

**Structure, Volume 24**

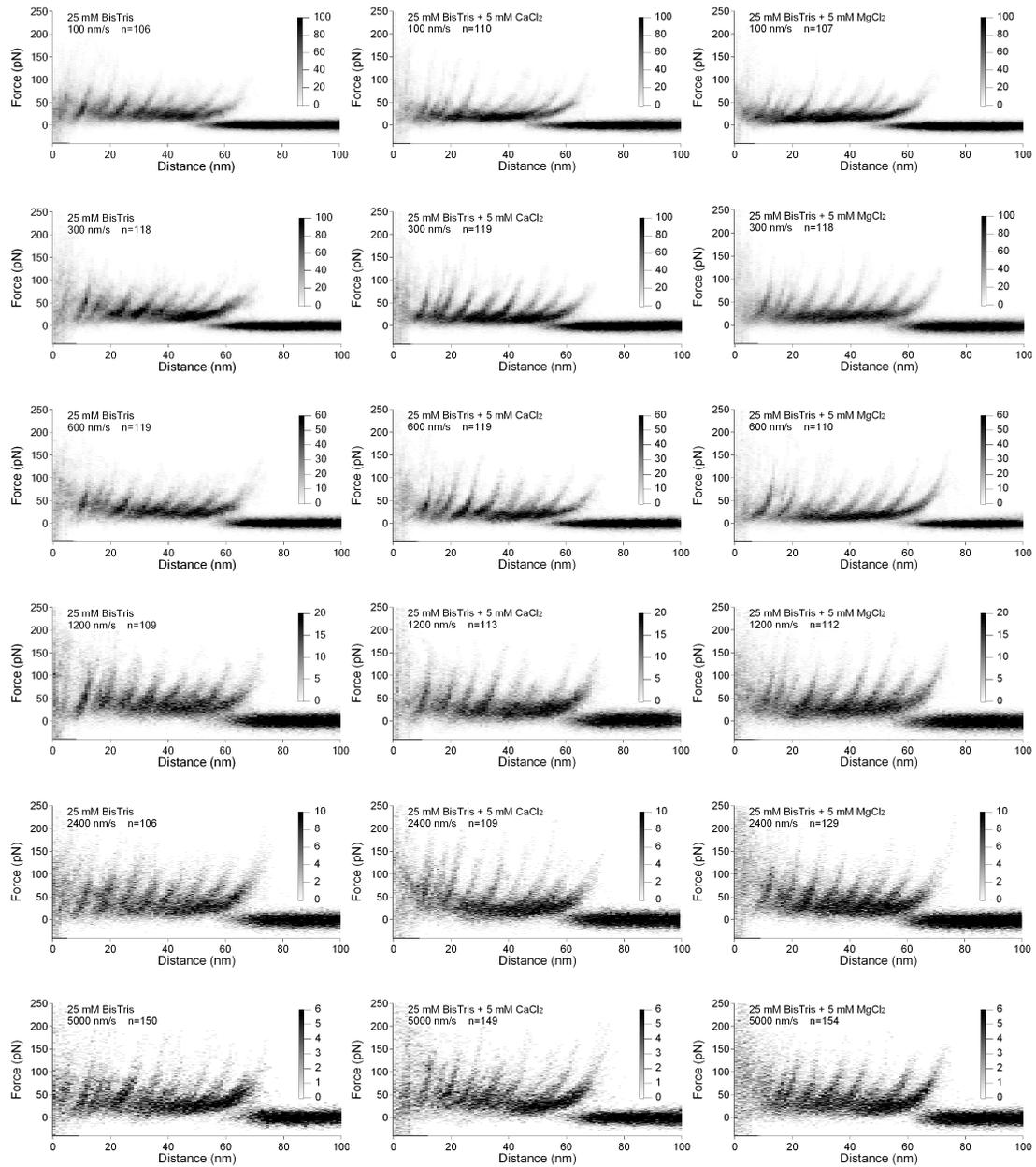
**Supplemental Information**

**Molecular Plasticity of the Human**

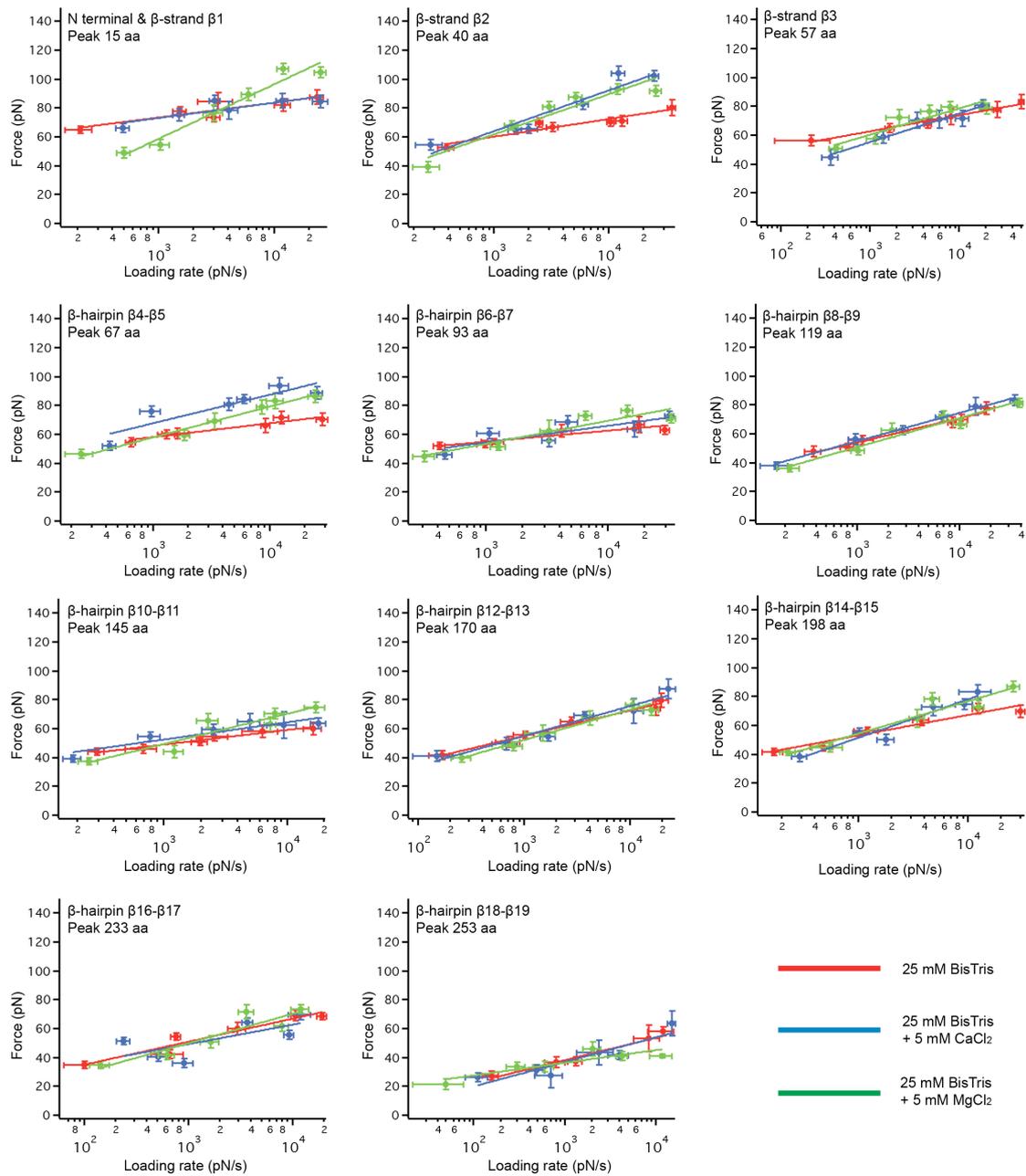
**Voltage-Dependent Anion Channel Embedded**

**Into a Membrane**

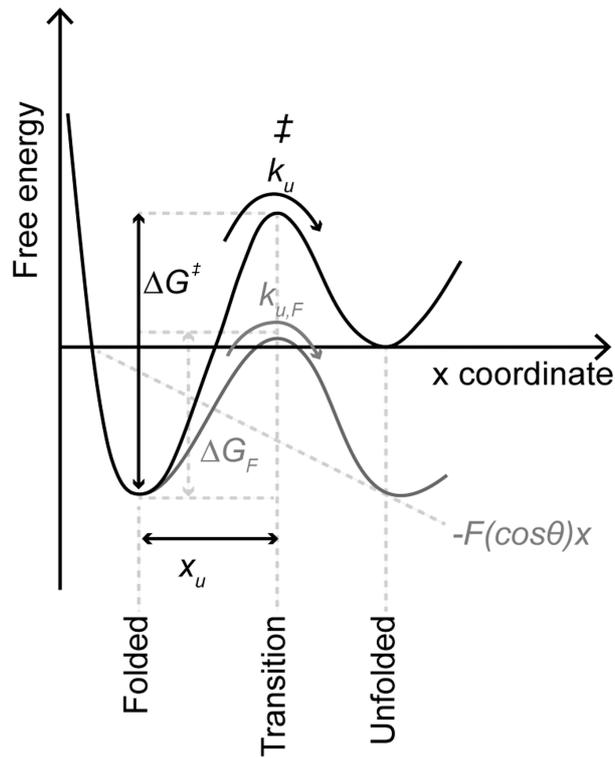
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Becker, Daniel J. Müller, and Markus Zweckstetter**



**Figure S1**, relates to **Figure 3** and **Table 1**. Superimposition of FD curves recorded upon unfolding of hVDAC1 in the absence and in the presence of calcium or magnesium. Buffer conditions, pulling velocities, and number ( $n$ ) of superimposed FD curves are indicated. Every superimposed FD curve has been recorded upon unfolding of a single hVDAC1 channel. The gray scale bar on the right allows the evaluation of events of high (black), lower (gray), and no (white) occurrence. Single-molecule force spectroscopy was recorded in buffer solution (25 mM BisTris, pH 6.8) and as indicated in the absence or in the presence of 5 mM  $\text{Ca}^{2+}$  or 5 mM  $\text{Mg}^{2+}$ .



**Figure S2, relates to Table 1. Dynamic single-molecule force spectroscopy (DFS) plots reveal loading rate dependent interactions stabilizing the structural segments of hVDAC1.** For each stable structural segment of hVDAC1 the most probable unfolding force was determined from the raw data (**Figure S1**) and plotted against the loading rate (Experimental Procedures). The fits of the experimental data (solid lines) using Eq. 1–3 are shown for hVDAC1 unfolded in the absence of divalent ions (red), 5 mM  $\text{Ca}^{2+}$  (blue), or 5 mM  $\text{Mg}^{2+}$  (green). Values for  $x_u$  and  $k_0$  obtained from fitting the DFS plots are given in **Table 1**. Error bars represent the standard error of most probable force and loading rate.



**Figure S3, relates to Table 1 and Figure 5. Schematic of an energy barrier stabilizing a structural segment of hVDAC1 against unfolding.** The folded state of a structural segment (e.g., for example a  $\beta$ -hairpin in case of hVDAC1) is separated from the unfolded state by a free energy barrier. In the absence of an externally applied force (i.e., at equilibrium) the folded structure can unfold at a certain transition rate ( $k_u$ ). To unfold the structure must overcome the transition state ( $\ddagger$ ).  $x_u$  characterizes the distance from the folded state to the transition state. The height of the unfolding free energy barrier separating the folded state from the unfolded state is given by  $\Delta G^\ddagger$ . This barrier, which is given by the free energy difference of the folded state and the transition state, therefore characterizes the activation free energy of unfolding. According to the Bell-Evans model (Bell, 1978; Evans, 1998; Evans and Ritchie, 1997), an externally applied force ( $F$ ) tilts the energy landscape by the mechanical energy ( $-F(\cos\theta)x$ ) and lowers the free energy barrier ( $\Delta G^\ddagger$ ) to  $\Delta G_F$ . Lowering of the free energy barrier is described by the mechanically applied pulling direction  $x$  and the angle  $\theta$  of the externally applied force ( $F$ ).

**Table S1, relates to Table 1. Significance tests of the parameters characterizing the energy barrier parameters  $x_u$ ,  $k_u$ , and  $\Delta G^\ddagger$  and the spring constant  $\kappa$  of the stable structural segments detected for hVDAC1 in different buffer solutions. Shown are  $P$ -values revealed from T-student tests of the parameters given in Table 1.**

Force peak position / Structural region	Ca <sup>2+</sup> vs control			
	$x_u$	$k_u$	$\Delta G^\ddagger$	$\kappa$
15 aa / N-terminus & $\beta$ 1	8.63225 10 <sup>-1</sup>	8.62419 10 <sup>-1</sup>	8.51244 10 <sup>-1</sup>	9.22322 10 <sup>-1</sup>
40 aa / $\beta$ 2	3.05692 10 <sup>-5</sup>	2.19535 10 <sup>-2</sup>	2.68579 10 <sup>-4</sup>	5.3541 10 <sup>-4</sup>
57 aa / $\beta$ 3	4.34067 10 <sup>-7</sup>	1.09213 10 <sup>-2</sup>	2.74325 10 <sup>-7</sup>	3.09731 10 <sup>-4</sup>
67 aa / $\beta$ 4- $\beta$ 5	6.22929 10 <sup>-5</sup>	2.69795 10 <sup>-1</sup>	1.4011 10 <sup>-3</sup>	1.53124 10 <sup>-2</sup>
93 aa / $\beta$ 6- $\beta$ 7	2.1159 10 <sup>-2</sup>	5.46752 10 <sup>-1</sup>	3.0968 10 <sup>-2</sup>	2.16478 10 <sup>-1</sup>
119 aa / $\beta$ 8- $\beta$ 9	1.47059 10 <sup>-3</sup>	7.08056 10 <sup>-3</sup>	1.06767 10 <sup>-2</sup>	4.99555 10 <sup>-3</sup>
145 aa / $\beta$ 10- $\beta$ 11	1.04417 10 <sup>-1</sup>	5.36127 10 <sup>-1</sup>	4.01567 10 <sup>-1</sup>	2.76425 10 <sup>-1</sup>
170 aa / $\beta$ 12- $\beta$ 13	1.51198 10 <sup>-2</sup>	8.58459 10 <sup>-2</sup>	3.10518 10 <sup>-2</sup>	7.42127 10 <sup>-2</sup>
198 aa / $\beta$ 14- $\beta$ 15	1.76505 10 <sup>-5</sup>	3.52599 10 <sup>-3</sup>	5.28258 10 <sup>-5</sup>	4.62344 10 <sup>-4</sup>
233 aa / $\beta$ 16- $\beta$ 17	4.59109 10 <sup>-1</sup>	4.57097 10 <sup>-1</sup>	5.99544 10 <sup>-1</sup>	4.92486 10 <sup>-1</sup>
253 aa / $\beta$ 18- $\beta$ 19	3.77248 10 <sup>-1</sup>	3.42859 10 <sup>-1</sup>	2.71483 10 <sup>-1</sup>	5.24156 10 <sup>-1</sup>

Force peak at contour length (aa)	Mg <sup>2+</sup> vs control			
	$x_u$	$k_u$	$\Delta G^\ddagger$	$\kappa$
15 aa / N-terminus & $\beta$ 1	4.62349 10 <sup>-5</sup>	2.65949 10 <sup>-4</sup>	6.71793 10 <sup>-5</sup>	6.15288 10 <sup>-6</sup>
40 aa / $\beta$ 2	3.58609 10 <sup>-5</sup>	2.35747 10 <sup>-2</sup>	2.32124 10 <sup>-4</sup>	7.1667 10 <sup>-4</sup>
57 aa / $\beta$ 3	9.48356 10 <sup>-5</sup>	1.94398 10 <sup>-1</sup>	1.35225 10 <sup>-4</sup>	2.83095 10 <sup>-2</sup>
67 aa / $\beta$ 4- $\beta$ 5	4.82471 10 <sup>-6</sup>	1.60301 10 <sup>-3</sup>	1.69816 10 <sup>-5</sup>	8.70332 10 <sup>-6</sup>
93 aa / $\beta$ 6- $\beta$ 7	1.67672 10 <sup>-4</sup>	1.81281 10 <sup>-1</sup>	3.16225 10 <sup>-4</sup>	7.60199 10 <sup>-3</sup>
119 aa / $\beta$ 8- $\beta$ 9	8.89912 10 <sup>-3</sup>	3.84503 10 <sup>-2</sup>	4.15668 10 <sup>-3</sup>	6.70167 10 <sup>-2</sup>
145 aa / $\beta$ 10- $\beta$ 11	4.37276 10 <sup>-6</sup>	4.88016 10 <sup>-2</sup>	1.79251 10 <sup>-5</sup>	2.63014 10 <sup>-3</sup>
170 aa / $\beta$ 12- $\beta$ 13	4.1602 10 <sup>-3</sup>	1.25082 10 <sup>-2</sup>	1.7947 10 <sup>-3</sup>	3.21037 10 <sup>-2</sup>
198 aa / $\beta$ 14- $\beta$ 15	2.3926 10 <sup>-4</sup>	2.90302 10 <sup>-2</sup>	1.33695 10 <sup>-3</sup>	4.25575 10 <sup>-3</sup>
233 aa / $\beta$ 16- $\beta$ 17	3.60765 10 <sup>-2</sup>	1.4135 10 <sup>-1</sup>	4.34655 10 <sup>-2</sup>	1.36833 10 <sup>-1</sup>
253 aa / $\beta$ 18- $\beta$ 19	4.43563 10 <sup>-3</sup>	4.46661 10 <sup>-3</sup>	9.94509 10 <sup>-3</sup>	1.51084 10 <sup>-3</sup>

## Supplemental References

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Evans, E. (1998). Energy landscapes of biomolecular adhesion and receptor anchoring at interfaces explored with dynamic force spectroscopy. *Faraday Discussions* *111*, 1-16.

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