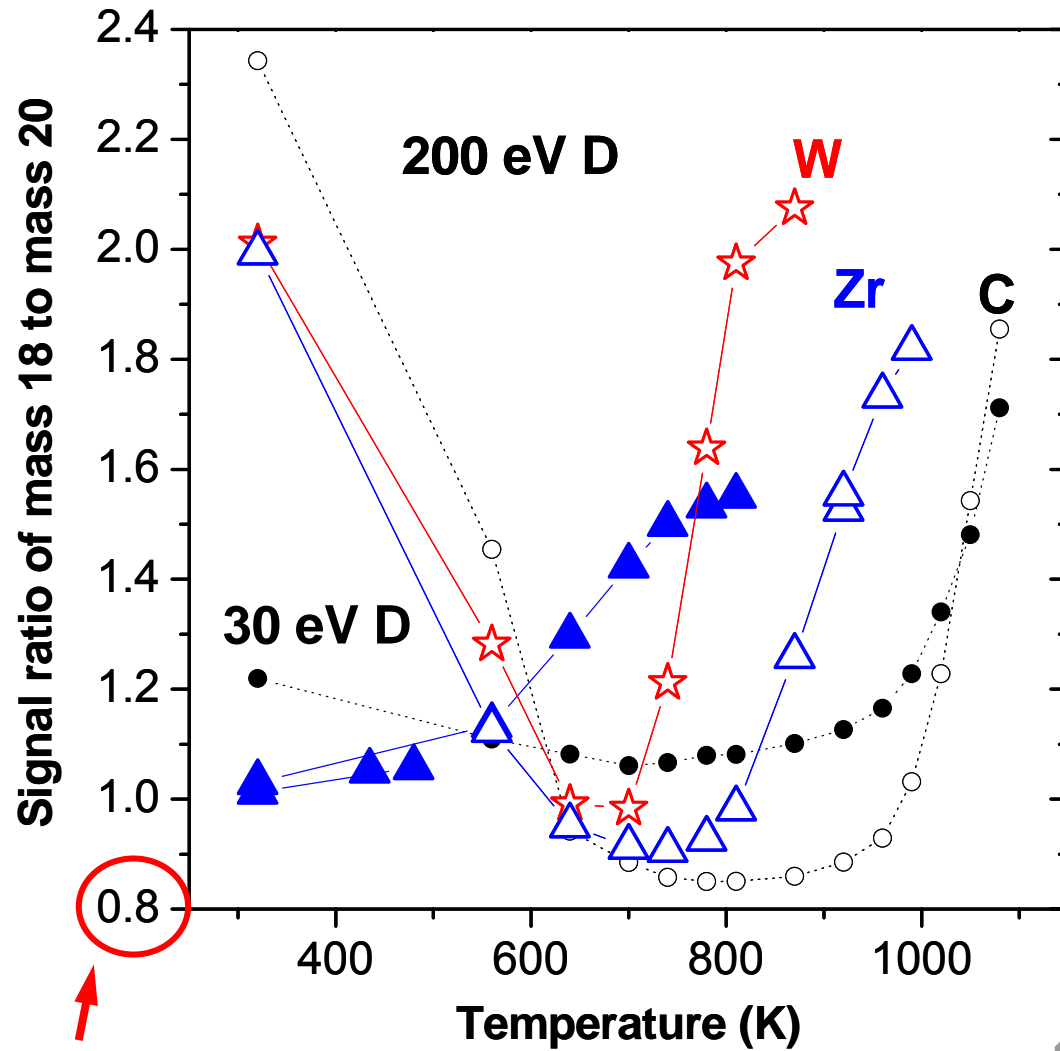


jump

# Temperature dependence of 200 eV D



# Ratio of QMS signal: Temperature dependence



**Methane cracking**

## Ratio mass 18 / mass 20:

- indicator of  $CD_3$  or cracking of heavier  $C_xD_y$
- changes of ratio
  - ↳ change in distribution of erosion species

## 200 eV:

- only methane at  $T_{max}$
- C: comparable to 1 keV
- doping:
  - ↳ changes at high T

## 30 eV:

- mainly methane at RT
- doping:
  - ↳ changes at high T
  - ↳ more  $CD_4$  at RT

- **production and characterization** of nano-structured metal-containing amorphous carbon films (0 – 20 at% Me) as model for mixed re-deposited layers
  
- **chemical erosion** strongly affected by doping
  - **total erosion yield drastically reduced**  
(factor of ~10 at elevated temperatures; at RT at least factor of 3)
  
  - doping changes **distribution of erosion species** to more CD<sub>4</sub> production (30 eV)
  
- ⇒ using only the signature of one species leads to wrong erosion yields (e.g. spectroscopic investigations on strongly polluted surface), but CD<sub>4</sub> is may be still indicator for variations

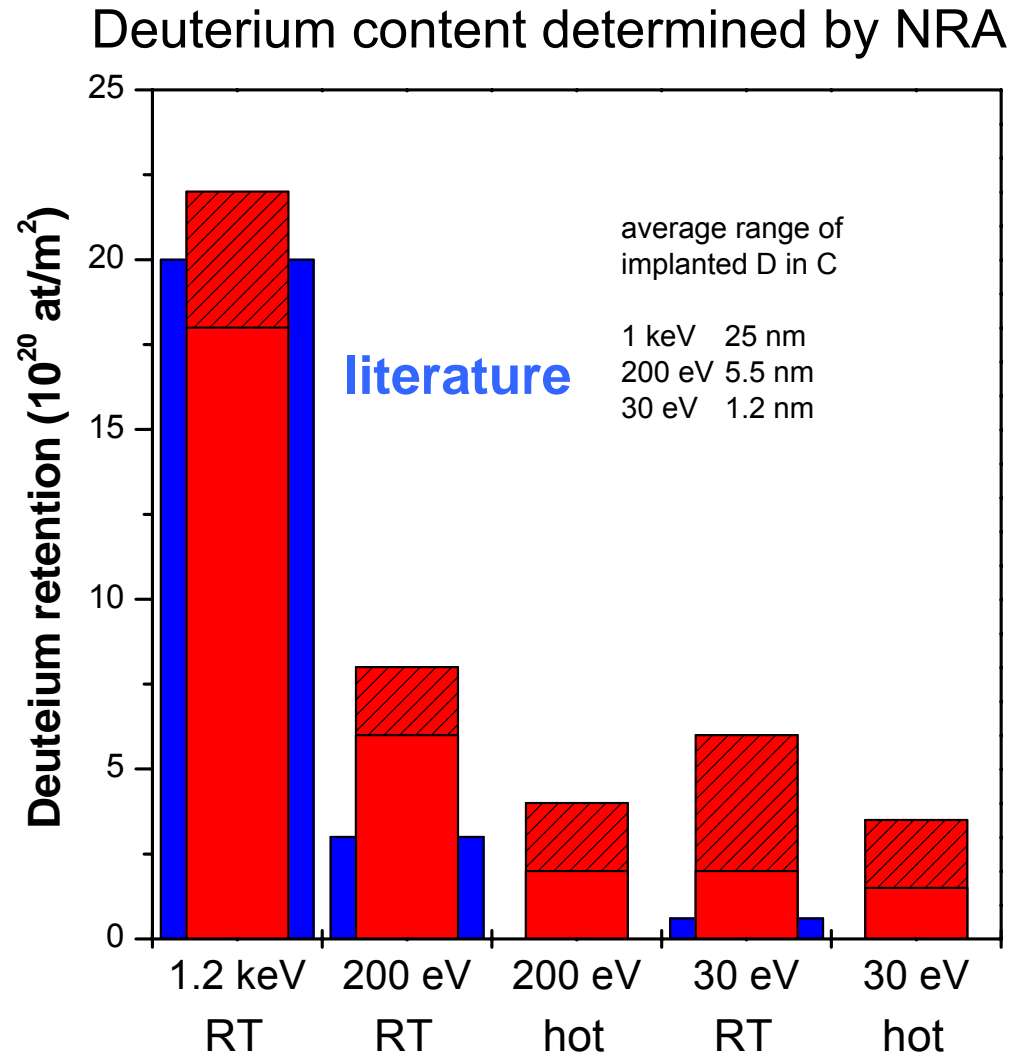
### **Contributors:**

**Ch. Adelhelm,**

**E. de Juan Pardo, J. Roth,**

**S. Lindig, A. Herrmann, B. Cieciva, I. Quintana Alonso, B. Dubiel, E. Welter ...**

The end



- fixed erosion condition
- fluence  $3 - 7 \times 10^{23}$  D/m<sup>2</sup>