

Effect of plasma response on the fast ion losses due to ELM control coils in ITER

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15 February 2016

Abstract

Mitigating edge localized modes (ELMs) with resonant magnetic perturbations (RMPs) can increase energetic particle losses and resulting wall loads, which have previously been studied in the vacuum approximation. This paper presents recent results of fusion alpha and NBI ion losses in the ITER baseline scenario modelled with the Monte Carlo orbit following code ASCOT in a realistic magnetic field including the effect of the plasma response. The response was found to reduce alpha particle losses but increase NBI losses, with up to 4.2% of the injected power being lost. Additionally, some of the load in the divertor was found to be shifted away from the target plates toward the divertor dome.

1 Introduction

Operating a high performance plasma in the H-mode normally results in edge localized modes (ELMs) which are violent relaxation processes of the edge pedestal region that rapidly deposit large amounts of energy in the divertor. The high power loads from ELMs are expected to be the primary driver for the erosion of the target plates in ITER, limiting the lifetime of the divertor cassettes [1]. Thus suppression or mitigation of ELMs is a critical part of the design and operation of ITER. One of the leading mitigation methods is the application of resonant magnetic perturbations (RMPs) on the plasma using an array of in-vessel ELM control coils (ECCs) [2]. While RMPs reduce the severity of the ELMs, the non-axisymmetric perturbations also reduce the confinement of energetic particles, resulting in increased fast ion losses and wall loads, both on the divertor and the blanket.

Results from experiments in DIII-D have yielded criteria associating the vacuum magnetic perturbation to ELM mitigation effectiveness [3]. The width of the region with overlapping magnetic islands, corresponding to the region of perturbation-induced stochasticity, should extend sufficiently far in from the separatrix. This criteria has further been linked to the formation of a transport-enhancing island on top of the edge pedestal [4]. The DIII-D criteria have been applied to ITER, and sufficient coil currents for ELM mitigation have been determined for several ITER operating scenarios [5].

The effect of ECCs on fast ion losses has previously been modelled in the vacuum approximation [6, 7, 8, 9], where it was presumed that plasma would respond to the applied RMP field by dampening the penetration of the perturbations and reducing losses. However, recent simulation results [10] suggest this is not generally the case. The plasma response can increase stochasticity near the edge, even while hindering island formation deeper inside the plasma. Also of interest is the effect on the distribution of losses, where the response may diffuse or concentrate the particle flux on the plasma facing components, possibly resulting in hot spots with high peak loads.

In this paper, the effect of ECCs and plasma response on fusion alpha and NBI ion losses in ITER 15 MA Q=10 baseline scenario is studied in the presence of magnetic perturbations from ferritic components.

2 Model and methods

The simulations of the wall loads in this study extend the methods previously applied to the 15 MA baseline case [11]. The particles were followed using the Monte Carlo orbit-following code ASCOT [12] in a realistic 3D magnetic field, including perturbations caused by the ripple-mitigating ferritic inserts and three pairs of European test blanket modules, which also contain ferritic material.

The plasma equilibrium and profiles (Figure 1) were prepared using JINTRAC [13]. The plasma profiles in the baseline scenario still include carbon as an impurity species, but its effect on fast ion losses has been found negligible [11]. The fusion alpha test particles were initialized uniformly in the plasma volume and weighted according to thermal fusion reactivity at their birthplace. Total fusion alpha power in the baseline scenario was 85 MW. NBI ions were generated for the two ITER injectors in both on-axis and off-axis configurations

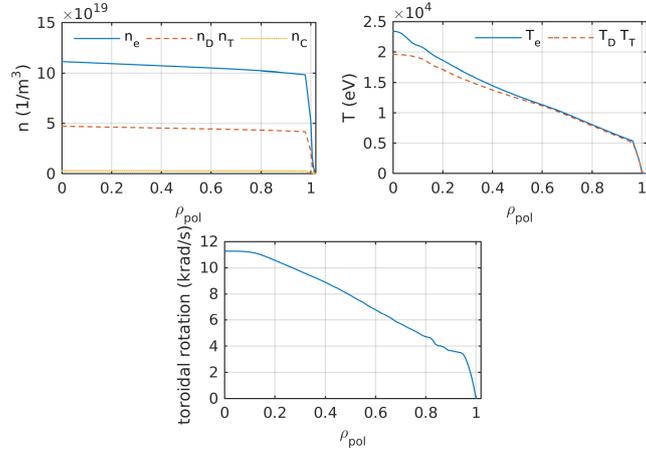


Figure 1: Electron, ion and carbon impurity densities (top left), electron and ion temperatures (top right) and toroidal plasma rotation velocity (bottom) in the 15MA baseline scenario.

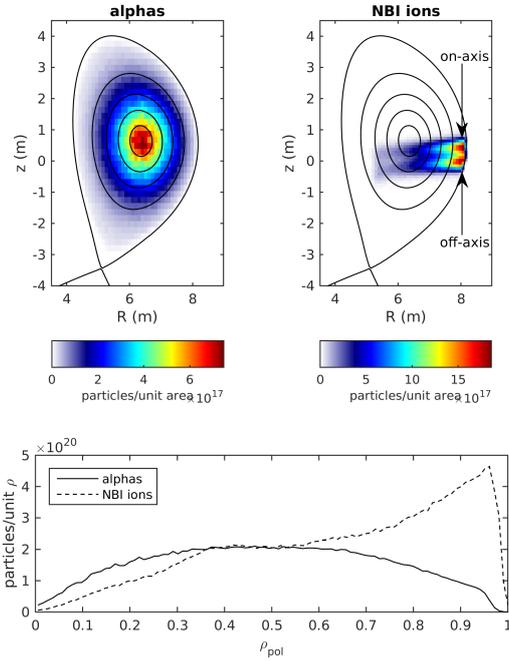


Figure 2: Initial distributions for the fusion alphas and NBI ions in the poloidal cross section (top) and as a function of the radial coordinate $\rho_{pol} = \sqrt{(\psi - \psi_{axis})/(\psi_{sep} - \psi_{axis})}$ (bottom).

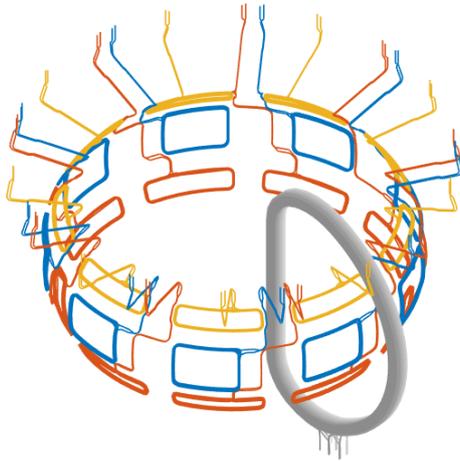


Figure 3: Upper, equatorial and lower ELM control coils and their current leads used in the calculation of the RMP field, together with an example of the TF coils.

with a total NBI heating power of 33 MW. An ensemble of 100 000 test particles was used when estimating the total losses for fusion alphas and the NBI ions in both configurations (Figure 2). An ensemble of 300 000 NBI test particles were used in the simulation for the peak heat load estimates.

The magnetic perturbations caused by the ferritic components were computed with the finite-element solver COMSOL [14]. In the first step, magnetization of the components was computed from the magnetic fields produced by the poloidal and toroidal coils and the plasma current. In the second step, the magnetic perturbations resulting from the magnetization were computed and added to the equilibrium magnetic field together with the toroidal field ripple. The RMP field produced by the ECCs was computed from a detailed coil geometry (Figure 3) using the Biot-Savart integrator BioSaw [8]. The coil currents were set according to the reference case for a 4.5 keV pedestal temperature baseline plasma, with an $n=3$ mode 45 kAt maximum current and phase shifts of 86° , 0° and 34° for the upper, equatorial and lower coil rows respectively [5].

The response of the plasma to the magnetic perturbations was computed using the resistive MHD code MARS-F [15]. The MARS-F model has been extensively benchmarked and validated against other models and experiments for the plasma response computations [16, 17, 18]. Response in the toroidal modes $n=1$ through $n=6$ was included, as the contribution from the higher n modes was found to be negligible. The original vacuum approximation was used for the higher modes. As shown in the Poincaré plots in Figure 4, the effect of the plasma response is to significantly reduce the width of the islands near the edge ($\rho_{\text{pol}} > 0.95$), resulting in field lines being rapidly lost to the wall. A shift of approximately 60-70 degrees in the toroidal island location can be seen, which is consistent with results in a similar study for ASDEX Upgrade [19]. Additionally, the plasma response shifts the location of the separatrix, evident in the displacement of the X-point by up to 5 mm (Figure 5).

To accurately determine the particle strike points on the first wall, a detailed

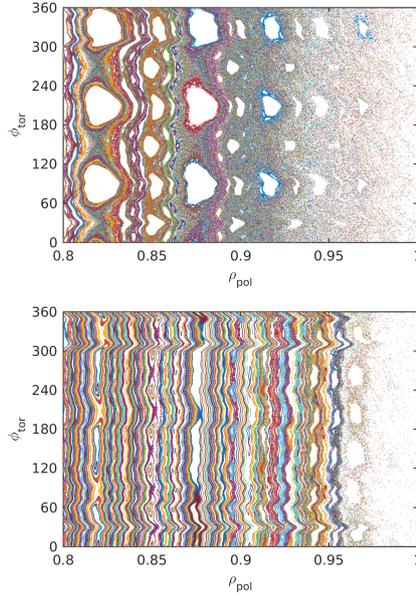


Figure 4: Poincaré plots of the magnetic field line structure close to the last closed flux surface on the outer midplane without (top) and with plasma response (bottom). Field lines were followed from the outer midplane until they intersected the wall or completed 5000 toroidal orbits.

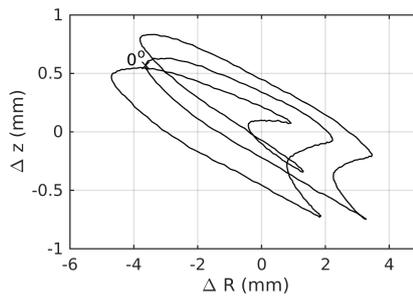


Figure 5: Displacement of the X-point, as determined by locating the local minimum of the poloidal magnetic field, in the plasma response case with respect to the vacuum approximation. The plot traces the displacement around the plasma in the toroidal direction.

Table 1: Total fast ion losses, with non-ECC results from [11]. Errors from the Monte Carlo method were estimated using bootstrapping.

	No ECC	With ECC	
		Vacuum	Response
<i>Alphas</i>			
Wall	40 kW	70 ± 4 kW	157 ± 5 kW
Divertor	130 kW	1925 ± 15 kW	1343 ± 12 kW
<i>NBI ions (on-axis)</i>			
Wall	7 kW	3 ± 1 kW	3 ± 1 kW
Divertor	1 kW	1273 ± 20 kW	1381 ± 27 kW
<i>NBI ions (off-axis)</i>			
Wall	7 kW	6 ± 1 kW	7 ± 1 kW
Divertor	1 kW	1026 ± 17 kW	1177 ± 23 kW

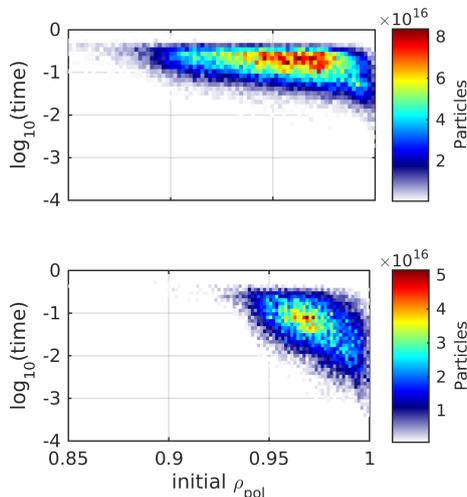


Figure 6: Distribution of lost NBI particles as a function of the radial coordinate ρ_{pol} of their birthplace and the time to reach the wall in the vacuum approximation (top) and with plasma response (bottom).

3D wall model was used in the simulations. The wall model is based on a CAD design of the first wall and divertor, which were simplified using a ray-tracing method and smoothing to approximately 300 000 triangles with a mean size of 25 cm^2 . To characterize the losses, the first wall and the divertor were distinguished in the wall model. The divertor was further divided into the inner and outer target plates, the dome covering the center part of the divertor, and the structures below the dome.

3 Fast ion losses

Both the fusion alpha particles as well as NBI ions have previously been found to be well confined in the baseline scenario without ECCs [11]. Including the perturbations from the ECCs has negligible effect on the energetic particle losses

Table 2: Fast ion losses to the divertor separated by strike point location. Monte Carlo errors were estimated using the bootstrapping method.

	Inner target	Outer target	Divertor dome	Below dome
<i>Alphas</i>				
Without response	825 ± 9 kW	877 ± 10 kW	205 ± 5 kW	18 ± 1 kW
With response	542 ± 7 kW	386 ± 7 kW	349 ± 7 kW	66 ± 3 kW
<i>NBI ions (on-axis)</i>				
Without response	795 ± 15 kW	238 ± 8 kW	188 ± 7 kW	52 ± 4 kW
With response	271 ± 11 kW	143 ± 8 kW	846 ± 21 kW	121 ± 8 kW
<i>NBI ions (off-axis)</i>				
Without response	597 ± 14 kW	220 ± 7 kW	173 ± 7 kW	35 ± 3 kW
With response	166 ± 7 kW	199 ± 9 kW	737 ± 19 kW	74 ± 5 kW

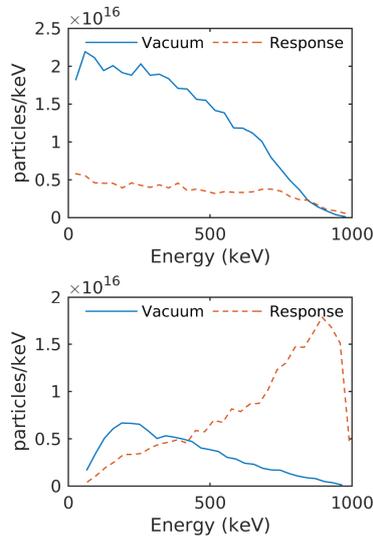


Figure 7: Energy distribution of the particles impacting the inner target (top) and divertor dome (bottom) in vacuum approximation and with plasma response.

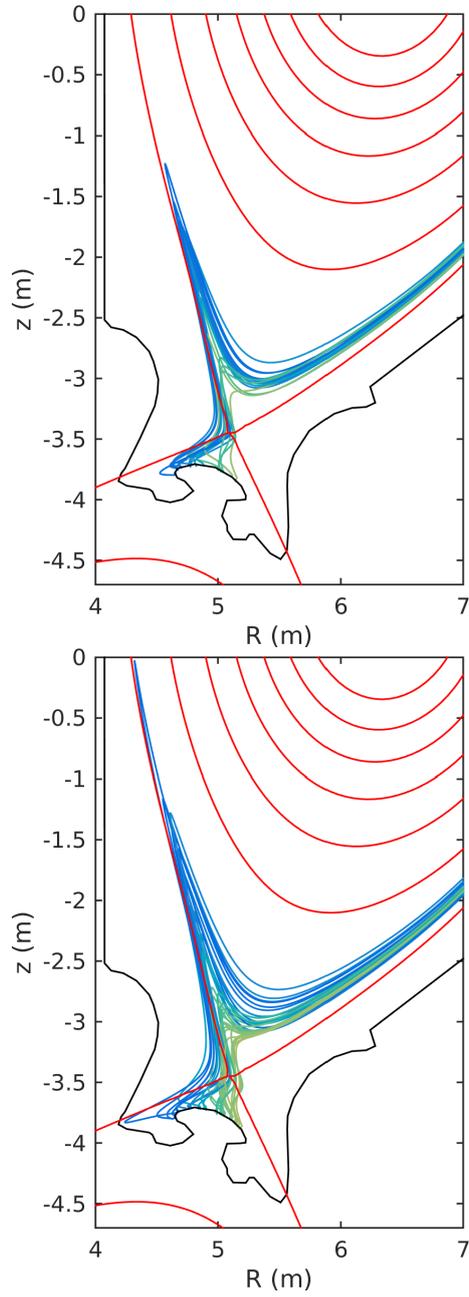


Figure 8: Typical trajectories of particles hitting the dome without plasma response (top) and with plasma response (bottom). Colour is used to distinguish particles with different strike points across the dome.

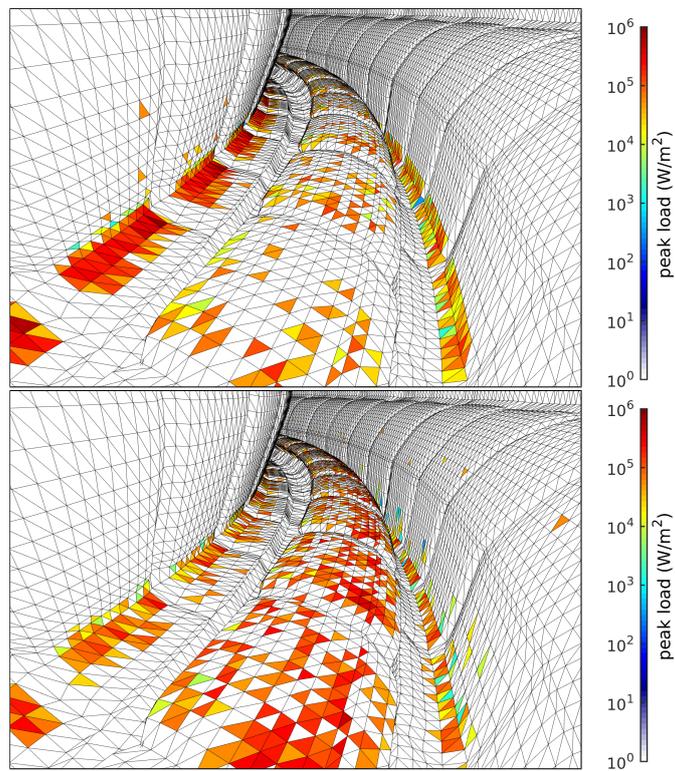


Figure 9: Peak loads due to NBI ions on the divertor targets and dome without plasma response (top) and with plasma response (bottom). Losses were also observed on elements on the underside of the dome.

to the wall (Table 1). The losses to the divertor increase dramatically, as the ECC-enhanced stochasticity rapidly depletes the particles produced or ionized near the edge.

Including the plasma response reduces fusion alpha power loss by 25% due to the shielding effect in $\rho_{\text{pol}} < 0.95$, as few alphas are born further out. However, the NBI losses increase by 8-15% with the plasma response, since their birth profile is peaked closer to the plasma edge where the stochasticity is enhanced. For the alpha particles, the losses with plasma response represent 1.8% of the total fusion alpha power. The NBI ion losses in the off- and on-axis configurations represent 3.6% and 4.2% of the total injected NBI power, respectively. The difference between the on-axis and off-axis losses is due to the off-axis injection trajectory being located below the midplane, where the particles can reach further inwards compared to the on-axis configuration.

In the vacuum approximation, the lost NBI particles originate primarily from $\rho_{\text{pol}} > 0.9$, while in the plasma response case the losses are concentrated to the region $\rho_{\text{pol}} > 0.94$ (Figure 6). These values closely correspond with the width of the stochastic region in Figure 4. Additionally, the lost particles reach the wall faster in the plasma response case, which is consistent with the shorter connection lengths of the field lines close to the edge.

Without plasma response, 80% of the power loss from NBI ions impinges on the target plates (Table 2). Upon application of the plasma response, the load is shifted towards the divertor dome, which then receives 62% of the losses.

While the energy distribution of the particles reaching the inner target is similar in the vacuum approximation and plasma response, the energy of the particles impacting the divertor dome is significantly higher with the response (Figure 7). This is consistent with the faster losses in the plasma response case (Figure 6), since the particles do not have the time to slow down through collisions. Thus it would appear the shift in losses is caused by particles on slightly wider banana orbits due to their higher energy in the plasma response case (Figure 8).

The peak fluxes in the divertor are approximately 1 MW/m^2 in both cases (Figure 9), which is within the design limits both for the targets as well as the divertor dome [20]. However, a significant heat load of up to 121 kW impinges on the underside of the dome.

4 Discussion

Based on the simulation results, it is apparent that the effect of the plasma response cannot simply be assumed to be favourable, but it depends on the operating scenario, plasma profiles and the source of energetic particles. While the effect on the alpha particle losses is benign, the NBI losses approach a significant fraction of the total NBI heating power. The losses are less than predicted in previous studies where full 90 kAt coil current was applied, but even the case presented here can noticeably reduce the available heating power margin and possibly limit the plasma performance. Redistribution of the losses due to the plasma response can also expose poorly protected areas to heating from fast ions, risking damage to the structures.

While including the effect of plasma response represents a step forward in the fidelity of ECC-induced fast ion loss analysis, further study is still called for.

With plasma response, the shielding and amplification of the perturbations is represented in the magnetic field structure, but the equilibrium and the plasma profiles are still modelled in the vacuum approximation. The lost field lines near the edge likely cannot support as steep pedestal profiles as those resulting from the vacuum approximation. The lower density near the edge would reduce both the fusion yield as well as neutral beam ionization near the edge, likely resulting in fewer losses. A self-consistent plasma equilibrium, including the effect of the perturbations and the plasma response, would thus be required.

With the level of detail in the wall model and the number of test particles used in the presented simulations, the peak loads on the divertor target plates can be estimated with good confidence. Modelling the peak heat load on the structures under the divertor dome, however, would require more detailed wall geometry that includes the cooling systems and support structures, to identify any localized heating that could damage the components.

Acknowledgements

This work was partially funded by Fusion For Energy Grant 379 and the Academy of Finland project No. 259675, and has also received funding from Tekes – the Finnish Funding Agency for Innovation under the FinnFusion Consortium. The work was carried out using the HELIOS supercomputer system at International Fusion Energy Research Centre, Aomori, Japan, under the Broader Approach collaboration between Euratom and Japan, implemented by Fusion for Energy and JAEA. The supercomputing resources of CSC - IT center for science were utilised in the studies. Some of the calculations were performed using computer resources within the Aalto University School of Science "Science-IT" project.

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