

## MHD analysis on the physics design of CFETR baseline scenarios

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**Abstract** The China Fusion Engineering Test Reactor (CFETR), currently under intensive physics and engineering designs in China, is a major project representative of the low-density steady-state pathway to the controlled fusion energy. One of the primary tasks of the physics design for CFETR is the assessment and analysis of the magnetohydrodynamic (MHD) stability of the proposed design schemes. Comprehensive MHD stability assessment of the CFETR baseline scenarios have led to preliminary progress that may further benefit engineering designs. For CFETR, the ECCD power and current required for the full stabilization of NTM have been predicted in this work, as well as the corresponding controlled magnetic island width. A thorough investigation on RWM stability for CFETR is performed. For 80% of the steady state operation scenarios, active control methods may be required for RWM stabilization. The process of disruption mitigation with massive neon injection on CFETR is simulated. The time scale of and consequences of plasma disruption on CFETR are estimated, which are found equivalent to ITER. Major MHD instabilities such as NTM and RWM remain challenge to steady state tokamak operation. On this basis, next steps on CFETR MHD study are planned on NTM, RWM, and SPI disruption mitigation.

**Keywords** magnetic fusion · CFETR · macro-instability · MHD model

## 1 Introduction

Based on the extrapolation from the empirical scaling laws obtained from decades of research efforts on tokamaks, for a sufficiently large size and a sufficiently strong magnetic field, the tokamak plasma may achieve steady-state self-sustained ignition. The complexity and economic cost associated with the tokamak size is expected to far exceed the existing tokamak devices in the world, often requiring collaborative efforts of multiple countries and unions for many years. For example, the ITER, jointly constructed by nine international governments, will reach a height of 30 meters after completion, costing more than 10 billion euros. Since the launch of the ITER program in 2006, after nearly 15 years of international cooperation and efforts, the construction of the main unit of the device is close to completion, and it is expected that the experimental operation will begin in 2025.

Besides being a partner in International Thermonuclear Experimental Reactor (ITER) [1], China has recently proposed to design and potentially build China Fusion Engineering Test Reactor (CFETR) [2]. The goal is to address the physics and engineering issues essential for bridging the gap between ITER and DEMO (DEMONstration Power Station), including achieving tritium breeding ratio (TBR)  $> 1$  and exploring options for DEMO blanket and divertor solutions [3–5]. During the past several years, significant progress has been made in CFETR conceptual physics and engineering design [6, 5, 7]. Since 2018, a new design version of CFETR has been made, by choosing a larger machine with major radius  $R = 7.2m$ , minor radius  $a = 2.2m$  and axis toroidal magnetic field  $B_T = 5 - 7T$  [7, 8]. The primary missions of the CFETR project are proposed to demonstrate the fusion energy production of 200–1000MW, generate the steady-state burning plasmas with duty time of about 50% and test the self-sustainable burning state with fusion gain,  $Q$ , about 20–30.

The China Fusion Engineering Test Reactor (CFETR), currently both under intensive physics and engineering designs in China, is one of the major projects representative of the low-density steady-state pathway to controlled fusion energy. One of the primary tasks of the physics designs for CFETR is the assessment and analysis of the magnetohydrodynamic (MHD) stability of the proposed design scenarios. This includes the determination of the parameter boundary for major MHD instabilities, the prediction of pre-cursor signals and saturation level of nonlinear MHD instabilities, and the evaluation of their control and mitigation schemes. Over the past few years, a comprehensive efforts have been devoted to such a task as a part of the physical design activities for CFETR, and considerable progress has been made towards the task goal. This paper reports these collective progresses as a snapshot of their current status. In particular, on the side of CFETR, analyses on the error field tolerance, ECCD suppression of neoclassical tearing mode (NTM), stability of resistive wall mode (RWM), and the effectiveness of disruption mitigation using massive gas injection (MGI) are presented and discussed. The results reported here in the paper are by no means final; most of the results are preliminary in nature, partly because of the constantly evolving nature of design scenarios, and partly because of the complexity of the tasks themselves. Nonetheless, the current report is meant to serve as an overall and initial assessment on one of key components, i.e. the MHD stability prospects, of the physical designs for one of the major magnetic fusion projects as the potential next significant step of the China fusion energy program.

The rest of the paper is organized as follows. In Sec. 2, the equilibrium scenarios of CFETR are introduced. In Sec. 3, progresses on the analyses of error field tolerance, ECCD suppression of neoclassical tearing mode (NTM), stability of resistive wall mode (RWM), and the effectiveness of disruption mitigation using massive gas injection (MGI) are reported respectively. We conclude with a summary and discussion in Sec. 4.

## 2 MHD equilibria of baseline scenarios for CFETR

To achieve the mission goal of fusion power production of 1GW, the self-consistent steady-state scenarios for CFETR with fully sustained non-inductive current drive as well as the hybrid scenarios are developed using a multi-dimensional code suite with physics-based models as shown in [9–11], where the tokamak equilibria are obtained with sufficiently low convergence error and expected to provide the bases for reliable ideal and resistive MHD stability analysis [12, 13]. In particular, the equilibrium profiles for the steady-state and hybrid scenarios presented in Figs. 1 and 2 respectively are the bases of our MHD stability analyses for CFETR reported later in this paper. A dominant bootstrap current together with auxiliary extra heating current drive is required in the steady-state scenarios. As a result, safety factor  $q$ -profiles with reversed magnetic shear in the core region and a minimum  $q$  value (i.e.  $q_{min}$ ) larger than 2 or 3 characterize the equilibria of steady-state scenarios. This feature shall benefit the stability of the dangerous internal kink modes and tearing modes with low poloidal numbers, whereas the external kink modes may still grow. The hybrid

scenarios, however, have much lower  $q_{min}$ , that may give rise to the internal MHD modes.

### 3 Assessments and analyses of the MHD stability of CFETR

#### 3.1 Ideal MHD mode and RWM stability

The steady-state plasmas in the large tokamak devices, such as ITER and CFETR, should operate in regimes where the resistive wall mode (RWM) is stable or marginal stable. Thus, an unstable RWM with low toroidal mode number limits the operational space of tokamak devices. The RWM can be viewed as the residual instability of the external kink mode, which is a low toroidal mode number MHD instability with global structure along the plasma torus, and can be driven by plasma current or pressure. For a pressure gradient driven external kink mode, it becomes unstable when  $\beta_N$  exceeds the Troyon no-wall limit [14], where  $\beta_N$  is the normalized  $\beta$ . Fortunately, this kind of external kink mode can be stabilized by a closed-fit perfect conducting wall outside the plasma torus. However, the presence of the resistivity in the conducting wall will lead to the penetration of the perturbed magnetic field, thus the external kink mode can still be unstable, and its growth rate depends on the field penetration time through the conducting wall, hence the name of RWM. Generally speaking, if no other control methods are considered, the unstable RWM can be stabilized by sufficiently rapid plasma rotation and certain kinetic effects such as those from trapped particles [15–17]. However, CFETR is designed to operate in scenarios with low plasma rotation, where the passive stabilization from kinetic effects are expected to work together with active stabilizing schemes in order to achieve a robust control of RWMs, as successfully demonstrated on many major tokamaks [18–20]. Therefore, for the initial operation phase of CFETR, we shall design the plasma scenarios along with the consideration of active control schemes for RWM.

The ideal MHD instabilities are evaluated using the single-fluid MHD models implemented in the MARS-F [21] and the AEGIS [22] codes. The details on the ideal MHD and the computational models in these two codes are briefly reviewed in Appendix 1 and Appendix 2. The passive kinetic stabilization has been established experimentally for years, which should be taken into account to fully determine the RWM stability (see e.g. [17, 16, 23, 24]), using the kinetic-MHD eigenvalue codes such as MARS-K and AEGIS-K for examples, among others [25–28]. As the first step towards the more complete kinetic-MHD analyses, here we limit our calculations to the single-fluid MHD models in order to evaluate the most unstable MHD instabilities and the required active control schemes for their stabilization, leaving the passive kinetic stabilization to serve as a potential source of additional margins of MHD stability for the designed CFETR scenarios.

##### 3.1.1 Instabilities of ideal MHD modes without wall

As aforementioned, for the steady state CFETR operation with high plasma pressure, Troyon no-wall limit is one of the first critical factors to consider for the stability of

the ideal MHD modes. The ideal MHD growth rates of the  $n = 1$  toroidal mode are scanned over  $\beta_N$  for all five CFETR SSO equilibria in absence of flow or wall using both MARS-F and AEGIS codes, including the corresponding target plasma pressure or  $\beta_N$  value of each equilibrium (Figs. 3 and 4).

Generally speaking, the results reported in Figs. 3 and 4 show a good agreement between MARS-F and AEGIS codes. Both results find that only the equilibrium 2 plasma with its design target  $\beta_N$  is stable to ideal MHD modes in absence of perfect conducting wall. For all other four equilibria with their corresponding target  $\beta_N$ , the ideal MHD modes are unstable. Note that the no-wall  $\beta_N$  limits of equilibria 1 and 2 are different, even though the two equilibria are similar, especially the  $q_{95}$  and the target  $\beta_N$ -values. This difference may derive from the different values of internal inductance  $l_i$  in scenario 1 and 2, which are 0.90 and 0.96 respectively, where the plasma internal inductance is computed using CHEASE code [29] with the following definition,

$$l_i = \frac{4\pi}{I^2 R_0} \int \frac{|\nabla\psi|^2}{R^2} \mathcal{J} d\psi d\chi \quad (1)$$

with  $\mathcal{J}$  being the Jacobian  $\mathcal{J} = |(\nabla\psi \times \nabla\chi) \cdot \nabla\phi|^{-1}$ . As a result, the no-wall  $\beta_N$  limits for the  $n = 1$  modes of equilibria 1 and 2 are obtained as 2.1 and 2.95 from MARS-F calculations, in comparison to the 2.21 and 2.33 from AEGIS calculations. Whereas the MARS-F calculation on the no-wall  $\beta_N$  limit seems more sensitive to the difference in equilibria, both MARS-F and AEGIS calculations agree on whether the design target  $\beta_N$  is above or below the no-wall  $\beta_N$  limit for all the CFETR equilibria considered.

Thus both MARS-F and AEGIS results in Figs. 3 and 4 indicate that the ideal MHD modes in CFETR scenarios 1,3,4 and 5 are unstable in absence of an ideal wall. Next we calculate and compare the instabilities of RWM among these four scenarios, assuming different models of CFETR wall. Based on the CFETR structure design including the first wall, the Tritium breeding module (TBM) blanket, and the vacuum vessels [30], their sketch and the corresponding plasma shape is plotted in Fig. 5(a) as one of the wall models considered in this study. The minor radius of vacuum vessel (VV) has been fixed to be double of plasma minor radius away from the plasma boundary, i.e.  $d_{VV} = 2a$ . However, here the TBM resistivity remains unknown, due to the unknown material and structure of the TBM. Thus in another model, an artificial conducting wall is imposed and shown in Fig. 5(b), where its shape conformal to the plasma shape and its resistivity based on the design for ITER are assumed in order to assess the most probable effects from wall.

### 3.1.2 Instabilities of RWMs with conformal wall

In this subsection, we shall assume an artificial conformal wall outside the plasma torus as shown in Fig. 5(b). The minor radius of wall is denoted as  $d_{wall}$ . Here, only an ideal plasma is considered without taking into account of plasma flow or resistivity.

The growth rates of the external kink modes in presence of an ideal wall or resistive wall as functions of the wall minor radius are computed using MARS-F code (Fig. 6). Here, the effective wall time is estimated to be  $\tau_w = 10^4 \tau_A$ . The vertical

dashed lines denote the minor radius of the TBM and VV in CFETR. One should keep in mind that the TBM and VV here used in the MARS-F calculation are the conformal walls instead of the actual walls with more realistic structures. Thus the  $\gamma\tau_A$  in Fig. 6 is in general expected to be slower than the actual mode growth rate in presence of the more realistic TBM and VV. If the VV is designed to stabilize the ideal external kink modes, it can be found from these results that the VV may be located too far away from the plasma boundary, such that there is nearly no effect of VV on the growth rate of those modes, except for the equilibrium of scenario 4. Although the  $q$  profile of Equilibrium 4 is quantitatively different from other equilibria, all the 5 equilibria share the common feature of having a wide core region with flat  $q$  profile. More importantly, a closer survey of Fig. 1 indicates that the current and the  $q$  profiles of Equilibrium 4 is well within the range of the continuous profile variations from Equilibrium 1 to Equilibrium 5. Thus even though the MARS-F calculation results for the equilibrium of scenario 4 in Fig. 6 show that the conformal walls at the TBM and VV radii appear to be far more stabilizing to the ideal and resistive wall modes than all other equilibrium cases, the equilibrium of scenario 4 itself can be readily obtained and sustained from the middle of the achievable range of equilibria. Therefore, in the following discussion, we shall take this scenario 4 as an example to investigate on the RWM control scheme for CFETR.

The marginal stability boundaries of the five SSO equilibria in presence of the perfectly conducting wall are also obtained from AEGIS calculations, along with the explicit effects of the equilibrium flux surface domain truncation (Fig. 7). Note that a small fraction of plasma edge region is truncated off in AEGIS computation domain in order to avoid the X-point singularity in the flux coordinate representation of tokamak equilibria, a practice similarly adopted in the MARS-F calculations as well. The  $q_a$  values and the corresponding normalized magnetic flux  $\psi$  at the truncated surface used to calculate the RWM growth rates of the equilibria eq1 to eq5 are listed in Table 2, respectively. In all these cases, the truncated surfaces extend sufficiently far out towards the separatrix so that all the dominant resonant mode components are included in integration to obtain maximal accuracy and convergence. For a fixed wall location, the ideal MHD mode growth rate in presence of a resistive wall in scenario 4 is the smallest. Furthermore, the radial profiles of the real part of the perturbed normal displacement computed using MARS-F and AEGIS codes are compared for the same target plasma  $\beta$  and resistive wall location at  $d_{wall} = 1.2a$ , which show similar global mode structures (Fig. 8).

### 3.1.3 Instabilities of RWMs with designed wall

In this sub-section, we consider the model for designed wall including both TBM and VV components, and evaluate the contribution of these structures to the growth rate of the ideal MHD modes. Based on the findings from previous subsection, here the analysis is focused on the equilibrium of scenario 4 as an example. In addition, because the VV is so far away from the plasma torus that the TBM has to be also taken into account. However, the exact properties of material of the TBM remains unknown at this stage. A parameter  $C$  for the ratio of resistivities between TBM

and VV is introduced as  $C = \tau_{TBM}/\tau_{VV}$ , and the VV wall time is assumed to be  $\tau_{VV} = 1865.3ms$ .

Fig. 9 compares the RWM growth rates as functions of the TBM location from MARS-F calculations for several different values of the ratio parameter  $C$ , as well as the case with a single ideal conducting wall, where the dependence of growth rate is on the ideal wall location. The ratio  $C$  designed for ITER is 0.05. As shown in Fig. 9, the growth rate of ideal MHD modes is higher with lower  $C$ -value due to higher resistivity of TBM. However, if TBM can achieve to the condition of blanket designed for ITER, this ideal MHD mode can become nearly marginal stable with the synergistic effect of TBM and VV.

### 3.1.4 Effect of plasma shaping on instabilities of RWM

Based on the geometry design for CFETR, we note that the VV boundary is far away from the plasma-vacuum interface, so that the effect of conducting wall on the growth rate of unstable MHD modes is expected weak. In this section, we shall gradually modify the shape of VV in the lower outboard corner. Only CFETR scenario 4 with the designed wall model, is evaluated in this section.

Our primary concern is the effect of the lower triangularity of VV shape, which is designed shaping feature mainly out of engineering considerations, on the growth rate of the ideal MHD modes. We introduce an analytic model for systematically scanning the lower triangularity, which can be written as

$$\rho' = \rho \left\{ 1 + \delta \exp \left[ -\frac{(\phi - \phi_m)^4}{2\kappa^2} \right] \right\}, \quad \phi \in [\phi_A, \phi_B] \quad (2)$$

where  $R' = \rho' \cos\phi$  and  $Z' = \rho' \sin\phi$ . A sketch of this model in the  $(R, Z)$  plane is shown in Fig. 10(a). The black curve L is the original VV shape designed for CFETR. The red curve  $L'$  is the new shape obtained from varying parameter  $\delta$  along the poloidal circumference between points A and B. In this analysis, other parameters are fixed as  $\phi_m = 0.8$  and  $\kappa = 0.2$ , and only the value of  $\delta$  is varied to obtain a family of new VV shapes (Fig. 10(b)). For the new family of VV shape and TBM with  $C = 0.05$ , the growth rates of the ideal MHD modes are shown to decrease with the magnitude of  $\delta$ , indicating a stabilizing effect as the VV draws closer to the plasma surface. However, such a stabilizing effect is rather limited (Fig. 10(c)).

### 3.1.5 Stabilization of RWM based on plasma flow

As mentioned earlier, the designed CFETR scenarios except scenario 2, are unstable to the ideal MHD modes in presence of resistive wall or in absence of wall. In this section, we evaluate the potential stabilization of these unstable RWMs by plasma flow. The conformal resistive wall is assumed to be located at  $d_{wall} = 1.2a$ .

In MARS-F calculations, the equilibrium of scenario 1 along with a uniform rotation profile is considered. The RWM growth rates are shown to decrease with rotation frequency, and such a rotational stabilization is also enhanced with higher ion Landau damping rate  $\kappa_{||}$  (Fig. 11(a)). Similar calculations using AEGIS code for

all five CFETR scenarios indicate that the unstable RWMs can all be stabilized by plasma rotation at a few percent (1.5%-2%) of Alfvén speed (Fig. 11(b)), where the shear-Alfvén continuum resonance in the rotating plasma leads to the stabilization of resistive wall modes.

### 3.1.6 Active control of RWM based on feedback

In addition to the passive stabilization of RWMs by wall design and toroidal rotation, we continue to evaluate active control scheme for the RWM in CFETR based on feedback coils, considering for example the equilibrium of scenario 2 with a conformal conducting wall. Three rows of feedback coils, the upper, middle and lower rows along the toroidal angle, are shown in Fig. 12, where  $\theta_c$ , normalized by  $\pi$ , denotes the poloidal angle of the coil location and the resistive wall is assumed to locate at  $r_w = 1.3$ .

For the feedback relation  $M_{sf}I_f = -G\psi_s(t)$  and the transfer function  $P(s) = \psi_s/M_{sf}I_f$ , the characteristic equation with proportional feedback satisfies  $1 + GP(s) = 0$ , where  $s$  is the Laplace variable representing the mode eigenvalue. Here  $G = |G|e^{i\Phi}$  is feedback gain, and  $|G|$  and  $\Phi$  represent its amplitude and phase respectively.  $\psi_s(t)$  is magnetic signal. And  $M_{sf}$  is the free-space mutual inductance between the feedback coil and the sensor loop, used largely to normalize the feedback gain.  $I_f$  is the current in active control coil.

Analysis indicates that the RWM can be stabilized by such a feedback coil system. Assuming only a set of middle active coils ( $\theta_c = 0$ ) are used, as shown in Fig. 13, the minimum critical gain is obtained to be  $|G| = 0.3$ , when the poloidal covering width of active coil  $W = 45^\circ$ , normalized by  $\pi$ . And the critical gain decreases as the radial position of active or sensor coils becomes closer to plasma surface. Normally, with a single set of active coils, we do not consider the phase of the feedback gain, since the feedback with real gain values produces the best stabilization. If only a set of upper and lower symmetric active coils are employed as in Fig. 14, when the gain amplitude  $|G| = 0.1$  is same for both upper and lower active coils and the poloidal covering width of active coils are  $W = 2|\theta_c|$ , the effectiveness of feedback system is best at the poloidal positions  $|\theta_c| = 11.7^\circ$  for upper and lower active coils, in the absence of phase angle. The smaller poloidal coverage indicates that the system of upper and lower symmetric active coils is more effective than the system of middle active coils alone for the stabilization of RWM. For the same feedback parameter of  $|\theta_c|$  as shown in Fig. 14(b), the critical gain is  $|G| = 0.2$ . Fig. 14(c-d) show that the RWM stabilization sensitively depends on the feedback gain phase. The best phases for reducing the RWM growth rate are  $\Phi_U \sim 50^\circ$  and  $\Phi_L \sim -50^\circ$ .

## 3.2 CFETR error field tolerance

The estimate on error field tolerance for CFETR is based on the design parameters that the major radius is  $R = 7.62m$ , the minor radius  $a = 2.25m$ , and the toroidal field  $B_T = 6.5T$ , and the assumptions that the safety factor at the 95% of magnetic flux  $q_{95} \sim 5.5$ , the electron density  $n_e = 8.94 \times 10^{19}m^{-3}$ , and the rotation frequency  $f =$



$2.34 \times 10^4 / (2\pi) \text{Hz}$  in the hybrid scenario. For comparison, we assume that in ITER the toroidal field  $B_T = 5.3 \text{T}$ , the safety factor at the 95% magnetic flux  $q_{95} \sim 3.2$ , the rotation frequency  $f = 3 \text{kHz}$ , and the electron density is same as that in CFETR. We evaluate the error field tolerances for both CFETR and ITER by extrapolation using theoretical scaling laws [31–34] and the experimental ones on the basis of the EAST error field penetration threshold data [35–39] (Table. 3).

According to the theoretical extrapolation [31–34], the error field tolerance ( $b_r/B_T$ ) of CFETR is similar to that of ITER, from both MHD and two-fluid models. Most extrapolation results on the error field tolerance using the experimental scalings [35–39] are similar for CFETR and ITER as well. However, when the safety factor at the 95% magnetic flux  $q_{95}$  is taken into account, such as in the case of EAST experimental scaling, the error field tolerance is larger than that in ITER where the  $q_{95} \sim 3.2$  in ITER is much lower than the  $q_{95} 5.5$  in CFETR. That is to say if  $q_{95}$  is higher in CFETR than that in ITER, then the CFETR operation would be less susceptible to error field. At present the correction field coils are designed for ITER. If CFETR operates in the ITER-like operational scenario, then the correction field coils are needed. If CFETR operates in much higher safety factor at the 95% magnetic flux than that in ITER, then the correction field coils may not be absolutely necessary.

### 3.3 Control of the neoclassical tearing modes by electron cyclotron current drive in CFETR

Neoclassical tearing mode (NTM), if uncontrolled, limits the performance of advanced tokamak devices such as CFETR. The NTM induced large magnetic islands can significantly degrade the plasma confinement or even lead to the plasma disruption. Thus, the control of NTMs is necessary for the steady operations of CFETR. To suppress NTMs, extra current drive can be deposited near the magnetic island region to compensate the loss of bootstrap current caused by the flattening of pressure inside the magnetic island. In the tokamak experiment, it has been verified that electron cyclotron current drive (ECCD) is an effective method to for that purpose. Here we numerically investigate the ECCD control schemes for NTMs in the hybrid scenarios of CFETR.

#### 3.3.1 Benchmark between MD and NIMROD on nonlinear tearing mode in hybrid scenario

For the purpose of investigating tearing instability of CFETR hybrid scenario, we first use polynomials to fit the original equilibrium profiles. Then we use the equilibrium solver NIMEQ to generate a new equilibrium on the NIMROD simulation mesh based on the fitted pressure and safety factor profiles, along with the CFETR boundary shape. Toroidal mode components  $n = 0 - 1$  are included in the nonlinear NIMROD simulation here. Plasma parameters are set as following:  $S = 10^5$ ,  $P_{rm} = 0.26$ ,  $\tau_A = 5 \times 10^{-7} \text{s}$ .

For the hybrid scenarios EQ3 shown in Fig. 2, the resistive tearing mode is found linearly unstable before nonlinear saturation from the time evolution of the

perturbed magnetic energy, as indicated by both MD and NIMROD simulation results in Fig. 15. The corresponding magnetic island and plasma flow patterns in the saturation phase given in the sub-figures of Fig. 15, show that the saturated island is dominated by the  $m/n=2/1$  structure, whose width is near 20% (33%) of the minor radius from the MD (NIMROD) simulation result.

### 3.3.2 MD simulation results on ECCD control of NTMs

For the MD simulations, Westerhof-Pratt's closure relation [40] is employed for the ECCD density  $j_d$  appearing in the Ohm's law Eq. (11), which can be calculated based on the following equations

$$\frac{\partial j_{d1}}{\partial t} = -j_{sc} - \nu_1 j_{d1} + \nu_{\parallel, res} \nabla_{\parallel} j_{d1} \quad (3)$$

$$\frac{\partial j_{d2}}{\partial t} = -j_{sc} - \nu_2 j_{d2} + \nu_{\parallel, res} \nabla_{\parallel} j_{d2} \quad (4)$$

$$j_d = j_{d1} + j_{d2} \quad (5)$$

Here,  $\nu_1$  and  $\nu_2$  denote the collision rates near the electron cyclotron waves driven 'hole' and 'bulge' at small and high perpendicular velocities respectively.  $\nu_{\parallel, res}$  is the parallel velocity of the resonant electrons. The source term for ECCD  $j_{sc}$  is assumed to be of the Gaussian distribution as

$$j_{sc} = j_{d0} \exp\left\{-4\left[\left(\frac{r-r_0}{\Delta_{rd}}\right)^2 + \left(\frac{\chi-\chi_0}{\Delta_{\chi}}\right)^2\right]\right\}$$

where  $r_0$  and  $\chi_0$  are the center of the Gaussian distribution in the radial and helical angle directions respectively,  $j_{d0}$  is the peak value of ECCD source,  $\Delta_{rd}$  and  $\Delta_{\chi}$  are the half deposition width of the distribution in the radial and helical angle directions respectively. Unless otherwise stated, the ECCD is aimed at the center of the O-point of the magnetic island. Other ECCD related parameters are set as  $\Delta_{rd} = 0.05$ ,  $\Delta_{\chi} = 0.2$ ,  $\nu_1 = 2.5 \times 10^{-3}$ ,  $\nu_2 = 0.5 \times 10^{-3}$  and  $\nu_{\parallel, res} = 2$ , all in SI units.

For the hybrid scenario EQ1 shown in Fig. 2, the classical  $m/n = 2/1$  tearing mode with  $f_b = 0$  is stable. However, the fraction of bootstrap current for the hybrid scenarios in CFETR is nearly 50%. Thus, the evolution of magnetic island with various fractions of bootstrap current is calculated and given in Fig. 16. It is found that the width of the saturated magnetic island is about  $0.2a$ , i.e. near  $40cm$  for the size of CFETR. This big magnetic island is very dangerous and can obviously lead to the major disruption of discharge. Therefore, ECCD must be employed to control the growth of the NTMs for CFETR.

If the ECCD is turned on after the magnetic island is saturated, as shown in Fig. 17(a), it is found that the magnetic island can be suppressed completely when the driven current  $I_{cd}$  is larger than 2% of the total plasma current ( $I_p = 13MA$ ). However, if the ECCD is turned on before the magnetic island is saturated, the strength of the driven current  $I_{cd}$  required for the suppression of NTM can be reduced. For instance, the required  $I_{cd}$  is near 1% of  $I_p$ , when the ECCD is turned on at  $t/\tau_a = 15000$ , as shown in Fig. 17(b). In fact, the required  $I_{cd}$  can be less than 1% of  $I_p$ , if the ECCD

can be turned on before  $t/\tau_a = 15000$  when the magnetic island width is smaller than  $0.025a$  or  $5cm$ . Dependence of the driven current for the suppression of NTM on the magnetic island width is given in Fig. 17(c). It can be clearly observed that the required  $I_{cd}$  is proportional to the width of magnetic island at the time when the ECCD is turned on. However, the required  $I_{cd}$  for NTM suppression levels out when the island size increases above a certain threshold.

To summarize, MD simulations find that the saturated island width in the hybrid scenarios of CFETR is about  $0.2a$ . The required ECCD for the suppression of the saturated NTM is just above 2% of the total plasma current  $I_p = 13MA$ . However, if the ECCD is turned on when the magnetic island width is less than a critical value, the required ECCD for the suppression of NTM can be reduced. Both the numerical and theoretical results indicate that the required ECCD is proportional to the size of magnetic island at the time when ECCD is turned on in the small magnetic regime, and becomes independent of island size in the large magnetic island regime.

### 3.3.3 TM8 simulation results on ECCD control of NTMs

The evolution of neoclassical tearing mode and its stabilization by electron cyclotron current drive for the hybrid scenario of CFETR are also numerically performed using the reduced MHD code TM8. The parameters of our numerical calculations are set as the following if not mentioned elsewhere: a localized distribution of current density from ECCD is applied at the resonant surface with  $w_{cd}/a = 0.04$ ,  $\chi_\perp = 12.5a^2/\tau_R$  and  $\chi_\parallel/\chi_\perp = 10^8$ , where  $a$  is the minor radius,  $w_{cd}$  the half width of driven current,  $\tau_R = a^2\mu_0/\eta$  the resistive time,  $\chi_\parallel$  and  $\chi_\perp$  are the parallel and perpendicular heat transport coefficients, respectively. The Lundquist number  $S = \tau_R/\tau_A$  is taken to be  $5.56 \times 10^6$ , where  $\tau_A$  is the Alfvén time. And  $r_s = 0.51a$  is the minor radius of the  $q = 2$  surface. The local bootstrap current density fraction at the resonant surface is set to be  $j_b/j_p = 0.3$  initially. The inverse aspect ratio  $\epsilon = a/R \simeq 0.31$  as designed.

For the hybrid scenario, the time evolution of the normalized 2/1 magnetic island width,  $w/a$ , is shown in Fig. 18. The solid curve is for the case without applying ECCD. The modulated current drive (MCD), which is in phase with the island's O-point, is applied at  $t/\tau_R = 0.05$  with  $I_{cd}/I_p = 0.059$  (dashed curve) and  $I_{cd}/I_p = 0.06$  (dot-dashed curve), where  $I_{cd}$  is the current driven by electron cyclotron wave (ECW), and  $I_p$  is the plasma current. Similar to Fig. 18a, the case for non-modulated current drive (NMCD) is also shown in Fig. 18b. It can be seen that there is a threshold in the driven current for mode stabilization.

When ECCD is applied during the island growth before nonlinear saturation, less driven current is expected to be required for mode stabilization. The time evolution of the island width is shown in Fig. 19a with MCD applied when the island width  $w = 0.01a$  is reached. The solid curve is for the case without ECCD. The dashed and dot-dashed curves are for  $I_{cd}/I_p = 0.017$  and  $0.018$ , respectively, which indicate that less driven current is required for the stabilization of a smaller magnetic island. The required  $I_{cd}/I_p$  for fully stabilizing the 2/1 mode is shown as a function of the island width in Fig. 19b, in which ECCD is applied when the island width  $w$  grows to the value shown by the horizontal axis. The solid (dashed) curve is for MCD (NMCD). For both MCD and NMCD, when applied before the nonlinear mode saturation, the

required driven current for mode stabilization increases with  $w$ , suggesting the advantage of applying ECCD earlier in time. For a smaller island width, the MCD scheme is much more effective than NMCD for stabilizing the NTM.

In the analyses using both MD and TM8 simulations reported above, the range of Lundquist number  $S = 10^5 \sim 5.56 \times 10^6$ , which is lower than the  $S$  values in more realistic regimes. Currently both MD and TM8 simulations on NTMs may have to rely on the less realistically large viscosity values to avoid numerical difficulties within the capability of affordable computing resource. Thus one should keep this limit in mind when applying the NTM analysis results here as potential guidance for the corresponding engineering design. Meanwhile, these analyses are subject to continued updates as the reliable  $S$  regimes of MD and TM8 simulations expand further upward.

### 3.4 Disruption mitigation simulation with massive neon injection on CFETR

Simulation evaluation of the disruption mitigation scheme with massive neon injection on CFETR using the 3D nonlinear MHD code NIMROD, which incorporates a radiation and atomic physics model taken from the KPRAD code, has been performed and the main findings are reported here. The time evolution of the several key discharge parameters are shown in Fig. 20. During the pre-thermal quench (pre-TQ) phase before  $t = 2ms$ , the thermal energy is dissipated gradually due to radiation cooling by the injected impurity (Fig. 20(b)), however, the core electron and ion temperatures remain relatively unchanged and even increases to a peak value by the end of the pre-TQ phase (Fig. 20(c)). Here the single-fluid MHD model is used in the simulation, where the ion and temperatures are the same, i.e.  $T_i = T_e = T$ . Although the temperature at magnetic axis  $T(0)$  itself decreases slowly during the pre-TQ phase (i.e.  $t = 0 - 2ms$ ) as shown in Fig. 20(c), the edge temperature and the major portion of the temperature profile drop much more rapidly during the same phase as clearly demonstrated in Fig. 22(a). Since the thermal energy is an integral over the entire plasma volume, this explains why the thermal energy decreases much faster than the temperature at magnetic axis  $T(0)$  itself, as can be seen in Fig. 20(b)-(c). Meanwhile, MHD activity grows to nonlinear saturation and the  $n = 1$  mode dominates from beginning (Fig. 20(a)). The thermal quench (TQ) phase starts when the core electron temperature starts to collapse at  $t = 2ms$ . By the end of TQ phase at  $t = 3.1ms$ , the thermal energy is almost totally dissipated and the core electron temperature drops to zero. Soon after the start of TQ phase, the  $n = 1$  mode reaches its peak magnitude and the magnetic field becomes completely stochastic (Fig. 21), leading to loss of plasma confinement entirely. The current quench (CQ) sets on after  $t = 3.1ms$ , i.e the end of TQ phase.

Profile evolution of ion temperature, impurity number density, electron number density, toroidal current density, radiation power and Ohmic heating during the neon injection process are obtained respectively from the simulation (Fig. 22(a)-(f)). The impurity density gradually penetrates into the core region from boundary as shown in Fig. 22(b), and the corresponding total electron density increases accordingly as a result of impurity ionization (Fig. 22(c)). The radiation power profile rises and shifts towards the core region along with the impurity penetration over time (Fig. 22(e)),

leading to the drop of the core ion temperature profile as shown in Fig. 22(a). At the same time, the plasma resistivity increases and the current density profile contracts as a consequence (Fig. 22(d)), which contributes to a strong localized deposition of Ohmic heating power at the cold region (Fig. 22(f)).

The plasma current drop beyond the end of the TQ phase shown in Fig. 20(d) is significantly slower than what would be expected from experiments. This is mostly the consequence of the realistically and relatively low resistivity value based on the collisional Spitzer model adopted in the simulation. Since the NIMROD code used in simulation here does not include the model for the necessary mechanisms that contribute to the more realistic current quench phase, the current decay shown in Fig. 20(d) is not used for the estimate of the CQ time scale, but only included and shown here for the completeness of simulation results. The simulation has been able to reproduce many key features of the thermal quench phase that are much more realistic in comparison to experiments, as also reported in other MGI simulation studies using NIMROD (e.g. [41–45]). Thus the simulation results on the TQ phase are the base of estimate for the CFETR scenario.

#### 4 Summary and discussion

In summary, the CFETR physics and engineering designs have provided unprecedented opportunities to the advancement in MHD theory and simulations. Comprehensive efforts on the assessment of MHD stability of the CFETR baseline scenarios have led to following preliminary progresses that may further benefit engineering designs.

For CFETR, the ECCD power and current required for the full stabilization on NTM have been predicted in this work, as well as the corresponding modulated magnetic island width. A thorough investigation on RWM stability for CFETR is performed. For 80% of the SSO scenarios, active control methods may be required for RWM stabilization. The process of disruption mitigation with massive neon injection on CFETR is simulated. The time scale of and consequences of plasma disruption on CFETR are estimated, which are found equivalent to ITER. Major MHD instabilities such as NTM and RWM remain challenge to steady state tokamak operation. On this basis, next steps on CFETR MHD study are planned. Further analysis on NTM control with ECCD system will be processed with TM8 code and NIMROD code, along with TORAY code, in order to provide more detailed and quantitative information on the required ECCD current amplitude and distribution and optimized injection angle for NTM stabilization. More careful prediction on RWM stability boundaries with kinetic effects included will be performed using MARS-K and AEGIS-K codes. On the other hand, the design and feasibility analyses on the RWM active and feedback control systems are also necessary for the unstable RWM scenarios. A new task of simulation on the disruption mitigation based on the shattered pellet injection (SPI) of impurity gas is expected to start, so that we can evaluate on the corresponding time scale, gas injection depth, MHD modes, and current distribution in vacuum chamber.

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## Appendix 1 MARS code

MARS-F code [21] is based on the single fluid, linearized resistive MHD model,

$$(\gamma + in\Omega)\xi = \mathbf{v} + (\xi \cdot \nabla)R^2\nabla\phi \quad (6)$$

$$\begin{aligned} \rho(\gamma + in\Omega)\mathbf{v} = & -\nabla p + \mathbf{j} \times \mathbf{B} + \mathbf{J} \times \mathbf{b} \\ & -\rho[2\Omega\hat{Z} \times \mathbf{v} + (\mathbf{v} \cdot \nabla\Omega)R^2\nabla\phi] - \nabla \cdot \Pi \end{aligned} \quad (7)$$

$$(\gamma + in\Omega)\mathbf{b} = \nabla \times (\mathbf{v} \times \mathbf{B} - \eta\mathbf{j}) + (\mathbf{j} \cdot \nabla\Omega)R^2\nabla\phi \quad (8)$$

$$(\gamma + in\Omega)\mathbf{p} = -\mathbf{v} \cdot \nabla P - \Gamma P \nabla \cdot \mathbf{v} \quad (9)$$

$$\mathbf{j} = \nabla \times \mathbf{b} \quad (10)$$

where  $R$  and  $\phi$  are the plasma major radius and geometric toroidal angle, and  $\hat{Z}$  is unit vectors along the vertical direction in the poloidal plane, respectively. The variables  $(\xi, \mathbf{v}, \mathbf{j}, \mathbf{b}, \rho, p)$  represent the plasma perturbed displacement, velocity, current, magnetic field, density and pressure, respectively. The corresponding equilibrium quantities are denoted by  $(\mathbf{J}, \mathbf{B}, P)$ .  $\Omega$  is the angular frequency of the plasma flow along the toroidal angle, and  $n$  is the toroidal harmonic number.  $\Pi$  is a viscous stress tensor, which is associated with the viscous force damping, such as the parallel sound wave damping.

Although the growth rate of the RWM is very slow, it eventually sets the upper limit on plasma pressure for the long pulse or steady-state advanced tokamak operations. MARS code is designed to compute the growth rate of the RWM and how to control it by the passive (the plasma rotation and drift kinetic resonances) and active (the feedback control system) methods.

MARS code has been benchmarked and extensively applied to model RWM and compare with the experimental observation. For examples, a kinetic version of MARS

found low-rotation threshold when applied to model a DIII-D discharge with balanced beam injection, agreeing with experimental observations [46]. MARS-F and its coupling to CARIDDI (CarMa) found quantitative agreement between the computed RWM growth rate and the experiments in RFX [47]. MARS-F has also modeled the resonant field amplification for a series of JET plasmas which agrees with experimental measurements [48]. [49] has compared the unstable RWM regime obtained using MARS-K with that in DIII-D experiments, revealing the impact of energetic particle losses and toroidal rotation drop in destabilizing the mode. Finally, the MARS-K modeling of stable RWM induced resonant field amplification quantitatively agrees with DIII-D experiments [50].

## Appendix 2 AEGIS code

The Adaptive Eigenfunction Independent Solution shooting (AEGIS) code employs the adaptive shooting method in the radial direction and Fourier decomposition in the poloidal direction [22]. Therefore, the AEGIS code has high resolution near the singular surfaces for the study of MHD instabilities. The AEGIS code has been used to study the linear behaviors of RWMs in ITER and the earlier smaller-sized design of CFETR scenarios [51, 52].

The following perpendicular MHD equation was solved in AEGIS,

$$-\rho_m(\omega + n\Omega + i\gamma_p)^2 \xi_\perp = \delta \mathbf{J} \times \mathbf{B} + \delta \mathbf{B} \times \mathbf{J} - \nabla \delta P$$

where  $\rho_m$  is the total apparent mass density,  $\omega$  the mode frequency,  $n$  the toroidal mode number,  $\Omega$  the toroidal rotation frequency,  $\gamma_p$  is a small parameter used to heal the numerical singularity while calculating the Alfvén damping,  $\xi$  is the fluid displacement, with subscript  $\perp$  denoting the perpendicular component to the magnetic field, and  $\mathbf{J}$ ,  $\mathbf{B}$ , and  $P$  are the equilibrium current density, magnetic field, and plasma pressure, respectively.

## Appendix 3 MD code

The reduced MHD model implemented in the MD code is given as follows [53]

$$\frac{\partial \psi}{\partial t} = [\psi, \phi] - \partial_z \phi - S_A^{-1}(j - j_b - j_d) + E_{z0} \quad (11)$$

$$\frac{\partial u}{\partial t} = [u, \phi] + [j, \psi] + \partial_z j + R^{-1} \nabla_\perp^2 u \quad (12)$$

$$\frac{\partial p}{\partial t} = [p, \phi] + \chi_\parallel \nabla_\parallel^2 p + \chi_\perp \nabla_\perp^2 p + S_0 \quad (13)$$

where  $\psi$  and  $\phi$  are the magnetic flux and electrostatic potential,  $j = -\nabla_\perp^2 \psi$  and  $u = \nabla_\perp^2 \phi$  are the current density and vorticity in the axial direction, respectively. The bootstrap current density is proportional to the pressure gradient as in  $j_b = -f \frac{\sqrt{\epsilon}}{B_\theta} \frac{\partial p}{\partial r}$ , with  $f$  measuring the strength of bootstrap current fraction, which is defined as

$f_b = \int_0^a j_b r dr / \int_0^a j_z r dr$ .  $S_A = \tau_\eta / \tau_A$  and  $R = \tau_v / \tau_A$  are the magnetic Reynolds number and kinematic Reynolds number, respectively, where  $\tau_\eta = a^2 \mu_0 / \eta$ ,  $\tau_v = a^2 / \nu$  and  $\tau_A = \sqrt{\mu_0 \rho} a / B_0$  are the resistive diffusion time, the viscous diffusion time, and the Alfvén time, respectively.  $\chi_\parallel$  and  $\chi_\perp$  are the parallel and perpendicular transport coefficients. The source terms  $E_{z0} = S_A^{-1} (j_0 - j_{b0})$  and  $S_0 = -\chi_\perp \nabla_\perp^2 p_0$  in equations (11) and (13) are chosen to balance the diffusion of equilibrium Ohm current and pressure, respectively. The length, time and velocity are normalized by the plasma minor radius  $a$ , Alfvén time  $\tau_A$  and Alfvén velocity  $V_A = B_0 / \sqrt{\mu_0 \rho}$  respectively. The Poisson bracket is defined as  $[f, g] = \hat{z} \cdot \nabla f \times \nabla g$ .

#### Appendix 4 TM8 code

The TM8 code has been used to model the physics of the ECCD stabilization of NTM [54], the drift-tearing modes [55], the double tearing modes [56], the mode coupling [57], the stochastic field [58], the resonant magnetic perturbation [59], and the error field [60]. The corresponding simulation results compare well with experiments.

The reduced MHD model implemented in the TM8 code includes the Ohm's law, the plasma vorticity equation, and the plasma pressure evolution equation [61]

$$\frac{\partial \psi}{\partial t} + \mathbf{v} \cdot \nabla \psi = E - \eta (j_p - j_b - j_d) \quad (14)$$

$$\rho \left( \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right) \nabla^2 \Theta = \mathbf{e}_t \cdot (\nabla \psi \times \nabla j_p) + \rho \mu \nabla^4 \Theta \quad (15)$$

$$\frac{3}{2} \left( \frac{\partial}{\partial t} + \mathbf{v} \cdot \nabla \right) p = \nabla \cdot (\chi_\parallel \nabla_\parallel p) + \nabla \cdot (\chi_\perp \nabla_\perp p) + Q \quad (16)$$

where  $\mathbf{v} = \nabla \Theta \times \mathbf{e}_t$ ,  $\Theta$  is the stream function,  $\mathbf{e}_t$  the unit vector in the toroidal direction, and  $j_p = -\nabla^2 \psi - 2nB_{0t} / (mR)$ ,  $j_b = -c_b \frac{\sqrt{\epsilon}}{B_\theta} \frac{\partial p}{\partial r}$ , and  $j_d$  are the plasma current density, the bootstrap current density, and the current density driven by electron cyclotron wave (ECW) in the  $\mathbf{e}_t$  direction, respectively.

#### Appendix 5 NIMROD/KPRAD code

In the NIMROD code [62], the 3D extended MHD model is coupled with an atomic and radiation physics model from the KPRAD code [41, 42, 63], and the implemented



equations for the coupled impurity-MHD model are as follows:

$$\rho \frac{d\vec{V}}{dt} = -\nabla p + \vec{J} \times \vec{B} + \nabla \cdot (\rho \mathbf{v} \nabla \vec{V}) \quad (17)$$

$$\frac{dn_e}{dt} + n_e \nabla \cdot \vec{V} = \nabla \cdot (D \nabla n_e) + S_{ion/rec} \quad (18)$$

$$\frac{dn_i}{dt} + n_i \nabla \cdot \vec{V} = \nabla \cdot (D \nabla n_i) + S_{ion/3-body} \quad (19)$$

$$\frac{dn_Z}{dt} + n_Z \nabla \cdot \vec{V} = \nabla \cdot (D \nabla n_Z) + S_{ion/rec} \quad (20)$$

$$n_e \frac{dT_e}{dt} = (\gamma - 1) [n_e T_e \nabla \cdot \vec{V} + \nabla \cdot \vec{q}_e - Q_{loss}] \quad (21)$$

$$\vec{q}_e = -n_e [\kappa_{\parallel} \hat{b} \hat{b} + \kappa_{\perp} (\mathcal{I} - \hat{b} \hat{b})] \cdot \nabla T_e \quad (22)$$

$$\vec{E} + \vec{V} \times \vec{B} = \eta \vec{J} \quad (23)$$

Here,  $n_i$ ,  $n_e$ , and  $n_Z$  are the main ion, electron, and impurity ion number density respectively,  $\rho$ ,  $\vec{V}$ ,  $\vec{J}$ , and  $p$  the plasma mass density, velocity, current density, and pressure respectively,  $T_e$  and  $\vec{q}_e$  the electron temperature and heat flux respectively,  $D$ ,  $\mathbf{v}$ ,  $\eta$ , and  $\kappa_{\parallel}(\kappa_{\perp})$  the plasma diffusivity, kinematic viscosity, resistivity, and parallel (perpendicular) thermal conductivity respectively,  $\gamma$  the adiabatic index,  $S_{ion/rec}$  the density source from ionization and recombination,  $S_{ion/3-body}$  also includes contribution from 3-body recombination,  $Q_{loss}$  the energy loss,  $\vec{E}(\vec{B})$  the electric (magnetic) field,  $\hat{b} = \vec{B}/B$ , and  $\mathcal{I}$  the unit dyadic tensor.

All particle species share a single temperature  $T = T_e$  and fluid velocity  $\vec{V}$ , which assumes instant thermal equilibration among the main ions, the impurity ions, and the electrons. Pressure  $p$  and mass density  $\rho$  in momentum equation (17) include contributions from the impurity species. Each charge state of impurity ion density is tracked in the KPRAD module and used to update the source/sink terms in the continuity equations due to ionization and recombination. Both convection and diffusion terms are included in each continuity equations where all the diffusivities are assumed same. Quasi-neutrality is maintained through the condition  $n_e = n_i + \sum Z n_Z$ , where  $Z$  is the charge of impurity ion. The energy loss term  $Q_{loss}$  in equation (21) is calculated from KPRAD module based on a coronal model, which includes contributions from bremsstrahlung, line radiation, ionization, recombination, Ohmic heating, and intrinsic impurity radiation. Anisotropic thermal conductivities are temperature dependent, i.e.  $\kappa_{\parallel} \propto T^{5/2}$  and  $\kappa_{\perp} \propto T^{-1/2}$ . Similarly, the temperature dependence of resistivity  $\eta$  is included through the Spitzer model.

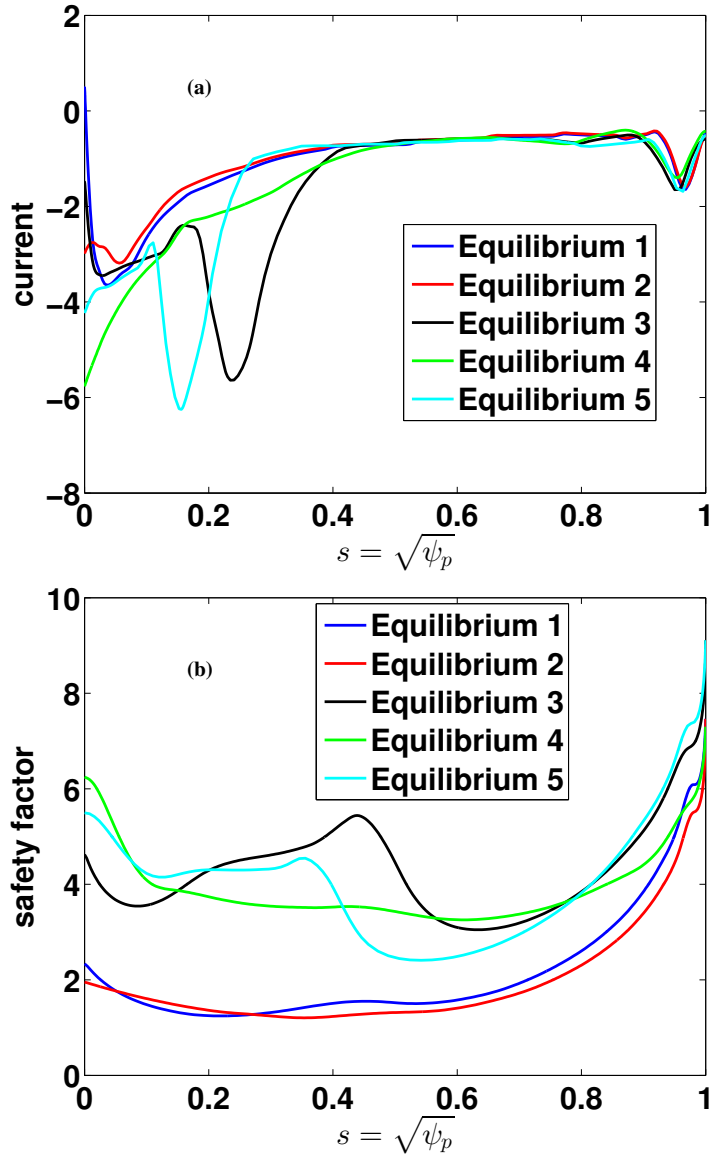
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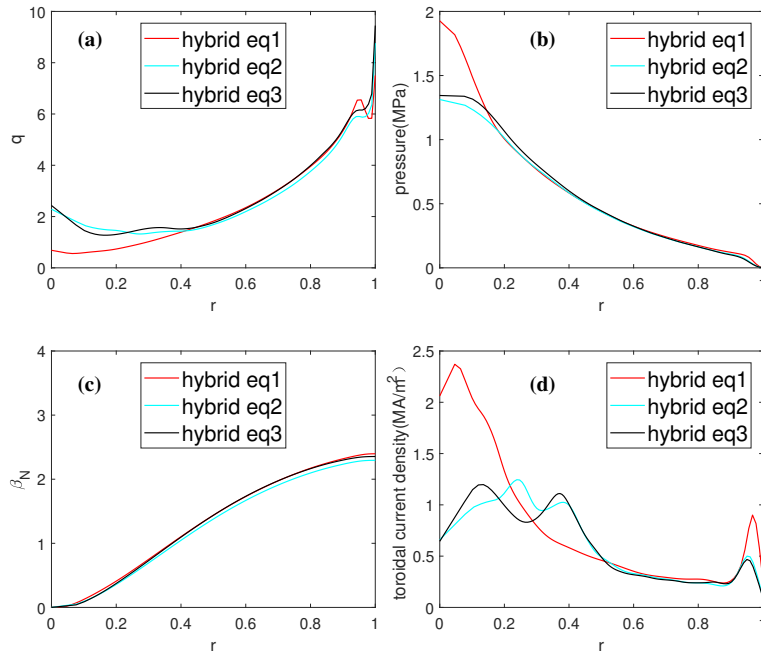
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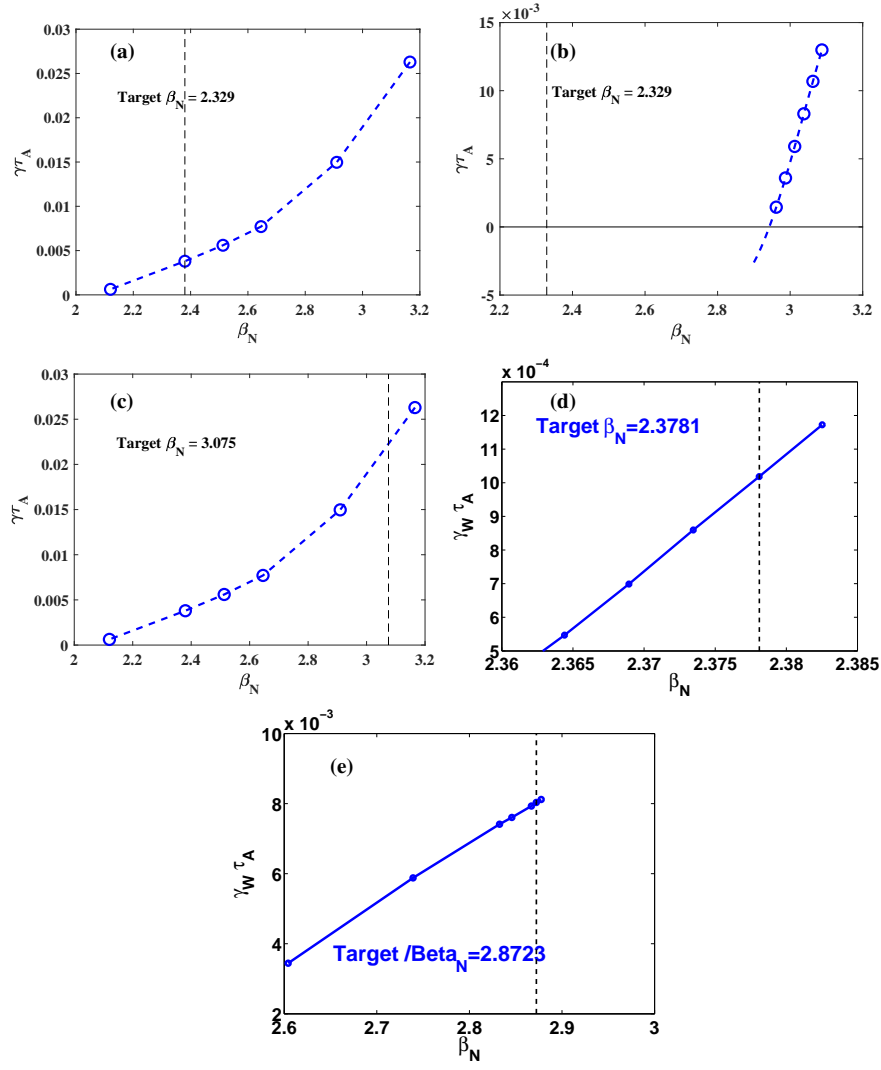
**Fig. 1** (a) Equilibrium plasma current density and (b) safety factor as functions of normalized minor radius in five CFETR steady-state scenarios (Other equilibrium parameters are shown in Table 1).

equilibrium	$R_0$	$B_0$	$a$	$q_{min}$	$q_0$	$q_{95}$	$q_a$	$\beta_N$
1	7.2	6.53	2.2358	1.2443	2.3663	6.0235	7.45	2.3799
2	7.2	6.53	2.1990	1.2049	1.9571	5.4053	7.45	2.3277
3	7.2	6.53	2.2117	3.0493	4.6612	6.8730	9.05	3.0751
4	7.2	6.53	2.1833	3.2566	6.2540	5.7156	7.2912	2.3781
5	7.2	6.53	2.2273	2.4089	5.4913	7.3602	9.0954	2.8720

**Table 1** Summary of key design parameters for the five CFETR SSO scenarios considered in this study.

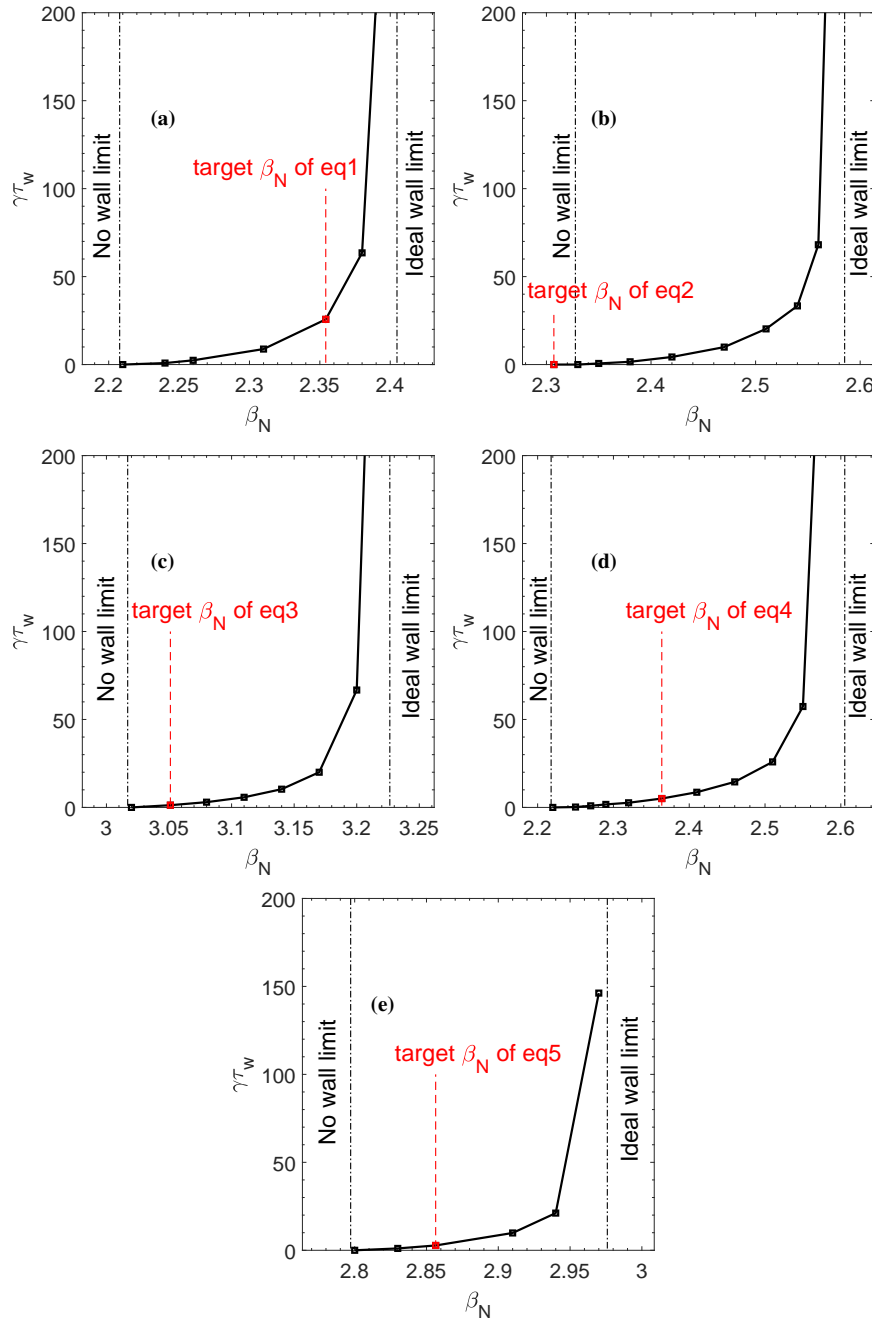


**Fig. 2** (a) Safety factor, (b) plasma pressure, (c) normalized  $\beta$ , and (d) toroidal plasma current density as functions of normalized minor radius for the equilibria of the three CFETR hybrid scenarios considered in this study.

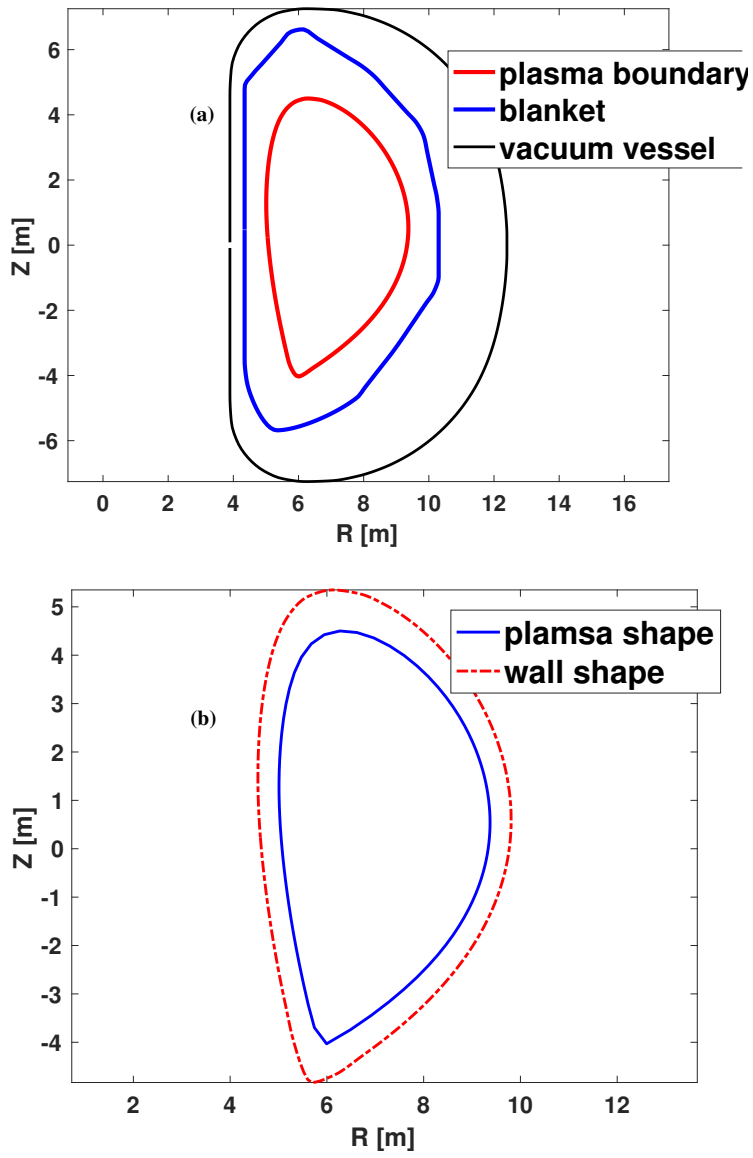


**Fig. 3** (a-e) Growth rates of the ideal MHD mode as functions of the plasma pressure  $\beta_N$  in absence of conducting wall for five different CFETR SSO scenarios from MARS-F calculations, where the vertical lines denote the designed plasma pressure  $\beta_N$  for each corresponding equilibrium.

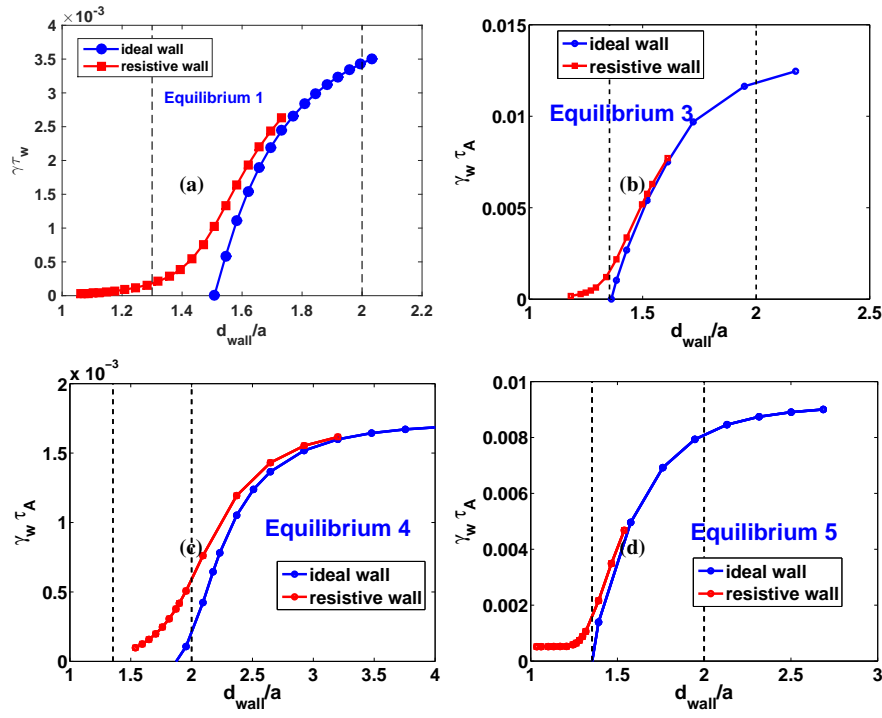




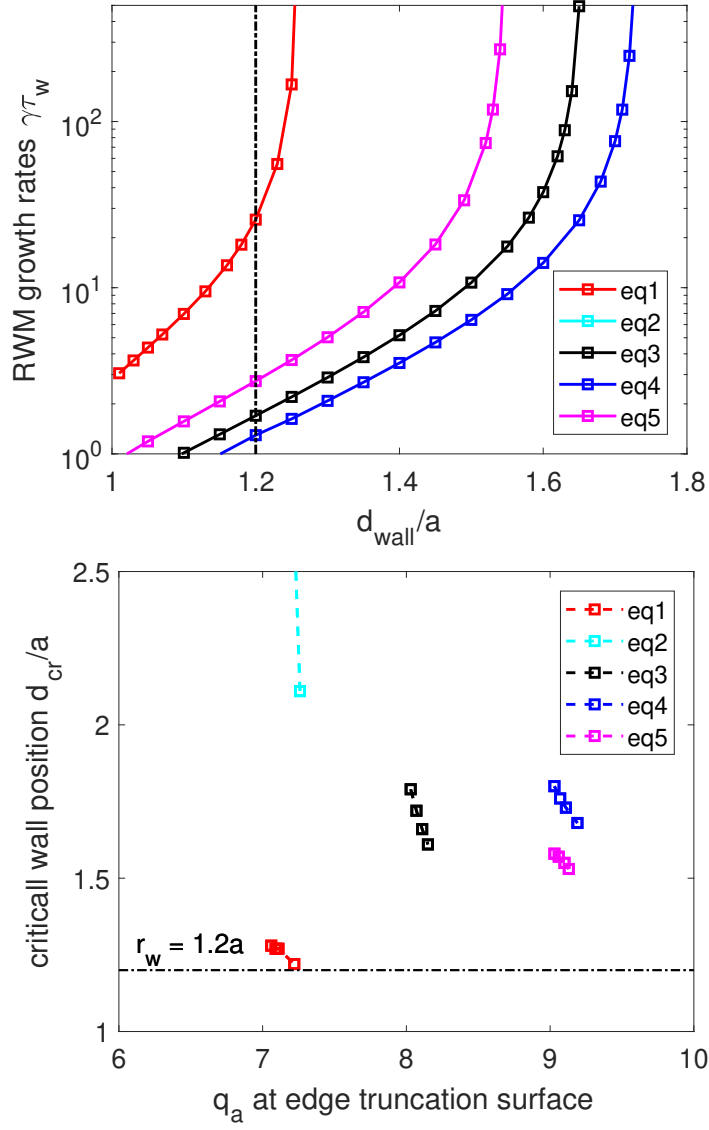
**Fig. 4** (a-e) Growth rates of the ideal MHD mode as functions of the plasma pressure  $\beta_N$  in absence of conducting wall for five different CFETR SSO scenarios from AEGIS calculations, where the vertical red lines denote the designed plasma pressure  $\beta_N$  for each corresponding equilibrium.



**Fig. 5** Two computational models for the designed CFETR wall. (a) Model A includes the plasma boundary (red curve), the blanket (blue curve), and the vacuum vessel (black curve) based on the CFETR engineering design [30]; (b) Model B includes an artificial wall (red dashed curve) conformal to the plasma shape (blue curve).



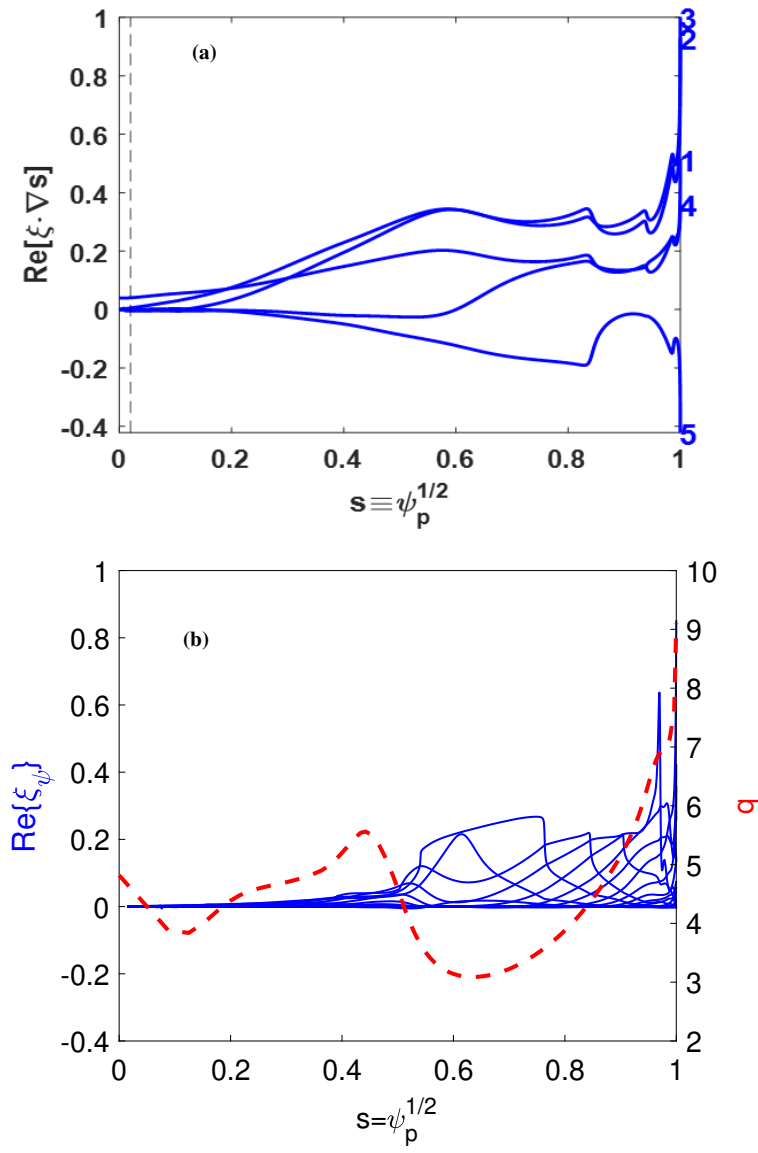
**Fig. 6** Growth rates of the  $n = 1$  ideal MHD modes from MARS-F calculations as functions of the wall minor radius, in presence of an ideal wall (blue curves) or a resistive wall (red curves), where the effective resistive wall time is fixed at  $\tau_w = 10^4 \tau_A$ . Here, the vertical dashed lines denote the minor radius of the TBM and VV designed for CFETR, at  $1.3a$  and  $2.0a$ , respectively.



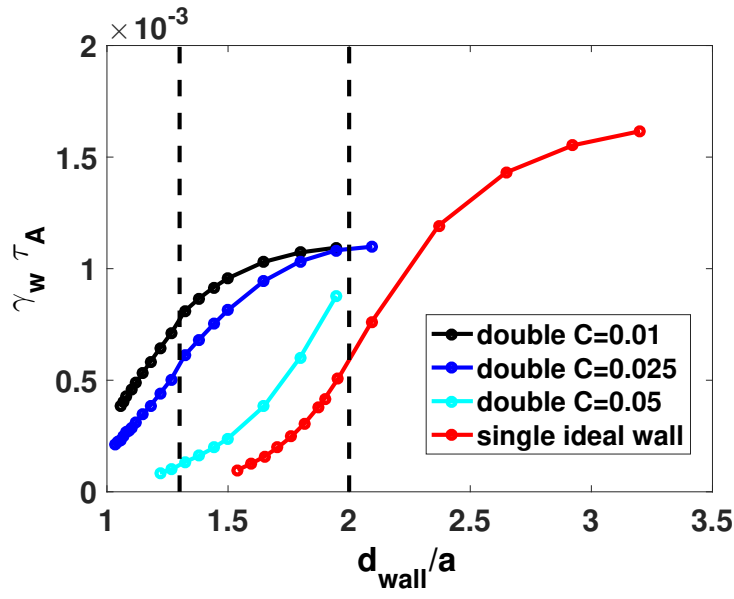
**Fig. 7** (a)  $n = 1$  RWM growth rates as functions of wall minor radius in presence of a conformal thin resistive wall for various CFETR scenarios (where for equilibrium 2, the  $n = 1$  ideal MHD mode is stable, thus no growth rate is shown), and (b) The critical positions of perfect conducting wall where ideal MHD modes turn unstable as functions of the truncation edge safety factor  $q_a$  for various CFETR scenarios from AEGIS calculations.

	eq1	eq2	eq3	eq4	eq5
$\psi$ @ truncated surface	99.40%	99.67%	99.75%	99.70%	99.60%
$q_a$ @ truncated surface	7.1	7.1	8.1	9.1	9.1

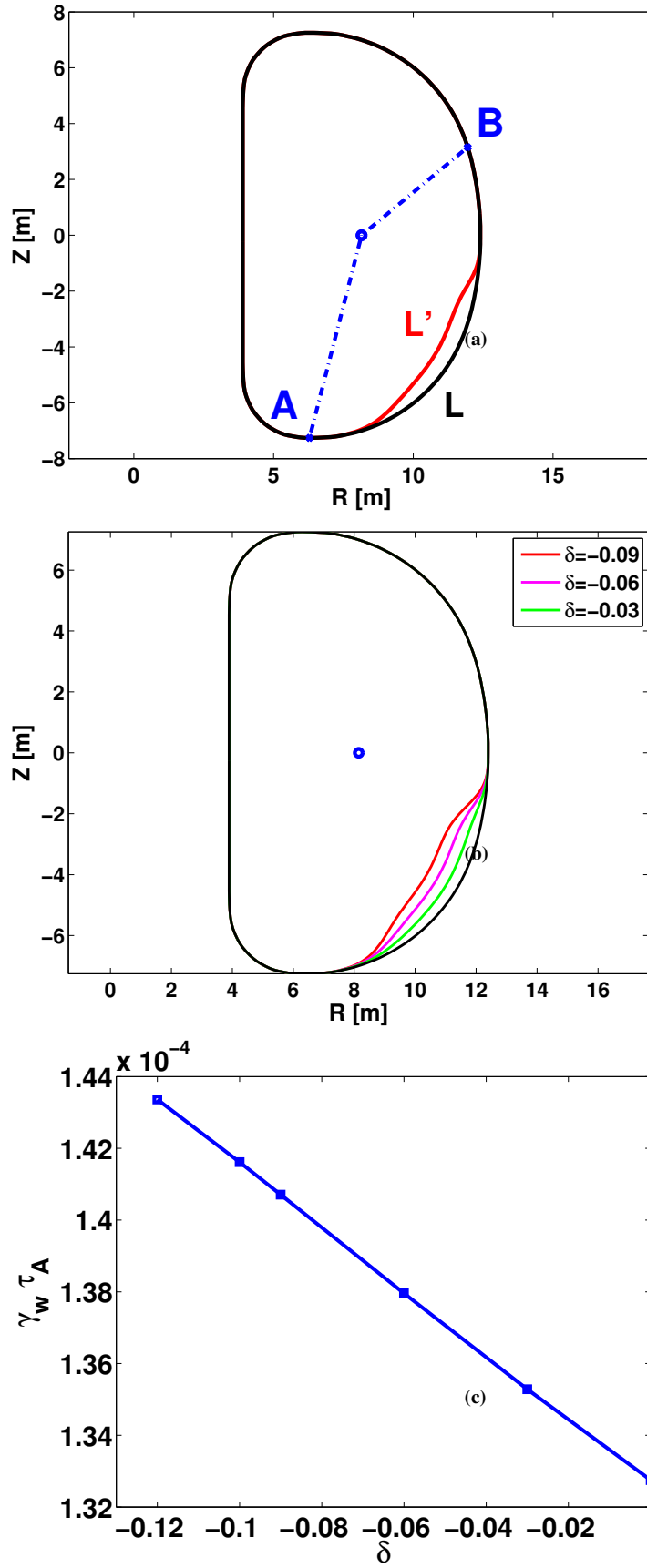
**Table 2** Normalized magnetic flux  $\psi$  and safety factor  $q_a$  at edge truncated surfaces for the equilibria eq1 to eq5.



**Fig. 8** Radial profiles of the real normal component of plasma displacement computed using (a) MARS code (with the geometric configuration shown in Fig. 5(b)), and (b) AEGIS code for equilibrium 4.

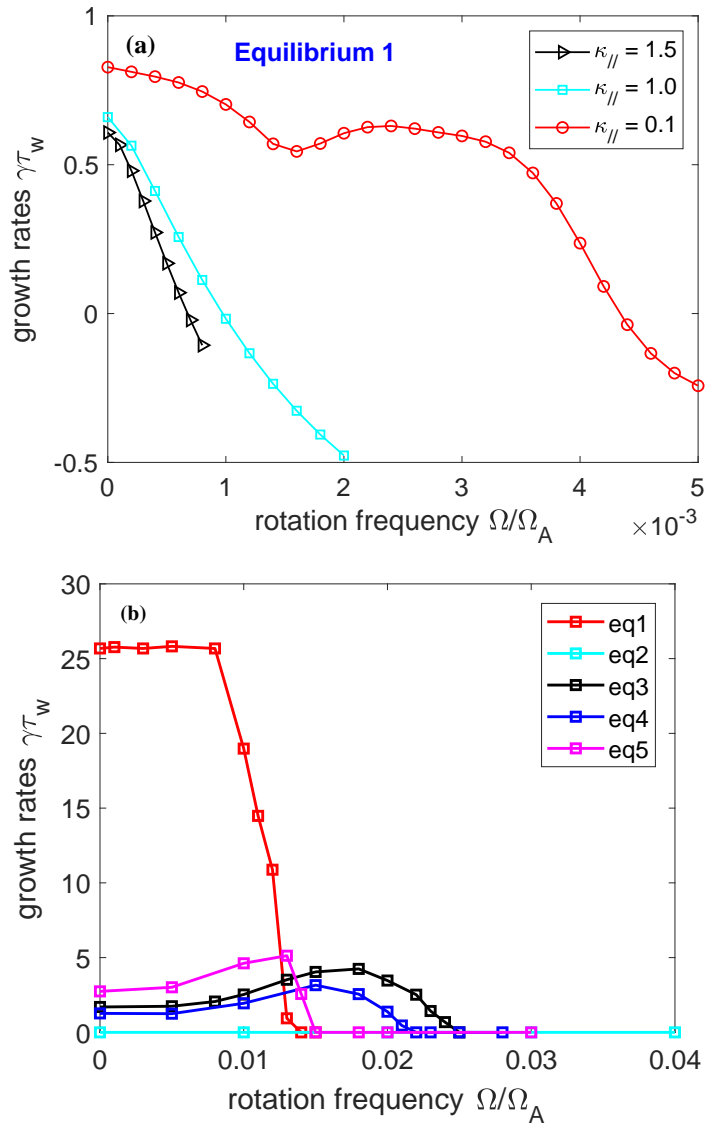


**Fig. 9** Growth rates of  $n = 1$  modes with different ratios of TBM and VV wall time  $C = \tau_{TBM}/\tau_{VV}$  as functions of the wall minor radius, where the VV wall time is fixed at  $\tau_{VV} = 1865.3\text{ms}$ . Here, the vertical dashed lines denote the minor radii of the TBM and VV locations designed for CFETR ( $1.3a$  and  $2.0a$  respectively).

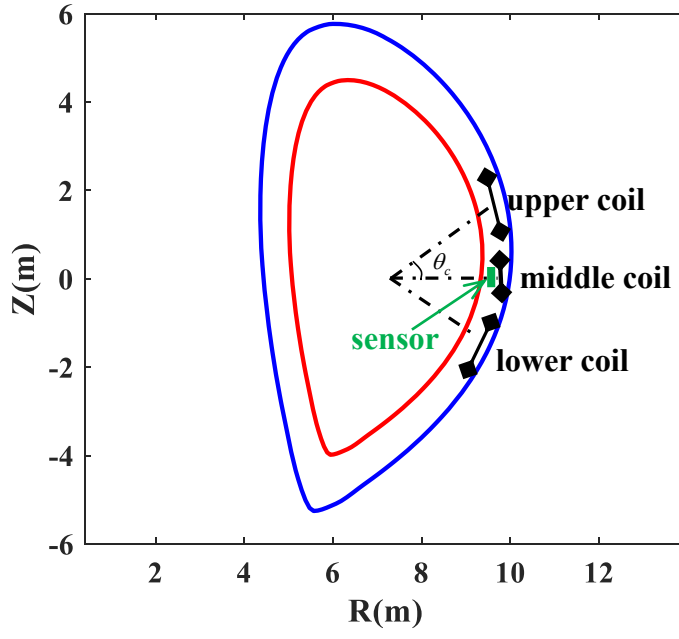


**Fig. 10** (a) A sketch of the modification of the lower low field side quarter of the plasma boundary shape, based on the CFETR design; (b) a family of new VV shape; (c) the RWM growth rate as a function of the shaping parameter  $\delta$ .

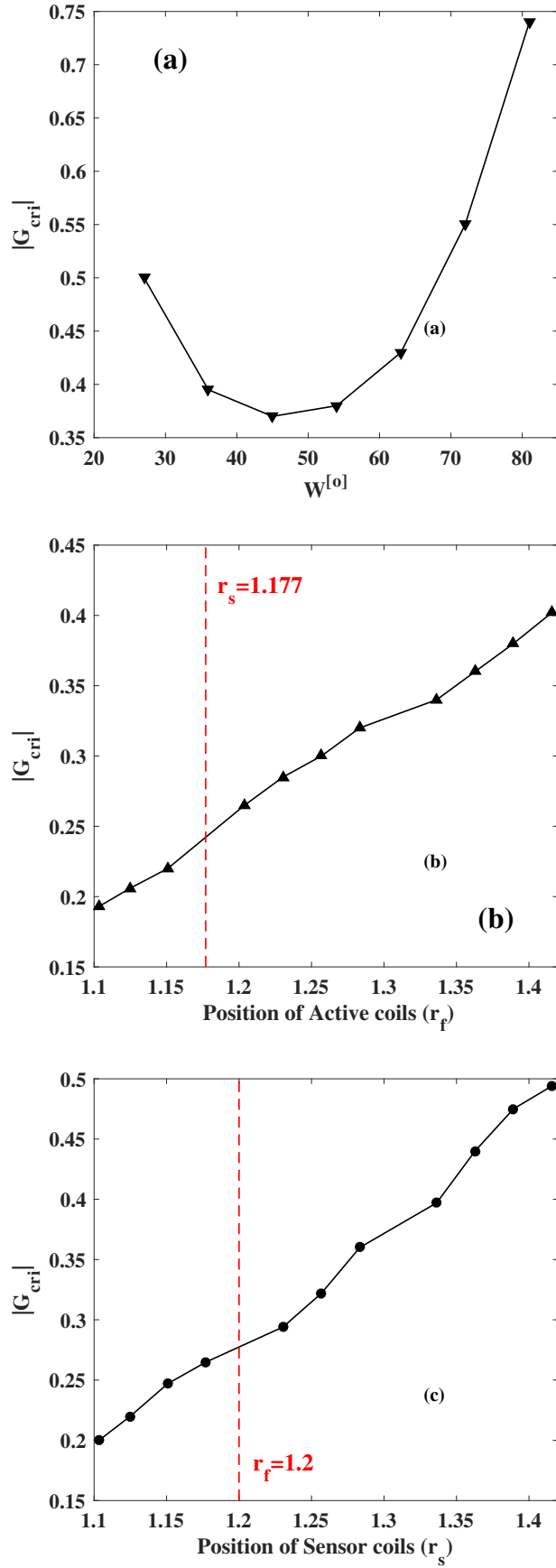




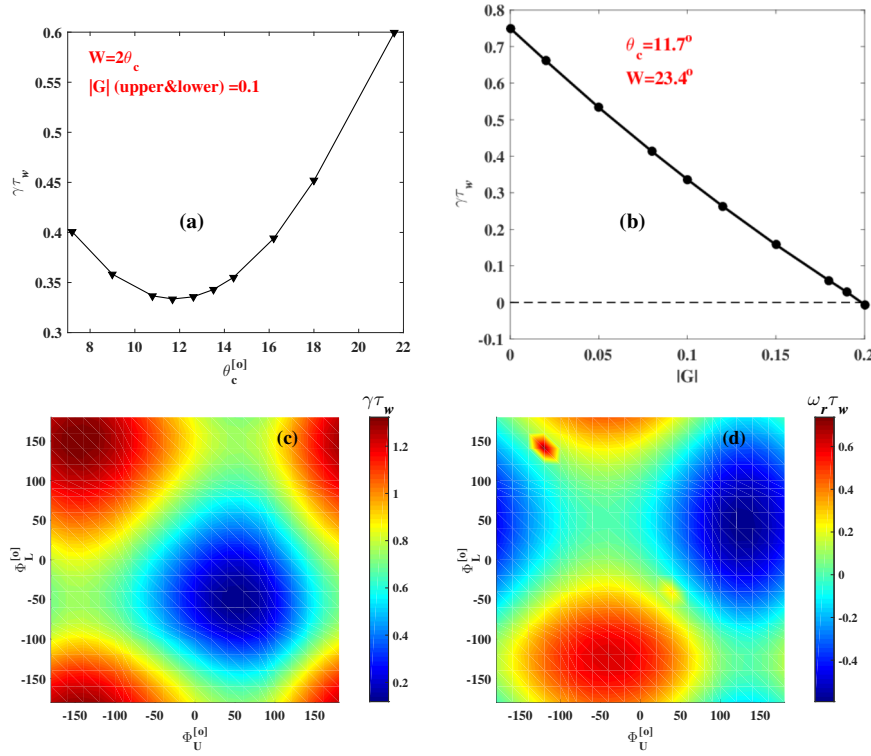
**Fig. 11** RWM growth rates as functions of the uniform toroidal rotation frequency obtained using (a) MARS-F and (b) AEGIS codes, for various values for the damping coefficient,  $\kappa_{||}$ . The rotation frequency is normalized by the Alfvén frequency at the magnetic axis.



**Fig. 12** Geometry of a CFETR configuration including the RWM feedback coils, the plasma boundary, and a single resistive wall ( $r_w = 1.3$  and  $\tau_w = 10^4 \tau_A$ ). Two sets of active coils, referred to as the middle and upper-lower symmetric coils, respectively, are located inside the wall. The sensor coil is located inside the wall, measuring the poloidal field perturbation.



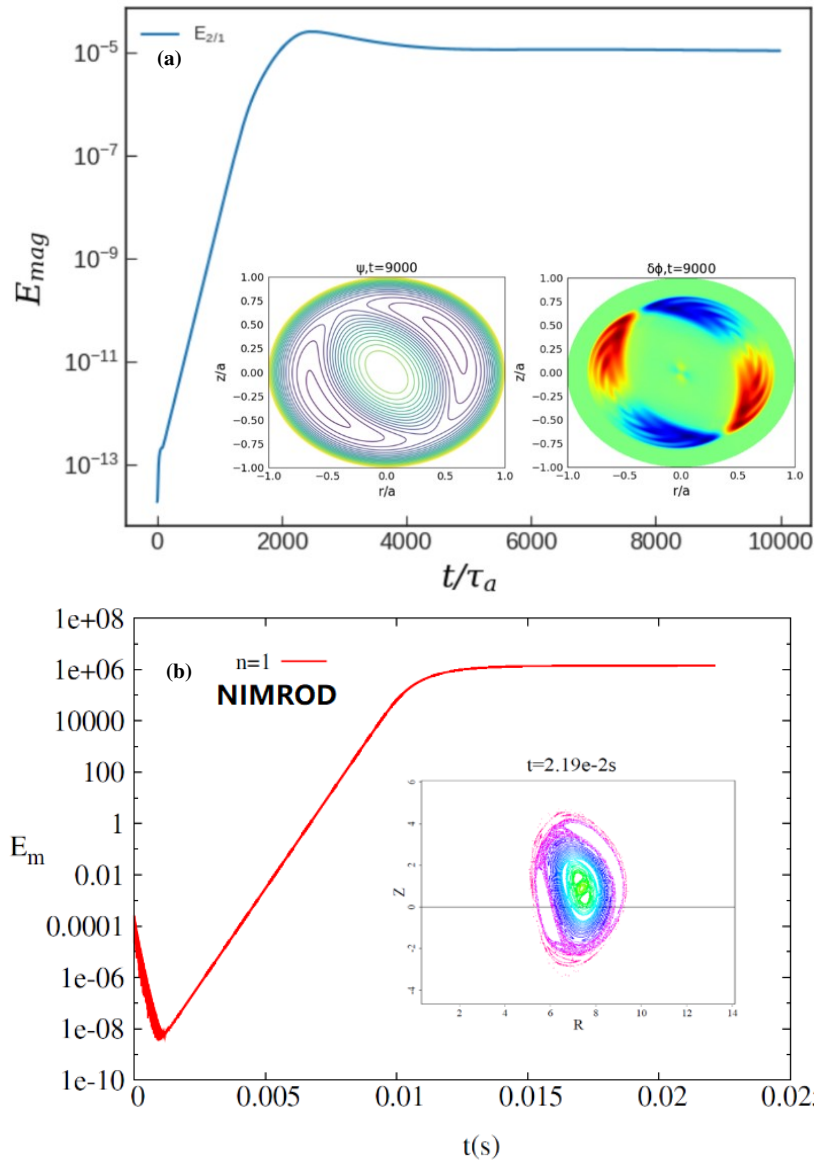
**Fig. 13** (a) The critical gain required for stabilization of the RWM as a function of the poloidal covering width of active coil  $W$  with fixed  $r_f = 1.283$  and  $r_s = 1.257$ . (b) and (c) are the critical gains as functions of the positions of active coils ( $r_f$ ) and sensor coils ( $r_s$ ), respectively, with fixed  $W = 45^\circ$ . The feedback system is assumed to be a set of middle control coils with zero polar angle and zero phase angle.



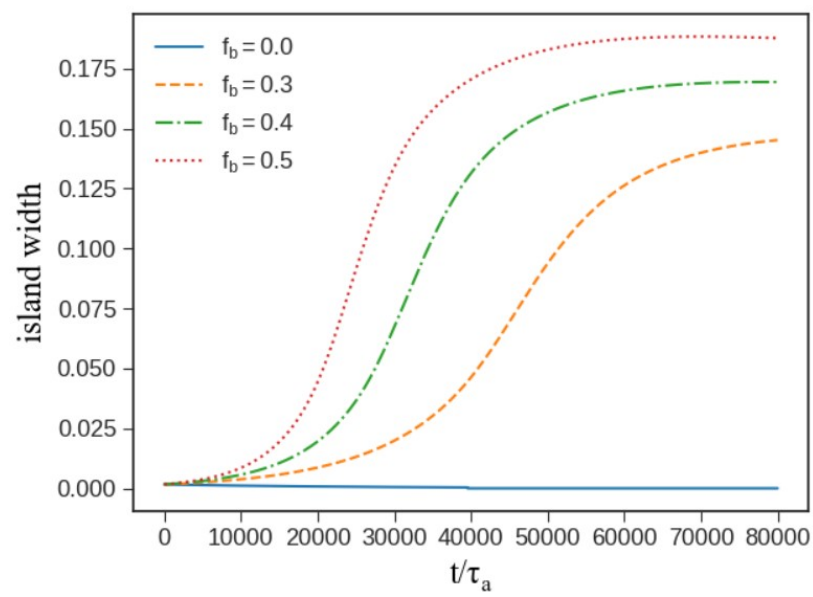
**Fig. 14** (a) Growth rate of RWM as a function of the poloidal location ( $\theta_c$ ) of the upper and lower symmetric active coils with the fixed gain  $|G| = 0.1$  and the poloidal covering width  $W = 2\theta_c$ . The optimal poloidal location is  $\theta_c = 11.7^\circ$ . (b) The growth rate of RWM as a function of the gain with fixed poloidal location. The critical gain is  $|G| = 0.2$  smaller than the middle active coil. Contours of (c) growth rate and (d) real frequency of RWM in the 2D space of the proportional feedback gain phases  $\Psi_U - \Psi_L$ , respectively.

Extrapolation		Physical Regime/Device	scaling(br/BT)	ITER(1e-4/BT)	CFETR(1e-4/BT)
Theory	SOC	visco-resistive	$ne^{(7/12)}BT^{(-7/6)}R0^{(1/2)}f0$	1.20	1.30
		Rutherford	$ne^{(3/5)}BT^{(-6/5)}R0^{(11/15)}f0$	1.61	1.82
		transition	$ne^{(1/2)}BT^{(-1)}R0^{(1/3)}f0^{(4/5)}$	0.91	0.94
		Waelbroeck	$ne^{(7/16)}BT^{(-7/8)}R0^{(1/3)}f0^{(5/8)}$	0.85	0.87
		polarization	$neBT^{(-9/5)}R0^{(-1/4)}$	0.37	0.24
		Sci+NTV	$neBT^{(-13/10)}R0$	3.12	2.94
	LOC	visco-resistive	$BT^{(-7/6)}R0^{(1/2)}f0$	0.35	0.38
		Rutherford	$ne^{(-1/60)}BT^{(-6/5)}R0^{(11/15)}f0$	0.44	0.50
		transition	$BT^{(-1)}R0^{(1/3)}f0^{(4/5)}$	0.32	0.33
		Waelbroeck	$BT^{(-7/8)}R0^{(1/3)}f0^{(5/8)}$	0.34	0.35
		polarization	$neBT^{(-9/5)}R0^{(-1/4)}$	0.37	0.24
		Sci+NTV	$ne^{(1/2)}BT^{(-13/10)}R0$	1.09	1.03
Experiment	EAST		$ne^{(0.55)}BT^{(-1.0)}q95^{(1.66)}f0$	0.62	1.54
	JET-2000		$ne^{(0.58)}BT^{(-1.274)}f0^{(0.5)}$	1.29	1.10
	JET-98		$ne^{(0.97)}BT^{(-1.2)}f0$	2.84	2.76
	COMPASS-C		$ne^{(0.55)}BT^{(-2.2)}f0$	0.19	0.12
	COMPASS-D		$ne^{(1.0)}BT^{(-2.9)}f0$	0.16	0.09
	DIII-D		$ne^{(0.99)}BT^{(-0.96)}f0$	2.02	1.68

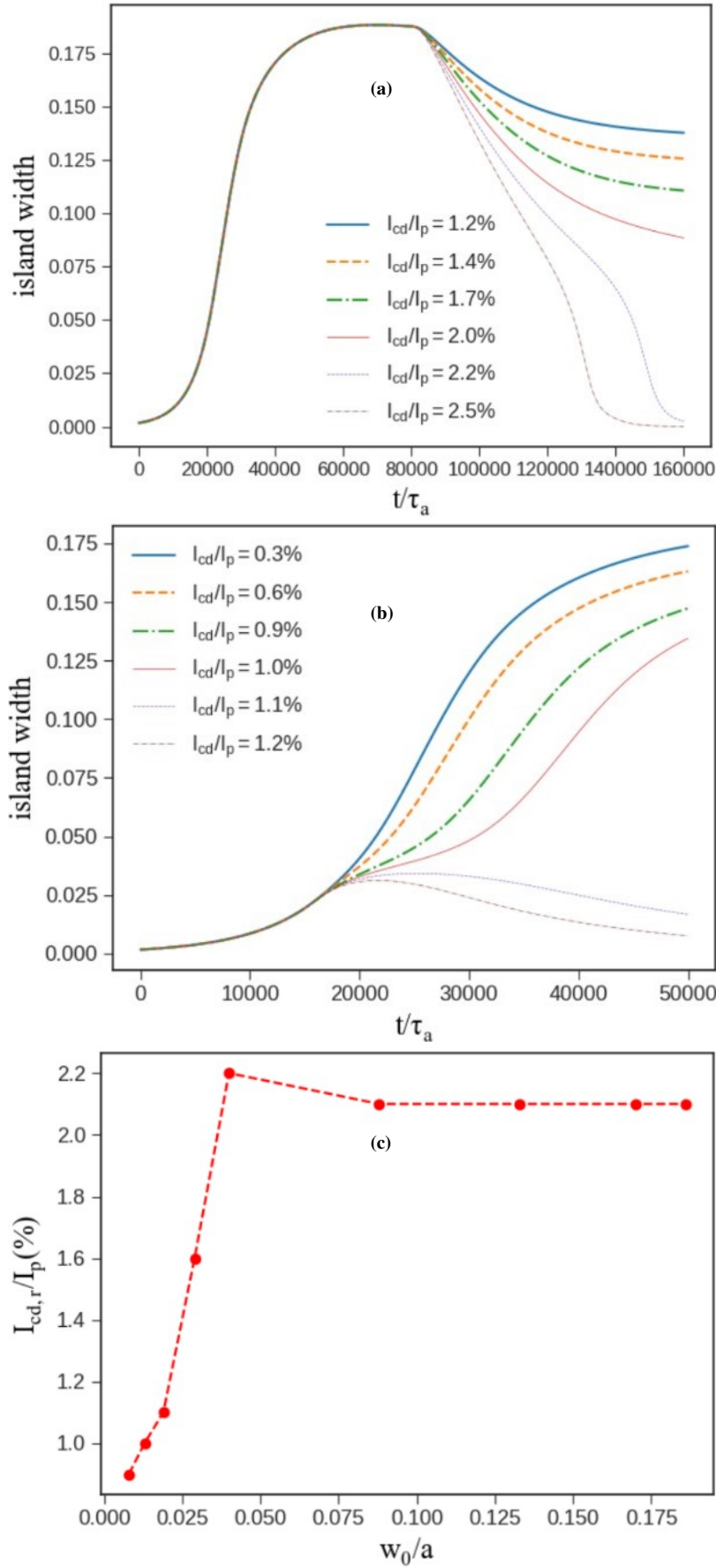
**Table 3** Extrapolation of error field tolerance towards ITER and CFETR using theoretical and experimental scalings. SOC indicates the assumption using saturated Ohmic confinement (energy confinement time independent with electron density, we assumes that the viscous diffusion time approaches to the energy confinement time here), whereas LOC indicates the assumption using linear Ohmic confinement (energy confinement time linear dependent with electron density).



**Fig. 15** (a) Nonlinear evolution of the  $m/n = 2/1$  resistive tearing mode in the hybrid scenario EQ3, together with the corresponding magnetic island and the plasma flow pattern in the saturation phase from the MD simulation. (b) Evolution of  $n = 1$  component of magnetic energy, together with the Poincare plot in the saturation phase from the NIMROD simulation.

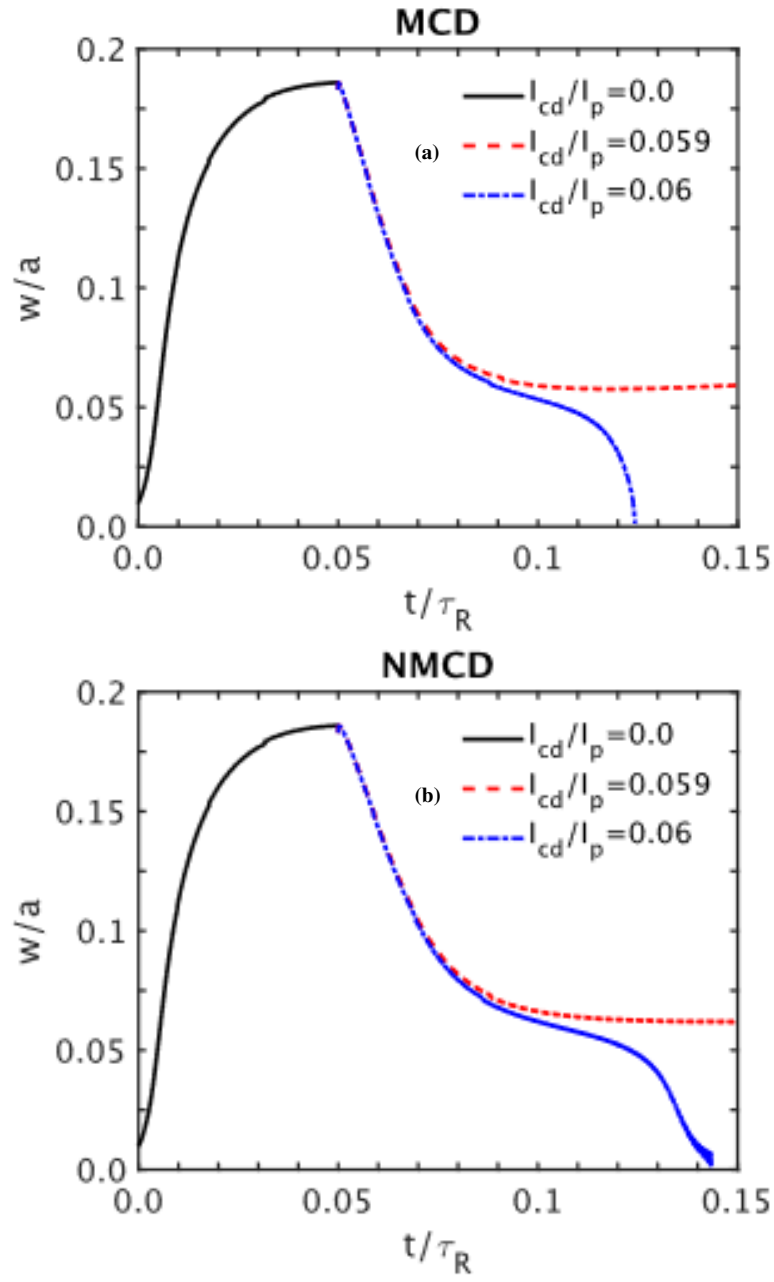


**Fig. 16** Evolution of magnetic island width for various fractions of bootstrap current from the MD simulations.

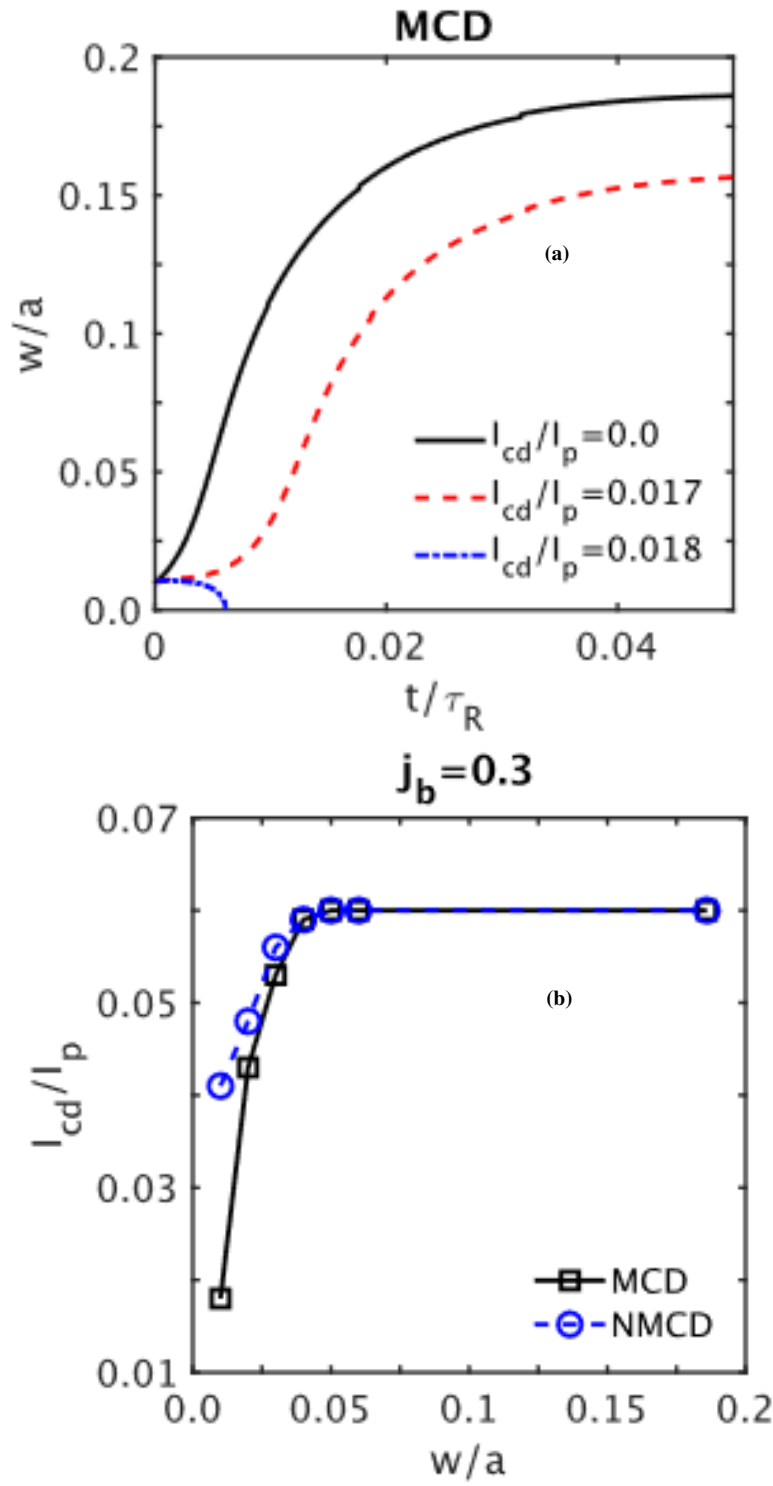


**Fig. 17** Evolution of magnetic island width from the MD simulations for different ECCD amplitudes, with ECCD being turned on at (a)  $t/\tau_a = 80000$  and (b)  $t/\tau_a = 15000$ , respectively. (c) Dependence of the driven current required for the suppression of NTM on the magnetic island width at the time when ECCD is turned on.

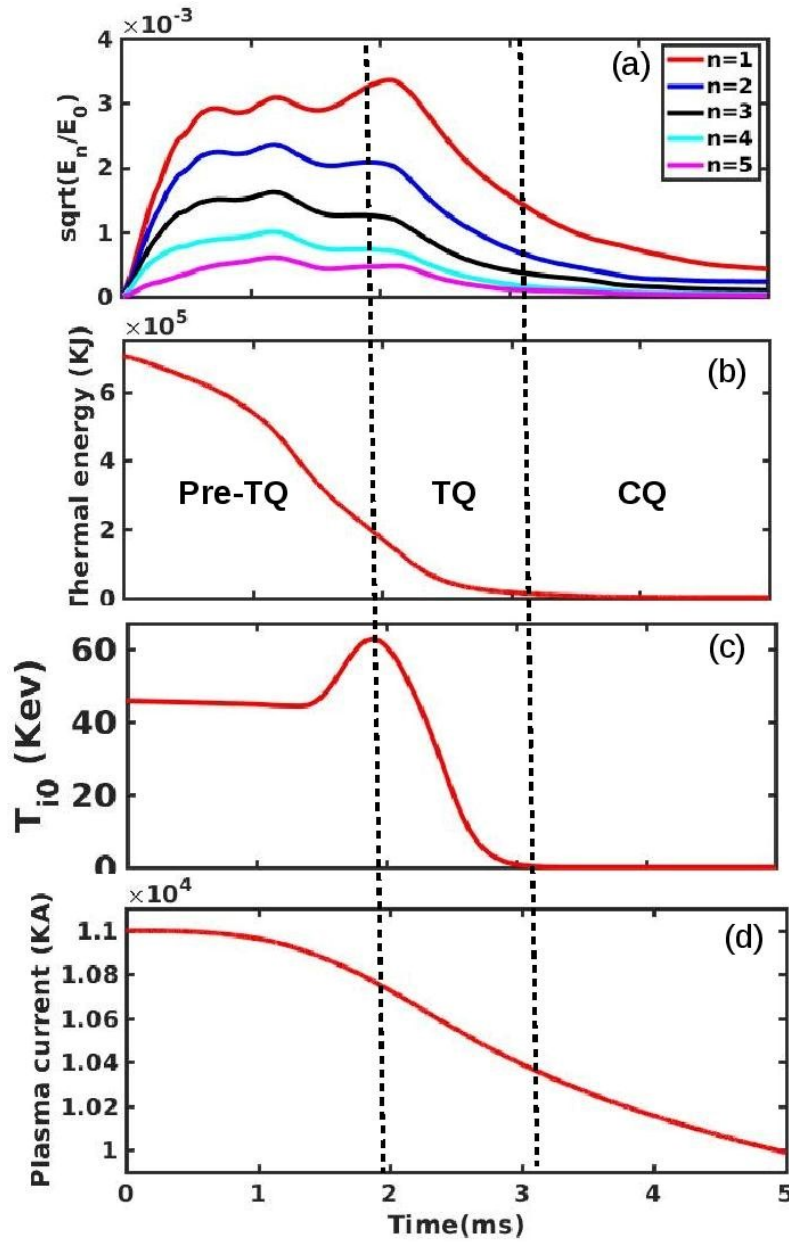




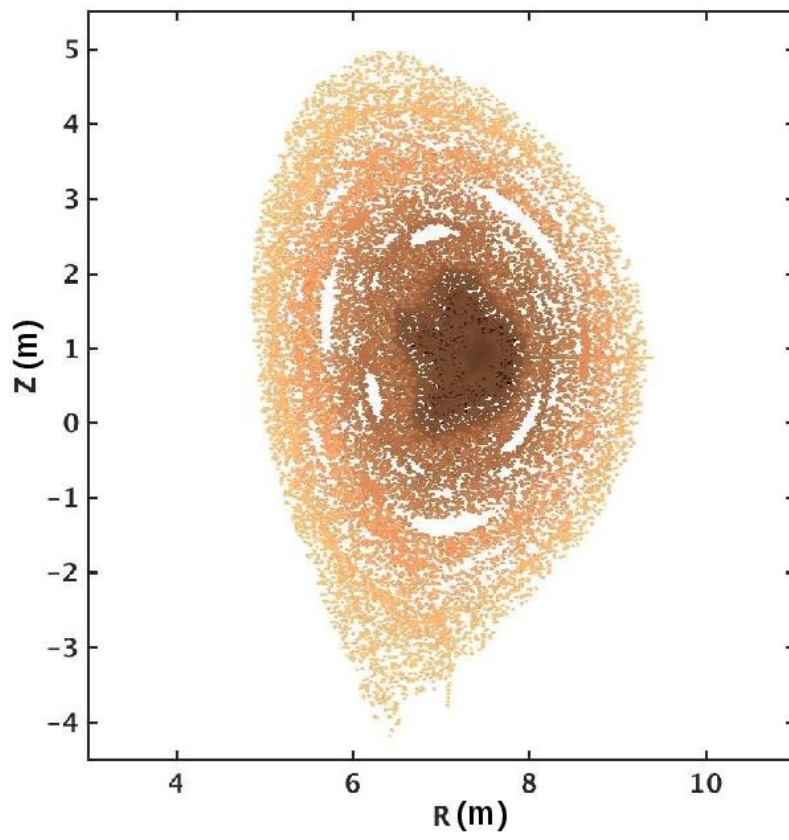
**Fig. 18** Time evolution of the normalized island width  $w/a$  from the TM8 simulations in absence (solid curve) or presence (dashed and dot-dashed curves) of ECCD for (a) MCD and (b) NMCD with  $I_{cd}/I_p = 0.059$  (dashed curve) and 0.06 (dot-dashed curves).



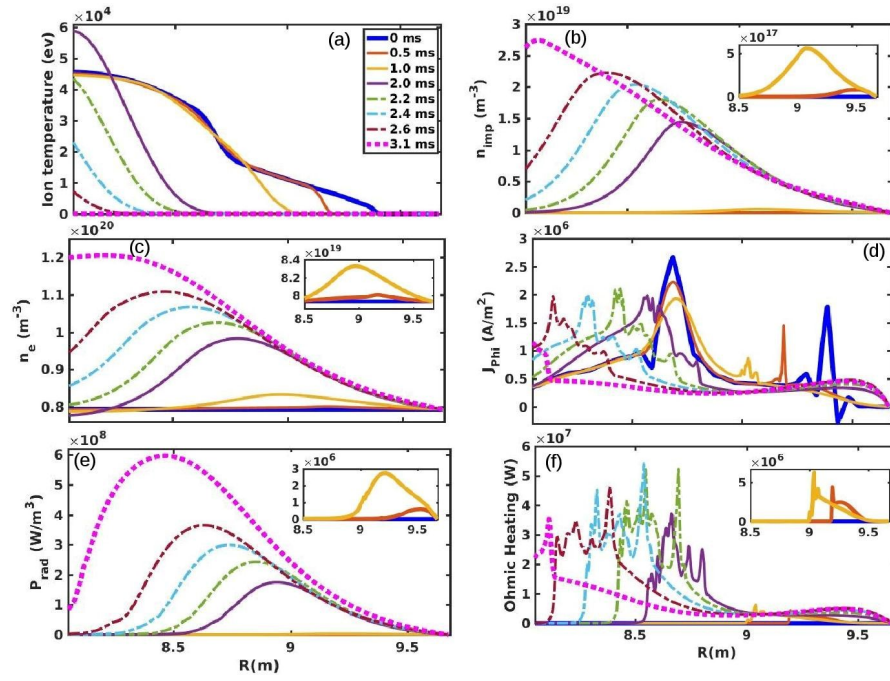
**Fig. 19** (a) Time evolution of the island width from the TM8 simulations in absence (solid curve) or presence (dashed curves) of ECCD. MCD is turned on when the island width  $w = 0.01a$  is reached, with  $I_{cd}/I_p = 0.017$  (dashed curve) and 0.018 (dot-dashed curve). (b) The required  $I_{cd}/I_p$  for mode stabilization as a function of the normalized island width. The solid (dashed) curve is for MCD (NMCD).



**Fig. 20** Time evolution of (a) normalized magnetic energy of each primary toroidal component (in unit  $(W_{mag,n}/W_{mag,0})^{1/2}$ ), (b) plasma thermal energy (kJ), (c) core temperature (keV), and (d) plasma current (kA) during an MGI process from a NIMROD simulation.



**Fig. 21** Poincare plot at the end of the TQ during an MGI process from a NIMROD simulation.



**Fig. 22** Profile evolution of (a) ion temperature, (b) impurity number density, (c) electron density, (d) toroidal current density, (e) radiated power density, and (f) Ohmic heating power during an MGI process from a NIMROD simulation.