RESEARCH ARTICLE



Modelling Soil Moisture in Hyper-Arid Conditions

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Abstract

In most land-surface models, the evolution of soil moisture is governed by soil-hydraulic processes. In hyper-arid soils, these processes break down, but soil moisture continues to show clear temporal variations, suggesting that other processes may be at work. We hypothesize that moisture in such soils varies due to evaporation in the soil and to vapour fluxes at the air–soil interface. To test this, we include vapour exchange between the air and soil in a land-surface model, apply the model to a desert site, and compare the simulated and observed soil moisture. The good agreement between the simulations and observations confirms our hypothesis. Using the model results, we examine the interactions between the soil-moisture and soil-vapour phases and influences of the soil-vapour phase on the surface energy balance.

Keywords Hyper-arid soils \cdot Land-surface models \cdot Soil moisture \cdot Soil vapour \cdot Surface energy balance

1 Introduction

Modelling soil moisture in arid regions is important because, in addition to its possible impact on the surface energy balance, desert microbiological and morphological processes may sensitively depend on soil moisture. For example, for aeolian-sand and dust-transport studies, the threshold friction velocity needs to be estimated, which depends critically on soil moisture (McKenna Neuman and Sanderson 2008). Improving the representation of soil moisture for arid regions in global climate models is important to better understand the physical processes underlying the long-term climate memory (Blender and Fraedrich 2006; Wang et al. 2010; Li and Wang 2020).

Soil moisture θ in hyper-arid regions is generally very low. In land-surface models (LSMs), the evolution of soil moisture is considered to be governed by soil-hydraulic processes. It is common that, for a given soil type, an air-dry soil moisture θ_r is prespecified to define the smallest value of θ possible. For the Brooks and Corey (1964) soil-hydraulic parameters, θ_r

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 $\approx 0.02 \text{ m}^3 \text{ m}^{-3}$ (for sand), and for the van Genuchten (1980) soil-hydraulic parameters, $\theta_r \approx 0.045 \text{ m}^3 \text{ m}^{-3}$. In some LSMs (e.g., Noah LSM, Chen and Dudhia 2001; Community Land Model, Oleson et al. 2013), θ_r is not used, but soil-hydraulic fluxes and evapotranspiration are close to zero at some critical soil moisture. In Chen and Dudhia (2001), for example, this critical soil moisture appears to be the wilting soil moisture θ_w . The smallest value of θ_w specified in the Noah LSM is 0.01 m³ m⁻³ for sand. Consequently, most LSMs do not effectively simulate soil moisture below a critical value, because in this situation the assumption that soil-hydraulic processes determine soil-moisture evolution breaks down.

However, the lowest soil moisture measured by Ishizuka et al. (2005a) in the Taklamakan Desert, China, in April 2002 using a time-domain reflectometer (TDR) was $\approx 0.005 \text{ m}^3 \text{ m}^{-3}$; oven-dry samples are as low as $\theta \approx 0.001 \text{ m}^3 \text{ m}^{-3}$, that is roughly an order of magnitude smaller than the lowest value of θ_r specified in LSMs. The soil moisture observed in the Taklamakan Desert, although very low, underwent clear temporal variations (Fig. 3), which suggests that, in arid soils, processes other than those considered in LSMs are at work. We hypothesize that, in arid soils, $\theta \leq \theta_r$ occurs due to internal soil evaporation and vapour fluxes at the air–soil interface. Conceptually, we divide the soil column into a saturated and an unsaturated zone, and the unsaturated zone into two subzones (Fig. 1). In subzone II, the evolution of the soil moisture θ is governed by Darcy flow, but in subzone I, by evaporation (and condensation) within the soil pores. To better model land-surface processes in arid regions, the exchange between the land surface and the atmosphere in the vapour phase should be considered.

We propose to include the exchange between air and soil in the vapour phase in landsurface modelling. The Atmosphere and Land Surface Interaction Scheme (ALSIS, Irannejad and Shao 1998; Shao and Irannejad 1999) is used as the basis for the model development. The revised ALSIS model, which is denoted as the ALSIS-D model, is tested using the observations reported by Ishizuka et al. (2005a). Based on model simulations, we examine the interactions between the soil-moisture and soil-vapour phases, and the influences of the soil-vapour phase on the surface energy balance.





2 Land-Surface Model Description

2.1 Hydrological Component

The Richards equation is used for modelling soil moisture

$$\partial \theta / \partial t = -\partial / \partial z [K(1 - \partial \psi / \partial z)] + S,$$
 (1)

where *t* is time, *z* is the soil depth, ψ is the soil water potential, *K* is the hydraulic conductivity, and *S* is a source term. The variables *K* and ψ depend nonlinearly on the soil moisture θ , and thus solving (1) requires the functions $K(\theta)$ and $\psi(\theta)$ as closure. One of the commonly used closures is the Brooks–Corey closure (Brooks and Corey 1964)

$$\psi(\theta) = \psi_{\rm s} \Theta^{-b},\tag{2}$$

$$K(\theta) = K_{\rm s} \Theta^{2b+3},\tag{3}$$

where ψ_s is the saturation soil water potential, K_s is the saturation hydraulic conductivity, b is a parameter related to the pore-size distribution, and Θ is defined as

$$\Theta = \frac{\theta - \theta_{\rm r}}{\theta_{\rm s} - \theta_{\rm r}},\tag{4}$$

with θ_s being the saturation soil moisture.

Clapp and Hornberger (1978) modified the Brooks–Corey closure by replacing the water retention function with a parabolic form for near saturation ($\psi_i \le \psi \le 0$), where ψ_i is the soil water potential at the inflection point. The near-saturation case is not of interest here, as our focus is on very dry situations. For $\psi < \psi_i$, the Clapp–Hornberger closure is formally the same as the Brooks–Corey closure, but with the value of θ_r in (4) set to zero.

Equation 1 is solved subject to an upper boundary condition satisfying the surface water balance

$$P_{\rm r} - I - E - R_{\rm f} = 0, \tag{5}$$

where P_r is the precipitation rate, *I* is the infiltration rate, *E* is the evaporation rate, and R_f is the surface runoff.

The evaporation rate is calculated using the bulk transfer formulation

$$E = -\rho_{\rm a} \frac{q_{\rm a} - q_0}{r_{\rm a}},\tag{6}$$

where ρ_a is the air density, q_a is the air specific humidity at reference level z_r , q_0 is the air specific humidity at the moisture roughness length z_{0q} , and r_a is the aerodynamic resistance for moisture flux from z_{0q} to z_r . One way of estimating q_0 uses the β -method (Kondo et al. 1990),

$$q_0 = \beta q_{\text{sat}}(T_{\text{s}}) + (1 - \beta)q_{\text{a}},\tag{7}$$

where $q_{\text{sat}}(T_s)$ is the saturation specific humidity at surface soil temperature T_s , and β is a coefficient related to surface moisture availability (Mahfouf and Noilhan 1991). The ALSIS model uses the β -method for computing evaporation using a β parametrization modified from Lee and Pielke (1992)

$$\beta = \begin{cases} 0.125[1 - \cos(\pi\theta/\theta_f)]^3 \ \theta > \theta_f\\ 1 \qquad \theta < \theta_f \end{cases}, \tag{8}$$

where $\theta_{\rm f}$ is the field capacity ($\approx 0.75\theta_{\rm s}$).

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2.2 Soil Temperature

The exchange of heat in soil occurs through the mechanisms of conduction, the flow of liquid water, the diffusion of vapour, and convection. In the ALSIS model, as in other LSMs, the three latter processes are neglected, such that the soil temperature, T, satisfies

$$\frac{\partial T}{\partial t} = \frac{\partial}{\partial z} D_{\rm h} \frac{\partial T}{\partial z},\tag{9}$$

where $D_h (= K_h/C_h)$ is the soil thermal diffusivity, K_h is the soil heat conductivity, and C_h is the soil volumetric heat capacity ($C_h = \rho_s c_s$, ρ_s and c_s are soil density and specific heat capacity, respectively). The quantities ρ_s , c_s , and K_h depend on the soil porosity and soil moisture. Neglecting the density and heat capacity of soil air, we obtain

$$C_{\rm h} = (1 - \theta_{\rm s})\rho_{\rm q}c_{\rm q} + \theta\rho_{\rm w}c_{\rm w},\tag{10}$$

and

$$K_{\rm h} = 419(a\theta + b\theta^{0.4}),\tag{11}$$

where ρ_q and c_q are the density and specific heat of quartz, respectively, and ρ_w and c_w are the density and specific heat of water, respectively. The constants *a* and *b* are soil-type dependent and are determined empirically for different soil types.

Surface soil temperature is calculated diagnostically by iteratively solving the surface energy balance equation

$$R_{\rm n}(T_{\rm s}) - LE(T_{\rm s}) - H(T_{\rm s}) - G(T_{\rm s}) = 0, \tag{12}$$

where R_n is the net radiation, H is the sensible heat flux, G is the ground heat flux, and L is the latent heat of vaporization.

Other model components of the ALSIS model (including surface radiation balance, calculation of canopy water storage, canopy evapotranspiration, canopy temperature, root distribution, aerodynamic resistance network, drag coefficients, surface runoff, infiltration, etc.) are as described in Irannejad and Shao (1998) and Shao and Irannejad (1999) and are not repeated here.

2.3 Soil-Vapour Phase

In the ALSIS model, soil-hydraulic and surface-hydrological processes govern the evolution of soil moisture and the lower limit of soil moisture is set to θ_r . At $\theta = \theta_r$, as (2) and (3) show, the function ψ is negative infinite and *K* is zero, i.e., at this point the soil-hydraulic processes break down and no longer influence the evolution of soil moisture. In practice, θ_r is an empirical constant. Even using the Clapp–Hornberger closure, for which θ_r is set to zero, the soil-hydraulic fluxes are too small at low soil moisture to influence its change. In accordance with our hypothesis, we have revised the ALSIS model by including the soil-vapour phase, the revised scheme is referred to as the ALSIS-D model here.

For a given volumetric soil moisture θ , the soil-air volume per unit soil volume is

$$\Delta = \theta_{\rm s} - \theta,$$

and the soil-air mass per unit soil volume is $\rho_a \Delta$. We denote C_v as the soil-vapour mass concentration (soil-vapour mass per unit soil volume) and C_w (= $\rho_w \theta$) as the soil-water mass concentration (soil-water mass per unit soil volume). For $\theta \ge \theta_r$, we have

$$\frac{\partial C_{\rm w}}{\partial t} = \rho_{\rm w} \frac{\partial}{\partial z} K \left(1 - \frac{\partial \psi}{\partial z} \right) - E_{\rm w} + \rho_{\rm w} S, \tag{13}$$

$$\frac{\partial C_{\rm v}}{\partial t} = -w \frac{\partial C_{\rm v}}{\partial z} + k_{\rm p} \frac{\partial^2 C_{\rm v}}{\partial z^2} + E_{\rm w}, \tag{14}$$

$$\frac{\partial I}{\partial t} = \frac{\partial}{\partial z} D_{\rm h} \frac{\partial I}{\partial z} - L E_{\rm w} \,, \tag{15}$$

where E_w (kg m⁻³ s⁻¹) is the evaporation rate per unit soil volume and k_p is the mean soil-vapour diffusivity, which we set to the molecular diffusivity κ_p (m² s⁻¹). Considering that k_p depends on the soil-pore structure and varies with depth, and an air-pressure gradient exists which drives systematic motion, we include an advection term, $w\partial C_v/\partial z$, in Eq. 14, with w being an advective velocity. The inclusion of the advection term is demonstrated to be necessary in Sect. 5. For $\theta < \theta_r$, Eq. 13 is simplified to

$$\frac{\partial C_{\rm w}}{\partial t} = -E_{\rm w}.\tag{16}$$

Consider now the evaporation rate per unit soil volume E_w . The evaporation rate per unit area of soil-water surface, e_p (kg m⁻² s⁻¹), can be expressed as

$$e_{\rm p} = -g_{\rm p}\rho_{\rm a} \big(q_{\rm p} - q_{\rm sat}(T)\big),\tag{17}$$

where $q_p = C_v/(\rho_a \Delta)$ (kg kg⁻¹) is the soil-air specific humidity and $q_{sat}(T)$ is the specific humidity at the soil temperature *T*. A conductance g_p (m s⁻¹) is related to the molecular diffusivity κ_p (m² s⁻¹) via $g_p = \kappa_p/l$, with *l* being a length scale (of order of the pore size). Equation 17 can also be written as

$$e_{\rm p} = -\frac{\kappa_p}{l\Delta} (C_{\rm v} - C_{\rm vs}), \tag{18}$$

with $C_{vs} = \rho_a q_{sat}(T)$, Δ being the soil-vapour mass concentration at soil-vapour saturation. Suppose the soil water per unit soil volume has a surface area A (m² m⁻³) exposed to soil air, then

$$E_w = -\frac{\kappa_{\rm p}}{l\Delta} A(C_{\rm v} - C_{\rm vs}),\tag{19}$$

with assumptions required concerning the properties of A and l. It is advantageous to assume that

$$A = a\sqrt{\theta\Delta}/l,\tag{20}$$

such that A = 0 for $\theta = 0$ or $\Delta = 0$, where *a* is a dimensionless coefficient of O(1). This reduces (19) by one parameter and leads to

$$E_w = \gamma \sqrt{\frac{\theta}{l\Delta}} (C_{\rm v} - C_{\rm vs}), \qquad (21)$$

with the parameter $\gamma = -a\kappa_p/l^2$ to be specified. Note that $O(\kappa_p)$ is 10^{-6} m² s⁻¹ and O(l) is 10^{-3} m, such that $O(\gamma)$ is O(1) s⁻¹.

More complicated considerations of the length scale *l* can be made. For example, suppose the pore size is *s*, with maximum s_{max} , and the normalized pore size is $s' = s/s_{max}$. If we assume that larger soil pores dry out first, we then have

$$\theta = \theta_{\rm s} P\left(s'\right),\tag{22}$$

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with $P(s') = \int_{0}^{s'} p(x) dx$ and p(x) being the pore-size probability density function. It is reasonable to set

$$l = s' s_{\max} = s_{\max} P^{-1}(\theta/\theta_s), \tag{23}$$

where P^{-1} is the inverse function of *P*.

At the air-land interface, in addition to evaporation (soil water to air vapour), a vapour flux (soil vapour to air vapour) needs to be included, which serves as the upper boundary condition for (14). This flux F_{cv} is given by

$$F_{\rm cv} = -g_{\rm pa}\rho_{\rm a}\Delta_1(q_{\rm p1} - q_0), \tag{24}$$

where Δ_1 and q_{p1} are, respectively, Δ and soil-air specific humidity in the first soil layer. The factor Δ_1 is included as it is the volume of the soil air responsible for the vapour flux. The molecular conductance g_{pa} is similar to g_p , but is computed as

$$g_{\rm pa} = \left(\frac{l}{\kappa_{\rm p}}g_{\rm a}\right)^{1/2},\tag{25}$$

where g_a is aerodynamic conductance as for evaporation.

3 Qira Field Experiment

The Qira data are used to drive the ALSIS-D model and compare with the ALSIS-D simulations. The Qira experiment was carried out at a Gobi site (36°54′07″N, 80°47′07″E) near the Qira Oasis south of the Taklimakan Desert in April 2002 by Mikami et al. (2002). The data collected during ADEC–IOP1 [the Asian Dust Experiment – Intensive Observation Period 1 in the period 1007 UTC 7 April—1041 UTC 18 April 2002 (97–108 Julian Day)] are used here (Ishizuka et al. 2005a). The site, located 13.7 km to the west of Qira and 1400 m above sea level, is characteristically Gobi and has no vegetation.

Soil samples were collected at the site during the period of 28 March to 15 April 2002. They were taken at nine locations in an area of 20×20 m² at 0.01-m and 0.05-m depths with a 50-mL soil cup. The samples were dried in an oven at 105 °C for 24 h for soil-moisture measurements. The oven-dried mass was measured using an electric balance with an accuracy of 10^{-7} kg (BP211D, Sartrius, Göttingen, Germany). The oven-dried soil-moisture measurements were then used to calibrate the TDR sensors deployed at the field site for measuring soil moisture.

Atmospheric variables, including wind speed, wind direction, air temperature, and air humidity, were monitored using an automatic weather station, with data recorded using a data logger (CR10X, Campbell Scientific, Utah, USA) at intervals of 1 min. The wind speed U was measured at 0.45, 1.38, and 3.8 m above ground level, and the wind direction at 3.8 m. In addition to soil moisture, soil temperature, soil heat fluxes, and radiation fluxes, including upwards and downwards shortwave and longwave radiation, were measured.

The forcing data used to drive the ALSIS-D scheme are shown in Fig. 2, including *SolDn* (solar radiation in W m⁻²), *LwDn* (longwave radiation in W m⁻²), T_{air} (air temperature in K), and q_{air} (specific humidity in kg kg⁻¹). As surface pressure was not measured, it is set to 870 hPa for the entire study period according to Mikami et al. (2005). It is seen that the air temperature was generally between 280 and 302 K, and specific humidity between 0.002 and 0.01 kg kg⁻¹, but mostly below 0.004 kg kg⁻¹. During the period, no rainfall was recorded.



Fig. 2 Atmospheric forcing data from the Qira experiment for driving the ALSIS-D model. **a** Time series of *SolDn* (shortwave flux, W m⁻²), *LwDn* (longwave flux, W m⁻²) and T_{air} (air temperature, K); **b** As (**a**), but for U (wind speed, m s⁻¹), and q_{air} (specific humidity, kg kg⁻¹). During the period, there was no rainfall. Surface pressure is set to a constant of 870 hPa

Soil moisture was measured using TDR sensors (CS615, Campbell Scientific, Utah, USA). The applicability of the TDR instrument in a hyper-arid environment was tested in a laboratory (Ishizuka and Mikami, 2005). The sensors were set horizontally at a depth of 0.01 m at nine points in the 20×20 m² sampling area. At the centre of the area, three TDR sensors were set at the depths of 0.01, 0.05, and 0.40 m, and at the other eight locations at the 0.05-m depth. Figure 3a shows the soil-moisture measurements for the depths 0.01 and 0.05 m. Three observations can be made: (1) at the site, the value of θ could be very low, especially at 0.01-m depth, becoming as low as 0.0054 m³ m⁻³; (2) even at such low values, the soil moisture θ underwent clear diurnal variations with an amplitude of about 0.001 m³ m⁻³; and (3) over the study period, a downwards trend can be detected, indicating an overall drying trend. Figure 3b shows the soil-moisture measurements at a depth of 0.4 m, where the soil moisture was roughly constant at 0.01 m³ m⁻³, but slightly increasing.

The Qira observations have been quality checked and used for other purposes in previous studies (Ishizuka and Mikami 2005; Ishizuka et al. 2005a, b; Shao and Mikami 2005). The dataset is again used here, because it is a rare and homogenized dataset suitable for testing soil-moisture modelling in a hyper-arid environment.

4 Results

The analysis of the model results focuses on (1) the exchange between the soil-moisture and soil-vapour phases; and on (2) the comparison of land-surface processes with and without the soil-vapour phase.



Fig. 3 Volumetric soil moisture θ (m³ m⁻³) measured using a TDR sensor at the Qira site: **a** θ at 0.01-m depth (SW L1 0.01 m) and 0.05-m depth (SW L1 0.05 m) at the centre location, and at 0.05-m depth at the other eight locations (SW No4, SW No5, etc.); **b** θ at 0.4-m depth (SW L3 0.4 m) at the centre location

4.1 Results with the Soil-Vapour Phase

For the simulations, the Clapp–Hornberger closure is used for its advantage of having one parameter less than the other similar closures. A soil layer of 1.21 m is divided into eight sublayers with thicknesses of 0.01, 0.02, 0.03, 0.05, 0.1, 0.2, 0.3, and 0.5 m, from top to bottom. The atmospheric forcing data are repeatedly used to drive the ALSIS-D model. The initial conditions of soil moisture and soil temperature are first estimated from the field measurements but then, after each repetition, set to the corresponding averages over the simulation time. The repetition is performed 10 times to allow these averages to become steady. The soil layer is divided into two horizons. The first horizon is sand, 0.51 m thick, consisting of the top six sublayers, and the second horizon is loamy sand, 0.7 m thick, consisting of the last two sublayers. The Clapp–Hornberger hydraulic parameters are set according to the tests reported in Shao and Irannejad (1999), with minor adjustments to obtain improved agreement with the measurements.

Due to the inclusion of soil vapour, we have introduced in (14) the soil vapour diffusivity κ_p and an advective velocity *w* and in (21) the γ parameter. A control experiment and a number of sensitivity experiments are performed, and the parametric values used for these experiments are listed in Table 1.

The Qira measurements show that soil moisture at 0.01 m and 0.05 m varied around 6×10^{-3} and 7×10^{-3} m³ m⁻³, with a variation range of around $\pm 1 \times 10^{-3}$ and 0.5×10^{-3} m³ m⁻³, respectively. Several parameters influence the model outcomes, and a quantitatively satisfactory simulation with respect to the field observations is achieved only after numerous trial and error experiments by varying model parameters.

Table 1 List of numerical experim	ents (Exp.) an	id parameters u	sed					
Purpose	Horizon	$k_{\rm s} ({\rm m}{\rm s}^{-1})$	$\theta_{\rm s} ({\rm m}^3 \; {\rm m}^{-3})$	ψs (m)	<i>q</i>	$\kappa_{\rm p} \ (10^{-6} \ {\rm m^2 \ s^{-1}})$	γ (s ⁻¹) (max, min)	$w (\mathrm{mms^{-1}})$
Control	1st 2nd	5.83e-5 3.70e-5	0.437 0.437	-0.120 -0.120	1.41 1.81	3 (2, 4)	0.6 (1, 0.2)	0.1
Exp. 1: No soil-vapour	As control						N.A.	N.A.
Exp. 2: No soil-vapour; three β schemes	As Exp. 1						N.A.	N.A.
Exp. 31: Sensitivity to κ_p	As control						$0.5\kappa_{\rm p}$ of control	0.1
Exp. 32: Sensitivity to κ_p	As control						$2.0\kappa_{\rm p}$ of control	0.1
Exp. 41: Sensitivity to γ	As control						0.5γ of control	0.1
Exp. 42: Sensitivity to γ	As control						2.0γ of control	0.1
Exp. 5: No soil-vapour advection	As control						$10\kappa_p$ of control; Soil vapour conductance at surface same as Control	O



Fig. 4 a Simulated volumetric soil moisture θ (m³ m⁻³) at depths 0.01, 0.05, and 0.4 m (corresponding to model layers 1, 3, and 6), labelled as MSM@.01 m, MSM@.05 m, and MSM@.4 m, respectively, compared with the observed soil moisture at the same depths, labelled as OSM@.01 m etc.; **b** As (**a**), but for soil temperature *T* (°C) Measurements at 0.01 m are missing due to instrument failure; **c** Simulated soil-vapour concentration C_V (kg·m⁻³) at soil depths 0.01, 0.05, and 0.4 m; **d** As (**a**), but for the simulation with no soil-vapour phase

The ALSIS-D simulated and observed soil moisture θ and soil temperature *T* are presented in Fig. 4a and b, with the model reproducing the observations reasonably well both quantitatively and quantitatively. The value of *T* undergoes diurnal variations with reduced amplitude and delayed phase as the soil depth increases, which is a well-known phenomenon resulting from the diurnal variation of radiation and soil heat conduction. The value of θ also varies diurnally with a reduced amplitude and delayed phase as the soil depth increases. Likewise, the soil-vapour concentration C_v shows a behaviour similar to the soil temperature. During the daytime, the value of C_v , is much higher than that during night-time. The simulated soil moisture with no soil-vapour phase is presented in Fig. 4d, illustrating no diurnal variations, as at such a low soil moisture, hydraulic processes cease to play a significant role. A comparison of Fig. 4a, d reveals that, under extremely dry conditions, the evolution of soil moisture is governed by evaporation in the soil and the soil -vapour and air-vapour exchange.

Figure 5a and b presents scatter plots of the soil temperature *T* versus the soil moisture θ for the first three model soil layers, and the soil-vapour concentration C_v versus θ , respectively. Both the soil temperature *T* and the soil moisture θ vary diurnally, oscillations, as already seen in Fig. 4a and b, but their oscillations are opposite in phase, i.e., as the soil temperature *T* reaches maximum in the daytime, the value of θ is minimum, and as the value of *T* reaches minimum at night-time, the value of θ is maximum. In contrast, the variables *T* and C_v are in phase, and so it follows that θ and C_v are opposite in phase. The phase relationship between the variables *T*, θ , and C_v reveals that the behaviour of θ and C_v is mainly governed by soil thermal processes.

Figure 6 further presents diurnal variations of the processes influencing soil moisture and soil vapour in the first soil layer, showing the first two terms on the right-hand side of (13),



Fig. 5 Scatter plots of **a** soil temperature T (°C) versus soil moisture θ (m³ m⁻³) for the first three soil layers, and **b** soil-vapour concentration $C_{\rm V}$ (g m⁻³) versus θ

namely, the terms E_w and $J_w \equiv \rho_w \frac{\partial}{\partial z} K\left(1 - \frac{\partial \psi}{\partial z}\right)$ (for visualization $10J_w$ is plotted). In general, the term J_w is two orders of magnitude smaller than the term E_w , because, under such dry conditions, the hydraulic fluxes are very small. The small variations in the value of J_w seen in Fig. 6 arise from evaporation (as described by Eq. 5) with $P_r = 0$ and $R_f = 0$, and the infiltration I = -E; for the first soil layer with depth dz_1 , $J_w \approx -E/dz_1$. Also plotted in Fig. 6 are normalized soil moisture and soil vapour (the normalization follows $x_{nm} = (x - \bar{x})/3\sigma_x$, with x being an arbitrary variable, \bar{x} its mean, and σ_x its standard deviation). Soil moisture shows a relatively short drying phase from early morning (0730 LT, local time = UTC + 8 h) to early afternoon (1430 LT) as the surface warms up and the value of E_w stays positive. During this period, soil moisture is converted to soil vapour, followed by a relatively longer wetting phase from early afternoon to early morning next day as the surface cools and the value of E_w stays negative. During this period, soil vapour are almost opposite in phase, and soil vapour has a relatively short increasing phase and long decreasing phase.

4.2 Impact on the Surface Energy Balance

We ask whether the inclusion of the soil-vapour phase has significant influences on the surface energy balance (see Eq. 12). To this end, we compare the differences of the energy fluxes between the control and experiment 1, model runs with and without the soil-vapour phase, respectively. The energy-flux difference is denoted as Δ , e.g., $\Delta R_n = R_n(\text{control}) - R_n(\text{experiment 1})$, $\Delta H = H(\text{control}) - H(\text{experiment 1})$, etc. The integrals of ΔR_n , ΔH , etc. over time are respectively denoted as CR_n , CH, etc. The statistical parameters of the energy fluxes for the control and the energy-flux differences between the control and experiment 1 (Table 2) show that the impact of the soil-vapour phase on the surface energy balance is small, especially on net radiation and latent heat flux. The small ΔR_n values originate from the differences in surface soil temperature, on which the soil-vapour phase does have a noticeable influence. The soil-vapour phase has a slightly more obvious influence on sensible heat and



Fig. 6 A section of the time series of soil-moisture sources E_w and J_w for the first soil layer. The normalized soil moisture, θ_{nm} , and normalized soil-vapour concentration, C_{vnm} , are also plotted. The soil moisture drying and wetting phases are marked

ground heat fluxes. This is because the vapour exchange between the soil and atmosphere does not involve latent heat but the exchange between soil moisture and soil vapour does, which then influences soil temperature and surface sensible-heat and ground-heat fluxes.

Figure 7a, b presents the variables R_n , H, LE, and G for the control experiment and the variables ΔR_n , ΔH , ΔLE , and ΔG to show the diurnal variations of the energy fluxes and the impact of the soil-vapour phase on the energy fluxes. Figure 7c presents the variables CR_n , CH, CLE, and CG for the complete observational period. Figure 7a reveals that the surface energy balance is typical for an arid land surface, for which the latent heat flux is negligibly small and the energy balance is mainly achieved between the net radiation, sensible heat, and ground heat fluxes. Figure 7b shows that ΔR_n is mostly weakly negative, but fluctuates over several W m⁻² (in this example ± 4 W m⁻²) during the daytime. The value of ΔH is mostly weakly positive but fluctuates (in this example) between 5 and – 15 W m⁻² during the daytime, while ΔG attains almost the same magnitude (but of opposite sign) as ΔH . Figure 7c shows that CR_n over the study period accumulates to about – 100 kJ m⁻², CH about 200 kJ m⁻², and CG about – 300 kJ m⁻². The variation in the quantities CR_n , CH, and CG indicate both diurnal and synoptic scale variations.

5 Discussion

The quantitative modelling of soil moisture and land-surface processes under extremely dry conditions can be affected by a number of parameters and are associated with uncertainties. We first ask whether it is possible to tune the conventional evaporation scheme to achieve the observed soil-moisture variations at the Qira site, without invoking the soil-vapour phase. To this end, we run the ALSIS model (no soil-vapour phase) with three different β functions, namely, (8, 26), and (27)

$$\beta = 0.25 \left[1 - \cos(\pi (\theta_1 / \theta_s)^2) \right], \tag{26}$$



Fig. 7 Time series of parameters **a** R_n , H, LE, and G showing their diurnal variations, **b** ΔR_n , ΔH , ΔLE , and ΔG , and **c** CR_n , CH, CLE, and CG

$$\beta = 0.50 \left[1 - \cos(\pi (\theta_1 / \theta_s)^1) \right].$$
(27)

Model simulations show that only varying β cannot reproduce the observed soil-moisture variations (not shown). With increased evaporation (e.g., by using Eq. 27), soil moisture in the top soil layer continues to dry out to zero, and soil moisture in deeper soil layers does not change with time (similar to Fig. 4d). We conclude that, without the soil-vapour phase, the model cannot reproduce the observed behaviour of soil moisture.

Additional runs (see Table 1) are made to test the model sensitivity to the parameters γ in (20), and κ_p and w in (14). In experiment 31 and 32, the value of κ_p of the control experiment is, respectively, decreased and increased by a factor of two. Figure 8 shows that an increased value of κ_p leads to an increased soil moisture and its (amplitude of) diurnal variation due to the increased soil-vapour exchange with the atmosphere and diffusion within the soil column. As the value of κ_p increases, the modelled soil moisture agrees better with the observations, but a noticeable phase delay persists.



Fig. 8 A section of observed and ALSIS-D simulated soil moisture at 0.01-m and 0.05-m soil depths with $\kappa_p = 3 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$ (Control), $1.5 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$ [experiment (Exp.) 31] and $6 \times 10^{-6} \text{ m}^2 \text{ s}^{-1}$ (Exp. 32)

Table 2 Statistics of the surfaceenergy fluxes for the control andthe surface-energy-fluxdifferences between the controland experiment 1	Variable	Mean $(W m^{-2})$	Std $(W m^{-2})$	Max (W m ⁻²)	$\min_{(W,m=2)}$
	$\overline{R_n}$	(w m) 76	185	(w m) 552	- 125
	H	70	132	600	- 86
	LE	0.01	0.01	0.05	0.00
	G	6	69	320	-418
	$\Delta R_{\rm n}$	- 0.1	0.7	8.0	- 9.2
The abbreviations Std, Max, and Min stand for standard deviation, maximum, and minimum, respectively	ΔH	0.2	2.2	36.8	- 32.4
	ΔLE	0.003	0.006	0.039	-0.026
	ΔG	- 0.3	2.9	40.5	- 45.8

In experiments 41 and 42, the value of γ of the control experiment is, respectively, reduced and increased by a factor of two. Figure 9 shows that as the value of γ increases, soil moisture decreases and the amplitude of its diurnal variation increases. This is understandable, because a larger γ value implies faster conversion between the soil-moisture and soil-vapour phases. It is also seen that an increased value of γ results in larger phase delays in the modelled soil moisture.

In experiment 5, the value of w in (14) is set to zero (no soil-vapour advection in soil), but κ_p is increased by a factor of 10 to achieve reasonable model–observation agreement in the top-layer soil moisture. Figure 10 presents the normalized observed and modelled soil moisture for soil layer 3, showing that, while the observed and control-simulated soil moisture are in reasonable phase agreement, albeit with a delay in the latter, the observed and experiment-5-simulated soil moisture are almost opposite in phase. Various other tests by varying other relevant parameters, such as κ_p and γ , but with the soil-vapour advection term in (14) switched off, do not give better results, suggesting that soil-vapour advection plays a role in the soil-moisture evolution.

The ALSIS-D simulations show that the soil-vapour exchange with the atmosphere is responsible for the observed variations of soil moisture under extremely dry conditions. However, as can be seen in Figs. 8, 9 and 10, the modelled soil moisture has a noticeable



Fig. 9 As Fig. 8, but simulated soil moisture for soil layers 1 and 3 with $\gamma = 0.6 \text{ s}^{-1}$ (control), 0.3 s⁻¹ [experiment (Exp.) 41] and 1.2 s⁻¹ (Exp. 42)



Fig. 10 Normalized observed soil moisture at 0.05 m (OSM@.05 m) and normalized modelled soil moisture at the same soil depth for the control (Control-MSM@.05 m) and experiment 5 (Exp5-MSM@.05 m)

delay in the phase in comparison with the observations. Tuning of the newly introduced parameters does not alleviate this deficiency. The most likely reason for the persisted phase delay is that we have assumed in the model that internal soil evaporation is related to the soil temperature, which has a phase delay in comparison to the temperature of the air. It may be that the air temperature in soil differs from the soil temperature, and it is the former temperature which influences the internal soil evaporation. Here, the temperature of the air in soil is not simulated.

6 Conclusions

In a hyper-arid environment, soil moisture in the top soil layer of depth 0.01 to 0.1 m, although very low, continues to show clear temporal variations, as observed by Ishizuka et al. (2005a) in the Taklamakan Desert. Existing land-surface schemes, in which soil-hydraulic processes

are assumed to determine the behaviour of soil moisture, cannot model such variations. We have shown that soil-moisture variations in hyper-arid conditions occur due to internal soil evaporation and vapour fluxes at the air-soil interface. Conceptually, the unsaturated soil zone can be further divided into two subzones. In subzone II, the evolution of soil moisture is governed by Darcy flow, and in subzone I, by evaporation and condensation in soil pores. To better model land-surface processes in arid regions, the air-soil vapour exchange needs to be considered.

We included the air–soil vapour exchange in the ALSIS-D model (revised version based on the ALSIS model, Irannejad and Shao 1998; Shao and Irannejad 1999). The main problem for inclusion of the soil-vapour phase in LSMs is to quantify the soil-moisture and soil-vapour exchange, namely, E_w , the evaporation rate per unit soil volume, which is computed here using Eq. 21. The new parameter γ , which is relatively unknown, is of O(1) and is expected to depend on soil pore characteristics. Using the ALSIS-D model, we simulated soil moisture at the Qira site and compared the model results with the observations. The following conclusions are made.

- The ALSIS-D model can reasonably well reproduce the observed soil-moisture behaviour at the Qira site, which confirms our hypothesis, and shows that soil-moisture evolution in hyper-arid conditions is primarily influenced by the soil-vapour phase.
- 2. The diurnal variation of soil moisture in hyper-arid conditions is closely related to soil temperature. Soil moisture shows a relatively short drying phase from early morning to early afternoon as the surface warms. During this time, E_w is positive and soil moisture is converted to soil vapour, followed by a longer wetting phase from the early afternoon to the early morning next day as the surface cools. During this time, E_w is negative and soil vapour is converted to soil moisture. Consequently, soil moisture and soil vapour are opposite in phase, while soil temperature and soil vapour are similar in phase.
- 3. The influence of the soil-vapour phase on the surface energy balance is not excessive, but nevertheless measurable. Due to the inclusion of the soil-vapour phase, the value of ΔR_n is on average weakly negative but fluctuates over several W m⁻² during the daytime; ΔH is weakly positive but fluctuates in the range of -15 to 5 W m⁻² during daytime; ΔG is weakly negative and balances the term $\Delta (R_n H)$. There is little influence on the latent heat flux *LE*, as the air-soil vapour exchange does not contribute to the latent heat flux. Over the Qira observational period (12 days), the cumulative net radiation, CR_n , sensible heat, *CH*, and ground heat, *CG*, amount to -100 kJ m⁻², 200 kJ m⁻² and -300 kJ m⁻², respectively.
- 4. To achieve a good agreement with the observed soil moisture at all three depths, it is found that a soil-vapour-advection process needs to be included in the ALSIS-D model, as otherwise, simulated and observed soil moisture are almost opposite in phase already at the 0.05-m soil depth. This suggests that soil-vapour advection may be occurring in the soil column, at least at the Qira Gobi site. It is not clear whether this is due to the special characteristics of the soil column at the field site (e.g., large pores due to the presence of rocks) or other processes which play an important role in general.

The ALSIS-D simulated soil moisture and observed soil moisture can agree well in magnitude, but the simulated soil moisture is somewhat delayed in phase. By simple tuning of the existing model parameters, we cannot alleviate this model deficiency, suggesting that other physical processes or nonlinear dependencies still need to be considered to fully explain the discrepancy. It is likely that internal soil evaporation depends on the air temperature in soil, which differs from the soil temperature. This consideration is yet to be tested. In the study period, the soil temperature was above the freezing point and the soil was not frozen. But in the Taklamakan Desert in winter, soil can be frozen. In this case, the basic concept presented here would remain valid, but some modifications would be necessary, such as the inclusion of sublimation and adjustment to Eq. 21. Because we have no frozen soil observation, this case is not investigated. The Taklamakan, as many other deserts on earth, is subject to frequent dust activities. Soil moisture is a key factor influencing the threshold friction velocity for aeolian activities. The modelling of soil moisture in extremely dry conditions, as shown here, is particularly relevant for aeolian research.

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