

## Localized Phase Contrast Imaging Measurements at Wendelstein 7-X

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Localized phase contrast imaging (PCI) measurements at the Wendelstein 7-X (W7-X) stellarator have been carried out using the masking technique pioneered at the Heliotron E stellarator [1] and the DIII-D tokamak [2]. The masking technique relies on the fact that turbulent fluctuations in magnetically confined plasmas generally have wave vectors,  $\mathbf{k}$ , which are almost perpendicular to the background magnetic field,  $\mathbf{B}$  [1, 2]. When this is combined with the line-integrated nature of PCI measurements [1, 2, 3, 4, 5], which makes the observed  $\mathbf{k}$  perpendicular to the line-of-sight (LoS) of the PCI laser beam, the direction of the  $\mathbf{k}$  observed by PCI becomes a function of the pitch angle of  $\mathbf{B}$  [1, 2, 3]. As illustrated in Fig. 1, the beam pattern in a focal plane of the plasma, caused by scattering off a fluctuation with wave vector  $\mathbf{k}$ , consists of an unscattered beam spot and two scattered beam spots with the same shape as the unscattered one, but shifted by vectors  $\propto \pm\mathbf{k}$  [1, 2]. It is therefore possible to obtain PCI measurements from a limited range of  $\mathbf{B}$  pitch angles, corresponding to a limited part of the PCI LoS, by placing a mask in a focal of the PCI system, which cuts off the scattered beam spots for  $\mathbf{k}$  outside the desired range of  $\mathbf{B}$  pitch angles [1, 2].

The ability to obtain localized PCI measurements depends critically on the unscattered beam spot size in the focal plane where the localization mask is placed, as a scattered beam spot covering a half-angle of  $\Delta\theta$  will contribute to the signal for  $\mathbf{B}$  pitch angles within  $\pm\Delta\theta$  of the one corresponding to its own  $\mathbf{k}$ ; this is illustrated in Fig. 1. To facilitate long-pulse operation, the portliner around the PCI laser beam at W7-X has been reduced in size, from previously having a radius of  $a = 68$  mm, to  $a = 42$  mm in the most recent experimental campaign [5]. Since the new  $a$  is similar to the typical 1/e electric field radius of the Gaussian beam used for PCI at W7-X,  $W = 40$  mm, it is of interest to determine the limit of the spot size in the focal plane imposed by the portliner. To do this, we note that, within a Fraunhofer diffraction framework, the beam pattern in the focal plane can be modeled by the Fourier transform of the truncated Gaussian,  $\mathbf{E}_0^a = \mathbf{C}_0 \Theta(a - r) e^{-r^2/W^2}$ , where  $\mathbf{C}_0$  is the beam amplitude vector,  $\Theta$  is the Heaviside function, and  $r$  is the distance from the beam axis. Defining the Fourier transform as

$\hat{\mathbf{E}}_0^a = \int_{\text{all } \mathbf{x}_\perp} \mathbf{E}_0^a e^{-i\mathbf{k}' \cdot \mathbf{x}_\perp} d\mathbf{x}_\perp$ , with  $\mathbf{x}_\perp$  being the coordinate perpendicular to the beam axis and  $\mathbf{k}'$  being the corresponding focal plane wave vector, while noting that the intensity is  $\propto |\hat{\mathbf{E}}_0^a|^2$ , we find

$$|\hat{\mathbf{E}}_0^a|^2(k') = 4\pi^2 C_0^2 \left[ \int_0^a r J_0(k'r) e^{-r^2/W^2} dr \right]^2, \quad (1)$$

where  $J_0(k'r) = [1/(2\pi)] \int_0^{2\pi} e^{-ik'r \cos(\theta)} d\theta$  is a Bessel function of the first kind of order zero and  $k' = |\mathbf{k}'|$ ,  $C_0 = |\mathbf{C}_0|$ . When  $a \rightarrow \infty$ ,  $|\hat{\mathbf{E}}_0^a|^2(k') \rightarrow \pi^2 C_0^2 W^4 e^{-k'^2 W^2/2}$ , showing that the size of the non-truncated Gaussian beam spot is  $\propto 1/W$ . To compare the spot size with the portliner present to the Gaussian case, we fit Eq. (1) by a Gaussian function

$$|\hat{\mathbf{E}}_{\text{fit}}|^2(k') = |\hat{\mathbf{E}}_{\text{fit}}|^2(0) e^{-k'^2 W_{\text{eff}}^2/2}, \quad (2)$$

we also note that the 1/e beam spot radius of Eq. (2) in  $\mathbf{k}'$  space is  $\sqrt{2}/W_{\text{eff}}$  and use this as a measure of the beam spot size in Fig. 1. Optimally, we would perform a least square fit of Eq. (2) to Eq. (1), while enforcing conservation of the power transported by the beam, i.e.,  $\int_{\text{all } \mathbf{k}'} |\hat{\mathbf{E}}_0^a|^2 d\mathbf{k}' = \int_{\text{all } \mathbf{k}'} |\hat{\mathbf{E}}_{\text{fit}}|^2 d\mathbf{k}'$ . Such a fit does, however, not admit a general closed form of  $W_{\text{eff}}$  and we shall therefore instead fit Eq. (1) by matching its Maclaurin series to that of Eq. (2) up to second order, which yields a simple analytical expression for  $W_{\text{eff}}$ . This method will match the least square fit in the limit of  $W/a \rightarrow 0$ , as both Eqs. (1) and (2) are Gaussian functions in that case. Even in the case of  $W/a \rightarrow \infty$ , the  $W_{\text{eff}}$  obtained by matching the Maclaurin series of Eqs. (1) and (2) up to second order only deviates from the least square fit conserving the beam power by 2.2% [6]. Matching the zeroth order terms of the Maclaurin series yields the fit amplitude,

$$|\hat{\mathbf{E}}_{\text{fit}}|^2(0) = |\hat{\mathbf{E}}_0^a|^2(0) = 4\pi^2 C_0^2 \left[ \int_0^a r e^{-r^2/W^2} dr \right]^2 = \pi^2 C_0^2 W^4 (1 - e^{-a^2/W^2})^2. \quad (3)$$

The first order term of the series is obtained by differentiating Eq. (1) with respect to  $k'$ ,

$$\frac{\partial |\hat{\mathbf{E}}_0^a|^2(k')}{\partial k'} = -8\pi^2 C_0^2 \left[ \int_0^a r J_0(k'r) e^{-r^2/W^2} dr \right] \left[ \int_0^a r^2 J_1(k'r) e^{-r^2/W^2} dr \right], \quad (4)$$

where  $J_1$  is a Bessel function of the first kind of order one. Since  $J_1(0) = 0$ , it is clear that  $\partial |\hat{\mathbf{E}}_0^a|^2(k')/\partial k'|_{k'=0} = 0$ . Differentiating Eq. (2),  $\partial |\hat{\mathbf{E}}_{\text{fit}}|^2(k')/\partial k' = -k' W_{\text{eff}}^2 |\hat{\mathbf{E}}_{\text{fit}}|^2(0) e^{-k'^2 W_{\text{eff}}^2/2}$ , so  $\partial |\hat{\mathbf{E}}_{\text{fit}}|^2(k')/\partial k'|_{k'=0} = 0$ , meaning that the first order terms of the Maclaurin series will match regardless of the fit parameters, as both Eqs. (1) and (2) have stationary points at  $k' = 0$ . To obtain the second order term of the series, we differentiate Eq. (4) with respect to  $k'$ ,

$$\begin{aligned} \frac{\partial^2 |\hat{\mathbf{E}}_0^a|^2(k')}{\partial k'^2} &= 8\pi^2 C_0^2 \left( \left[ \int_0^a r^2 J_1(k'r) e^{-r^2/W^2} dr \right]^2 - \left[ \int_0^a r J_0(k'r) e^{-r^2/W^2} dr \right] \right. \\ &\quad \left. \times \left\{ \int_0^a r^3 \left[ J_0(k'r) - \frac{J_1(k'r)}{k'r} \right] e^{-r^2/W^2} dr \right\} \right). \end{aligned} \quad (5)$$

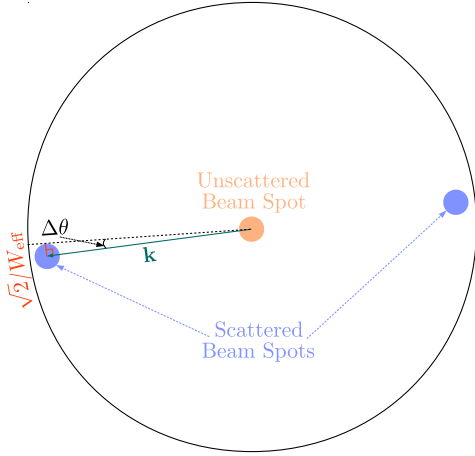


Figure 1: Beam pattern due to scattering off fluctuation with wave vector  $\mathbf{k}$  in a focal plane. The scattered beam spots have the same shape as the unscattered one and their separations from it are  $\propto \pm \mathbf{k}$ .

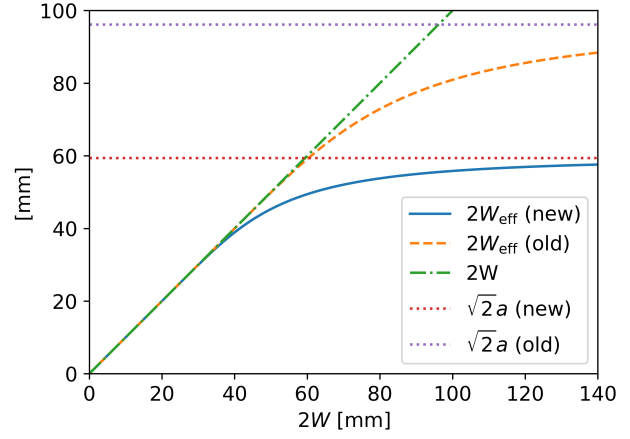


Figure 2:  $2W_{\text{eff}}$  from Eq. (7) for the new (solid line) and old (dashed line)  $a$  at W7-X, along with  $2W$  (dashed-dotted line) and the new/old  $\sqrt{2}a$  (dotted lines), versus  $2W$ . For  $2W < a$ ,  $2W_{\text{eff}} \approx 2W$ , while  $2W_{\text{eff}} \rightarrow \sqrt{2}a$  for  $2W > 3a$ .

Next, we evaluate Eq. (5) for  $k' \rightarrow 0$ , recalling that  $J_1(k'r)/(k'r) \rightarrow 1/2$  when  $k'r \rightarrow 0$ ,

$$\begin{aligned} \left. \frac{\partial^2 |\hat{\mathbf{E}}_a|^2(k')}{\partial k'^2} \right|_{k'=0} &= -4\pi^2 C_0^2 \left( \int_0^a r e^{-r^2/W^2} dr \right) \left( \int_0^a r^3 e^{-r^2/W^2} dr \right) \\ &= -\pi^2 C_0^2 W^6 (1 - e^{-a^2/W^2}) [1 - (1 + a^2/W^2) e^{-a^2/W^2}]. \end{aligned} \quad (6)$$

We further note that  $\partial^2 |\hat{\mathbf{E}}_{\text{fit}}|^2(k')/\partial k'^2 = (k^2 W_{\text{eff}}^2 - 1) W_{\text{eff}}^2 |\hat{\mathbf{E}}_{\text{fit}}|^2(0) e^{-k^2 W_{\text{eff}}^2/2}$ . Combining this with Eq. (3) yields  $\partial^2 |\hat{\mathbf{E}}_{\text{fit}}|^2(k')/\partial k'^2|_{k'=0} = -\pi^2 C_0^2 W^4 W_{\text{eff}}^2 (1 - e^{-a^2/W^2})^2$ , which finally allows us to compute  $W_{\text{eff}}$  by setting  $\partial^2 |\hat{\mathbf{E}}_{\text{fit}}|^2(k')/\partial k'^2|_{k'=0} = \partial^2 |\hat{\mathbf{E}}_0|^2(k')/\partial k'^2|_{k'=0}$ ,

$$W_{\text{eff}} = W \sqrt{1 - \frac{a^2/W^2}{e^{a^2/W^2} - 1}}. \quad (7)$$

For  $a^2/W^2 \rightarrow \infty$ ,  $W_{\text{eff}} \rightarrow W$ , as expected. When  $a^2/W^2 \rightarrow 0$ ,  $W_{\text{eff}} \rightarrow a/\sqrt{2}$ , in agreement with the corresponding estimate of [6]. At W7-X,  $a/\sqrt{2} = 29.7$  mm, while the least square fit  $W_{\text{eff}}$  conserving the beam power is  $0.723a = 30.4$  mm [6], illustrating the closeness of the two fits. Figure 2 shows  $2W_{\text{eff}}$  for the old and new  $a$  at W7-X, along with  $2W$  and  $\sqrt{2}a$  for the old/new  $a$ , versus  $2W$  up to a value of 140 mm, which is the maximum beam size allowed by the W7-X PCI system [3]. From Fig. 2, we conclude that  $2W_{\text{eff}} \approx 2W$  for  $2W < a$ , while  $2W_{\text{eff}}$  increases significantly slower than  $2W$  for  $2W_{\text{eff}} > a$ , and approaches the asymptotic limit of  $\sqrt{2}a$  for  $2W > 3a$ . Although  $2W > a$  for the typical PCI laser beam size at W7-X ( $2W = 80$  mm) with both the new and old  $a$ , we note that the reduction of  $2W_{\text{eff}}$  relative to  $2W$  is more significant

for the new  $a$  ( $2W_{\text{eff}} = 53.8$  mm) than for the old  $a$  ( $2W_{\text{eff}} = 72.9$  mm), as expected. The above results make it possible to determine a lower limit of the  $\mathbf{B}$  pitch angle which can be resolved by cutting off part of the beam in the focal plane. Using the geometry of Fig. 1, with the assumption of small  $\Delta\theta$  and the fact that  $W_{\text{eff}} < 0.723a$ , we find

$$\Delta\theta \approx \frac{\sqrt{2}}{kW_{\text{eff}}} > \frac{1.956}{ka}. \quad (8)$$

Equation (8) illustrates that it is generally easier to localize modes with larger  $k$ , as their scattered beam spots cover a smaller angle, in agreement with [1, 2] and Fig. 1. The experimental  $\Delta\theta$  limit is expected to be somewhat larger than that of Eq. (8) due to diffraction effects beyond the Fraunhofer model [2], but Eq. (8) still serves as an ultimate lower bound. For the new typical effective beam radius at W7-X ( $W_{\text{eff}} = 26.9$  mm) and ion temperature gradient (ITG) driven modes around  $k \approx 6 \text{ cm}^{-1}$ , which have the largest linear growth rate for standard electron cyclotron resonance heated plasmas at W7-X [4],  $2\Delta\theta \approx 10^\circ$  from Eq. (8). On the other hand, the variation of the pitch angle of  $\mathbf{B}$  along the PCI LoS ranges from  $15^\circ$  to  $20^\circ$  on the outboard side of W7-X in different magnetic configurations [3]. Using these estimates, we thus see that localization of typical ITG turbulence PCI features down to half the minor radius is feasible on the outboard side of W7-X. On inboard side of W7-X, the variation of the pitch angle of  $\mathbf{B}$  along the PCI LoS is approximately  $5^\circ$  in all magnetic configurations [3] and the ability to obtain localized PCI measurements on the inboard side is rather limited as a result. Detailed results related to the W7-X PCI localization masks will be presented in a future publication.

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