Pre-conceptual design of the port cell section for the EU DEMO equatorial EC system

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Abstract— The EU DEMO Tokamak will be equipped with an Electron Cyclotron system for plasma heating and magnetohydrodynamic control. Up to six launchers will be installed into equatorial ports with the aim to inject maximum 130 MW millimeter wave power at dedicated positions into the plasma. The mm-waves will be generated in gyrotrons placed in a distinct building at distant location. From this gyrotron hall, a combined transmission line system of quasi-optical multi-beam mirrors and individual waveguides will propagate the mmwaves into the tokamak building. That followed, an optical system, composed of mitre-bends, diamond windows, valves, and microwave bellows, connects the transmission line through the gallery and the port cell with the EC launchers. This paper presents the pre-conceptual CAD design of this latter section of the EC system. Based on its general scheme and the given waveguide trajectories, the model takes into account the available space in the port cell with respect to required clearance for supply systems, assembly and maintenance. At the pre-conceptual state, the design includes CAD models of all relevant millimeter wave components in realistic dimensions at a level of details, appropriate to demonstrate the feasibility of the concept.

Keywords— DEMO, ECRH, Port Plug, Heating and Current Drive, MHD control, CAD

I. INTRODUCTION

For the EU DEMO tokamak, electron cyclotron (EC) heating, systems for launching plasma (MHD) Magnetohydrodynamic control and instability suppression are under development. Since during the pre-conceptual design phase no plasma scenario has been finally qualified for DEMO, the pre-conceptual design study of the EU DEMO equatorial EC system is carried out on the basis of the 2017 engineering baseline, the 2018 physics baseline, and the blanket separated design (BSD) approach. In figure 1 an overview of the EU DEMO pre-conceptual design with its main systems is given [1], [2].

Up to six of these launching systems will be installed into equatorial ports with the aim to inject a delivered radio frequency (RF) power of maximum 130 MW at frequencies of 170 GHz and/or 136 GHz/204 GHz [1].

The reference design study of the EC launchers features the concept of MHD control (mainly Neo-classical Tearing Modes – NTM) by two mid steering antennas (MSAs) [3] with a partially quasi-optical beam layout and steerable mirrors at a recessed position behind the outboard breeding blanket (BB) segments. These antennas consist of three

beamlines each and are installed into the upper and the lower area of the equatorial ports. The upper antenna targets the q=3/2 surface and the lower antenna targets the q=2 surface for power deposition in the plasma.

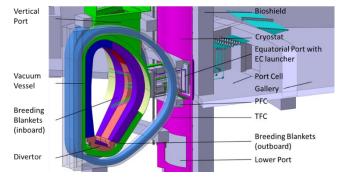


Fig. 1. Overview of the EU DEMO EC system integration

For plasma heating purposes an open-ended waveguide concept with 2×8 beamlines and a set of two times two fixed mirrors is designed. The plasma heating system is arranged by two bundles, staggered in poloidally symmetric positions with respect to the toroidal DEMO reference plane (tokamak mid-plane) in the center area of the port. In figure 2 an outline of the EC launcher optical system is given.

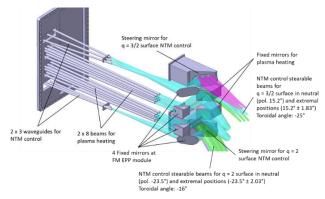


Fig. 2. Pre-conceptual design of the optical system of the EC launcher.

The millimetre wave power will be generated outside the Tokamak building in gyrotrons in a dedicated RF (radio frequency) building. From there it will be transmitted into the EC launching system by transmission lines (TLs), guided through the assembly hall into the gallery and afterwards into the port cell of the Tokamak building.

The current reference TL configuration for the confinement system features two-frequency gyrotrons as RF sources. In a dedicated area in the assembly hall, for each EC system port, 2 clusters of 9 beams each, coming from two space-saving multi-beam transmission lines (MBTL) are split in single-beam TLs and continue their paths through evacuated waveguides (WGs) up to the launcher [1]. In the port cell an isolation valve and a diamond window separate the tokamak vacuum from the TL vacuum. This is also the confinement barrier to prevent any release from Tritium to the outside. The CAD model of the EC port cell section comprises the TLs from the rear side of the port (i.e. the first confinement system's structural barrier) up to the SIC-2 valve between the gallery and the assembly hall.

To set up the CAD model of the EC port cell section, CAD data for the Tokamak building, the TL trajectories (constraining skeletons) and the EC launcher system were prepared and integrated into a CAD assembly. Then the required components of the TL system were created and constrained with the geometry skeletons. The microwave components of which the TL system is made of, are sketched in CATIA as dummies with realistic dimensions on a preconceptual level only in order to demonstrate the feasibility of the concept, regarding space constraints, installation and maintenance.

II. EC PORT CELL TRANSMISSION LINE PRE-CONCEPTUAL DESIGN

Hereinafter the work carried out in 2021 on the port cell section of the equatorial EU DEMO EC system is described in detail. For a first overview, figure 3 shows the preconceptual EC system port cell TL CAD model at a glance.

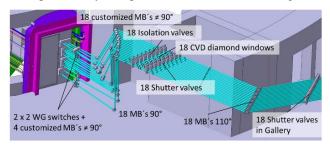


Fig. 3. Pre-conceptual layout of the transmission lines of the EC system in port cell #10.

A. Input data

The pre-conceptual design of the EU DEMO EC launcher is carried out through several work packages and dedicated tasks, which are assigned to specialized European design groups. For integral systems as the EC port cell system it is essential to define interfaces properly and to integrate design studies from different tasks coherently. To set up the CAD model of the EC port cell section, the following input data were collected from associated partners:

- TL routing with beam trajectories.
- · Tokamak building with bioshield
- EC launcher integration model.

B. Port allocation

The current EU DEMO tokamak layout features 16 ports of each type (upper, equatorial, lower ports) in different

levels. They are arranged equally with an angle of 22.5° around the vertical axis of the central Tokamak CS. For the EC systems location, equatorial ports in the Tokamak building level L1 are defined. Two potential arrangements are sketched: One with EC, IC and NBI heating systems (not discussed in this paper) and a second one with EC only. The latter is currently chosen to be the preferred one.

The input data CAD models of the TL trajectories are created with their radial extension aligned to the CATIA xz-plane of the TGCS (Tokamak Global Coordinate System), which is, simply said, the CAD design reference plane agreed for all DEMO components.

For setting up a suitable CATIA assembly for the EC port cell system it is necessary to arrange the input data relative to the dedicated positions. This has been made for the EC system WG trajectories in ports #10, #12 and #14, according to the reference layout. The positioning of the three WG trajectories components was achieved by angular constraining around the z-axis of the TGCS:

Port #10: -146.25°
Port #12: -101.25°

• Port #14: -56.25°

The 3D components of the CAD assembly of the port cell EC system then are constrained to the dedicated port skeleton (i.e. WG trajectories).

C. Tokamak Building integration

The relevant components of the Tokamak building are integrated into the CAD model in order to analyse interfaces and potential collisions between the building and EC system components on a preliminary basis. The EC port is located at the equatorial port level (i.e. level L1) of the tokamak building.

It must be mentioned, that further integration with Remote Maintenance (RM) is expected to add new requirements, e.g. since the transfer cask will require further clearance (if this concept is chosen) of up to 300 mm between the outer edges of components and all building elements affected. Figure 4 shows the EC port cell system integrated into the port #10 building structure. The floor of L2 (i.e. the ceiling of L1) is not shown in the picture.

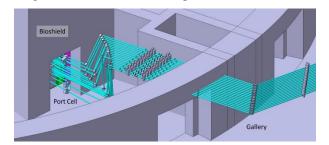


Fig. 4. Port #10 EC system building integration (floor L2 in no-show mode).

III. OPTICAL SYSTEM LAYOUT

For the optical system several concepts have been investigated [1] and a preferred configuration with the splitting mirror (see green box in figure 5) in the assembly hall has been chosen. The schematic layout is shown in

figure 5. It features the SIC-1 isolation valve between the EC port and the diamond window and a SIC-2 shutter valve between the window and the rear sided port cell wall. Another SIC-2 shutter valve is installed behind the port cell wall inside the gallery. All sections between the particular valves are equipped with vacuum service components. The valves allow the enclosure of dedicated sections of the TLs in case of failure of the window or during maintenance.

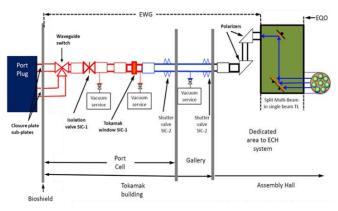


Fig. 5. Transmission line scheme (reference configuration).

 2×3 TLs are connected with the MHD control antennas and 2×8 TLs provide MW power to the plasma heating antennas. Since 18 TLs are installed into the port cell, four of them can switch the provided power between the MHD antennas and the plasma heating antennas by WG switches. Numbering the TLs from 1 to 18 from right to left, the TLs are connected to the antennas as follows:

TL 2 – 5, 7, 8: Upper plasma heating antenna
 TL 6, 9: Upper MHD control antenna / upper plasma heating antenna
 TL 10: Lower MHD control antenna
 TL 11 – 14, 16, 17: Lower plasma heating antenna
 TL 15, 18: Lower MHD control antenna / lower plasma heating antenna

Upper MHD control antenna

IV. OPTICAL SYSTEM DUMMIES

TL 1:

In order to set up a CAD assembly of the EC port cell section, the relevant components must be known and available in CAD. The detailed design of these components (i.e. valves, WGs, diamond windows, etc.) is complex and thus not included in the pre-conceptual design phase. Nevertheless, a CAD model with the potential to evaluate the feasibility of the pre-conceptual design requires such components at least on a level which mimics their typical dimensions. Thus, for the relevant ones, 3D CAD dummies were created on the basis of comparable components, designed for ITER. The WG inner diameter of the ITER components, from which the dummies are basically derived, is 50 mm. Thus, for the dimensions of potential DEMO components with an inner diameter of 63.5 mm, an increase of the dimensions by a factor of 63.5 / 50 = 1.27 would be logic. However, this was not made yet, since also technical innovations might allow a more compact design of the DEMO port cell components.

A. Waveguides

The WGs for the EC system TLs are expected to be actively cooled. This can be achieved by machined cooling channels in the WG structure or alternatively by heat conduction towards rigidly attached cooling sleeves or cooling stripes attached to the outer surface of the WGs. The consequence of such a design is a moderate increase of the diameter of the WGs and also of the joint flanges. For the preconceptual CAD model of the port cell TLs, detailed cooling design was not part of the task but the main dimensions of the WG dummies were derived from the ones, designed for ITER. The standard WG length was chosen to be 4,200 mm, the inner diameter is 63.5 mm (2.5 inches). The outer diameter of the WGs is 75 mm and the diameter of the joint flanges is 120 mm.

There are standardized WGs with a length of 500 mm as well which connect the optical components (diamond windows, valves) in the port cell, but apart from that all other WGs are of individual length due to the non-symmetric layouts. This is why the length of the WG was parameterized in the CATIA specification tree in order to adjust the length particularly for the required dimension. The length ranges from 220 mm up to 5,722 mm. Especially for the longer ones (>4,200 mm), the acceptance of WGs of such length requires further check regarding material choice, manufacturing, mechanical properties, cooling aspects and handling.

The flanges of the WG joints are subject to an integration of double metallic seals (DMS), alignment rims and suitable bolt holes for stable and precise assembly to each other. An alternative joining solution is supposed to be realized with welded seals to ensure optimum tightness of the joints. However, none of the features mentioned above were designed in detail at the pre-conceptual level of the EC system.

B. Mitre-bends

The trajectories of the TLs in the port cell and the gallery are sharply bent several times. For the pre-conceptual design, the technical implementation of these sharp bents is considered to be realized by mitre-bends. Such mitre-bends are used in the EC TLs in ITER and they are designed by SPC [4] for the ITER port cell section and by the US ITER Project Office (USIPO) for the gallery and assembly hall sections. Based on the main dimensions of the SPC design, mitrebends are modelled for the EU DEMO EC system as preconceptual dummies (cf. figure 6, left side).

The mitre-bends have typical dimension of ca. 200 x 200 mm² along the direction of the trajectories and a width of ca. 140 mm. The flanges for WG-attachment have a diameter of 120 mm. The angle between the WG channels is 110° for the set of mitre-bends in the gallery (in between the shutter valves) and is 90° for the set of mitre-bends connecting the quasi-vertical section of WGs and the WGs heading towards the closure plate. For the remaining mitrebends the angle between the WG channels is individual. It is currently between 86° and 99° and can be adjusted in the CAD model by changing the angular parameter in the driving geometry. No cooling channels, joints or connectors are included in the dummy models, since so far they serve as placeholders in the TL layout only.

C. Windows

Millimeter waves must be injected into the Tokamak vacuum chamber with minimum loss of power, which is why a dielectric component shall separate mechanically the WGs in the port cell from the ones in the evacuated torus, where the fusion reaction is taking place. Diamond offers optimum dielectric and thermal characteristics, which is why an artificial variant of Diamond (created by Chemical Vapour Deposition (CVD)) is used as confinement barrier, providing excellent properties for low-loss transmission of electromagnetic waves.

KIT has designed the CVD diamond windows for ITER with an internal WG passage of 50 mm diameter, operating at a frequency of the millimetre waves of 170 GHz at maximum power of 1.3 MW [5]. For DEMO two types of CVD diamond windows are considered: First the fixed frequency ITER-like windows with the diamond disc installed perpendicular to the EC waves with a slightly larger inner diameter of 63.5 mm. Secondly, the so called Brewsterangle broadband windows which are needed for the frequency step-tunable EC system. For the latter a much larger disk diameter is required to achieve the 67.2° brewster angle, creating an elliptical CVD diamond barrier, which is necessary to allow broadband transmission of frequencies around 170 GHz as foreseen in the system variant in which frequency-steering is used for NTM stabilization using steptunable gyrotrons [6]. At the present stage of the design no final decision on the type of window that will be used for the DEMO EC system has been made. Thus, for the setup of the EC system port cell model a dummy of an ITER-like CVD diamond window has been created because no conceptual design of a brewster window is available so far. This dummy allows the illustration of the concept and the evaluation of space constraints regarding installation and maintenance of the window independently from its type, since both variants of diamond windows are expected to be related in diameter and the different length is not an issue for integration of the window into the TL.

The dummy model of the window has a length of 160 mm, a diameter of 115 mm for the window housing and of 120 mm for the joint flanges. The model is shown at the right side of figure 6 below.

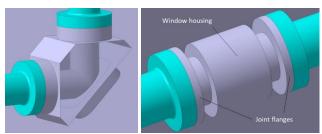


Fig. 6. Dummy CAD models of TL Mitre-bends (left) and CVD diamond window (right)

D. Waveguide switches

The millimetre wave power for NTM-control as well as for plasma heating by EC is generated in gyrotrons in the RF building and then transmitted through 18 TLs per port. Twelve TLs are used for plasma heating and two TLs serve for MHD control exclusively. The remaining four TLs are equipped with WG switches which are installed into the

straight WG sections nearest to the closure plate. These switches allow to apply the beam power either to plasma heating WGs or towards MHD control WGs.

Currently no EU DEMO WG switches are available as CAD models, thus the concept of these WG switches is derived from the ITER TL switches [7], designed by ITER-US for switching EC power between the upper and the equatorial launchers in ITER.

Based on this type of WG switch, corresponding dummies for the DEMO EC system port cell layout were modelled in CATIA. The WG diameter is chosen to 63.5 mm and the outer dimensions are 350 mm x 250 mm x 200 mm. Apart from the WG passages no internals are designed. An illustration of the WG switch dummy is given on the left side in figure 7 below.

E. Isolation- and Shutter valves

The schematic optical system layout indicates three valves in the EC TL, of which one is a shutter valve of safety class 1 (SIC-1) and two more are isolation valves with safety class 2 (SIC-2). They can provide confinement barriers in case of failure of a component (e.g. an unlikely crack of a diamond window and resulting leakages) or they can separate the TL sections for maintenance of the system.

Based on the preliminary design of the ITER EC shutter valves [8], CAD dummies were created for the model of the DEMO EC port cell TLs. The typical dimension of the ITER valve is 467 x 230 x 150 mm³. The dummy model has typical dimensions of 470 x 230 x 100 mm³. The lower radial extension was chosen since the flange joints were not modelled for the DEMO valve dummy, as the radial extension of the valve is uncritical for feasibility checks. The dummies are used for both, SIC-1 and SIC-2 valves in the port cell system assembly (cf. figure 7, right)

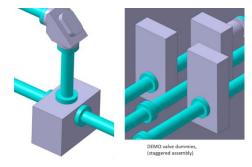


Fig. 7. Dummy CAD models of WG switch (left) and shutter / isolation valves (right)

F. Waveguide feed-throughs

In total 2 x 3 WGs for NTM – control and 2 x 8 WGs for plasma heating have to be guided through the closure plate of each EU DEMO EC equatorial launcher. The feed-throughs must be capable to align the optical systems on both sides, invessel and ex-vessel, properly and they must guarantee safe integrity of the first containment barrier. Moreover, they must allow effective and quick disassembly for maintenance tasks. The pre-conceptual design of the EU DEMO EC launcher features so-called Closure Plate Sub-Plates (CPSP) as feed-throughs for the in-vessel side, to which dedicated bunches of three (MHD-control) or eight (plasma heating) WGs, respectively, are connected.

Since it is not yet defined, whether the CPSP's have to contribute to thermal insulation between the in-vessel and the ex-vessel section of the EC system, additional WG feed-through dummies were sketched with a thickness of 200 mm, being part of the ex-vessel system and allowing the integration of cooling channels and fastening and alignment elements. A reasonable change of the thickness of the feed-throughs in the future is seen as uncritical in terms of the functionality of the system. Figure 8 shows the CPSP/WG-feed-through dummies in position with associated WGs attached.

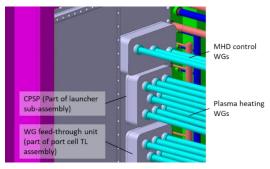


Fig. 8. CPSP/WG-feed-through dummy CAD models.

V. PORT CELL TL CAD MODEL

The port cell CAD model of the TLs was constructed in its entirety for port #10, since also the EC launcher CAD assembly is positioned at this port.

An essential design requirement is the required clearance between the TLs, especially at locations, where millimetre wave components other than WGs are located. For the trajectories the clearances in critical areas are summarized below:

- Minimum clearance next to closure plate for installation of WG switches: ab. 200 mm
- Horizontal clearance for SIC-1 valve, diamond windows and SIC-2 port cell valve: ab. 196 mm
- Horizontal clearance for SIC-2 valve in the gallery: ab. 170 mm
- Vertical clearance between the trajectories and L1 ceiling: 250 mm

The section with the SIC-1 isolation valve, the diamond window and the port cell SIC-2 shutter valve was positioned close to the port cell wall at the elevated section of the trajectories in order to allow compact integration into a mounting frame which can be positioned underneath the ceiling of L1. Such a mounting frame (not contained in the model) has the advantage of deviating forces and moments coming from the WGs from sensitive components like valves and diamond windows. As a starting value the valves and the windows are arranged with WGs of 500 mm length in between each other. The position of this section is displayed in figure 9.

To inject the millimetre-wave power either into the MHD – control system or into the plasma heating system, WG switches are installed into the section of the TL which is next to the closure plate. The WG switch dummies were constrained in the CAD assembly related to the beam trajectories and their intersection points.

The shutter valves in the gallery were installed in the section where the trajectories are approximately in parallel with the port cell rear wall. They are connected with the mitre bends by standard WGs with a length of 4,200 mm. This choice is made randomly and can be easily adapted to any purpose (e.g. maintenance needs).

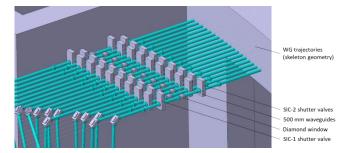


Fig. 9. Arrangement of SIC-1 isolation valves, diamond windows and SIC-2 shutter valves in port #10.

The TLs break through the rear wall of the port cell (cf. figure 9). No detailed design of this penetration has been made so far. It is expected that either an integral WG element will be mounted into the wall with joint flanges on both sides to connect with the TL WGs or an opening will be designed which allows convenient installation and maintenance for the TLs. Operational isolation requirements of the port cell, millimetre-wave losses and installation and maintenance considerations will be the main drivers of this design decision.

As a first analysis of the EC port cell TL integration the subsequent observations can be stated:

- a. There is a potential clash between the WG switches and the bioshield due to similar radial position in the port cell (cf. figure 10). Thus, further investigation on the concept of the bioshield door and/or the radial position of the WGs is required.
- b. The distance between the WG trajectories at the position of the port cell valves and the diamond window is currently 196 mm. This does not cause clashes between any components (at least as long as valves are not at the same radial position), however, for convenient installation and maintenance an increase of the horizontal distance (which is 300 mm in ITER for a similar installation) is recommended.
- c. The isolation- and the shutter valves in their current position and with current dummy dimensions have collisions with the ceiling of L1 of 85 mm. A potential solution might be an installation of the valves in an upside-down position.
- d. The WG trajectories in the gallery have a horizontal distance of 170 mm. This clearance is rather small and might create issues with installation and maintenance of the SIC-2 shutter valves and the mitre-bends as well. However, an increase of the distance between the trajectories by 250 mm to 300 mm would be possible only with modification of the gallery structural elements, or working on two-levels waveguide assemblies.

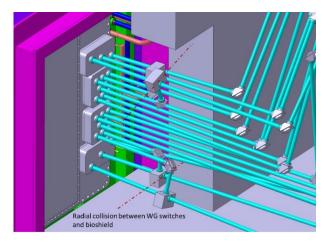


Fig. 10. Radial collisions of WG switches and bioshield.

VI. MAINTENANCE CONSIDERATIONS

Even at the early stage of a pre-conceptual design of EU DEMO components it is essential to take into account maintenance considerations. For the EC port cell section first maintenance considerations have been made with the set-up of the CAD model.

Approaching the transfer cask for port plug maintenance towards the closure plate requires a substantial clearance. A first engineering guess assumes this clearance to be 300 mm towards all sides. For the TLs in port #10 this preliminary requirement is fulfilled, however, the transfer cask will not pass the valves in the port cell in case their collision with the ceiling would be resolved by turning them upside-down.

The maintenance concept for the EC port plug describes removal of the SM EPP [9] module without dismantling the ex-vessel WGs/TL assembly. This procedure, performed by a standard cask, being able to take components with a cross-section of the maximum extent (e.g. the closure plate) would not pass the section, where the ex-vessel WGs are attached to the WG feed-throughs. For this concept, either a "half-width" transfer cask must be available or the standard transfer cask must be able to approach the closure plate in a position with an offset to the left (looking towards the plasma).

Removal of the FM EPP module [9] requires removal of the front section of the TLs, nearest to the closure plate (i.e. the WGs, connected with the WG switches, the first set of mitre-bends and the vertical WGs, heading towards the ceiling of L1, cf. figure 11). In order to minimize human access, it is expected, that the whole assembly of that section will be removed as a unit.

Repair / maintenance of TL components right underneath the ceiling is expected to be uncritical, if nuclear safety regulations are met. The shutter valves allow the break of the vacuum in particular sections and the space situation is relaxed to allow either human access or to approach dedicated Remote Handling tools. Repair / maintenance of TL components in the gallery seem to be uncritical at this early stage.

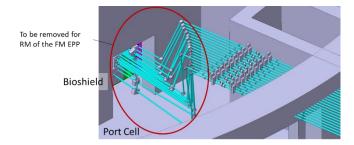


Fig. 11. Components to be removed for FM EPP RM.

VII. CONCLUSIONS

A CAD model of the EC port cell section has been set up. It features relevant elements of the Tokamak building, the EC equatorial launcher assembly, a set of geometrical skeletons which control the assembly of the system and the EC port cell system itself. The 3D components of the EC port cell section were designed as dummies with realistic dimensions on a preconceptual level. The EC transmission line section was modelled for equatorial port #10 and serves to proof the feasibility of the concept in terms of space allocation, clearance between the components and RM capability.

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REFERENCES

- [1] M.Q. Tran et al.: Status and future development of Heating and Current Drive for the EU DEMO, Fusion Engineering and Design, 2022, in press.
- [2] C. Bachmann et al.: Containment structures and port configurations, Fusion Engineering and Design, 2021, 112966, DOI: 10.1016/j.fusengdes.2021.112966
- [3] T. Franke et al.: Integration Concept of an Electron Cylotron System in DEMO, Fusion Engineering and Design 168, 112653, 2021, DOI: 10.1016/j.fusengdes.2021.112653
- [4] P.S. Silva et al.: Thermal mechanical analyses of the mm-wave miter bend for the ITER electron cyclotron upper launcher first confinement system, proceedings of the 13th ISFNT conference, Kyoto (JP), 2017, DOI: 10.1016/j.fusengdes.2018.03.047
- [5] G. Aiello: Design evolution of the diamond window unit for the ITER EC H&CD upper launcher, Fusion Engineering and Design, Volume 146, Part A, September 2019, DOI: 10.1016/j.fusengdes.2018.12.075
- [6] C. Wu et al.: Basic design considerations for a frequency step-tunable electron cyclotron wave system to suppress NTMs in DEMO, Fusion Engineering and Design 173 (2021) 112931.
- [7] D. Youchison et al.: ITER ECH Switch Design and Analysis, 2017,
 Fusion Science and Technology, 72:3, 324330, 2017 DOI: 10.1080/15361055.2017.1333855)
- [8] A.M. Sanchez et al.: Mechanical analyses of the ITER electron cyclotron upper launcher first confinement system, proceedings of the 29th SOFT conference, Prague (CZ), 2017, DOI: 10.1016/j.fusengdes.2017.02.105
- [9] P. Spaeh et al.: Structural pre-conceptual design studies for an EU DEMO equatorial EC port plug and its port integration, Proceedings of the 14th ISFNT conference, 2019, Budapest (HU), https://doi.org/10.1016/j.fusengdes.2020.111885