

# Recent improvements to the ICRF antenna coupling code “RAPLICASOL”

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## Abstract

In this paper we discuss recent improvements to the ICRF antenna coupling code “RAPLICASOL”, its ability to handle curved antenna geometries, to simulate ICRF wave propagation through plasmas with arbitrary 3D density and magnetic field profiles, and its validation against other ICRF codes such as TOPICA and ERMES.

## 1 Introduction

Ion cyclotron range of frequencies (ICRF) is a commonly used heating method in tokamaks. The design of ICRF antennas, which must couple as much power as possible while minimizing impurity production via RF sheath excitation, relies heavily on numerical modelling and simulations. Thus, the ability to quickly calculate the coupled power and electromagnetic fields near an ICRF antenna, even in highly non-trivial plasma conditions, is of great value. The tool we discuss in this paper, an ICRF coupling code called “RAPLICASOL”, does just that.

RAPLICASOL is a Finite Element code, originally developed by J. Jacquot [1]. It is based on the commercial software COMSOL. It solves Maxwell’s equations, in cold plasma and in the frequency domain, near the ICRF antenna, and calculates the S-matrix, from which quantities of direct experimental interest such as the coupling resistance and coupled power can be calculated.

In section 2, we discuss the validation of RAPLICASOL against other ICRF codes. In section 3, we show RAPLICASOL’s recently added ability to handle both arbitrary 3D density profiles and arbitrary 3D magnetic field profiles, and in section 4 the newly added ability to handle curved antenna geometries.

## 2 Validation efforts

### 2.1 TOPICA

In [2], we compared RAPLICASOL with a thoroughly validated ICRF code, TOPICA [3, 4]. For the ASDEX Upgrade (AUG) 2-Strap (2S) antenna, we found that the voltage reflection coefficients at the antenna ports as calculated by RAPLICASOL

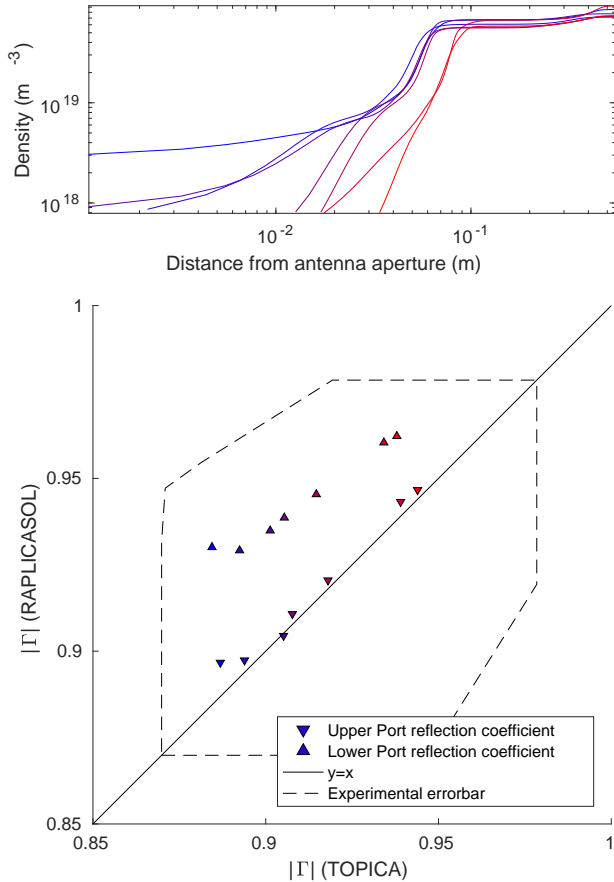


Figure 1: Comparison of port voltage reflection coefficients as calculated by RAPLICASOL and TOPICA for 7 different density profiles. Unlike in [2], this comparison was done with curved geometry in both RAPLICASOL and TOPICA.

and TOPICA agreed to within 2% (using a flat AUG 2S antenna geometry in both cases). This remains true for a wide range of plasma density profiles. Related quantities such as the S- and Z-matrix entries, coupling resistance, coupled power, optimal matching settings, and even the near RF fields, were also found to be in good agreement.

A similar comparison, this time using the curved antenna geometries that will be discussed in section 4, is shown in figure 1. Both the RAPLICASOL and the

TOPICA calculations predict reflection coefficients that lie within the error bars of the corresponding experimental measurements.

This agreement is achieved despite the fact that RAPLICASOL requires vastly fewer computational resources than TOPICA: the required number of CPU-hours for the AUG 2S antenna is reduced, from about 3000 (5 hours on 600 CPUs) to about 100 (3 hours on 32 CPUs).

## 2.2 ERMES & the LH resonance

The standard Finite Element formulation of Maxwell’s equations, using Nédélec “edge” vectorial basis-functions [5], has several flaws when applied to cold plasma: it is unable to handle resonances (notably the LH resonance, where  $S = 0$  in the dielectric tensor), and its convergence, when using iterative solvers, is unreliable (the latter is believed to be caused by the former). For this reason, it has become standard practice to resort to poorly-justified resonance-avoidance techniques in most ICRF codes, including RAPLICASOL and TOPICA. For example, a discontinuous density jump may be used to avoid the LH resonance [6], or a non-physical loss mechanism may be introduced.

The recently developed fully open-source ERMES code [7, 8] provides a less ad-hoc solution to this problem. By imposing  $\nabla \cdot \vec{D} = 0$  (microscopic current continuity) everywhere, ERMES converges even in the presence of the LH resonance. The physical validity of this approach remains to be ascertained, especially in light of [9], but numerical results in figure 2 confirm that the numerical issues around the resonance (previously described in [6]) are avoided.

## 3 3D density & magnetic field

EMC3-Eirene [10] and VMEC [11] are codes which can calculate 3D density and magnetic field distributions throughout the tokamak. In previous work [12] we showed that RAPLICASOL can simulate ICRF wave propagation through plasmas with such 3D density distributions, a capability we successfully used to predict the influence of local gas puffing on ICRF

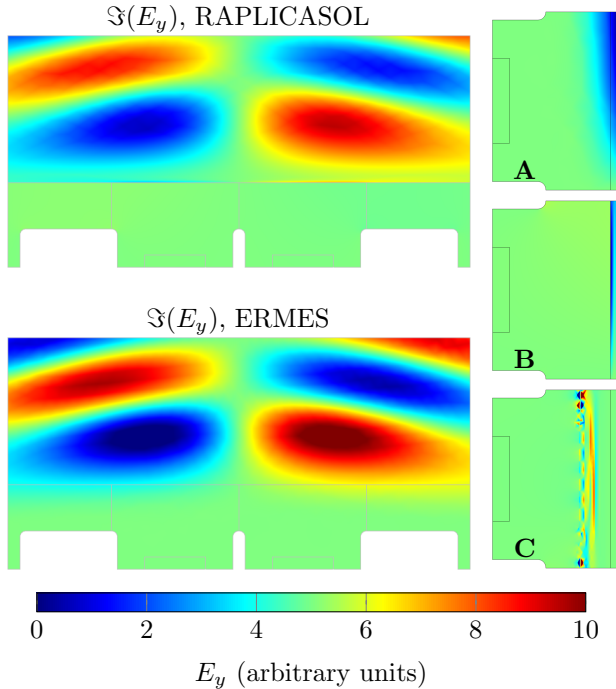


Figure 2: Left:  $\Im(E_y)$  on a 2D antenna like in [6], as calculated by ERMES and RAPLICASOL. Right: detail view of  $\Im(E_y)$  in (A) ERMES with continuous density, (B) RAPLICASOL with discontinuous vacuum-plasma transition, (C) RAPLICASOL with continuous density, where the solution is numerically ill-behaved near the LH resonance.

power coupling [10]. Now, RAPLICASOL can also import arbitrary 3D vector fields for the confining magnetic field  $\vec{B}_0$ . We also adapted the Perfectly Matched Layers used to artificially damp the wave [13] to work in 3D conditions (although further validation is still required). We intend to use this capability to model ICRF power coupling in tokamak plasmas that are perturbed in various ways [14, 15].

## 4 Curved procedural geometry

The geometry in RAPLICASOL is procedural: it is not usually imported from external CAD models<sup>1</sup>, but rather generated programmatically from a large number of numerical parameters that specify the antenna, such as the width, height and depth, details of the folded straps, and number and angle of Faraday Screen bars. Until now, only flat antenna geometries were available. Now, we have also constructed a procedural geometry for the curved AUG 2-strap antenna (figure 3). It is constructed to resemble the corresponding TOPICA model as closely as practically possible, within the limitations of COMSOL's geometry generation capabilities.

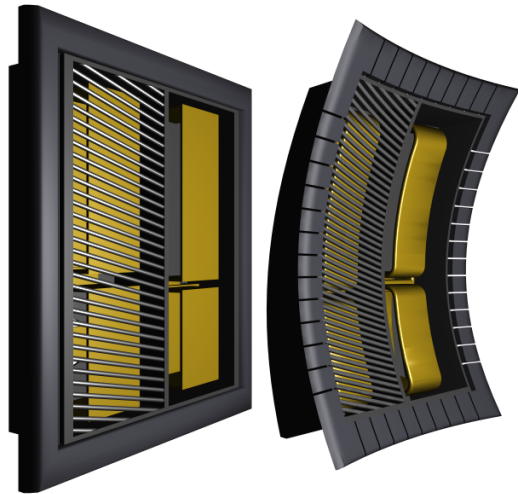


Figure 3: Old flat and new curved model of the AUG 2-strap antenna, with some of the Faraday Screen bars removed for clarity.

The advantages of the curved geometry are twofold: first, it is a better approximation to the true shape of the antenna. This is not just due to the curvature: it was noted in [2] that several existing flat models of the AUG 2S antenna have inaccuracies be-

<sup>1</sup>One reason for this is that TOPICA CAD models specify and mesh surfaces, while RAPLICASOL meshes volumes, and it is not generally possible to automatically convert from one to the other. In practice, only the simplest TOPICA geometries can be reliably imported into RAPLICASOL.

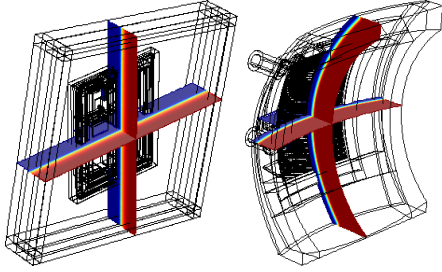


Figure 4: The curved geometry removes the need to flatten density and magnetic field distributions.

yond the absence of curvature. Having the correct geometry is especially important when we are interested in the detailed behaviour of the electric field near the antenna. Second, having a curved geometry frees us from having to deform/flatten density or magnetic field distributions to make them match the flat antenna model (figure 4).

## 5 Conclusion

In this paper we have discussed several recent improvements to the ICRF code RAPLICASOL, including validation, improvements to the geometry, and ability to handle 3D density and magnetic field profiles.

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