## Pressure Profile Consistency in ASDEX Discharges

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#### 1. Introduction

Ohmically (OH) and additionally heated "L-mode" Tokamak discharges exhibit an electron temperature Te profile invariance against changes in power deposition profiles and plasma density and are only influenced by the safety factor qa. This has led to the concept of "profile consistency" where the local transport coefficients are not only a function of local plasma parameters but might also depend on non-local processes adjusting the Te profiles. At present, there exists no coinvincing model for this profile consistency, first introduced by B. Coppi to describe the current density behaviour and the connected Te profiles of Ohmic heated plasmas. But if the thermal transport is governed, for instance, by electromagnetic modes, not only the current density should show a canonical profile, but also the pressure (p) gradient profiles. Moreover, these profiles can adjust after changes of the heating deposition much faster than the current density, and any deviation from the canonical profile might then result in an additional heat transport which can be expected to act complementory on ion and electrons.

According to Kadomtsev /1/, a pressure profile consistency arises from the existence of relaxed states with thermal and poloidal field minimized subject to a single (constant current) or two constraints (constant current and helicity of the magnetic field). With such a strong principle the resulting pressure and current density profiles depend on the ratio  $\mathbf{q_a/q_o}$  only and, depending on the constraint, are finite or zero, respectively, at the plasma boundary r=a. Profiles for both cases approach each other at high  $\mathbf{q_a/q_o}$ . In this paper we examine the total pressure profile shapes in all phases of ASDEX discharges (OH, L and H mode) and compare them with the  $T_e$  profiles.

2. T<sub>e</sub> and pressure profiles in OH and L mode discharges
There is no commonly agreed format of the T<sub>e</sub> profile normalization showing an invariance for different operating conditions. With increasing order of <sup>1</sup> University of Stuttgart; <sup>2</sup> Ioffe Institute; <sup>3</sup> University of Heidelberg; <sup>4</sup> University of Washington, Seattle, USA; <sup>5</sup> N.R.C.N.S. "Democritos", Athens, Greece; <sup>6</sup> Inst. for Nuclear Research, Swierk, Poland;

the profile consistency quality, the possibilities proposed are:  $T(0)/\langle T \rangle$ , T(r)/T(a/2) or ln(T(r)/T(a/2)) and  $1/T \cdot dT/dr$ . Using the normalization T(r)/T(a/2) ASDEX  $T_e$ -profiles coincide within the error bars and discharge to discharge variations outside the q=1 surfaces  $(r_{Q=1} = a/q_a)$ for all OH- and L-mode discharge conditions as is shown in Fig. 1 (Thomson scattering measurements). Data from discharges are used for which transport analyses with the TRANSP code have been carried out including stationary and unstationary discharge phases and the following parameter variations:  $I_p=300\pm440$  kA,  $\bar{n}_p=1\pm11\cdot10^{19} m^{-3}$ ;  $P_h\leq 3.8$  MW; strong on- and off-axis heating deposition profiles /2/ and pellet refuelled discharges /3/. For different qa-values deviations can be seen at radii r<ra=1, but differences exist also in the confinement zone between q=1 and q=2 (which is roughly at  $r_{0=2} \approx a/\sqrt{q_a/2}$ ). This is more clearly demonstrated in Fig. 2 showing for the same discharges the radial profiles of the upper and lower bounds of the normalized Te scale length rre given by the inverse logarithmic derivative  $r_{Te}/a = -(T_e/dT_e/dr)/a$ . Part of the  $q_a$ -dependence is certainly due to the Te-flattening inside the sawtooth region. At fixed qa there is a weak Te profile response to changes in the heating profile yielding broader profiles, i.e. higher rTe, with increasing off-axis heat deposition. The latter is obtained by using a lower energy/nucleon of the injected fast neutrals or an increasing density (beam deposition at larger radii, broader resistivity profile due to higher collisionality and reduced To(0)).

The total kinetic pressure profiles are obtained by using the TRANSP analyses code. Input data are the  $n_{\rho}(r,t)$  and  $T_{\rho}(r,t)$  profiles measured by a 16-spatial channel multi-pulse Thomson scattering system and supplemented by a HCN-laser interferometer and ECE diagnostic (4 channels both), the bolometrically measured profiles of the radiation losses and global parameters like the loop voltage  $V_L$ ,  $I_D$ ,  $\beta_{D\perp}$  from diamagnetic flux measurements and βp,,+li/2 as deduced from poloidal fields and fluxes. Lacking a measurement of the full ion temperature T; profiles for all discharges we assume a spatially constant enhancement factor a of about 2 to 3 of the ion heat diffusivity xi over the neoclassical value as calculated by Chang and Hinton, checking the resulting T; profiles for their compatibility with the available neutron production and Ti measurements (passive and active CX diagnostic, Doppler broadening of impurity lines). The calculated kinetic pressures include also the contributions due to the anisotropic fast beam ions (using Monte Carlo calculations for the deposition and slowing-down of the beam particles) and are in good agreement with the magnetically measured ones. Fig. 3 shows the pressure scale length  $r_{\rm D}$  for the discharges of Fig. 1 and 2 exhibiting a somewhat stronger separation of the two qa data sets, which are not in disagreement with the Kadomtsev p(a)=0 pressure profiles. The influence of the  $\chi_1$  assumption was estimated by taking  $\alpha$ values between 1 and 5, yielding rp variations below 10%.

3. H-mode profiles

The invariance of the pressure profiles is even more impressive if we look at their time development during single discharges as is shown for a  $\beta$ -limit discharge in Fig. 4. Fig. 4a demonstrates the strong  $T_{\rm e}$  profile variation at the L/H mode transition where the  $T_{\rm e}$  profile flattens in the

center (higher  $r_{Te})$  and develops shoulders towards the boundary. After reaching  $\beta_{max}$  the  $T_e$  profiles flatten even more in the center due to increasing central radiation losses /4, 5/. As also the density profiles form shoulders in the H-mode, the electron pressure  $(p_e)$  profiles do the same (see Fig. 4b) but are by far not comparable to the second class of Kadomtsev-profiles with  $p(a) \not \!\!\!\! + \!\!\! 0$  which would have nearly constant  $r_p$  for 0.5 acr < a. Contrary to  $p_e$ , the total pressure profile is nearly time independent. In this discharge, the fast ions contribute up to 40 % of the pressure and a comparable amount to the pressure gradient and the ion temperature is well above  $T_e$ . The universality of the p profile shape is also demonstrated by comparing H-mode discharges both with Ho and Do injection, i.e. different deposition profiles (see Fig. 5). The disappearance of the  $q_a$ -dependence might be partly caused by the lack of sawteeth.

## 4. Conclusions

The total pressure profiles of ASDEX discharges exhibit a canonical shape which is preserved also in the H-mode contrary to a changing  $T_{\rm e}$  profile shape. There exists one exception namely the high confinement pellet refuelled discharges revealing a steeper pressure gradient and smaller scale lengths /3/. For instances in a  $q_{\rm a}$ =2.5 ohmic pellet discharge the  $r_{\rm p}/a$  profile is about at the lower bound of the gas fuelled discharges shown in Fig. 3. This might be related to the process limiting the pressure shape yielding a lower bound for the  $r_{\rm p}$  profile which is nearly reached in these pellet discharges. It is interesting that only in the pellet discharges  $n_{\rm i}$ -values below 1 are observed over a large part of the plasma column.

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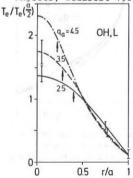
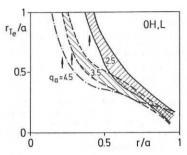
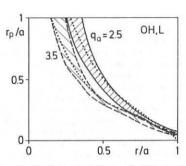


Fig.1: Averaged  $T_e$  profiles normalized to  $T_e(a/2)$  vs. flux surface radius r in ohmic and L-mode discharges at  $q_a$ = 2.5±0.1, and  $q_a$ =3.5 ± 0.2, and for a comparison discharge at  $q_a$ =4.5.



<u>Fig.2:</u> Radial profiles of the upper and lower bounds of the  $T_e$  scale length  $r_{Te}$ =- $T_e$ /d $T_e$ /dr) normalized to a for the discharges used in Fig. 1 (OH, L-mode).



 $\underline{Fig.3:}$  Radial profiles of the upper and lower bounds of the normalized presure scale length  $r_p/a$  (OH, L-mode). The dotted lines are the Kadomtsev pressure profiles with p(a)=0 for  $q_a = 2.5$  and 3.5.

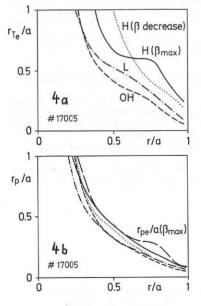


Fig.4: Radial profiles of the normalized  $T_{\rm e}$  and p scale lengths for a beam heated ASDEX discharge ( $q_{\rm a}$ =3.7) in different discharge phases (OH, L, H-mode).

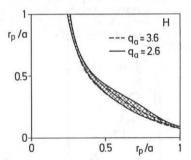


Fig.5: Radial profiles of the bounds of the normalized pressure scale length for beam-heated H mode discharges.