

# Experience with High-Z Plasma Facing Materials and Extrapolation to Future Devices

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June 22, 2010

## Abstract

The use of refractory metal plasma facing components requires intensive research in all areas, i.e. in plasma wall-interaction, in the physics of the confined plasma, diagnostic, and in material development. Only a few present day divertor tokamaks - mainly Alcator C-Mod and ASDEX Upgrade - gained experience with the refractory metals molybdenum and tungsten, respectively. ASDEX Upgrade was stepwise converted from graphite to tungsten PFCs. In line with this transition a reduction of the deuterium retention by almost a factor of ten has been observed due to the strong suppression of D co-deposition with carbon. The deuterium retained in W is in line with laboratory results in contrast to Alcator C-Mod, where the D retention in Mo is more than a factor of ten larger than in corresponding laboratory experiments. As expected from the sputtering threshold of Mo and W, negligible erosion by the thermal divertor background plasma is found in these experiments under low temperature divertor conditions. However, erosion by fast particles and intrinsic impurities, which additionally might be accelerated in rectified electrical fields observed during ion cyclotron frequency heating, plays an important role. The Mo and W concentrations in the plasma centre are strongly affected by plasma transport and variations up to a factor of 50 are observed for similar influxes. However, it could be demonstrated that sawteeth and turbulent transport driven by central heating can suppress central accumulation. The inward transport of high-Z ions at the edge can be efficiently reduced by 'flushing' the pedestal region caused by frequent edge instabilities. Extrapolations to ITER and DEMO are difficult since the physics of plasma transport is not yet completely understood, the particle and energy fluxes are orders of magnitude higher and the technical boundary conditions in DEMO strongly differ from those of present day devices.

# 1 Introduction

After the decision for the construction of ITER, plasma wall interaction moved strongly into the focus of magnetic confinement fusion research because it can sensitively influence the plasma performance and reactor availability. A future reactor cannot rely on low-Z plasma facing components (PFCs) due to the strong degradation of their thermo-mechanical properties under neutron irradiation and the high expected erosion. Moreover, there are strict limits on the tritium in-vessel inventory, not allowing large amounts of T co-deposited with carbon or beryllium. Therefore a solution with refractory metal as armour material has to be developed, or a completely different approach as for example liquid PFCs has to be adopted (see for example [1]), which lies outside the scope of this paper. The use of refractory metal PFCs requires intensive research in all areas, i.e. in plasma wall-interaction, in the physics of the confined plasma, and in material development. Nevertheless the fusion community only reluctantly uses them as plasma facing materials (PFMs). The reason can be found in its strong ability to hamper plasma operation as found in early W limiter tokamak experiments (see below) and - on the other side - the very beneficial behaviour of carbon based PFCs in respect to power handling capabilities and plasma compatibility. Due to its highest melting temperature, very high sputtering threshold and its rather benign radioactive behaviour after neutron irradiation, tungsten (W) is the first choice for the use at PFCs, although molybdenum (Mo) and its alloys can serve in most cases as an equivalent in the investigations in present day devices. This paper presents a short overview on early (Sec. 2) and present day experience (Sec.3) with refractory (high-Z) PFCs. In Sec. 4 an extrapolation to ITER is attempted and the main issues for DEMO on top of it are sketched. Sec. 5 concludes the paper.

# 2 A Brief Look into History

In early days of fusion research the vacuum compatibility of the in-vessel components was one of the highest priorities. For example, the vacuum liner in the ORMAK tokamak was coated with gold, which was selected because its chemical inertness [2]. Therefore, it was a small step to the use of refractory metals as PFM when going to devices with higher heating capabilities and therefore higher demands for the power handling by the PFCs. However, by improving the vacuum and the conditioning of the vacuum vessel, which essentially means the reduction of oxygen and carbon and their compounds, the plasma properties also improved, but at the same time strong central radiation from the high-Z material became evident. Eventually, this led to a degradation and even to hollow electron temperature profiles as observed in the PLT tokamak [3]. Following these observations the route for the PFC diverged into two branches of tokamak devices: High field tokamaks ( $B_t > 5 - 8$  T) operating at high current and high plasma densities kept the high Z-components. Tokamaks operating at moderate current densities, i.e. devices with larger cross section exchanged their high-Z

components for medium-Z materials (as stainless steel) and finally to low-Z materials as graphite or even beryllium. Earlier reviews on the experiments and results with high-Z plasma facing components can be found in [4-6]. Today, Alcator C-Mod (C-Mod) and ASDEX Upgrade (AUG), which belongs to the second branch but has progressively exchanged its graphite PFCs to W PFCs during the last ten years, are the only two divertor tokamaks using all refractory PFCs (Mo and W, respectively). There are two other tokamaks - TRIAM-1M and FTU - which use Mo limiters and JT-60U just recently equipped 1/21 of the toroidal circumference of its outer divertor with W coated graphite tiles. Additionally, the limiter tokamak TEXTOR performs various experiments with Mo and W test-limiters, exploring mainly erosion and melting of both materials.

### 3 Recent Results with High-Z Metal PFCs

#### 3.1 Erosion and Melting

Physical sputtering results from elastic energy transfer from incident particles to target atoms. Surface atoms can be ejected, if enough energy is transferred to overcome the surface binding energy. At low ion energies, where the transferred energy to surface atoms is comparable with the surface binding energy, the sputtering yield decreases strongly and becomes zero below a threshold energy. The threshold energy for the onset of sputtering from light projectiles on a substrate consisting of heavier species can be determined from momentum and energy conservation in an elastic collision. The sputtering thresholds for H, D and T on W are  $\approx 450$  eV, 210 eV and 140 eV, respectively [7] and therefore the erosion by background ions is almost negligible. In C-Mod, a good agreement between measured and simulated influx could be achieved for ohmic discharges when taking Mo self-sputtering and sputtering by  $\approx 2\%$   $B^{3+}$  (from boronisation) into account [8]. Similarly, W sputtering in ASDEX Upgrade could be explained in a wide range of divertor plasma temperatures by assuming an admixture of 1-2 % low-Z impurities (C, O) in the charge state of  $Z = 4$  [9]. When comparing the gross erosion, typically measured by spectroscopic means, with the net erosion from probe measurements, a difference by a factor of up to 10 is found under low temperature high density conditions [9]. This is attributed to ‘prompt redeposition’ as it was already observed in W marker experiments [10]: For high-Z materials the gyro-radius in the external field can be larger than the ionisation length, which can lead to deposition of the eroded particle directly after its erosion. More recent investigations show about a factor of three reduction for campaign integrated erosion in the divertor of ASDEX Upgrade [11], which may be attributed to the fact that the divertor plasma is not always dense enough for a high prompt re-deposition fraction. Details of this process are still under investigation, because it could diminish further the low sputtering yield under ITER high density, low temperature conditions. Besides the erosion by a thermal steady state plasma, erosion by transients can play an important role, because they can lead to increased yields or even to melting of the surfaces

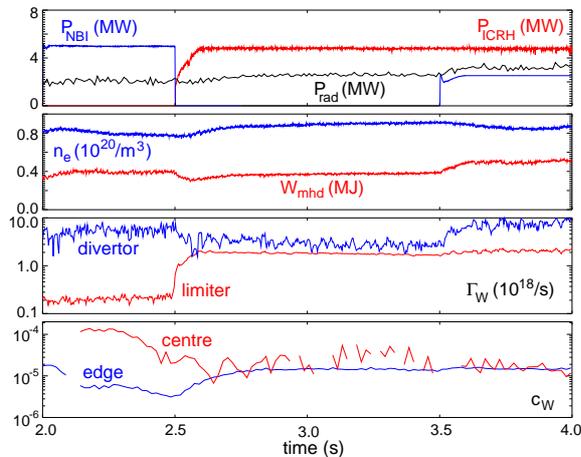


Figure 1: W influx and W concentration in ASDEX Upgrade during discharge #23476. The two top graphs present the heating power ( $P_{NBI}$ ,  $P_{ICRH}$ ) and total radiation ( $P_{rad}$ ) as well as the line averaged density ( $n_e$ ) and the stored energy ( $W_{mhd}$ ) of the plasma. The third graph highlights the W influx ( $\Gamma_W$ ) from the limiters and the divertor and the bottom insert shows the deduced W concentration ( $c_W$ ) at the plasma edge and the centre (from [12]).

by the rapid energy deposition. In H-Mode (high confinement mode) plasmas, which are envisaged as the standard operating scenario for ITER, there are periodic edge instabilities observed, ejecting periodically particles and energy on a sub ms timescale. During these so called edge localized modes (ELMs), not only the particle flux is increased, but also the particles energy, because they originate from the hot edge region ('pedestal') of the main plasma. Measurements in ASDEX Upgrade using high spatial and temporal resolution reveal, that under high density conditions, the W sputtering in between ELMs is strongly suppressed and that the sputtering during ELMs contributes up to 90% of the total W erosion. Another important process for increasing the sputter source of refractory PFCs is the acceleration of plasma and impurity ions in the rectified sheath due to ion cyclotron resonance heating (ICRH). This is reported from Alcator C-Mod as well as from ASDEX Upgrade [11, 13–15], where the Mo fluxes and W fluxes, respectively, increase by about a factor of ten during the operation of ICRH. In both experiments it is also found that the divertor impurity source is almost unchanged and, although being still larger than the limiter source, the impurity concentration in the main plasma is clearly dominated by the limiter source. This hints to a good divertor retention of M and W, respectively, which was also determined quantitatively by trace W injections in ASDEX Upgrade [16]. As an example, figure 1 shows the temporal evolution of some plasma parameters for an ASDEX Upgrade discharge (#23476) with different heating methods [12]. The W-influx is deduced from the WI line at

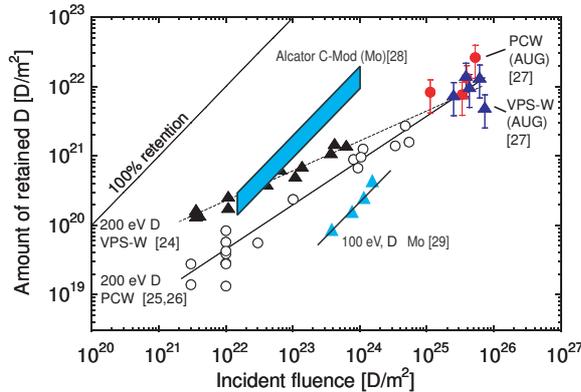


Figure 2: Deuterium retention in W and Mo. The data are taken from the references indicated in the figure. The laboratory measurements are performed at room temperature. Please note, W (Poly Crystalline (PC) and Vacuum Plasma Spray (VPS)) was irradiated with 200 eV deuterium and Mo was irradiated with 100eV D. Whereas laboratory data and data taken from AUG fit together, there is a discrepancy by more than a factor of 10 in the case of Mo in Alcator C-Mod.

400.9 nm as described in [11]. The W concentration is deduced from the quasicontinuum emission at 5 nm and the spectral line at 0.794 nm emitted from Ni-like  $W^{46+}$  [17]. The first gives the W concentration close to the plasma edge (around  $T_e \approx 1$  keV), whereas the latter represents the central concentration ( $\approx 3$  keV) in typical ASDEX Upgrade discharges. During the first phase (until  $t = 2.5$  s) the plasma is heated by neutral beam injection (NBI) only. During this phase the W source at the limiter in the main chamber is more than a factor of ten smaller than the divertor W source. At the same time the W concentration is strongly peaked, as can be seen from the ratio of the central to edge W concentration, which is about 20. This strong peaking is usually explained by neoclassical inward drifts (see Section 3.4), which can be dominant in the absence of large turbulent transport or macroscopic instabilities as sawteeth [18]. At  $t = 2.5$  s the NBI is switched off and at the same time the ion cyclotron resonance heating (ICRH) is switched on. Immediately, the limiter source increases by a factor of 10. On a longer timescale - reflecting the 'slow' particle transport within the plasma - the edge W concentration rises (by about a factor of 4), but at the same time the central concentration decreases to a value close to that at the edge. This phase is characterised by dominant anomalous transport, which tends to reduce W density gradients. In the third phase of the discharge from  $t = 3.5$  s on, a part of the NBI is switched on again, resulting in an increased W source in the divertor, which is not reflected in the main chamber concentrations at all, consistent with the above mentioned behaviour. As an additional erosion process, W erosion by arcs was investigated post mortem in AUG with profilometry, SEM, EDX, RBS, and colorimetry [19]. The arc tracks were observed at

different locations, i.e. at tiles with direct plasma contact, such as divertor targets, as well as components remote from the plasma. The track orientation and pattern allow to distinguish between arcs burning during glow discharges and during plasma operation. The arcs during plasma operation clearly dominate and are especially found at the baffle region of the inner divertor in a 10 mm wide region near to the leading edge of the individual tiles around the whole toroidal circumference. They are covering more than 10 % of this area and removed the complete tungsten coating (3–4 $\mu$ m). Droplets splashed from the arc track are detected at the surface close to the arc. Similar droplets are found all over the vessel [20], pointing to the fact that arcs could significantly contribute to the dust inventory. This is especially important since this source can barely be accounted for by spectroscopic means and estimations on dust productions based on spectroscopic erosion measurements could significantly underestimate the actual value. As stated already above, a further erosion mechanism could be melting and subsequent melt layer losses. However, in ASDEX Upgrade, there is not enough energy deposited neither during ELMs nor during disruption, to cause melting. Although surface melting is observed during disruptions in Alcator C-Mod, a quantitative assessment is not available yet. Controlled experiments on melt layer behavior are mainly performed in TEXTOR using bulk W test limiters [21]. Spectroscopic measurements of the atomic tungsten flux from a hot W surface indicate that no enhancement of atomic tungsten release exceeding physical sputtering and normal thermal sublimation for temperatures below 3700 K occurs under the present experimental conditions. The experiments with different types of tungsten limiters in TEXTOR also demonstrate that liquid tungsten can move rapidly. The motion is perpendicular to magnetic field lines and it was attributed to the thermo-electron emission current and the resulting  $j \times B$  force. As a result, tungsten melting can lead to a large material redistribution without ejection of molten material to the plasma.

## 3.2 Hydrogen Retention

As stated in the introduction, one of the major goals of replacing carbon paced PFCs to refractory metal PFCs is the reduction of hydrogen retention. In parallel with the transition of AUG from graphite to tungsten, a reduction of the deuterium retention by almost a factor of ten has been observed. This is due to the strong suppression of D co-deposition with carbon as investigated by post-mortem surface analysis [22]. Additionally, dynamic gas balance measurements, where the retention is derived from the difference of the puffed and the pumped amount of gas [23] show a similar reduction, in line with expectations from laboratory measurements on the deuterium retention in W [24–26]. Detailed TDS, NRA and SIMS investigation reveal however, that the diffusion in bulk W is deeper than observed in similar samples from D irradiation in the laboratory [27].

In Alcator C-Mod the hydrogen retention was studied using a 'static' gas balance method, where all pumps are switched off or separated from the vacuum vessel and the retained amount is calculated from the injected gas puff and from the

pressure inside the vacuum level after the discharge [28]. The Mo surfaces are found to retain large fractions, 20 - 50% of the D2 gas fueled. It is concluded that the retention occurs through ion bombardment, implantation and diffusion to trap sites. The above number can also be interpreted that roughly 1% D of the incident ion fluence is retained. No saturation of the retention rate was observed even after 25 s of integrated plasma exposure, which is concluded to be consistent with trapping sites in Mo. Differences between C-Mod and laboratory retention results [29] are thought to be due to such factors as the multiply ionized low-Z ions incident on the surface directly creating traps, the condition of Mo (impurities, annealing) and the high-flux densities in the C-Mod divertor, which are 10 - 100 times those used in laboratory studies. These results are summarized in Fig. 2 together with results from laboratory measurements.

### 3.3 Blisters, Bubbles and Mixed Material Effects

Although the exposure of PFMs in present day tokamaks is the most realistic test of their behaviour under fusion plasma conditions, there is a big gap towards ITER or a reactor concerning the particle fluence impinging on the surfaces, because of the very low duty cycle of present day fusion devices. In order to close this gap, experiments are performed in (linear) plasma devices, allowing much larger irradiation times.

Under high hydrogen fluence, low surface temperature conditions ( $< 600$  K) blistering of W can be observed (see for example [30,31]), which could increase the hydrogen inventory and lead to increased erosion if the blister cap is removed in course of power loading [32]. Many investigations have been performed to uncover the detailed conditions for the formation of blisters. Very recently, experiments performed in PISCES-B revealed [33] that blisters are completely suppressed and the hydrogen retention is drastically reduced, when He is added to the hydrogen in a percentage fraction.

In the temperature range of 1000 to 2000 K a nano-structure is formed at the W surface if it is exposed to He ions with energies above 20 eV [34–36]. Its formation is observed in pure He plasmas as well as in mixtures of He and H. The thickness of this nanostructure can reach several microns, depending on He flux and fluence. The time dependence hints to a diffusional process that is slower than the diffusion of He in W but much faster than void/bubble diffusion [35], but other formation processes as for example the coalescence of helium bubbles at the surface are also discussed [36]. The impact of W surface nanostructure morphology on fusion reactor performance is not yet fully clear but these structures could potentially lead to a larger W erosion and to an increased dust production.

If tungsten is not the only PFM in a tokamak, mixed material effects could influence the performance of the W PFCs. An especially obvious example for such an effect is the formation of a low melting Be-W alloy as observed in PISCES-B [37]. The formation of the alloy depends delicately on the amount of Be in the plasma, the plasma conditions leading to either deposition of Be or a steady erosion of W and the surface temperature which strongly influences the Be diffu-

sion into W and its sublimation [38–40]. The complexity of this process requires detailed modelling (or experiments) in order to judge the potential impact of it (see Sec. 4).

### 3.4 Transport and Suppression of Central Accumulation

Apart from the influx, the central impurity concentration depends strongly on transport which can be divided in the region of open field lines, the so called scrape off layer (SOL) and the confined plasma. The experimental investigations on transport in the SOL region are scarce and rather indirect. By use of a sublimation probe, W was injected in the divertor and at the midplane SOL of ASDEX Upgrade [16], revealing a divertor retention of 16 in a medium density H-mode discharge in line with the observation described in Sec. 3.1 and results from C-Mod [13]. In H-modes, one has to subdivide the confined plasma into the pedestal and core region. In the reactor relevant regime of type-I ELMs, the pedestal, with its steep pressure gradient, breaks down during an ELM and a substantial part of the pedestal plasma is ejected. In between ELMs, tungsten moves into the pedestal region due to strong inward particle drift [41, 42]. If the next ELM arrives in due time this tungsten is removed, before further penetrating towards the central plasma. An increase of the ELM frequency and a reduction of the W content can be achieved by external means, so called ELM pace making [43–45].

In the core plasma, an inward particle drift can lead to accumulation in the centre. In a simple picture, the diffusion consists of an anomalous and a neo-classical part  $D = D_{an} + D_{neo}$ . Recently it has been shown that  $D_{an}$  is only weakly  $Z$  dependent and that the anomalous convective part is usually very small for higher  $Z$  [46]. Therefore the convective contribution is assumed to be purely neo-classical with  $v = v_{neo}$ . If the deuterium density profile is not particularly flat this, in general, leads to accumulation of high- $Z$  elements in the core. The neoclassical accumulation has been experimentally observed in several devices [45, 47–49, 51]. However, if the heat flow in the core is sufficiently high, anomalous transport can easily exceed the neoclassical effects, especially that of high- $Z$  ions because  $D_{neo}$  decreases with  $Z$ . Therefore increasing  $D_{an}$  has a much stronger effect on the impurity density profile, than on the background plasma. Consecutively a small increase of  $D_{an}$  deteriorates the performance only weakly while suppressing strongly the high- $Z$  contamination. First hints for a beneficial influence of central ICRH on the central radiation were already seen in W test-limiter experiments in TEXTOR [50]. However, the effect of central heating reducing central impurity accumulation by stimulating anomalous transport was first identified in ASDEX Upgrade [52] and the recipe was confirmed in several other devices [51, 53, 54]. The effect is clearly seen in Fig. 1 and is further exemplified in Fig. 3, which presents the peaking of the W concentration ( $c_W$ ) as a function of background density peaking at ASDEX Upgrade. Discharges with pure NBI heating (black circles) show strongest peaking, whereas central ECRH reduces the  $c_W$  peaking significantly already at low additional heating power [45].

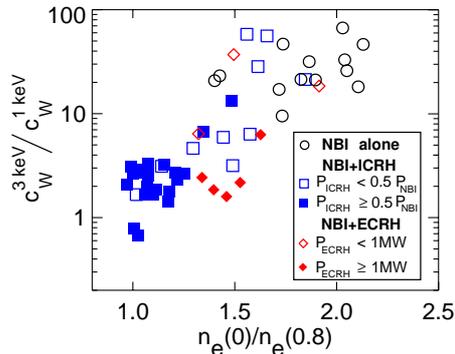


Figure 3: Peaking of the W concentration ( $c_W$ ) as a function of background density peaking in ASDEX Upgrade. Discharges with pure NBI heating (black circles) show strongest peaking, whereas central ECRH reduces the  $c_W$  peaking significantly already at low additional heating power (after [45]).

## 4 Extrapolation to Future Devices

### 4.1 ITER

One of the main arguments for ITER to start with a CFC divertor, is the huge power deposition during unmitigated transients (see table 1), which are expected to appear in the initial operational phase [55] and which could easily lead to melting of W components [57,58]. Since present day tokamaks are barely capable of reaching such conditions, it is not clear how these melt layer will evolve and what consequences have to be expected for the lifetime of the components and for the contamination of the main plasma. Although extensive modeling has been performed to address the questions raised above (see for example [56] and references therein), it is not clear yet how large the melt layer losses will be and whether vapour shielding can efficiently lower the melt erosion. Recent simulations based on experiments performed in plasma guns and quasi-stationary plasma accelerators predict a strong distortion of the surface already after 100 ELMs with an energy of  $1.6 \text{ MJ m}^{-2}$  and a duration of  $\tau = 0.5 \text{ ms}$  [59].

In [60] and [61] two complementary approaches were made to extrapolate the deuterium retention data from present day tokamaks and laboratory devices to the tritium retention in ITER. Different scenarios concerning the material mix for the first wall and divertor were investigated. Both investigations came to the conclusion, that the T-retention is mainly governed by co-deposition when using the low-Z PFCs Be and C. According to this analyses the initial ITER PFM mix will lead to a much larger T inventory (more than a factor of 10) compared to a full W device, where the T inventory is governed by implantation and retention in traps. It has to be stated that there is only very little information on the role of n-induced traps, which could increase the amount of retained T when

Table 1: Expected unmitigated ELMs and disruptions (Disr.) in ITER during the initial operational phase in hydrogen and helium at reduced plasma current ( $I_p = 7.5$  MA) and during the DT phase ( $I_p = 15$  MA) [55] (L: L-Mode, H: H-Mode).

$I_p$ (MA)	Event	Energy (MJ)	freq. (Hz)	$\tau_{rise}$ (ms)	$E_{Div}$ (MJm <sup>-2</sup> )
7.5	ELMs	5	2 - 4	0.35 - 0.70	1.2
7.5	Disr. (L)	30 - 60	-	1.5 - 3.0	0.3 - 1.1
7.5	Disr. (H)	30 - 60	-	1.5 - 3.0	0.5 - 2.1
15	ELMs	20	1 - 2	0.25 - 0.5	9.5
15	Disr. (H)	88 - 175	-	1.5 - 3.0	3.1 - 12.5

approaching 1 dpa, the amount of neutron damage expected during the lifetime of the ITER divertor. However, only very recently data were presented, which were gained in experiments using Si ions to simulate the n-damage, pointing to a very small increase of T retention by n-induced traps under ITER conditions [62].

Due to the very narrow temperature range where alloying of Be with W takes place (900 to 1500K), no alloying is expected under steady state conditions in ITER [38–40] and even the deposited Be may actually alleviate potential problems caused by W blistering and the formation of nanoscopic W morphology due to the He irradiation [63]. However, since excursions to higher temperatures will be induced by transients, the appearance of alloying or the change in surface morphology, which would result in larger erosion rates and dust production, cannot be completely excluded and calls for further investigations.

Concerning the plasma transport of W, DIVIMP calculations based on B2-Eirene simulations suggest that even for a full W coverage of the ITER PFCs edge concentrations below  $2 \cdot 10^{-5}$  can be expected for high density operation [64]. These calculations use 'averaged' transport coefficient scaled from edge parameters in present day devices. However, as observed in ASDEX Upgrade, there is a delicate balance of the mostly inward directed impurity transport in between ELMs and the 'flushing' of the impurities during the ELM. Whether this effect is approximated adequately with the 'averaged' transport of the simulations is not clear, but the need for frequent ELMs as a necessary prerequisite for sufficiently low tungsten content in the plasma goes in line with the demand of ITER to keep the energy per ELM small. However, it has to be stated, that the scaling of the 'flushing' effect is not yet investigated. Suppression of ELMs by increasing the overall edge transport with edge resonant magnetic field perturbations as pioneered by DIII-D [65, 66] and JET [67, 68], may also be a solution. However, common to these experiments is the tendency that the separatrix temperature increases during the ELM suppression phases, which is consistent with an increase of  $Z_{eff}$  compared to similar discharges without edge perturbation as reported by [69] and which would be counter productive in the

case of high-Z PFCs.

Simulations for the central transport in ITER with the ASTRA code using GLF23 model [70] suggest that the anomalous particle transport should be significantly larger than the neoclassical one, leading only to very moderate peaking of the W concentration [45,71]. Moreover, recent theoretical work [46,72] shows two dominant turbulent transport mechanisms for high Z-ions. Neither of them leads to a substantial accumulation of tungsten with respect to the deuterium density.

## 4.2 DEMO

The extrapolation to reactor is even more difficult than to ITER, since the boundary conditions are completely different to present day devices. The main differences are the much higher operating temperatures (coolant at 600 - 700° C) and the huge neutron fluence ( $\approx 10 \text{ MWa}^{-1}\text{m}^{-2}$  at the end of lifetime [73]), to which the components will be exposed. The high temperature is needed to yield a high thermodynamical efficiency. It will strongly reduce the T retention and may anneal the defects caused by neutron irradiation, but it will also strongly promote the T penetration through the components leading to a new class of challenges. The combination of the high power load and the high temperature of the cooling medium will allow almost no transients, requesting operation modes not achieved so far. A much more elaborate analysis on the challenges for plasma facing components of a future fusion reactor was discussed at a recent workshop at the UCSD and will be published in [74].

## 5 Conclusion

The use of refractory metal PFCs requires intensive research in all areas, i.e. in plasma wall-interaction, in the physics of the confined plasma, diagnostic, and in material development. Only a few present day divertor tokamaks - mainly Alcator C-Mod and ASDEX Upgrade (AUG) - gained experience with the refractory metals molybdenum and tungsten, respectively. Although a quite large hydrogen retention of Mo is found in Alcator C-Mod, the reason for which is not yet resolved, the expected strong reduction of hydrogen retention is observed in ASDEX Upgrade after the transition to all W PFCs, in line with results from plasma simulators and laboratory experiments. The sputtering threshold of Mo and W is quite high, such that in contrast to carbon PFCs, negligible erosion by thermal divertor background plasma is found in these experiments. However, erosion by fast particles and intrinsic impurities, which additionally might be accelerated in rectified electrical fields observed during ion cyclotron frequency heating, plays an important role. W is only partly ionized in the confined plasma, even at reactor relevant temperatures in the range of 10 to 20 keV. The resulting strong radiation thus sets an upper limit for an acceptable W concentration of only a few  $10^{-5}$ . The W concentration in the plasma centre

is strongly affected by plasma transport and variations up to a factor of 50 are observed for similar influxes, due to a pronounced neoclassical inward drift in the main plasma as well as in the pedestal region of H-modes. However, it could be demonstrated that sawteeth and turbulent transport driven by central heating can suppress central W accumulation. The inward transport of high-Z ions at the edge can be efficiently reduced by 'flushing' the pedestal region provided by frequent edge instabilities (ELMs). Among the challenges remain the strong increase of the W/Mo source and W/Mo concentration resulting from ICRH and the need for rigorous modelling for the extrapolation of the results from present day devices to ITER. Most of them are currently addressed and results are expected in the upcoming years. Clearly, not all questions posed by ITER can be answered in present high-Z devices, amongst which are the effects of material mixing with Be, the melt behaviour under transients or the change of the hydrogen retention due to damage by high energy neutron irradiation [61]. Some answers may be provided by the ITER-like wall project in JET [75], which will employ a similar configuration of PFCs as ITER, namely Be in the main chamber and tungsten in the divertor, but others have to be answered by dedicated experiments in other plasma devices or by modelling. Similar conclusions are drawn in a very recent paper by Brooks et al. [76], in which a very beneficial behaviour is predicted for ITER equipped with all W PFCs under the condition that the effects of ELMs can be mitigated. Looking further into the future to a DEMO device there will be a new class of challenges, which will even not be tackled sufficiently in ITER. The main differences will be the necessity to operate the PFCs at high temperature and the neutron fluence they receive during their lifetime. From these two issues there result a lot of consequences not only for the PFCs themselves but also for the plasma scenarios. Therefore, developing PFCs for DEMO and beyond will require a focused R&D campaign on high heat flux components for DEMO but also large advances in the control of the edge plasma especially the complete suppression of large transients.

## Acknowledgment

The author would like to thank the teams of Alcator C-Mod, ASDEX Upgrade, JT-60U, PISCES-B and TEXTOR as well as the members of the European Taskforce on Plasma Wall Interaction for supplying their most recent data and publications.

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