Classical Diffusion in Tokomak

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Abstract: The mass flow perpendicular to the magnetic surfaces is calculated for rotational symmetric systems. The influence of an induced electric field on the classical diffusion is included. The formula will be simplified for a special selfconsistent Tokomak case with magnetic surfaces of nearly circular cross section. It will be shown that a stationary equilibrium with vanishing mass flow has no physical meaning for realistic Tokomak conditions.

The influence of an induced electric field produced by ohmic heating in a toroidal discharge has not been taken into account in the work of Pfirsch-Schlüter on classical diffusion [1]. The effect of this electric field consists in an additional E x B drift which decreases the classical diffusion. If we want to calculate this effect we must start with the magnetohydrodynamic equation

From the condition $\nabla \vec{t}$ = 0 there results the differential equation for 1.

 $\frac{\partial \mathcal{L}}{\partial e} \frac{\partial F}{\partial t} - \frac{\partial \mathcal{L}}{\partial t} \frac{\partial F}{\partial F} = - \frac{2c \mathbf{g} \mathbf{d}_{\mathrm{P}}}{B_{\mathrm{o}} R \mathbf{d}_{\mathrm{F}}} \frac{\partial F}{\partial t}$ (2)

which is to be solved by the general solution:

Here we have used cylindrical coordinates (g, θ , z), with g the distance from the torus axis, θ - the direction of the main magnetic field $B_{0} = B_{0} \frac{R}{S}$, R - the distance of the center of the discharge vessel from the torus axis, z - the distance from the torus plane. We shall also introduce a system of polar coordinates:

> $z = r \sin \vartheta$ ---- (4) $Q - R = - r \cos \theta$

It is known that the magnetic field can be generated by a scalar function F [2],

> $B_r = -\frac{1}{gr}\frac{\partial F}{\partial g}$, $B_g = \frac{1}{g}\frac{\partial F}{\partial r}$ ---- (5)

where the lines F = const coincide with the lines p = const. The contribution of the magnetic field of the diamagnetic currents to the main magnetic field B_A is neglected.

In equation (2) the assumption was made $|B| = |B_{\Theta}| \left[1 + \frac{B_{M}}{B_{\Theta}}\right]^{1/2} = |B_{\Theta}|$, where $B_{M}^{2} = \frac{1}{5^{2}} \left(\left(\frac{\partial P}{\partial r}\right)^{2} + \frac{1}{r^{2}}\left(\frac{\partial P}{\partial \theta}\right)^{2}\right)$. This assumption is not used in the following equations. The free function $\lambda_{O}(F)$ is determined by Ohm's law:

$$\vec{E} + \frac{1}{c} \left[\vec{v} \times \vec{B} \right] = \frac{m}{ne^2 \tilde{c}} \left(-\frac{c}{B^2} \left[\vec{v} \rho \times \vec{B} \right] + \frac{1}{2} \lambda \vec{B} \right) + \frac{1}{2ne} \vec{V} \rho \quad - - - - (7)$$

Ohm's law in this form can be received only for constant temperature.

(That means: \vec{U} - Mass velocity, n - particle density, e -electron charge, m - electron mass, 7 - electron-ion collision time.) The difference between the conductivity parallel and perpendicular to the magnetic field is taken into account by a factor 2. The 1 73 electric field ->

consists of a scalar field in the meridional (\mathbf{Q}, \mathbf{z}) plane and the induced field in direction - θ

$$\left(\frac{1}{c}\frac{\partial \vec{A}}{\partial t}\right)_{\theta} = E_{\theta} \quad , \quad E_{\theta} = E_{\theta} \quad \frac{R}{S} \tag{9}$$

If we multiply equation (7) scalar with B and integrate over a magnetic surface F = const, we obtain:

$$\lambda_{c}(F) = \frac{c}{\beta_{c}R} \frac{d_{P}}{dF} = \frac{\int_{0}^{M} fg\left(\frac{\partial F}{\partial F}\right)^{-1} d\vartheta}{\int_{0}^{M} fg\left(\frac{\partial F}{\partial T}\right)^{-1} d\vartheta} + \frac{2nc^{2}E_{0}}{m\partial_{2}} \left\{ 1 - \frac{\int_{0}^{M} fg^{-1}\left(\frac{\partial F}{\partial T}\right)^{-1} d\vartheta}{\int_{0}^{M} \left(\frac{\partial F}{\partial T}\right)^{-1} fg^{-1} d\vartheta} + \frac{2nc^{2}E_{0}}{\int_{0}^{M} \left(\frac{\partial F}{\partial T}\right)^{-1} fg^{-1} d\vartheta} + \frac{2nc^{2}E_{0}}{m\partial_{2}} \left\{ 1 - \frac{\int_{0}^{M} fg^{-1}\left(\frac{\partial F}{\partial T}\right)^{-1} fg^{-1} d\vartheta}{\int_{0}^{M} \left(\frac{\partial F}{\partial T}\right)^{-1} fg^{-1} d\vartheta} + \frac{2nc^{2}E_{0}}{d\theta} + \frac{2nc^{2}E_{$$

The formula for the mass flow M is obtained using the vector product of equation (7) with B:

$$\mathcal{M} = \int_{0}^{\infty} (m\vec{v}, \frac{\partial F}{\partial F})^{2} ng t \frac{|VF|}{|\frac{\partial F}{\partial T}|} dd = \frac{2\pi mc^{2}}{e^{2}\tau \partial_{t}^{2}} \frac{dP}{dF} A(F) - \frac{\pi mc^{2}}{e^{2}\tau} \frac{dP}{dF} B(F) - \frac{2\pi mcE_{c}}{B_{0}^{2}R} C(F) - (11)$$
with
$$A(F) = \int_{c}^{t} fg \frac{(VF)^{2}}{|\frac{\partial F}{\partial \tau}|} dd_{3} B(F) = \int_{0}^{t} fg \frac{\partial F}{\partial T} |\frac{\partial F}{dd} - \frac{\left(\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd\right)\left(\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd\right)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{dt} - \frac{(12)}{\int_{0}^{t} fg (\frac{\partial F}{\partial T})^{-1} dd} \int_{0}^{t} \frac{\partial F}{\partial T} |\frac{\partial F}{\partial T} - \frac{\partial F}{\partial T} |\frac{\partial F}{\partial T} |\frac{\partial F}{\partial T} - \frac{\partial F}{\partial T} |\frac{\partial F}{\partial$$

The first term A(F) accounts for the classical diffusion in a straight cylinder, the second term B(F) contains the Pfirsch-Schlüter diffusion and the third term C(F) gives the contribution of the electric field.

In the following now we shall look for a special simple Tokomak case. The Maxwell equation for the meridional magnetic field is:

$$t B_n = \frac{y_n}{c} i_0 = - - - - - - (13)$$

This equation will be solved in the approximation of a high discharge current.

$$i_{0} = \frac{2\pi e^{2}T}{m} E_{0} = \frac{2\pi e^{2}T}{m} \frac{R}{g}$$
(14)

We apply a homogeneous vertical magnetic field $\tilde{\beta}_{\rm g} = \frac{\Im\,\alpha^2}{R^2\,\,\delta^2} -$ (15)

(J - total current, a-plasma radius) and obtain the solution for the magnetic surfaces:

$$F = \frac{\alpha}{4} \left(x - \frac{\varepsilon}{4} x \cos \vartheta \right), \quad x = \frac{v}{6}, \quad \alpha = \frac{\vartheta_{II}}{4} \frac{\varepsilon}{mc} \frac{\varepsilon}{6} \frac{R}{6} \left(\frac{\varepsilon}{6} \right)$$
(16)

In this configuration with nearly circularly shaped surfaces we can use a simplified expression for the mass flow:

$$\mathcal{H} = -\frac{4\pi^2 R + mc^2}{e^2 \tau} \frac{4}{\beta_c^2} \left(4 + \frac{4\pi^2}{\ell^2} \right) \frac{d\rho}{d\tau} - 4\pi + \frac{2}{\beta_c} \frac{\mathcal{E}_c Cn}{\beta_c} \left(\frac{L}{2\pi} \right) \right) \frac{L}{2\pi} = \frac{d}{2\ell^2 \beta_c} \qquad --(17)$$

- - - - - (18)

that the electric field in realistic cases is too small to prevent the plasma diffusion. An interesting stationary stage with M = 0 can be achieved only when a temperature gradient is considered [3, 4].

References

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